

« ÄÌ - I

1. pÄö¾ÄÄÄÄÿ « ÊôÄ ¼ì ÿ ÕðÐ ÿ ù

1.1 ÓýÛ ÿ Ä

ðÊÛì ò |Äì Õð Çÿ (Rigid bodies) pÄ°;ÄÉ, ¾ðÄ |ÄôÄ, pÄì ÿ Çö ÄüË « ÊÄÄÌ ò « Ê×ðÐ ÿ ÈŞÄ pÄüÄÄø ÿ Ì ò (Physics). pÄì ÿ Ç Ä ÄÄÜì Ì ò Äì ¾Ä pÄö¾ÄÄÄÄì ò (Mechanics). pÄö¾ÄÄÄÄø |Äì Õð Çÿ pÄì ò (Motion), pÄì ò ÿ ÿ Ä¾üì |Ä Ä° (force), Ä° ÄÉìø |Äì Õð ÿ ÿ òÄì ÜËÄ ŞÄ Ä(work), |Äì Õð Çÿ ¾Äÿ, ÿ üËø ÿ Ä Ä ÄüË ÜËÄÿ ÿ ÈÈ. pÄö¾ÄÄÄø ÿ ÿ ðÄì ÿ Çö ÄÄÿÄì ð¾Ä |Äì ÈÄÄø ÄÉì ÿ Ûì Ì ò ¾È× ÿ Ì ò Äì ¾ÄŞÄ |Äì ÈÄÄÖì Ì |Äì pÄö¾ÄÄÄÄì ò.

|Äì ÐÄì pÄö¾ÄÄÄÄ Ä ÿ ÄÄÄø (statics) ÄüÜò pÄì ÄÄø (Dynamics) ±È pÖÄ ÿ Çì ò ÄÄÄ Äì. ÿ ÄÄÄÈ |Äì Õð Çÿ ÄÐ |ÄüÄì ò Ä° Çö ÄüË ÜÜÄÐ ÿ ÄÄÄø. |Äì Õð Ç pÄì ¼Äì ÿ òÛò Ä° Çö ÄüËÜò ÄüÜò pÄì ò ±üÄ¾ð¾Äø ÿ ÿ ðø ±ýÄ¾Ä ÄüËÜò « ÊÄÄÌ ò Äì ¾Ä pÄì ÄÄÄì ò.

1.2 pÄö¾ÄÄÄÄÿ « ÊôÄ ¼ « ÄÌ ÿ Ûò (units) ÄìÄì ½í ÿ Ûò (Dimensions)

|Äì Õð Çÿ ÄøŞÄÜ ¾ý ÿ Ä ÿ Ç « ÇÄÌ Ä¾ý ã ÄÄì ŞÄì « øÄÐ ±ñ ½Ä ÿ Äý ã ÄÄì ŞÄì ÿ ½÷ð¾ÖËÖò. ±Ì ðÐì ÿ ð¾Äì ÿ Õ |Äì ÕÇÿ ÿ Çö, « Äö, ÿ Äö, ÄÖÄý, ± ¼ « ¾ý ¾Äñ Äö ÿ ÄÄüË È « ÇÄÖì Ì ÜËËÖò. |Äì Õð Çö ¾ÄöÄì ð¾Ä ÜÜÄ¾üì « Ç Ä ÿ |Äì Ðð pýÈÄ ÄÄ¾ÄÈÄì ò. |Äì Õð Çÿ ¾ý ÿ Ä ÿ Ç ÿ òðÐ ½Ä « Ç Ä ÿ ÿ ÿ Äì ÿ ÈÄì ÿ ÿ ÄÄì ÿ Õ ÄÄì ½ð ÿ ¾ p ÿ ½ðÄÐ ÄÈì ò.

Û |Äì Õð ÄÄÄ¾ÄÈ « ÇÄÌ ò ¾ý ÿ Ä ÿ Çö |ÄüËÜò Ì ÜË ò. ÿ Äì ÿ Èý ¾ý ÿ Ä Ä « ÇÄÌ Ä¾üì « ð¾ý ÄÄÿ ÿ ò ÒÄì ¾Ä Ä « ÊôÄ ¼ « ÇÄì Ì ÿ ÿ ÿ Ì (basic unit) « ÿÄËöÄ ¼Äø « ð¾ý ÄÄÿ « Ç Ä Ä ÄÄÜì Äì. « ÿÄËöÄ ¼ « Ç× « ð¾ý ÄÄÿ « ÊôÄ ¼ « Äì ±Èì Ò¾ÄÄì ò. ±Ì ðÐì ÿ ð¾Äì ÿ Õ |Äì ÕÇÿ ÿ Çö ÿ ¾Ä « ¾üì ò ¾ì ó¾Ä « ÊôÄ ¼ « ÇÄì È "Û ÿ ýÈÄð¾Ä" « øÄÐ "µ÷ « È" ±ýÈ « Äìø ÿ ½ì ÿ ¼ ÖËÖò.

pÄö¾ÄÄÄÄø p¼ò |ÄüÜò Äìø ÿ (Quantities) « øÄÐ ¾ý ÿ Ä ÿ (Qualities) ÿ Ä ÿ ÿ Äì ÿ Èý ¾È ò¾Ä « Ä ÿ ŞÄüì ÿ ÿ ÄÐ pÄÄì ¾Ä ÿ ò Äì ò. ÿ ïó¾Ä ÿ Äì ò ÿ Çÿ « ÊôÄ ¼Äø ÿ ÿ ò ÿ ÄüË ÿ Çö (length), ÿ È(Mass), ÿ Äö(Time) ÿ ÄÄüËÿ « ÊôÄ ¼ « Äì Çÿ ÄìÄÄì ÄüË Äìø ÿ Ç « ÇÄ¼ÖËÖò. ±ÈŞÄ ÿ Çö, ÿ È, ÿ Äö ÿ Ä ÿ ýÜ Äìø ÿ Ûò « ÊôÄ ¼ Äìø ÿ (Fundamental Quantities) ±È×ò ÄüËÈøÄì Äìø ÿ Ûò « ÄüËÿ ÄÄö¾Ä Äìø ÿ ÇÈ×ò (Derived Quantities) Ò¾ÄÄì ò.

pöä ýÜ « ÊôÄ ¼ Äìø « ÄÌ ÿ ÿ ÿ Äì ÿ Èý « ÊôÄ ¼ ÄìÄì ½ð ÿ ¾Ä (basic dimension) ý ÿ ÈÈì ÿ ÿ ÿ Ì (unity) ÄüË « ÇÄÌ ò Äìø Çÿ ÄìÄì ½í ÿ Çì ½ì ÿ ¼ ÖËÖò. ÄüË ÈÄ Äìø Çÿ ÄìÄì ½í ÿ « ÊôÄ ¼ Äìø Çÿ ÄìÄì ½í ÿ Çì ÿ òð Ä ÄÄÜì òÄì Ä¾ø « ÄüË ÈÄÄö¾Ä « øÄÐ pÄñ ¼Ä¾ÄÈ ÄìÄì ½í ÿ ÿ (Derived or secondary Dimensions) ±È ÿ ÜÜÄ÷.

or secondary dimensions of quantities)

$\int C_0, \int \dot{E}, \int \dot{A} \dot{o} - \int \dot{A} \dot{A} \dot{U} \dot{E} \dot{y} \ll \dot{A} \dot{I} \int \dot{C} \ll \dot{E} \dot{o} \dot{A} \int \dot{A} \dot{I} \int \dot{C} \dot{E} \dot{i}$
 $\int \dot{A} \dot{U} \dot{E} \dot{p} \dot{A} \dot{U} \dot{A} \dot{A} \dot{o} \dot{A} \dot{i} \dot{o} \dot{C} \dot{y} \ll \dot{A} \dot{I} \int \dot{C}, \ll \dot{A} \dot{U} \dot{E} \dot{y} \dot{A} \dot{A} \dot{A} \dot{E} \dot{U} \dot{i} \dot{i}$
 $\int \dot{U} \dot{E} \dot{A} \dot{i} \dot{U} \ll \dot{E} \dot{o} \dot{A} \int \dot{A} \dot{i} \dot{o} \dot{C} \ll \dot{A} \dot{I} \int \dot{C} \dot{y} \dot{A} \dot{A} \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{E} \dot{A} \dot{i} \dot{o}. \pm \dot{E} \dot{S} \dot{A} \ll \dot{U} \dot{A} \dot{o} \int \dot{A} \dot{i} \dot{o} \dot{C} \dot{y} \dot{A} \dot{i} \dot{A} \dot{i} \int \dot{C} \dot{o} \dot{o}, \ll \dot{E} \dot{o} \dot{A} \int \dot{A} \dot{i} \dot{o} \dot{C} \dot{y} \dot{A} \dot{i} \dot{A} \dot{i} \int \dot{C} \dot{o}$
 $\dot{D} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{U} \dot{E} \dot{A} \dot{i} \dot{o} \dot{C} \dot{y} \dot{U} \pm \dot{E} \ll \dot{A} \dot{i} \dot{o} \dot{A} \dot{i} \dot{o}.$

$\pm \dot{I} \dot{o} \dot{D} \dot{i} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{S} \dot{A} \dot{o} (\text{Velocity}) \pm \dot{y} \dot{A} \dot{D} \dot{p} \int \dot{A} \dot{o} \int \dot{A} \dot{A} \dot{A} \dot{i} \dot{o} \int \dot{o},$
 $\int \dot{S} \dot{A} \dot{o} \int \dot{U} \dot{i} \dot{o} \dot{U} \dot{C} \dot{A} \dot{C} \int \dot{A} \dot{i} \dot{o} \ll \dot{C} \dot{A} \dot{o} \int \dot{A} \dot{o} \dot{A} \dot{o} \dot{I} \dot{A} \dot{A} \dot{U} \dot{i} \int \dot{o} \dot{A} \dot{o} \dot{I} \dot{U} \dot{C} \dot{D}. \pm \dot{E} \dot{S} \dot{A}$
 $\int \dot{S} \dot{A} \dot{o} \int \dot{S} \dot{A} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{C} \dot{o}, \int \dot{S} \dot{A} \dot{o} - \int \dot{A} \dot{A} \dot{U} \dot{E} \dot{y} \ll \dot{E} \dot{o} \dot{A} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o}$
 $\ll \dot{C} \times \dot{C} \dot{o} \dot{A} \dot{A} \dot{U} \dot{i} \dot{A} \dot{i} \dot{o}. - \int \dot{A} \dot{i} \dot{o} \int \dot{S} \dot{A} \dot{o} \int \dot{O} \dot{A} \dot{E} \dot{C} \dot{A} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o}.$

$\int \dot{C} \dot{o}, \int \dot{E}, \int \dot{A} \dot{o} - \int \dot{A} \dot{A} \dot{U} \dot{E} \dot{y} \ll \dot{E} \dot{o} \dot{A} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{U} \int \dot{y} \dot{U} \pm \dot{E}$
 $\ll \dot{E} \dot{C} \dot{A} \dot{i} \dot{o} \ll \dot{A} \dot{C} \dot{i} \dot{i} \dot{E} \dot{C} \dot{i} \dot{o} \pm \dot{O} \dot{o} \dot{D} \int \dot{C} \dot{i} \dot{E} \dot{L}, \dot{M}, \dot{T} \int \dot{C} \dot{o} \int \dot{A} \dot{i} \dot{o} \ll \int \dot{A} \dot{o} \dot{O} \dot{i}$
 $\int \dot{E} \dot{C} \dot{A} \dot{i} \dot{o} \int \dot{C} \dot{A} \dot{o} \dot{I} [\dot{L}] [\dot{M}] [\dot{T}] \pm \dot{E} \pm \dot{O} \int \dot{A} \dot{o} \int \dot{A} \dot{i} \dot{o}. \int \dot{S} \dot{A} \dot{o} \int \dot{S} \dot{A} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{C} \dot{o}$
 $\int \dot{A} \dot{y} \dot{A} \dot{o} \int \dot{U} \dot{o} \pm \dot{O} \int \dot{A} \dot{i} \dot{o}.$

$$[\int \dot{S} \dot{A} \dot{o}] = \left[\frac{\int \dot{p} \int \dot{A} \dot{A} \dot{A} \dot{i} \dot{o}}{\int \dot{S} \dot{A} \dot{o}} \right] = \left[\frac{\dot{L}}{\dot{T}} \right] = [\dot{L} \dot{T}^{-1}]$$

$\int \dot{S} \dot{A} \dot{o} \int \dot{A} \dot{E} \dot{C} \dot{A} \dot{o} \int \dot{A} \dot{i} \dot{o} (\text{derived quantity}) \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o}, \ll \int \dot{A} \dot{U} \dot{i} \int \dot{A} \dot{C} \ll \dot{A} \dot{C} \dot{E}$
 $\int \dot{p} \int \dot{A} \dot{o} \int \dot{A} \dot{A} \dot{A} \dot{i} \dot{o}, \int \dot{S} \dot{A} \dot{o} - \int \dot{A} \dot{A} \dot{U} \dot{E} \dot{y} \ll \dot{A} \dot{I} \int \dot{C} \dot{i} \dot{o} \dot{A} \dot{A} \dot{U} \dot{i} \int \dot{A} \dot{i} \dot{o}. \pm \dot{E} \dot{S} \dot{A}$

$$\int \dot{S} \dot{A} \dot{o} \int \dot{S} \dot{A} \dot{o} \ll \dot{A} \dot{I} = \frac{[\ll \dot{E}]}{[\dot{A} \dot{C} \dot{E} \dot{i} \dot{E}]} - \int \dot{o}. \mu \int \ll \int \dot{A} \dot{o} \dot{O} \dot{i} \int \dot{A} \dot{C} \ll \dot{A} \dot{I} \int \dot{C} \dot{A} \dot{U} \dot{S} \dot{E} \dot{i} \int$$

$\ll \int \dot{A} \dot{o} \dot{A} \dot{y} \ll \dot{A} \dot{I} \int \dot{C} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{U} \dot{E} \dot{C} \dot{i} \int \dot{o} \dot{S} \dot{A} \dot{i} \dot{D}, \int \dot{A} \dot{i} \dot{D} \dot{A} \dot{i} \int \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{C} \dot{y}$
 $\ll \dot{C} \times \int \dot{S} \dot{i} \dot{o} \int \dot{U} \dot{i} \dot{i} \int \dot{U} \dot{C} \int \dot{A} \dot{o} \dot{D} \dot{A} \dot{o} \int \dot{A} \dot{o} \int \dot{A} \dot{A} \dot{y} \dot{A} \dot{i} \int \dot{o} \dot{D} \int \dot{S} \dot{A} \dot{i} \int \dot{A} \dot{i} \dot{o}.$

$\int \dot{S} \dot{A} \dot{o} \int \dot{S} \dot{A} \dot{o} \ll \dot{E} \dot{o} \dot{A} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{U} \dot{E} \dot{A} \dot{i} \int \dot{A} \dot{i} \dot{o} \ll \dot{E} \dot{C} \dot{A} \dot{i} \int \dot{o} \ll \dot{C} \dot{A} \dot{i} \int \dot{o}, \int \dot{A} \dot{o} \int \dot{O} \dot{E} \dot{A} \dot{C} \dot{o}$
 $\int \dot{U} \dot{E} \dot{A} \dot{i} \int \dot{A} \dot{i} \dot{o} \ll \dot{E} \ll \dot{A} \dot{C} \ll \dot{E} \dot{C} \dot{A} \dot{i} \int \dot{o} \ll \dot{C} \dot{A} \dot{i} \int \dot{o}, \int \dot{A} \dot{o} \int \dot{O} \dot{E} \dot{A} \dot{C} \dot{o}$
 $\int \dot{p} \int \dot{U} \dot{E} \dot{A} \dot{i} \int \dot{O} \dot{A} \dot{C} \dot{o} \int \dot{E} \dot{A} \dot{C} \dot{o} \int \dot{A} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{y} \dot{E} \dot{A} \dot{D} \int \dot{A} \dot{i} \dot{o} \ll \dot{A} \dot{C} \ll \int \dot{E} \dot{C} \dot{i} \int \dot{o}$
 $\ll \dot{C} \dot{A} \dot{i} \int \dot{o}.$

$\int \dot{O} \dot{O} \int \dot{E} \dot{A} \dot{C} \dot{o} \int \dot{O} \dot{D} \int \dot{A} \dot{U} \int \dot{E} \int \dot{O} \int \dot{E} \int \dot{i} \int \dot{o} \ll \dot{A} \dot{I} \int \dot{C} \dot{A} \dot{U} \int \dot{E} \int \dot{A} \dot{y} \dot{A} \dot{o} \int \dot{A} \dot{y} \dot{A} \dot{o} \int \dot{o}$
 $\int \dot{A} \dot{o} \int \dot{E} \int \dot{C} \dot{i} \int \dot{A} \dot{i} \int \dot{C} \dot{S} \dot{A} \dot{i} \int \dot{o}.$

- (i) $\int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{C} \ll \int \dot{A} \dot{U} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{E} \int \dot{A} \dot{D} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{C} \int \dot{A} \dot{C} \int \dot{o}$
- (ii) $\ll \dot{E} \dot{o} \dot{A} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{U} \dot{i} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{S} \dot{A} \dot{i} \int \dot{A} \dot{i} \dot{o} \ll \dot{A} \dot{I} \ll \dot{C} \times \int \dot{S} \dot{i} \dot{o} \int \dot{C} \dot{o} \int \dot{A} \dot{A} \dot{y} \dot{A} \dot{i} \int \dot{o}$
- (iii) $\ll \dot{C} \times \int \dot{S} \dot{i} \dot{o} \int \dot{C} \dot{o} \int \dot{O} \dot{A} \dot{C} \dot{o} \int \dot{E} \dot{A} \dot{C} \dot{o} \int \dot{A} \dot{o} \dot{D} \dot{A} \dot{A} \dot{i} \int \dot{o} \int \dot{p} \int \dot{O} \int \dot{i} \int \dot{o}$
 $\ll \dot{C} \times \int \dot{S} \dot{i} \dot{o} \int \dot{C} \dot{y} \int \dot{A} \dot{y} \int \dot{A} \dot{i} \int \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{U} \dot{E} \dot{C} \ll \int \dot{A} \dot{o} \int \dot{A} \dot{o}.$
- (iv) $\int \dot{O} \dot{A} \dot{C} \dot{o} \int \dot{E} \dot{A} \dot{C} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \ll \dot{C} \times \int \dot{S} \dot{i} \dot{o} \int \dot{U} \dot{i} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o}$
 $\int \dot{A} \dot{i} \dot{o} \int \dot{E} \dot{A} \dot{C} \dot{o} \int \dot{A} \dot{A} \dot{y} \dot{A} \dot{i} \int \dot{o} \ll \dot{C} \times \int \dot{S} \dot{i} \dot{o} \int \dot{C} \dot{y} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o}$
 $\int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{A} \dot{U} \dot{i} \int \dot{o} \int \dot{A} \dot{y} \int \dot{A} \dot{i} \int \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o}.$

$\pm \dot{I} \dot{o} \dot{D} \dot{i} \int \dot{A} \dot{i} \dot{o} \int \dot{S} \dot{A} \dot{o} \int \dot{S} \dot{A} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o}$
 $\int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{O} \dot{E} \dot{A} \dot{C} \dot{o} \int \dot{O} \dot{D} \int \dot{A} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{O} \dot{E} \dot{A} \dot{C} \dot{o} \int \dot{E} \int \dot{i} \int \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{U} \dot{A} \dot{A} \dot{i} \int \dot{U} \dot{A} \dot{i} \int \dot{E} \int \dot{A} \dot{i} \dot{o} \int \dot{A} \dot{i} \dot{o} \int \dot{S} \dot{E}$
 $\int \dot{A} \dot{o} \int \dot{A} \dot{o} \int \dot{U} \dot{C} \dot{D}:$

$$[\int \dot{S} \dot{A} \dot{o} \int \dot{A} \dot{A} \dot{o}] = \frac{[1 \ll \dot{E}]}{[\dot{A} \dot{C} \dot{E} \dot{i} \dot{E}]} = \frac{[30.5 \int \dot{o} \cdot \dot{A} \dot{I}]}{[1 \dot{A} \dot{C} \dot{E} \dot{i} \dot{E}]} = 30.5 \left[\frac{1 \int \dot{o} \cdot \dot{A} \dot{I}}{1 \dot{A} \dot{C} \dot{E} \dot{i} \dot{E}} \right] - \int \dot{o}.$$

$$\text{ÅÊð¾Ã} \ll \text{Ä}_s \text{Ø} = 30.5 \left[\frac{0.01\text{m}}{1\text{வினாடி}} \right]$$

±ÉŞÅ, |Äð;ü Ó· ÈÅØ ŞÅ_Å¾ð¾üì ;Ä $\left[\frac{1 |^\circ \cdot \text{Åf}}{1\text{வினாடி}} \right]$ ±ýÈ « Ä_sý, 30.5
 Å¼í ì , Ä;ð¾ý Ó· ÈÅØ ŞÅ_Å¾ð¾ý µÄÀì ì ì î °ÄÄì ò.

$$\text{ÅÊð¾Ã} \ll \text{Ä}_s \text{Ø} = 30.5 \left[\frac{10^{-2}}{1\text{வினாடி}} \right]$$

pÄñ ¼;ÄÐ;ü· Äò Ä;Ä; ½í , Çì , Ä;ÜðŞÄ;Ð ´Ö Ó· Èì ì , ó¾
 « Äì ´ü;Ä;ýÉý « Ç×Ş_s;ø , Ç Äü;È;Ö Ó· Èì ì , ó¾ « Äì
 « Ç×Ş_s;ø Çý Å¼í , Ä;üÉ¼, Ó¾ðÓ· ÈÄý « Äì « Ç×Ş_s;ø
 ´ü;Ä;ý· ÈÖö « ¾üì ¾üÈ ÄÖð;Ä;Ö· Çì °;÷¾ Ä;¾Ä¾Öð ´ýÈ;ø
 |ÄÖì ¼ ŞÄñ Ì ò. « öŞÄ;Ð Ä· ÈÄÓ· ÈÅØ ÄÄýÄì ò¾ðÄð¾ « Äì
 « Ç×Ş_s;ø ü « ÈðÐð ¾;ðÄðì (cancel) 0¾ÄÖ· È « Äì -
 « Ç×Ş_s;ø Üì ì , ó¾ |, Øì Ç;ø °;÷¾ Ä;°Äý Å¾Ö· Äò |ÄÈÄ;ø.

±Ì òÐì , ð¾; , Ä;ð¾ý Ó· ÈÅØ, ¾· °ŞÅ_ð¾ý « Äì $\frac{1\text{அடி}}{1\text{வினாடி}}$ - Ì ò. þí Ì
 « È « Ç×Ş_s;· Ä, |^\circ \cdot \text{Åf} « Ç×Ş_s;Äý Ä;ÄÄ;_ò Äý ÄÖÄ;Ü Ä;üÉ¼ ÓÈÖö:
 (¾· °ŞÅ_ð) = $\frac{1\text{அடி}}{1\text{வினாடி}}$

$$= \frac{[1\text{அடி}] \left[\frac{30.5\text{செ.மீ}}{1\text{அடி}} \right]}{1\text{வினாடி}}$$

$$= 30.5 \left[\frac{1\text{செ.மீ}}{1\text{வினாடி}} \right]$$

$$\text{ÅÊð¾Ã} \ll \text{Ä}_s \text{Ø} = 30.5 \left[\frac{10^{-2}\text{m}}{1\text{வினாடி}} \right] - Ì ò.$$

ŞÄÖö Ä;ð¾ý Ó· ÈÅØ ¾· °ŞÅ_ð ÄÉ;Èì Ì 22 « È_sÇ;É;ø, « ·¾
 |Äð;ü Ó· ÈÅØ Äý ÄÖÄ;Ü « ÈÄ;_Ä;ø.

$$[¾· °ŞÅ_ð] = 22 \left[\frac{1\text{அடி}}{1\text{வினாடி}} \right]$$

$$\frac{22 [1 \ll \text{È}] \left[\frac{30.5 |^\circ \cdot \text{Åf}}{1 \ll \text{È}} \right]}{1 \text{ÄÉ;È}}$$

$$= 22 \times 30.5 \left[\frac{1 |^\circ \cdot \text{Åf}}{1 \text{ÄÉ;È}} \right]$$

$$\text{ÅÊð¾Ã} \ll \text{Ä}_s \text{Ø} = 22 \times 30 \left[\frac{10^{-2}\text{m}}{1\text{வினாடி}} \right]$$

þí Ì « Äì - « Ç×Ş_s;ø , Çò 0¾ÄÖ· Èì ì ¾üÈÄ;Ü Ä;üÉ¼ öŞÄ;Ð,
 ¾· °ŞÅ_ð·¾ « ÈÄ; Ì ò ±ñ ½;É '22' Ä;ÜÄ¾· Ä ±ýÄ·¾ì , ÅÉ;_
 ŞÄñ Ì ò.

1.5 (1) ÅÈÄ¾ pÄüÄÄø Ä;°Çý Ä;Ä; ½í , Ç Ä· ÄÄÜð¾ø

Q ±ýÄÐ ÅÈÄ¾ ´Ö pÄüÄÄø Ä;°· Äì Ì È;ð ð ò. Qì Ì , ó¾
 Ä;Ä; ½í , Ç « ÈöÄ·¾ð Ä;Ä; ½ « Äì « Ç×Ş_s;ø Çý ÅÈ_sÇ;ø (powers)

Áÿ ÁÔÁ; Ú ±Ø¾Á; õ.

$$[Q] = [L^x M^y T^z] = [\text{நீ}^x \text{நி}^y \text{கா}^z]$$

பீ Ì x,y,z ±ýÁË ÁËô | ÁÔì ±ñ ù. « Á §ÿ, ±¾ÿ Ì ÉÔ ÷ ¼ÁËÁ; §Á; Áÿ ÉÁ; §Á; பÔì Á; õ. §ÁÔõ Q Á; °Áÿ Á; Á; ½í ù ÿÿ¾ÿ x-ÁË, ÿÿ ÉÁÿ y-ÁË, §ÿÁð¾ÿ z-ÁË ÿ, ÁÁüË; Á ÁÁÜì ôÁ Ì õ ±É × õ ÜËÁ; õ.

´Õ°Á Ôì Á ÁËÁ¾ Á; °ÿ Çÿ Á; Á; ½í ÿ Çì ÿ ½í ÿ Á; §Á; õ.

1. ÁÁôØ (Area): ÿÿõ, « Áõ, ÿ ÁÁüËÿ | ÁÔì üÁÁË; ÷ ÁÁôÁÇ × « ÇÁ¾ôÁ Ì Á¾; ÷, ÁÁôÁÇÁÿ Á; Á; ½í ù [L²] ÿ Ì õ.

$$[ÁÁôÁÇ \times] = [\text{ÿÿõ} \times \text{Áõ}] = [L \times L] = [L^2]$$

2. ÁÔÁÿ (Volume): ´Õ | Á; ÒÇÿ ÁÔÁÿ, « ¾ý ÿÿ, « Á, ÿ ÁÁì Çÿ | ÁÔì üÁÁË; ÷ « ÇÁ¾ôÁ Ì Á¾; ÷, ÁÔÁËÿ Á; Á; ½í ù [L³] ÿ Ì õ.

$$\begin{aligned} \text{ÁÔÁÿ} &= [\text{ÿÿõ} \times \text{Áõ} \times \text{ÁÁõ}] \\ &= [L \times L \times L] \\ &= [L^3] \end{aligned}$$

3. « ¼÷ð¾ÿ (Density): ´Õ | Á; ÒÇÿ « ¼÷ð¾ÿ « ¾ý µÁÁ Ì ÁÔÁËÿ ÿÿ ÉÁ; Ì õ.

$$[\text{« } \frac{1}{4} \div \text{ð} \frac{3}{4}] = \left[\frac{\text{ÿÿ É}}{\text{ÁÔÁÿ}} \right] = \left[\frac{M}{L^3} \right] = [ML^{-3}]$$

4. ¾ÿ °§Á õ (Velocity): பஊ µÁÁ Ì §ÿÁð¾ÿ | ÁÜõ ப¼ô | ÁÁ÷í °Á; Ì õ.

$$[\text{¾ÿ } \circ \text{§Á } \circ] = \left[\frac{\text{ப¼ô | ÁÁ÷í } \circ}{\text{§ÿÁõ}} \right] = \left[\frac{L}{T} \right] = [LT^{-1}]$$

5. ÓÍ Ì õ (Acceleration): பஊ µÁÁ Ì §ÿÁð¾ÿ ¾ÿ °§Á ÷¾ÿ ÿüÁ Ì Á; ÜÁ; ¼; Ì õ.

$$[\text{ÓÍ } \text{Ì } \circ] = \left[\frac{\text{¾ÿ } \circ \text{§Á } \circ}{\text{§ÿÁõ}} \right] = \left[\frac{LT^{-1}}{T} \right] = [LT^{-2}]$$

6. ÿó¾õ (Momentum): ´Õ | Á; ÒÇÿ ÿó¾õ, « ¾ý ÿÿ É, ¾ÿ °§Á ÷ ÿ, ÁÁüËÿ | ÁÔì üÁÁË; ÷ « ÇÁ¾ôÁ Ì õ.

$$\begin{aligned} [\text{உந் தம்}] &= [\text{நிறை} \times \text{திசைவேகம்}] \\ &= [M \times LT^{-1}] \\ &= [M L T^{-1}] \end{aligned}$$

7. Áÿ ° (Force): Áÿ °Á; Éஊ, ÿäð¾Ëÿ பñ ¼; ஊ Á¾ôÁË, | Á; ÒÇÿ ÿÿ É, ÓÍ Ì õ ÿ, ÁÁüËÿ | ÁÔì üÁÁË; ÷ « ÇÁ¾ôÁ Ì õ. ±É §Á,

$$\begin{aligned}
 [\dot{A}c^{\circ}] &= [\dot{c}^{\circ} \text{ EXÓT } i, \ddot{o}] \\
 &= [M \times LT^{-2}] \\
 &= [MLT^{-2}]
 \end{aligned}$$

8. $\frac{3}{4}i\ddot{l}$ (Impulse): $\frac{3}{4}i\ddot{l} \pm y\Delta\theta \dot{A}c^{\circ} \text{ ÁüÜö } \mathcal{S}_z\ddot{A}\ddot{o} \text{ p}^{\circ} \text{ Á}_s\mathcal{C}\mathcal{Y}$
 $\dot{A}\ddot{O}i \text{ , üÄÄÉ } i\emptyset \ll \mathcal{C}\mathcal{A}\mathcal{C}\mathcal{A}\mathcal{O}\mathcal{A}\mathcal{I} \ddot{o} . \pm \text{É } \mathcal{S}\mathcal{A}$,
 $\frac{3}{4}i\ddot{l} \dot{A}c^{\circ} \times \mathcal{S}_z\ddot{A}\ddot{o}$

$$\begin{aligned}
 [\frac{3}{4}i\ddot{l}] &= [\dot{A}c^{\circ} \times \mathcal{S}_z\ddot{A}\ddot{o}] \\
 &= [MLT^{-2} \times T] \\
 &= [MLT^{-1}] \\
 &= [MLT^{-1}]
 \end{aligned}$$

$[\frac{3}{4}i\ddot{l}] \text{ , } - \text{ó}\frac{3}{4}\ddot{O} \text{ } \rightarrow \text{ , } \mathcal{C}\mathcal{A}\mathcal{A}\mathcal{U}\mathcal{E}\mathcal{Y} \text{ } \dot{A}i\mathcal{C}\mathcal{A}i \text{ } \frac{1}{2}i \text{ , } \ddot{u} \text{ } \circ\mathcal{A}\mathcal{A}i \text{ , } \text{p}\ddot{O}\ddot{A}^{\circ} \frac{3}{4}i$
 $\text{ , } i\ddot{n} \text{ , }]$

9. $\mathcal{S}\mathcal{A}^{\circ} \ddot{A}$ (work)

$$\begin{aligned}
 \mathcal{S}\mathcal{A}^{\circ} \ddot{A} &= \dot{A}c^{\circ} \times \dot{A}c^{\circ} \circ i \text{ } | \circ \mathcal{A}\mathcal{U}\mathcal{A}\mathcal{I} \text{ } \ddot{O}\mathcal{U}\mathcal{C}\mathcal{C}\mathcal{Z} \text{ , } \ddot{O}\ddot{o} \text{ } | \frac{3}{4}i^{\circ} \ddot{A} \times \\
 [\mathcal{S}\mathcal{A}^{\circ} \ddot{A}] &= [\dot{A}c^{\circ} \times \dot{A}c^{\circ} \circ i \text{ } | \circ \mathcal{A}\mathcal{U}\mathcal{A}\mathcal{I} \text{ } \ddot{O}\mathcal{U}\mathcal{C}\mathcal{C}\mathcal{Z} \text{ , } \ddot{O}\ddot{o} \text{ } | \frac{3}{4}i^{\circ} \ddot{A} \times] \\
 &= [MLT^{-2} \times L] \\
 &= [ML^2T^{-2}]
 \end{aligned}$$

10. $\text{p}\hat{A}i \text{ , } \rightarrow \ddot{u}\ddot{E}\emptyset$ [Kinetic Energy]

$$\begin{aligned}
 \text{p}\hat{A}i \text{ , } \rightarrow \ddot{u}\ddot{E}\emptyset &= \frac{1}{2} \times \dot{c}^{\circ} \ddot{E} \times (\frac{3}{4}c^{\circ} \circ \mathcal{S}\mathcal{A}_s\ddot{o})^2 \\
 [\rightarrow \ddot{u}\ddot{E}\emptyset] &= [\dot{c}^{\circ} \ddot{E} \times (\frac{3}{4}c^{\circ} \circ \mathcal{S}\mathcal{A}_s\ddot{o})^2] \\
 &= [M \times (LT^{-1})^2] \\
 &= [ML^2T^{-2}]
 \end{aligned}$$

$[\mathcal{S}\mathcal{A}^{\circ} \ddot{A} \text{ , } \rightarrow \ddot{u}\ddot{E}\emptyset \text{ } \rightarrow \text{ , } \mathcal{C}\mathcal{A}\mathcal{A}\mathcal{U}\mathcal{E}\mathcal{Y} \text{ } \dot{A}i\mathcal{C}\mathcal{A}i \text{ } \frac{1}{2}i \text{ , } \ddot{u} \text{ } \circ\mathcal{A}\mathcal{A}i \text{ , } \text{p}\ddot{O}\ddot{A}^{\circ} \frac{3}{4}i$
 $\text{ , } i\ddot{n} \text{ , }]$

11. $\frac{3}{4}c\ddot{E}y$ (Power): $\frac{3}{4}c\ddot{E}y \pm y\Delta\theta \mu\mathcal{A}\mathcal{A}\mathcal{I} \mathcal{S}_z\ddot{A}\ddot{o} \frac{3}{4}c\ddot{E} \text{ } | \circ \ddot{O}\mathcal{A}\mathcal{O}\mathcal{A}\mathcal{O} \frac{1}{4} \mathcal{S}\mathcal{A}^{\circ} \ddot{A}$.

$$\begin{aligned}
 \frac{3}{4}c\ddot{E}y &= \frac{i \circ \ddot{O}\mathcal{A}\mathcal{O}\mathcal{A}\mathcal{O} \frac{1}{4} \mathcal{S}\mathcal{A}^{\circ} \ddot{A}}{\mathcal{S}_z\ddot{A}\ddot{o}} \\
 [\frac{3}{4}c\ddot{E}y] &= \left[\frac{i \circ \ddot{O}\mathcal{A}\mathcal{O}\mathcal{A}\mathcal{O} \frac{1}{4} \mathcal{S}\mathcal{A}^{\circ} \ddot{A}}{\mathcal{S}_z\ddot{A}\ddot{o}} \right] \\
 &= \left[\frac{ML^2T^{-2}}{T} \right] \\
 &= [ML^2T^{-3}]
 \end{aligned}$$

12. $\mathcal{S}_s i \frac{1}{2}\ddot{o}$ (Angle): $\mathcal{S}_s i \frac{1}{2}\ddot{o} \text{ } \frac{3}{4} \mathcal{S}\mathcal{A}\mathcal{E}\mathcal{A}\mathcal{E} \emptyset \ll \mathcal{C}\mathcal{A}\mathcal{C}\mathcal{I} \text{ } \ddot{o}\mathcal{S}\mathcal{A}i\mathcal{D}$

$$\mathcal{S}_s i \frac{1}{2}\ddot{o} (\text{r}) = \frac{\mathcal{A}\ddot{o} \frac{1}{4} \mathcal{A}\emptyset}{-\mathcal{A}\ddot{o}}$$

±ÉŞĀ,

$$[S_{,i} \frac{1}{2} \ddot{\theta}] = \left[\frac{\text{வட்டவிலை}}{\text{ஆரம்}} \right]$$

$$= \left[\frac{L}{L} \right]$$

$$= [L^0]$$

±ÉŞĀ, $S_{,i} \frac{1}{2} \ddot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \frac{1}{2} \dot{\theta} \hat{u}_j \hat{u}_i \hat{A}_j \hat{D}$.

13. $S_{,i} \frac{1}{2} \dot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D}$ (Angular velocity): $\rho \hat{D} \mu \hat{A} \hat{A} \hat{I} \quad S_{,i} \hat{A} \hat{o} \hat{u}_i \hat{A}_j \hat{A}_i \hat{D}$
 $\hat{A} \hat{u}_i \hat{o} S_{,i} \frac{1}{2} \dot{\theta} \hat{u}_i \hat{A}_j \hat{A}_i \hat{D}$.

$$S_{,i} \frac{1}{2} \dot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D} (\hat{S}) = \left[\frac{S_{,i} \frac{1}{2} \dot{\theta}}{S_{,i} \hat{A} \hat{o}} \right]$$

$$\pm \hat{E} \hat{S} \hat{A} [S_{,i} \frac{1}{2} \dot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D}] = \left[\frac{S_{,i} \frac{1}{2} \dot{\theta}}{S_{,i} \hat{A} \hat{o}} \right]$$

$$= \left[\frac{L^0}{T} \right]$$

$$= [T^{-1}]$$

14. $S_{,i} \frac{1}{2} \ddot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D}$ (Angular Acceleration):

$\rho \hat{D} \mu \hat{A} \hat{A} \hat{I} \quad S_{,i} \hat{A} \hat{o} \hat{u}_i \hat{A}_j \hat{A}_i \hat{D} \quad S_{,i} \frac{1}{2} \dot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D} \quad \hat{u}_i \hat{A}_j \hat{A}_i \hat{D} \quad \hat{A}_j \hat{A}_i \hat{D}$

$$S_{,i} \frac{1}{2} \ddot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D} = \frac{S_{,i} \frac{1}{2} \dot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D}}{S_{,i} \hat{A} \hat{o}}$$

$$\pm \hat{E} \hat{S} \hat{A} [S_{,i} \frac{1}{2} \ddot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D}] = \left[\frac{S_{,i} \frac{1}{2} \dot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D}}{S_{,i} \hat{A} \hat{o}} \right]$$

$$= \left[\frac{T^{-1}}{T} \right] = [T^{-2}]$$

15. $\hat{u}_i \hat{A}_j \hat{A}_i \hat{D} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D}$ (Moment of inertia):

$$\hat{u}_i \hat{A}_j \hat{A}_i \hat{D} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D} = \hat{u}_i \hat{A}_j \hat{A}_i \hat{D} (\hat{I} \hat{A}_j \hat{A}_i \hat{D} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D})^2$$

±ÉŞĀ

$$[\text{நிலைமத் திருப்புதிறன்}] = \text{நிறை} \times (\text{சுழற்சி ஆரம்})^2$$

$$= [M \times L^2]$$

$$= [ML^2]$$

16. $S_{,i} \frac{1}{2} \dot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D}$ (Moment of momentum) : $\hat{u}_i \hat{A}_j \hat{A}_i \hat{D} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D}$, $S_{,i} \frac{1}{2} \dot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D}$ $\hat{u}_i \hat{A}_j \hat{A}_i \hat{D}$ $\hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D}$
 $S_{,i} \frac{1}{2} \dot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D} \pm \hat{E} \hat{o} \hat{A}_i \hat{D}$.

$$[S_{,i} \frac{1}{2} \dot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D}] = [\hat{u}_i \hat{A}_j \hat{A}_i \hat{D} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D} \times S_{,i} \frac{1}{2} \dot{\theta} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D}]$$

$$= [M L^2 \times T^{-1}]$$

$$= [M L^2 T^{-1}]$$

17. $\hat{u}_i \hat{A}_j \hat{A}_i \hat{D} \hat{u}_i \hat{o} \hat{A}_j \hat{A}_i \hat{D}$ (Torque)

±ÉŞĀ

$$\begin{aligned} \text{Work done} &= (\text{Force} \times \text{Displacement}) \\ &= [ML^2 \times T^{-2}] \\ &= [ML^2T^{-2}] \end{aligned}$$

18. Young modulus

$$\begin{aligned} \text{Young modulus} &= \frac{\text{Stress}}{\text{Strain}} \\ &= \frac{\text{Force/area}}{\text{Extension/original length}} \\ \text{Young modulus} &= \left[\frac{MLT^{-2}/L^2}{L/L} \right] \\ &= [ML^{-1}T^{-2}] \end{aligned}$$

19. Pressure:

$$\begin{aligned} \text{Pressure} &= \frac{\text{Force}}{\text{Area}} \\ [\text{Pressure}] &= \left[\frac{MLT^{-2}}{L^2} \right] \\ &= [ML^{-1}T^{-2}] \end{aligned}$$

20. Surface Tension

$$\begin{aligned} \text{Surface Tension} &= \frac{\text{Force}}{\text{Length}} \\ [\text{Surface Tension}] &= \left[\frac{MLT^{-2}}{L} \right] \\ &= [MT^{-2}] \end{aligned}$$

21. Coefficient of Viscosity

$$\begin{aligned} \text{Coefficient of Viscosity} &= \frac{\text{Shear stress}}{\text{Shear strain rate}} \\ &= \frac{\text{Force/area}}{\text{Velocity difference/length}} \\ \text{Coefficient of Viscosity} &= \left[\frac{ML^{-1}T^{-2}}{LT^{-1}/L} \right] \\ &= [ML^{-1}T^{-1}] \end{aligned}$$

22. Shear Stress: Ss

$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$

$$(|\vec{A}| |\vec{B}| \cos \theta) = \left[\frac{|\vec{A}| |\vec{B}| \cos \theta}{|\vec{A}| |\vec{B}| \times} \right] = \left[\frac{MLT^{-2}}{L^2} \right] = [ML^{-1}T^{-2}]$$

23. Ούτιλ δόση (Torque) - T_q

$\vec{\tau} = \vec{r} \times \vec{F}$

$[\text{Ούτιλ δόση}] = (\text{Απόσταση} \times \text{Δύναμη})$

$$= (L \times MLT^{-2}) = [ML^2T^{-2}]$$

1.6 « ÄĬ ÇŸ » " Äö Û ö, Ä" °ÄŸ ĨÄĐİ Šĭ ðÄĬĬ ö (Systems of Units and Concept of a Force)

1.6 (1) °ĭ÷ÄÄĭ « ÄĬ ÇŸ » " Äö (Absolute System of Units)

ÿÇö, ÿ" È, ŠÿÄö Ñ ÇÄ Äĭ °Ç ÇŸ « ÈöÄ" ¼ö Äĭ ÇÄĭ ½Ĭ Çĭ ø Äü ĨÈøÄĭ
 ÞÄüÄÄø Äĭ °Ç ÇŸ Äĭ ÇÄĭ ½Ĭ " Çĭ ½Ĭ ¼ ÖÈö. « ÈöÄ" ¼ « ÄĬ Û
 ±øÄĭ Þ¼Ĭ ÇÖö " ŠÄÄĭ ¾ÇÄĭ È ĨÄĭ ÖüÄĬ ö Ä" Äø ÄÄŸÄĬ ð¾öÄĬ Ä¾ĭ ø
 « ÈöÄ" ¼ Äĭ °Ç ÇŸ « ÄĬ Û °ĭ÷ÄÄĭ « ÄĬ Çĭ ĨĬ ĨĬ ÛÇöÄĬ ö. ÿÇö, ÿ" È,
 ŠÿÄö Ñ ÇÄÄüÈüĬ ĨÄĭ °ĭ÷ÄÄĭ « ÄĬ Û " Ö °ĭ÷ÄÄĭ « " Äö Ä Ä" ÄÄÜĬ Ĩ ö.
 ÞĬ °ĭ÷ÄÄĭ « " Äö Ö " ÈÄø Ä" °Äĭ ÈĐ °ĭ÷ø¾ Äĭ °ÇÄĭ Ĩ Ö¾öÄĬ ö. ±È ŠÄ
 Ä" °ÄŸ Äĭ ÇÄĭ ½Ĭ " Ç « ÈöÄ" ¼Ĭ °ĭ÷ÄÄĭ « ÄĬ ÇŸ Äĭ ÇÄĭ ½Ĭ Çĭ ø
 Ä" ÄÄÜĬ Šĭ ö.

ÿä ð¼ÈŸ ÞÄñ ¼ĭ ÄĐ ÞÄĬ Ä¾öÄÈ
 Ä" ° = ÿ" È XÖĬ Ĩ ö Ñ Ĩ ö

±È ŠÄ

$$[Ä" °] = [ÿ" È XÖĬ Ĩ ö]$$

$$= [M \times LT^{-2}]$$

$$= [MLT^{-2}] - Ĩ ö.$$

ĨÄĐĭ ÄÈö¾Ä Ö" È" ÄĬ " Äĭ Û ö ŠÄĭ Đ ÿ" È 1 Ç. Ç;
 ÖĬ Ĩ ö = 1 ÄÈ/Ä² ±Ÿ Èĭ Ä¾ĭ ø,

$$Ä" ° = ÿ" È XÖĬ Ĩ ö$$

$$= 1 Ç. Ç \times 1 ÄÈ / Ä²$$

$$= 1 (Ç. Ç \times 1 ÄÈ / Ä²) - Ĩ ö.$$

Ä" °ÄŸ Äĭ ÇÄĭ ½Ĭ Û, (Ç. Ç ÄÈ/Ä²) ±Ÿ Ü Ñ Ä¾ĭ ø Ä" °, « ¾Ÿ « Ä ø
 (Ç. Ç ÄÈ/Ä²) ±Ÿ ÈĬ ö. ±È ŠÄ µÄĬ ÿ" È ÖüÇ ĨÄĭ Öü ŸÈŸÄĐ ĨÄøÄÖĬ
 « ö ĨÄĭ ÖÇø ¾Ÿ ¾Ç" °Ä ŠÄŠÄ µÄĬ ÖĬ Ĩ ö " ¾ züÄĬ ðĐö Ä" ° " ÖÄ
 Ä" °ÄĬ ö (one unit of force). ĨÄĐĭ Ö" ÈÄø ÄĐ¼÷, ÇŠÄĭ Çĭ ö, ÄÈĭ È
 Ñ ÇÄÄüÈŸ ÄÈö¾Ä °ĭ÷ÄÄĭ « ÄĬ Çø, Ä" °ÄŸ °ĭ÷ÄÄĭ « ÄĬ, ÿä ð¼Ÿ
 ±È öÄĬ Ä¾ĭ ö.

$$1 \text{ ÿä ð¼Ÿ} = (1 \text{ Ç. Ç}) (1 ÄÈ / Ä²)$$

ĨÄĐĭ " ° ÄÈ Çĭ ö, ÄÈÈĭ È" Ö" ÈÄø Ä" °ÄŸ °ĭ÷ÄÄĭ « ÄĬ " ¼Ÿ (Dyne)
 ±È öÄĬ ö. « ¾ĭ ÄĐ " Ö Çĭ ö ÿ" È ÖüÇ ĨÄĭ ÖÇŸ ÄĐ ĨÄüÄÖĬ
 « ö ĨÄĭ ÖÇø, ¾Ÿ ¾Ç" °Ä ŠÄŠÄ (1 " ° ÄÈ/Ä²) ÖĬ Ĩ ö " ¾ Ä" ÇÄĬ Ĩ ö Ä" °
 " Ö" ¼Ÿ Ä" °ÄĬ ö.

« üÄĭ ŠÈ Ä" ö¼Ÿ Ö" ÈÄø Ä" °ÄŸ °ĭ÷ÄÄĭ « ÄĬ Ä × ñ ¼ø
 (Poundal) - Ĩ ö. " ÖÄ × ñ Ĩ ÿ" È ÖüÇ ĨÄĭ ÖÇŸ ÄĐ ĨÄüÄÖĬ,
 « ö ĨÄĭ ÖÇø ¾Ÿ ¾Ç" °Ä ŠÄŠÄ, (1 « È/Ä²) ÖĬ Ĩ ö " ¾ Ä" ÇÄĬ Ĩ ö Ä" ° " Ö
 Ä × ñ ¼ø Ä" °ÄĬ ö.

°ĭ÷ÄÄĭ « ÄĬ ÇŸ Ä¾öö Û ±øÄĭ Þ¼Ĭ ÇÖö " ŠÄ
 « ÇÄĭ È" ÄÄĭ, × ö, ðÄÄÈöö Ä" °Äĭ ø Äĭ ¾Çĭ öÄ¼ĭ ÄÖö " üÇÈ.

°ĭ÷ÄÄĭ « ÄĬ ÇŸ « " Äö Ö" È, ÞÄüÄÄø ÞÄ" ĨÄÈ ð È Çø
 ÄŸ ÄüÈöÄĬ ÈĐ.

°ĭ÷ÄÄĭ « ÄĬ " Çö ¾øÄÄ « " Äö Ö" È ÇŸ « ð¼Ä" ½ ÄŸ ÄÖÄĭ Ü:

$\dot{A}_i \dot{\omega} \frac{1}{4} \dot{\gamma} \dot{O} \dot{E} \dot{A} \dot{\omega}, \dot{A} \dot{\omega} \dot{A} \dot{\gamma} \dot{O} \dot{A} \dot{A} \dot{E} \dot{\omega} \dot{O} \dot{O} \dot{i} \dot{=} \dot{O} \frac{3}{4} \ll \dot{A} \dot{I} \dot{A} \times \dot{n} \dot{I} \dot{\pm} \dot{\omega} \frac{1}{4}$
 $\dot{\pm} \dot{E} \dot{o} \dot{A} \dot{I} \dot{o}. \dot{O} \dot{A} \times \dot{n} \dot{I} \dot{\pm} \dot{\omega} \dot{E} \dot{O} \dot{U} \dot{C} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{\gamma} \dot{A} \dot{D} \dot{I} \dot{O} \dot{A} \dot{U} \dot{A} \dot{I} \dot{o} \dot{O} \dot{A} \dot{A} \dot{E} \dot{\omega} \dot{O} \dot{A} \dot{\omega} \dot{O}$
 $\dot{A} \times \dot{n} \dot{I} \dot{\pm} \dot{\omega} \frac{1}{4} \dot{A} \dot{I} \dot{o}, \dot{\pm} \dot{E} \dot{S} \dot{A},$

$$1 \dot{A} \times \dot{n} \dot{I} \dot{\pm} \dot{\omega} \frac{1}{4} = g \dot{A} \times \dot{n} \dot{I} \dot{o} \dot{C} \dot{I} \dot{o}.$$

$g \dot{\gamma} \dot{A} \dot{\omega} \dot{O} \dot{p} \frac{1}{4} \dot{O} \dot{3} \dot{4} \dot{U} \dot{O} \dot{1} \dot{4} \dot{o} \dot{A} \dot{I} \dot{U} \dot{A} \dot{I} \dot{A} \dot{3} \dot{4} \dot{I} \dot{o}, \dot{S} \dot{A} \dot{I} \dot{A} \dot{I} \dot{o} \dot{\pm} \dot{\omega} \frac{1}{4}, \dot{A} \dot{I} \dot{o} \dot{\pm} \dot{\omega} \frac{1}{4},$
 $\dot{A} \times \dot{n} \dot{I} \dot{\pm} \dot{\omega} \frac{1}{4} \dot{A} \dot{A} \dot{U} \dot{E} \dot{\gamma} \dot{A} \dot{\omega} \dot{O} \dot{I} \dot{U} \dot{o} \dot{p} \frac{1}{4} \dot{O} \dot{3} \dot{4} \dot{U} \dot{O} \dot{1} \dot{4} \dot{o} \dot{A} \dot{I} \dot{U} \dot{A} \dot{I} \dot{o}.$

$\dot{C} \dot{E} \dot{A}, \dot{\mu} \dot{=} \dot{O} \dot{i} \dot{=} \dot{O} \frac{3}{4} \dot{A} \dot{I} \dot{O} \dot{A} \dot{I} \dot{I} \dot{O} \dot{3} \dot{4} \dot{E} \dot{I} \dot{o}, \ll \frac{3}{4} \dot{\gamma} \dot{A} \dot{I} \dot{A} \dot{I} \dot{2} \dot{I} \dot{U} \dot{C} \dot{A} \dot{O} \dot{1} \dot{4} \dot{E} \dot{\gamma}$
 $\dot{p} \dot{A} \dot{n} \dot{I} \dot{A} \dot{D} \dot{A} \dot{O} \dot{A} \dot{E},$

$$[\dot{C} \dot{E}] = \left[\frac{\dot{A} \dot{\omega}}{\dot{O} \dot{I} \dot{I} \dot{o}} \right] = \left[\frac{[F]}{[LT^2]} \right] = [FL^{-1}T^2] \quad \dot{-} \dot{I} \dot{o}.$$

$\dot{A} \dot{\omega}, \dot{C} \dot{O}, \dot{S} \dot{A} \dot{O} \dot{-} \dot{A} \dot{A} \dot{U} \dot{E} \ll \dot{E} \dot{o} \dot{A} \dot{\omega} \frac{1}{4} \dot{A} \dot{I} \dot{O} \dot{C} \dot{I} \dot{S} \dot{A} \dot{U} \dot{I} \dot{U} \dot{U} \dot{o} \dot{S} \dot{A} \dot{I} \dot{D},$
 $\dot{A} \dot{\omega} \dot{A} \dot{\gamma} \dot{O} \dot{i} \dot{=} \dot{A} \dot{A} \dot{I} \ll \dot{A} \dot{I}, \dot{O} \dot{S} \dot{A} \dot{I} \dot{A} \dot{I} \dot{o} \dot{A} \dot{\omega} \dot{\pm} \dot{E} \dot{I} \dot{I} \dot{U} \dot{C} \dot{o} \dot{A} \dot{I} \dot{o}. \ll \dot{o} \dot{S} \dot{A} \dot{I} \dot{D},$
 $\dot{C} \dot{E} \dot{A} \dot{\gamma} \dot{O} \dot{i} \dot{=} \dot{A} \dot{A} \dot{I} \ll \dot{A} \dot{I}, \dot{O} \dot{S} \dot{A} \dot{I} \text{ (Slug)} \dot{\pm} \dot{E} \dot{o} \dot{A} \dot{I} \dot{o}.$

$\dot{O} \dot{S} \dot{A} \dot{I} \dot{A} \dot{I} \dot{o} \dot{A} \dot{\omega} \dot{O} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{\gamma} \dot{S} \dot{A} \dot{O} \dot{I} \dot{A} \dot{O} \dot{A} \dot{O} \dot{I} \frac{3}{4} \dot{\gamma} \frac{3}{4} \dot{O} \dot{A} \dot{S} \dot{A} \dot{S} \dot{A}$
 $\ll \dot{o} \dot{I} \dot{A} \dot{I} \dot{O} \dot{U} \dot{I} \dot{I} \text{ (1 A/A}^2 \text{) } \dot{O} \dot{I} \dot{I} \dot{o} \dot{\omega} \frac{3}{4} \dot{A} \dot{C} \dot{A} \dot{I} \dot{A} \dot{I} \dot{E} \dot{I} \dot{o}, \ll \dot{o} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{\gamma} \dot{C} \dot{E}$
 $\ll \dot{C} \times \dot{O} \text{ " } \dot{A} \dot{D} \dot{I} \dot{S} \dot{A} \dot{I} \text{ " } \dot{\pm} \dot{E}, \dot{C} \dot{A} \dot{O} \dot{1} \dot{4} \dot{E} \dot{\gamma} \dot{p} \dot{A} \dot{n} \dot{I} \dot{A} \dot{D} \dot{A} \dot{O} \dot{A} \dot{E}$
 $\dot{A} \dot{A} \dot{U} \dot{I} \dot{A} \dot{I} \dot{o}. \ll \frac{3}{4} \dot{A} \dot{D}, \dot{C} \dot{A} \dot{O} \dot{1} \dot{4} \dot{E} \dot{\gamma} \dot{A} \dot{O} \dot{A} \dot{E},$

$$F = m \cdot a$$

$\dot{p} \dot{I} \dot{I} \dot{F} = 1 \dot{C} \dot{C} \dot{A} \dot{\omega}; a = 1 \dot{A} \dot{A} \dot{C}^2 \dot{\pm} \dot{\gamma} \dot{E} \dot{I} \dot{A} \dot{3} \dot{4} \dot{I} \dot{o} m = 1 \dot{-} \dot{I} \dot{o}$
 $\dot{\pm} \dot{E} \dot{S} \dot{A} \dot{C} \dot{E} = 1 \dot{I} \dot{A} \dot{D} \dot{I} \dot{S} \dot{A} \dot{I} \dot{-} \dot{I} \dot{o}.$

$\dot{C} \dot{A} \dot{O} \dot{1} \dot{4} \dot{E} \dot{\gamma} \dot{A} \dot{O} \dot{A} \dot{E}, \dot{O} \dot{S} \dot{A} \dot{I} \dot{A} \dot{I} \dot{o} \dot{A} \dot{\omega}, \dot{O} \dot{I} \dot{A} \dot{D} \dot{I} \dot{S} \dot{A} \dot{I} \dot{C} \dot{E} \dot{O} \dot{U} \dot{C}$
 $\dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{O} \dot{I} \dot{A} \dot{U} \dot{A} \dot{I} \dot{o} \dot{S} \dot{A} \dot{I} \dot{D}, \frac{3}{4} \dot{\gamma} \frac{3}{4} \dot{O} \dot{A} \dot{O} \ll \dot{o} \dot{I} \dot{A} \dot{I} \dot{O} \dot{U} \dot{I} \dot{I}, 1 \dot{A} \dot{A} \dot{C}^2 \dot{O} \dot{I} \dot{I} \dot{o} \dot{\omega} \frac{3}{4}$
 $\dot{A} \dot{C} \dot{A} \dot{I} \dot{o}. \dot{-} \dot{E} \dot{I} \dot{o}, \dot{O} \dot{A} \dot{A} \dot{E} \dot{\omega} \dot{O} \dot{A} \dot{O} \dot{A} \dot{E}, 1 \dot{S} \dot{A} \dot{I} \dot{A} \dot{I} \dot{o} \dot{A} \dot{\omega}, 1 \dot{S} \dot{A} \dot{I} \dot{A} \dot{I} \dot{o}$
 $\dot{C} \dot{E} \dot{O} \dot{U} \dot{C} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{O} g \dot{A} \dot{A} \dot{C}^2 \dot{O} \dot{I} \dot{I} \dot{o} \dot{\omega} \frac{3}{4} \dot{A} \dot{C} \dot{A} \dot{I} \dot{\gamma} \dot{E} \dot{D}. \dot{-} \frac{3}{4} \dot{A} \dot{I} \dot{o},$

$$1 \dot{S} \dot{A} \dot{I} \dot{A} \dot{I} \dot{o} \dot{A} \dot{\omega} = (1 \dot{I} \dot{A} \dot{D} \dot{I} \dot{S} \dot{A} \dot{I}) (1 \dot{A} \dot{A} \dot{C}^2) = (1 \dot{C} \dot{C}) (g \dot{A} \dot{A} \dot{C}^2)$$

1.6 (3) $\dot{O} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{\gamma} \dot{C} \dot{E} \dot{O} \dot{O}, \dot{\pm} \dot{\omega} \frac{1}{4} \dot{O} \dot{O}$

$\dot{O} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{\gamma} \dot{C} \dot{E} \text{ (Mass)} \ll \frac{3}{4} \dot{A} \dot{I} \dot{A} \dot{I} \dot{O} \dot{A} \dot{I} \dot{O} \dot{n} \dot{A} \dot{A} \dot{\gamma} \text{ (Matter)}$
 $\ll \dot{C} \dot{A} \dot{I} \dot{o}. \dot{p} \dot{\omega} \frac{3}{4} \dot{O} \dot{C} \times \dot{A} \dot{I} \dot{o} \dot{3} \dot{4} \dot{I} \dot{U} \dot{E} \dot{C} \dot{A} \dot{O} \dot{1} \dot{4} \dot{E} \dot{\gamma} \dot{p} \dot{A} \dot{n} \dot{I} \dot{A} \dot{D} \dot{A} \dot{O} \dot{A} \dot{E}$

$F = m a \dot{\pm} \dot{\gamma} \dot{E} \dot{I} \dot{A} \dot{3} \dot{4} \dot{I} \dot{o} a = \frac{F}{m} \dot{-} \dot{I} \dot{o}. \dot{-} \frac{3}{4} \dot{A} \dot{I} \dot{o} \dot{O} \dot{I} \dot{E} \dot{O} \dot{A} \dot{O} \dot{1} \dot{4} \dot{A} \dot{\omega} \dot{I} \dot{A} \dot{I} \dot{O} \dot{U}$

$\dot{\gamma} \dot{E} \dot{\gamma} \dot{A} \dot{D} \dot{I} \dot{A} \dot{U} \dot{A} \dot{I} \dot{o} \dot{I} \dot{A} \dot{I} \dot{O} \dot{D} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{O} \dot{2} \dot{U} \dot{A} \dot{I} \dot{o} \dot{O} \dot{I} \dot{I} \dot{o} \ll \frac{3}{4} \dot{\gamma} \dot{C} \dot{E} \dot{I} \dot{I} \dot{\pm} \dot{\omega} \frac{3}{4}$
 $\dot{A} \dot{C} \dot{O} \dot{3} \dot{4} \dot{O} \dot{U} \dot{C} \dot{D}. \dot{S} \dot{A} \dot{O} \dot{O} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{\gamma} \dot{C} \dot{E} \ll \frac{3}{4} \dot{A} \dot{I} \dot{p} \dot{O} \dot{I} \dot{I} \dot{o} \dot{S} \dot{A} \dot{I} \dot{D} \ll \dot{D} \frac{3}{4} \dot{\gamma}$
 $\dot{C} \dot{A} \dot{A} \dot{\pm} \dot{C} \dot{O} \dot{4} \dot{O} \dot{A} \dot{I} \dot{U} \dot{E} \dot{I} \dot{I} \dot{U} \dot{A} \dot{3} \dot{4} \dot{O} \dot{A}. \dot{-} \frac{3}{4} \dot{A} \dot{I} \dot{o} \dot{O} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{\gamma} \dot{C} \dot{E} \dot{\pm} \dot{\gamma} \dot{A} \dot{D}$
 $\ll \dot{o} \dot{I} \dot{A} \dot{I} \dot{O} \dot{U} \frac{3}{4} \dot{\gamma} \dot{C} \dot{A} \dot{A} \dot{I} \dot{U} \dot{E} \dot{I} \dot{I} \dot{U} \dot{A} \dot{3} \dot{4} \dot{O} \dot{I} \dot{o} \frac{3}{4} \dot{A} \dot{I} \dot{o} \dot{3} \dot{4} \dot{\gamma} \ll \dot{C} \dot{A}$
 $\ll \dot{o} \dot{A} \dot{D} \ll \frac{3}{4} \dot{A} \dot{I} \dot{O} \dot{U} \dot{C} \dot{C} \dot{A} \dot{A} \dot{O} \dot{3} \dot{4} \dot{\gamma} \text{ ((inertia)} \ll \dot{C} \dot{A} \dot{I} \dot{E} \dot{I} \dot{O} \dot{E} \dot{D}. \dot{C} \dot{E} \dot{I} \dot{I}$
 $\dot{\pm} \dot{n} \dot{A} \dot{\omega} \dot{O} \dot{A} \dot{O} \dot{I} \dot{S} \dot{A} \dot{-} \dot{n} \dot{I}. \ll \dot{D} \dot{\pm} \dot{o} \dot{S} \dot{A} \dot{I} \dot{D} \dot{o} \dot{A} \dot{I} \dot{E} \dot{I} \dot{3} \dot{4} \dot{D}. \dot{\pm} \dot{E} \dot{S} \dot{A} \dot{C} \dot{E} \dot{O} \dot{\pm} \dot{n} \dot{1} \dot{2} \dot{C}$
 $\text{(scalar)} \dot{-} \dot{I} \dot{o}. \dot{O} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{\gamma} \dot{\pm} \dot{\omega} \frac{1}{4} \ll \dot{o} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{\gamma} \dot{A} \dot{D} \dot{I} \dot{A} \dot{U} \dot{A} \dot{I} \dot{o} \dot{O} \dot{A} \dot{A} \dot{E} \dot{\omega} \dot{O}$
 $\dot{A} \dot{\omega} \dot{A} \dot{I} \dot{o}. \dot{O} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{\gamma} \dot{C} \dot{E} m \dot{-} \dot{\omega} \dot{O} \dot{A} \dot{A} \dot{E} \dot{\omega} \dot{O} \dot{I} \dot{I} \dot{o} g \dot{-} \dot{\omega} \dot{O}$
 $\dot{p} \dot{O} \dot{O} \dot{A} \dot{\gamma} \ll \frac{3}{4} \dot{\gamma} \dot{\pm} \dot{\omega} \frac{1}{4} \dot{O} \dot{i} \dot{=} \dot{A} \dot{A} \dot{I} \ll \dot{A} \dot{I} \dot{C} \dot{O} W = mg \dot{-} \dot{I} \dot{o}.$

$$\therefore m = \frac{W}{g}$$

$\dot{O} \dot{A} \dot{A} \dot{E} \dot{\omega} \dot{O} \dot{I} \dot{I} \dot{o} \dot{p} \frac{1}{4} \dot{O} \dot{3} \dot{4} \dot{U} \dot{O} \dot{1} \dot{4} \dot{o} \dot{A} \dot{I} \dot{U} \dot{A} \dot{I} \dot{A} \dot{3} \dot{4} \dot{I} \dot{o} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{\gamma} \dot{\pm} \dot{\omega} \frac{1}{4} \dot{O} \dot{O}$
 $\dot{A} \dot{I} \dot{U} \dot{A} \dot{I} \dot{U} \dot{E} \dot{A} \dot{D}. \dot{-} \dot{E} \dot{I} \dot{o} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{\gamma} \dot{C} \dot{E} \dot{\pm} \dot{U} \dot{A} \dot{O} \dot{3} \dot{4} \dot{O} \dot{O} \dot{A} \dot{I} \dot{E} \dot{I} \dot{3} \dot{4} \dot{\pm} \dot{n} \dot{1} \dot{2} \dot{I} \dot{o}.$

$\dot{O} \dot{I} \dot{E} \dot{O} \dot{A} \dot{O} \dot{1} \dot{4} \dot{p} \frac{1}{4} \dot{O} \dot{3} \dot{4} \dot{O} \dot{O} \dot{I} \dot{A} \dot{I} \dot{O} \dot{C} \dot{\gamma} \dot{\pm} \dot{\omega} \frac{1}{4} \dot{A} \dot{W} \dot{S} \dot{A} \dot{I} \dot{A} \dot{I} \dot{o}$
 $\dot{A} \dot{\omega} \dot{A} \dot{I} \dot{o} \text{ (kgf)} \ll \dot{U} \dot{A} \dot{O} \dot{3} \dot{4} \dot{\gamma} \dot{O} \dot{A} \dot{A} \dot{E} \dot{\omega} \dot{O} \dot{I} \dot{I} \dot{o} g \dot{A} \dot{D} \dot{1} \dot{4} \dot{I} \dot{A} \dot{E} \dot{I} \dot{E}^2 \text{ (m/s}^2 \text{)}$

$$m \times \frac{1}{2} \rho \pi r^2 v^2 = m \left(\frac{1}{2} \rho v^2 \right) \times \frac{1}{2} \rho \pi r^2 v^2$$

$$\frac{1}{2} \rho \pi r^2 v^2 = \frac{W}{g} \left(\frac{1}{2} \rho v^2 \right) \times \frac{1}{2} \rho \pi r^2 v^2$$

$$\frac{1}{2} \rho \pi r^2 v^2 = 9.81 \left(\frac{W}{g} \right) \left(\frac{1}{2} \rho v^2 \right) \times \frac{1}{2} \rho \pi r^2 v^2$$

$$\frac{1}{2} \rho \pi r^2 v^2 = \frac{W \times \text{கி.கி/வி}^2}{g (\text{மீ/வி}^2)} \times 9.81 \text{ஆகும்}$$

1.6 (4) Unit of force (Formula for unit of force)

$$1 \text{ } \frac{1}{2} \rho v^2 = (1 \text{ } \frac{1}{2} \rho) \times (1 \text{ } v^2)$$

$$= 1000 \times 100 \left(\frac{1}{2} \rho \right) \times v^2$$

$$= 10^5 \left(\frac{1}{2} \rho \right) \times v^2$$

$$= 10^5 \times \frac{1}{2} v^2$$

$$1 \text{ } \frac{1}{2} \rho v^2 = (1 \text{ } \frac{1}{2} \rho) \times (1 \text{ } v^2)$$

$$= 454 \left(\frac{1}{2} \rho \right) \times 30.5 \left(\frac{1}{2} \rho \right)$$

$$= 1384.7 \left(\frac{1}{2} \rho \right)$$

$$= 1384.7 \times \frac{1}{2} v^2$$

$$1 \text{ } \frac{1}{2} \rho v^2 = 1000 \left(\frac{1}{2} \rho \right) \times v^2$$

$$= 1000 \left(\frac{1}{2} \rho \right) \times \frac{1}{2} v^2$$

$$= 1000 \times g \times \frac{1}{2} v^2$$

$$= 1000 \times 9.81 \times \frac{1}{2} v^2$$

$$= 9.81 \times 10^5 \times \frac{1}{2} v^2$$

$$= 9.81 \times \frac{1}{2} v^2$$

$$1 \text{ } \frac{1}{2} \rho v^2 = 1 \text{ } \frac{1}{2} \rho v^2 \times \frac{1}{2} v^2$$

$$= 1 \times g \times \frac{1}{2} v^2$$

$$= 1 \times 32.2 \times \frac{1}{2} v^2$$

$$= 32.2 \times \frac{1}{2} v^2$$

$$= 32.2 \times 1384.7 \times \frac{1}{2} v^2$$

$$= 44587.34 \times \frac{1}{2} v^2$$

$$= 0.4457834 \times 10^5 \times \frac{1}{2} v^2$$

$$= 0.4457834 \times \frac{1}{2} v^2$$

1.7 Law of Dimensional Homogeneity

Dimensional homogeneity states that the dimensions of the terms in an equation must be the same. For example, in the equation $\frac{1}{2} \rho v^2 = \frac{W}{g} \left(\frac{1}{2} \rho v^2 \right) \times \frac{1}{2} \rho v^2$, the dimensions of $\frac{1}{2} \rho v^2$ on the left must equal the dimensions of the right-hand side. This is satisfied because the dimensions of $\frac{W}{g}$ are $\frac{MLT^{-2}}{LT^{-2}} = M$, and the dimensions of $\frac{1}{2} \rho v^2$ are $\frac{ML^{-3} \times L^2 T^{-2}}{1} = ML^{-1} T^{-2}$. Therefore, the dimensions of the right-hand side are $M \times ML^{-1} T^{-2} = M^2 L^{-1} T^{-2}$, which is not equal to the dimensions of the left-hand side. This indicates that the equation is not dimensionally homogeneous.

1.7 (1) Unit of force

Unit of force = MLT^{-2} (Simple)

pendulam) « " Äx S_zÄð^{3/4}ü_jÉ °ÁýÄ_jðÉý « " Äð " Äð | ÄÈ
 SÄñ ÈÄÖôÄ^{3/4}_iì |_jüÇ×ö.
 °Äý « " Äx S_zÄð, Äñí_j Ç °_iÄüÜ þÖì_jÈÐ ±Éì
 |_jüSÄ_jÄ_jÄý « Ð
 (i) °øíñÉý Ç È(M),
 (ii) ÄüÉý Ç Ö(L),
 (iii) ®÷òð Öí_jö_j -_jÄÄü_jÈð | Ä_jÜðÐ « " ÄÄ^{3/4}_iì |_jüÇ×ö.

Q ±ýÄÐ ²/₄Ä_j | ³/₄Ö Ä_j°Ä_j Ä_j Ì ÈÄ_j | ÄýÉ_jø « ³/₄ý Ä_jÄ_j ¹/₂í_j Ç
 Ä_jÄ_jÜì_j ò Ä_jöðÄ_jí [Q]=[M^xL^yT^z]±Éì |_jñ_j Ä_j x,y,z -_jÄÄüÉý
 Ä^{3/4}òð_j Ç_j ¹/₂í_j ¹/₄ ÖÈðð,
 ±ÉSÄ þí_j « " Äx S_zÄð = k (Ç È)^x(Ç Ö)^y(Öí_jö_j)^z -_j ò, k,x,y,z
 ±ýÄÈ Ä_jÈÄ_jü.

$$\begin{aligned} \ll \frac{3}{4} \text{ÄÐ } T &= KM^x L^y (LT^{-2})^z \\ &= KM^x L^{y+z} T^{-2z} - \text{ì } \text{ö} \end{aligned}$$

þÖðÈÖð - üÇ_j ò³/₄ Ä_j°Ä_j Ç_jý ÄÈð | ÄÖì_j ±ñ_j Ç_j °ÄðÄ_j òÐSÄ_jÄ_jÄý
 $x = 0; y + z = 0; 2z = -1;$

$$\text{அல்லது } x = 0; y = -z = \frac{1}{2} \text{ ஆகும்}$$

$$\text{எனவே } T = K\sqrt{1/g} \text{ ஆகும்}$$

ký Ä^{3/4}ö_j ò Ä_jÄ_j ¹/₂í_j Ç_jý Ö_j ÈÄð_j ¹/₂ ÖÈÄ_j ³/₄í_j Ä_jø « ³/₄ý Ä^{3/4}ö_j Ä_j
 S_j°_j ³/₄ È Ö_j ÈÄð_j ¹/₂SÄñ_j í_j ò. « üÄ_jÜ_j ¹/₂í_j ¹/₄Äð_j ³/₄Ä^{3/4}òð_j 2f -_j ò.
 ±ÉSÄ_j T = 2f√1/g

1-7 (2) þÄüÄÄø Ä_j°Ä_j Ü_jì_j Ç_j ¹/₄SÄÖüÇ_j | ³/₄ ¹/₄Ä_j Ä_j °Ä_jÄ_j÷ð³/₄ø

þÄüÄÄø Ä_j°Ä_j Ç_j | ³/₄ ¹/₄÷ðÄ_j òÐð_j Ö_j °ÁýÄ_jð_j ¹/₄ð ÄÈðÄÄ_j òSÄ_jÐ
 (Derived) °ÁýÄ_jðÉý þÖ òÈí_j Ç_jÖð Ä_jÄ_j ¹/₂í_j ü °ÄÄ_j þÖì_j SÄñ_j í_j ò.
 þÐSÄ Ä_jÄ_j ¹/₂í_j µ_jÄø Ç_jÄ^{3/4} ±Éì ÜÈðÄ_j ò. « ³/₄ÄÐ ¹/₂í_j Äø Ö_j ÈÄð
 þÄüÄÄø Ä_j°Ä_j Ç_jý | ³/₄ ¹/₄Ä_j Ä_j Ä_jÇ_jÖÄ_j òÐð_j °ÁýÄ_jí_j ü ±øÄ_jÄ_j ³/₄ « ÇÄð_j
 Ö_j È Ü_jì_j ò | Ä_jÖðÐð. þð³/₄ðÐÄð_j ³/₄Ä_j |_jñ_j Ä_j°Ä_j Ç_jý | ³/₄ ¹/₄÷ð
 °ÁýÄ_jí_j ü Ä_jÄ_j ¹/₂í_j Ç_jý òÐüÇÉÄ_j « øÄÐ ÖÄñ Äð_j üÇÉÄ_j ±É
 « ÈÄÄ_jð ±í òÐì_j ò¹/₄_j R = $\frac{U^2 \sin 2r}{g_0}$ ±ýÈ °ÁýÄ_jð_j ¹/₄ ±í òÐì_j |_jüÇ×ö.

°ÁýÄ_jðÉü_jÉ Ä_jÄ_j ¹/₂í_j Ç_j þÖðÈí_j Ç_jÖð ±ø³/₄×ö. « øSÄ_jÐ

$$\begin{aligned} [L] &= \left[\frac{L}{T} \right]^2 \cdot \frac{L^0}{[L/T^2]} \\ &= \left[\frac{L^2 T^2}{T^2 L} \right] \\ &= [L] \end{aligned}$$

Ä_jÄ_j ¹/₂í_j ü òÐüÇÉ. -³/₄Ä_jø R = $\frac{U^2 \sin 2r}{g_0}$ ±ýÈ ÇÄ^{3/4}°Ä_jÉÐ.

1.7(3) Ö_j þÄüÄÄø Ä_j°Ä_j þÖ « ÇÄð_j Ö_j È_j Ç_jý « Ä_j Ü_jì_j

$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$. « $\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$. $\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$. $\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$. $\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$.

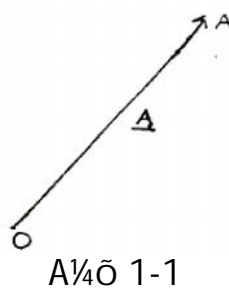
$\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$.

$\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$.

- (i) $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$.
- (ii) $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$.
- (iii) $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$.
- (iv) $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$.

1.8 (1) $\vec{v} = \frac{d\vec{r}}{dt}$

$\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$.



$\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$. « $\vec{v} = \frac{d\vec{r}}{dt}$.

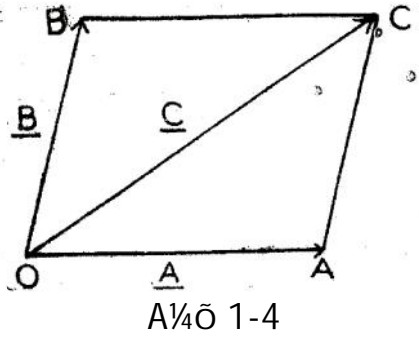
1.9 Addition or Resultant of Vectors

Let \vec{A} and \vec{B} be two vectors. Their resultant \vec{R} is given by $\vec{R} = \vec{A} + \vec{B}$. This is represented by the triangle rule where \vec{R} is the third side of a triangle formed by \vec{A} and \vec{B} .

Let \vec{A} and \vec{B} be two vectors. Their resultant \vec{R} is given by $\vec{R} = \vec{A} - \vec{B}$. This is represented by the triangle rule where \vec{R} is the third side of a triangle formed by \vec{A} and $-\vec{B}$.

1.9 (1) Parallelogram Law

The resultant of two vectors \vec{A} and \vec{B} is found by the parallelogram law. A parallelogram is completed by drawing lines parallel to \vec{A} and \vec{B} . The diagonal from the origin is the resultant \vec{C} .



Let \vec{A} and \vec{B} be two vectors. Their resultant \vec{C} is found by the parallelogram law. The resultant \vec{C} is the diagonal of the parallelogram formed by \vec{A} and \vec{B} .

$\vec{OA} + \vec{OB} = \vec{OC}$

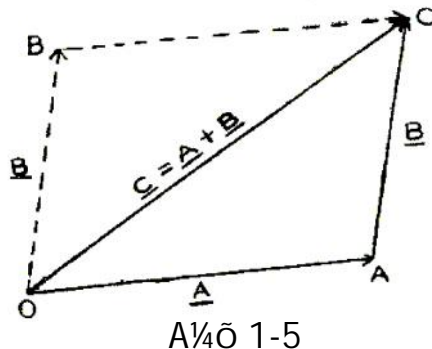
The order of addition does not matter. $\vec{A} + \vec{B} = \vec{B} + \vec{A}$. This is known as the commutative property of vector addition.

Vector addition is commutative: $\vec{A} + \vec{B} = \vec{B} + \vec{A}$.

1-9 (2) Triangle Law

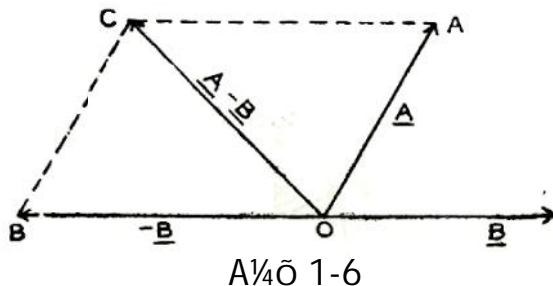
The triangle rule states that if two vectors \vec{A} and \vec{B} are placed end-to-end, their resultant \vec{C} is the third side of the triangle. $\vec{A} + \vec{B} = \vec{C}$.

« ÊôðûÇç, A ý ÑÉôðûÇç (tip) « " ÁÔÁ; Úô ±Î òÐô, Aý « ÊôðûÇç, Bý ÑÉôðûÇç - ÇÄü" Êî §÷òÐô - ñ ¼j| ò §ç÷§ç; ðí ò Ðñ Í , A, B - ÇÄ ¾ç" °Äç Ççý ÛÍ ¾ç" Äì Ì Êç Ì ò. Á¼ô 1.5ø OA, AC ±ýÄÉ A, B ±ýÈ þÕ ¾ç" °Äç " Çì Ì Êç Ì Á;Äý, OC « ÄÜËý | ¾ç" Ì ÄÄý ¾ç" °ÄçÄì ò.



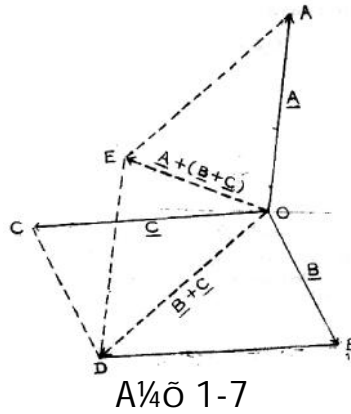
þ" ½, Ä Ä¾ç" °ÄÉ,
 $OA + OB = OC$
 - É;ø $OB = AC$ (¾ç" ¼ÄüÈ ¾ç" °Äç" Ä þ" ½Ä; , þ¼ô | ÄÄ÷îç | °öÄÄ; ò.)
 ±É §Ä, ΔOAC ø
 $OA + AC = OC$
 « ¾ç" ÄÐ $A + B = C$ - Ì ò.
 §ÄÓô, " « Ê-ÑÉç" « " Áôðì Ì (Tip-to-tail fashion) ²üÄ ΔOBC ,
 $OB + BC = OC$ - Ì ò.
 « ¾ç" ÄÐ $B + A = C$ - Ì ò
 $\therefore A + B = C = B + A$ ±ýË; Ì ò.
 ±É §Ä, þí Ì ò "¾ç" °Äç" Ûð¼ø" Ä;ÄüÜ « " Áôðì Ì þ" °óÐûÇÐ.

1-9 (3) - Õ ¾ç" °Äç" Ä, Äü; È; Õ ¾ç" °Äç" ÄÖóÐ, Äç¾ç" ø
A, B ±ýÈ ¾ç" °Äç" Ççø, A ÄÄÖóÐ, B Äì, B ±ýÈ ¾ç" °Äç" Ä ¾ç" °Äç" ÄüËÄ" ÄÄ×ò.



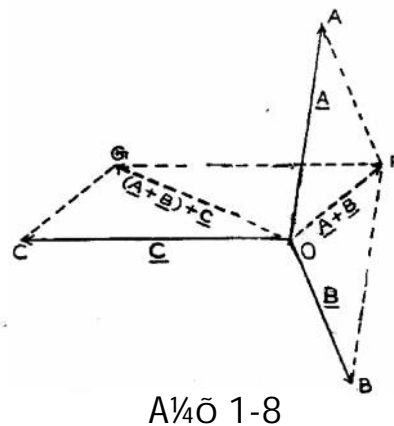
Á¼ô 1-6ø O ±ýÈ ðûÇç (tip) OA, OB ±ýÄÉ A-B - ÇÄ ¾ç" °Äç" " Çì Ì Êç ÇçËÉ. OA, OB - ÇÄüËý | ¾ç" Ì ÄÄ" È, þ" ½, Ä Ä¾ç" °ÄÉ, O ÄÄÉÄ Ä" Äó¾ç" ò, OC ±ýÈ ä" ÄÄð¼ø « ÊçÄì ò.
 « ¾ç" ÄÐ $OA + OB = OC$
 $A + (-B) = A - B$ - Ì ò.

1.9 (4) $\vec{OA} + \vec{OB} + \vec{OC} = \vec{OD}$ where D is the tip of the resultant of $\vec{OA}, \vec{OB}, \vec{OC}$ starting from O .
 The resultant \vec{OD} is equal to $\vec{OA} + \vec{OB} + \vec{OC}$.
 The resultant \vec{OD} is equal to $\vec{OA} + (\vec{OB} + \vec{OC})$.
 The resultant \vec{OD} is equal to $(\vec{OA} + \vec{OB}) + \vec{OC}$.
 $\vec{OD} = \vec{OA} + \vec{OB} + \vec{OC} = \vec{OA} + (\vec{OB} + \vec{OC}) = (\vec{OA} + \vec{OB}) + \vec{OC}$



« $\vec{OA} + \vec{OB} + \vec{OC} = \vec{OD}$ where D is the tip of the resultant of $\vec{OA}, \vec{OB}, \vec{OC}$ starting from O .
 $\vec{OD} = \vec{OA} + \vec{OB} + \vec{OC} = \vec{OA} + (\vec{OB} + \vec{OC}) = (\vec{OA} + \vec{OB}) + \vec{OC}$ »

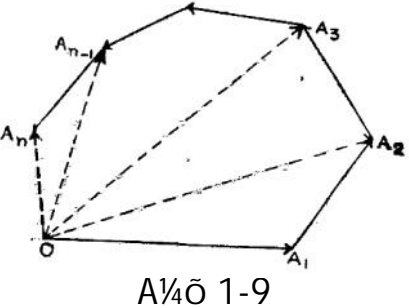
$\vec{OD} = \vec{OA} + \vec{OB} + \vec{OC} = \vec{OA} + (\vec{OB} + \vec{OC}) = (\vec{OA} + \vec{OB}) + \vec{OC}$
 The resultant \vec{OD} is equal to $\vec{OA} + (\vec{OB} + \vec{OC})$.
 The resultant \vec{OD} is equal to $(\vec{OA} + \vec{OB}) + \vec{OC}$.



« $(\vec{OA} + \vec{OB}) + \vec{OC} = \vec{OA} + (\vec{OB} + \vec{OC})$ » (Associative Law of Addition)
 $\vec{OA} + \vec{OB} + \vec{OC} = \vec{OA} + (\vec{OB} + \vec{OC}) = (\vec{OA} + \vec{OB}) + \vec{OC}$

$\frac{1}{2}, \frac{3}{4} \vec{A} \otimes \underline{A_1, A_2} \rightarrow \vec{A} \vec{A} \vec{E} \vec{Y} \quad | \frac{3}{4} | \vec{A} \vec{A} \vec{Y} \quad \underline{R_1} \text{ } \vec{n} \hat{I}, \ll \frac{3}{4} \hat{U} \frac{1}{4} \vec{y} \quad \underline{A_3} \text{ } \vec{3} \hat{I}$
 $\vec{S} \circ \div \frac{3}{4} \frac{1}{4}, \quad \vec{C} \cdot \frac{1}{4} \hat{I} \hat{I} \hat{O} \quad | \frac{3}{4} | \vec{A} \vec{A} \vec{Y} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \quad \underline{R_2} \quad \pm \vec{y} \vec{A} \vec{D}, \quad \underline{A_1, A_2, A_3} \rightarrow \vec{A} \vec{A} \vec{U} \vec{E} \vec{Y}$
 $\hat{U} \hat{I} \frac{3}{4} \vec{A} \ll \vec{E} \vec{A} \vec{C} \hat{I} \hat{O}. \quad \ll \hat{I} \text{ } \vec{1} \text{ } \vec{E} \vec{S} \vec{A}, \quad \ll \hat{I} \text{ } \frac{3}{4} \hat{I} \text{ } \hat{O} \vec{D} \quad \vec{A} \vec{O} \hat{O} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \cdot \vec{A} \ll \frac{3}{4} \hat{U} \hat{I}$
 $\vec{O} \vec{y} \vec{A} \hat{O} \frac{3}{4} \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \cdot \vec{C} \vec{y} \quad \hat{U} \hat{I} \frac{3}{4} \vec{A} \vec{A} \cdot \vec{A} \vec{A} \vec{U} \hat{I} \hat{I} \hat{O} \quad | \frac{3}{4} | \vec{A} \vec{A} \vec{Y} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \cdot \vec{O} \vec{A} \vec{C}$
 $\vec{p} \vec{U} \frac{3}{4} \vec{A} \vec{I} \pm \vec{O} \vec{A} \vec{I} \hat{O} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \cdot \vec{C} \vec{y} \quad \hat{U} \hat{I} \frac{3}{4} \vec{A} \vec{A} \cdot \vec{O} \vec{A} \vec{C} \cdot \vec{C} \times \quad | \frac{3}{4} | \vec{A} \vec{A} \vec{Y} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \cdot \hat{I}$
 (Final Resultant Vector) $\vec{O} \vec{A} \vec{A} \vec{I} \vec{S}, \vec{p} \vec{O} \hat{I} \hat{I} \vec{A} \vec{I} \vec{U} \vec{A} \vec{I} \vec{U} \vec{E} \vec{A} \vec{A} \vec{I} \vec{S}, \vec{A} \vec{I} \vec{S}, \vec{A} \vec{I} \vec{O}.$

$\ll \vec{u} \vec{A} \vec{I} \vec{S} \vec{E} \quad \text{"NÉC-« E"} \quad \ll \vec{A} \vec{O} \hat{I} \hat{I} \quad \vec{2} \vec{u} \vec{E} \vec{A} \vec{I} \vec{U} \vec{O}, \quad \underline{A_1, A_2, \dots, A_i, \dots, A_n}$
 $\rightarrow \vec{A} \vec{A} \vec{U} \vec{E} \vec{Y} \quad \hat{U} \hat{I} \frac{3}{4} \vec{A} \vec{A} \cdot \vec{A} \vec{A} \vec{U} \hat{I} \vec{S}, \quad \vec{O} \vec{E} \hat{O} \hat{O}. \quad \vec{p} \hat{I} \hat{I} \quad \vec{O} \pm \vec{y} \vec{E} \vec{D} \vec{A} \hat{I} \vec{S}, \quad \hat{O} \hat{O} \vec{U} \vec{C} \vec{A} \vec{C} \otimes \underline{A_1}$
 $\pm \vec{y} \vec{E} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \cdot \vec{y} \ll \vec{E} \hat{O} \hat{O} \vec{U} \vec{C} \vec{C} \ll \vec{A} \vec{O} \vec{A} \vec{I} \vec{U} \pm \hat{I} \text{ } \hat{O} \vec{D} \quad \underline{A_2} \vec{y} \ll \vec{E} \hat{O} \hat{O} \vec{U} \vec{C} \vec{C} \underline{A_1} \vec{y} \quad \vec{N} \vec{E} \vec{C} \vec{A} \vec{C}$
 $| \vec{A} \vec{I} \vec{O} \hat{O} \vec{D} \vec{A} \vec{I} \vec{U} \vec{O}, \quad \underline{A_3} \vec{y} \ll \vec{E} \hat{O} \hat{O} \vec{U} \vec{C} \vec{C} \underline{A_2} \vec{y} \quad \vec{N} \vec{E} \vec{C} \hat{O} \hat{O} \vec{U} \vec{C} \vec{C} \vec{A} \vec{C} \otimes | \vec{A} \vec{I} \vec{O} \hat{O} \vec{D} \vec{A} \vec{I} \vec{U} \vec{O} \pm \hat{I} \text{ } \hat{O} \vec{D}$
 $\vec{p} \vec{U} \frac{3}{4} \vec{A} \vec{I} \vec{S}, \quad \underline{A_n} \vec{y} \ll \vec{E}, \quad \underline{A_{n-1}} \vec{y} \quad \vec{N} \vec{E} \vec{C} \vec{A} \vec{C} \otimes | \vec{A} \vec{I} \vec{O} \hat{O} \vec{D} \vec{A} \vec{I} \vec{U} \vec{O} \ll \vec{A} \vec{O} \vec{D}, \quad \underline{A_1} \vec{y} \ll \vec{E} \hat{O} \hat{O} \vec{U} \vec{C} \vec{C}$
 $\vec{O} \vec{S} \quad \underline{A_n} \vec{y} \quad \vec{N} \vec{E} \vec{C} \hat{O} \hat{O} \vec{U} \vec{C} \vec{C} \vec{O} \frac{1}{4} \vec{y} \quad \vec{S} \circ \div \hat{O} \vec{D} \quad \vec{n} \frac{1}{4} | \hat{I} \hat{I} \hat{O} \quad \vec{S} \vec{I} \div \vec{S} \vec{I} \hat{I}, \quad \pm \vec{O} \vec{A} \vec{I} \hat{O} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \cdot \vec{C} \vec{y}$
 $\hat{U} \hat{I} \frac{3}{4} \vec{A} \vec{A} \cdot \vec{A} \vec{A} \vec{U} \hat{I} \hat{I} \hat{O}. \quad \vec{A} \frac{1}{4} \hat{O} \quad 1-9 \vec{p} \hat{O}, \quad \text{"O} \hat{I} \vec{S} \vec{I} \frac{1}{2} \vec{A} \frac{3}{4} \vec{C} \ll \vec{O} \vec{A} \vec{D} \quad \text{"NÉC-« E"} \ll \vec{A} \vec{O} \hat{O} \vec{O} \vec{E} \hat{O} \vec{A} \vec{E},$



$$\underline{OA_1} + \underline{A_1 A_2} = \underline{OA_2}$$

$$\underline{OA_2} + \underline{A_2 A_3} = \underline{OA_3}$$

$$\underline{OA_{n-1}} + \underline{A_{n-1} A_n} = \underline{OA_n}$$

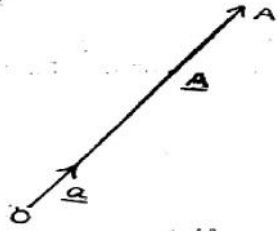
$\vec{p} \cdot \vec{A} \cdot \vec{C} \hat{I} \hat{U} \vec{O} \vec{E} \frac{1}{4},$
 $\underline{OA_1} + \underline{A_1 A_2} + \underline{A_2 A_3} + \dots + \underline{A_{i-1} A_i} + \dots + \underline{A_{n-2} A_{n-1}} = \underline{OA_n} \quad \vec{n} \hat{I} \hat{O}. \quad \pm \vec{E} \vec{S} \vec{A}, \quad | \frac{3}{4} | \vec{A} \vec{A} \vec{Y} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C}$
 $\underline{OA_n} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \cdot \vec{C} \vec{y} \quad \hat{U} \hat{I} \frac{3}{4} \vec{A} \vec{A} \cdot \vec{A} \vec{A} \vec{U} \hat{I} \hat{I} \hat{O} \vec{E} \vec{D}.$

1.10 $\vec{\mu} \vec{A} \vec{A} \hat{I} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C}$ (Unit Vector)

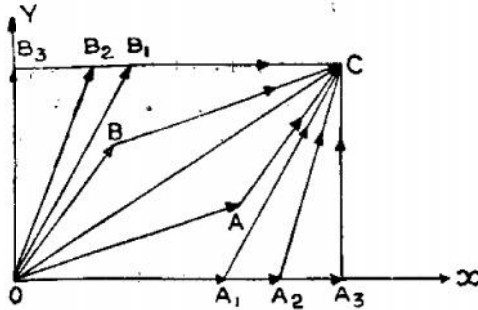
$\pm \vec{n} \quad \vec{A} \frac{3}{4} \hat{O} \hat{O} \vec{y} \vec{U} \vec{U} \vec{C} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \quad \vec{\mu} \vec{A} \vec{A} \hat{I} \quad \hat{O} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \quad | \hat{I} \hat{I} \hat{O}.$

1.10 (1) $\vec{\mu} \vec{A} \vec{A} \hat{I} \quad \hat{O} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \cdot \vec{A} \hat{O} \vec{A} \vec{A} \vec{y} \vec{A} \hat{I} \quad \hat{O} \vec{D} \frac{3}{4} \hat{O}$

$\vec{A} \frac{1}{4} \hat{O} \quad 1-10 \hat{O} \ll \vec{O} \hat{O} \hat{I} \vec{S} \vec{I} \hat{I} \quad \underline{OA} \pm \vec{y} \vec{A} \vec{D}, \quad \underline{A} \pm \vec{y} \vec{E} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \cdot \vec{A} \hat{I} \hat{I} \hat{E} \vec{C} \hat{I} \vec{E} \vec{D}. \quad \ll \hat{O}$
 $\frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \cdot \vec{S} \vec{A} \vec{S} \vec{A} \quad \vec{\mu} \vec{A} \vec{A} \hat{I} \quad \pm \vec{n} \quad \vec{A} \frac{3}{4} \hat{O} \hat{O} \vec{U} \vec{C} \vec{C}, \quad \vec{a} \pm \vec{y} \vec{U} \vec{O} \quad \vec{\mu} \vec{A} \vec{A} \hat{I} \quad \hat{O} \quad \frac{3}{4} \vec{C} \cdot \vec{O} \vec{A} \vec{C} \cdot \vec{A} \pm \hat{I} \hat{I} \vec{S} \times \hat{O}.$



1-12. $\vec{OC} = \vec{OA}_1 + \vec{OA}_2 + \vec{OA}_3$, $\vec{OC} = \vec{OB}_1 + \vec{OB}_2 + \vec{OB}_3$

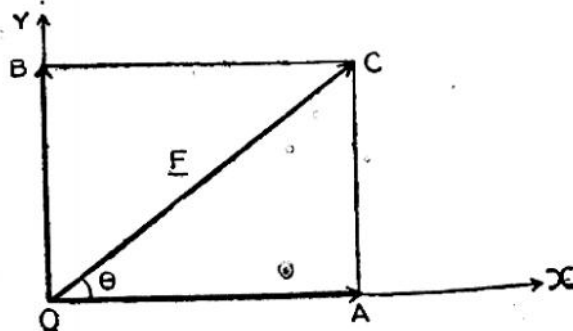


1-12

1-12. $\vec{OC} = \vec{OA}_1 + \vec{OA}_2 + \vec{OA}_3$, $\vec{OC} = \vec{OB}_1 + \vec{OB}_2 + \vec{OB}_3$

1-12 (1) $\vec{OC} = \vec{OA}_1 + \vec{OA}_2 + \vec{OA}_3$

1-13. $\vec{OC} = \vec{OA} \cos \alpha$, $\vec{OC} = \vec{OB} \sin \alpha$



1-13

1-13. $\vec{OC} = \vec{OA} \cos \alpha$, $\vec{OC} = \vec{OB} \sin \alpha$

1-13. $\vec{OC} = \vec{OA} \cos \alpha$

$$OA = OC \cos \alpha$$

$$\therefore F_x = F \cos \alpha$$

$$OB = OC \sin \alpha$$

$$\therefore F_y = F \sin \alpha$$

±ÉŞĂ $F \pm y \hat{e}$ $\frac{3}{4} \hat{c}$ „ $\pm y \hat{e}$ $\frac{3}{4} \hat{c}$ „ $\frac{1}{2} \hat{c}$ « „ $\hat{A} \hat{I} \hat{o}$ $\frac{3}{4} \hat{c}$ „ $\hat{A} \hat{O} \hat{o}$,
 « $\hat{o} \frac{3}{4} \hat{c}$ „ $\hat{o} \hat{I} \hat{o}$ $\frac{3}{4} \hat{c}$ „ $\hat{o} \hat{A} \hat{I} \hat{o}$ $\frac{3}{4} \hat{c}$ „ $\hat{A} \hat{O} \hat{o}$, \pm $\hat{p} \hat{y}$ \hat{o} „ $\hat{I} \hat{U} \hat{U}$ „ \hat{u} \hat{O} „ $\hat{E} \hat{S} \hat{A}$ $F \cos$ „
 $F \sin$ „ $\pm y \hat{e}$ $\hat{I} \hat{o}$.

$O_x O_y$ $\frac{3}{4} \hat{c}$ „ \hat{o} „ \hat{C} i, j $\pm y \hat{e}$ $\mu \hat{A} \hat{I} \hat{o}$ $\frac{3}{4} \hat{c}$ „ $\hat{A} \hat{c}$ „ \hat{u} \hat{A} „ $\hat{A} \hat{A} \hat{U} \hat{i} \hat{l}$ „ $\hat{A} \hat{y} \hat{e}$ $\hat{I} \hat{o}$.

$$\underline{OC} = \underline{OA} + \underline{AC}$$

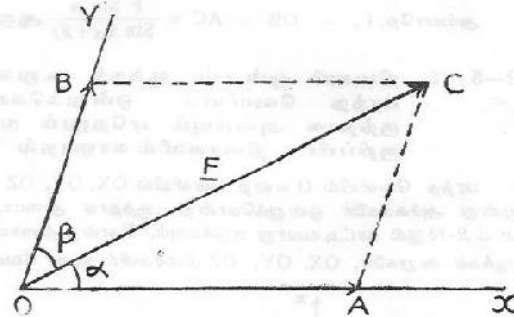
$$= \underline{OA} + \underline{OB}$$

$$\underline{F} = \underline{F_x} + \underline{F_y}$$

$$= F_x \hat{i} + F_y \hat{j} = F \cos \alpha \hat{i} + F \sin \alpha \hat{j} \pm y \hat{e} \hat{I} \hat{o}.$$

1.12 (2) $\frac{3}{4} \hat{c}$ „ $\hat{A} \hat{c}$ „ $\hat{y} \hat{e} \hat{y}$ \hat{o} „ $\hat{I} \hat{U} \hat{U}$ „ \hat{C} $\frac{2}{3} \hat{U} \hat{o}$ $\hat{p} \hat{O}$ „ $\hat{I} \hat{E} \hat{O} \hat{A} \hat{O} \hat{o}$ $\frac{1}{4} \hat{c}$ „ $\hat{C} \hat{O}$ „
 $\hat{I} \hat{o}$ $\frac{3}{4} \hat{c}$

$\hat{A} \hat{I} \hat{o}$ 1-14 $\hat{p} \hat{o}$, OC $\pm y \hat{e}$ $\frac{3}{4} \hat{c}$ „ $\hat{I} \hat{o}$, F $\pm y \hat{e}$ $\frac{3}{4} \hat{c}$ „ $\hat{A} \hat{C} \hat{y}$ „ \hat{n} $\hat{A} \hat{I} \hat{o}$ „ $\hat{A} \hat{I} \hat{o}$ „ $\hat{I} \hat{E} \hat{O}$ „ $\hat{O} \hat{X}$, $\hat{O} \hat{Y} \pm y \hat{e}$ $\hat{p} \hat{O}$ $\frac{3}{4} \hat{c}$ „ $\hat{C} \hat{O}$, \underline{F} $\hat{p} \hat{y}$



$\hat{A} \hat{I} \hat{o}$ 1-14

\hat{o} „ $\hat{I} \hat{U} \hat{U}$ „ \hat{C} „ $\hat{I} \hat{o}$ $\frac{3}{4} \hat{c}$ „ $\hat{S} \hat{A} \hat{n}$ „ $\hat{I} \hat{o}$. $Ox, Oy \pm y \hat{e}$ „ \hat{A} „ \hat{A} „ \hat{O} „ $\hat{E} \hat{S} \hat{A}$ OC „ \hat{y} „ r, s
 $\pm y \hat{e}$ $\frac{3}{4} \hat{c}$ „ $\hat{I} \hat{o}$ „ $\hat{C} \hat{o}$ $\frac{3}{4} \hat{c}$ „ $\hat{I} \hat{o}$ „ $\hat{A} \hat{I} \hat{o}$ „ $\hat{I} \hat{U} \hat{U}$ „ $\hat{C} \hat{x} \hat{o}$. $\hat{C} \hat{A} \hat{I} \hat{o} \hat{o} \hat{D}$ Ox, Oy „ $\hat{U} \hat{i} \hat{l}$
 \hat{p} „ $\frac{1}{2} \hat{A} \hat{j}$ „ \hat{A} „ $\hat{A} \hat{O} \hat{o}$ „ $\frac{3}{4} \hat{c}$ „ $\hat{I} \hat{o}$ „ \hat{u} Oy, Ox „ $\frac{3}{4} \hat{c}$ „ $\hat{I} \hat{o}$ „ \hat{C} „ \hat{O} „ $\hat{E} \hat{S} \hat{A}$ B, A „ $\pm y \hat{e}$ $\hat{p} \hat{I} \hat{o}$ „ $\hat{C} \hat{O}$
 $\hat{I} \hat{o}$ „ $\hat{A} \hat{O} \hat{o} \hat{A} \hat{I} \hat{o}$.

\hat{p} „ $\frac{1}{2} \hat{A}$ „ $\hat{A} \hat{O} \hat{o} \hat{A} \hat{E}$, \underline{OA} , \underline{OB} „ \hat{A} „ \hat{A} „ Ox, Oy „ $\frac{3}{4} \hat{c}$ „ $\hat{C} \hat{O}$ „ $\underline{F} \hat{y}$
 \hat{o} „ $\hat{I} \hat{U} \hat{U}$ „ $\hat{C} \hat{I} \hat{o}$ „ « $\hat{A} \hat{U} \hat{E} \hat{y}$ „ \hat{n} „ $\hat{A} \hat{I} \hat{o} \hat{o}$ „ \hat{C} „ F_x, F_y „ $\pm y \hat{e}$ „ $\hat{U} \hat{i} \hat{l}$ „ $\hat{E} \hat{O}$ „ $\hat{x} \hat{o}$.

$\hat{A} \hat{I} \hat{o}$ 1-14

$$\angle OAC = 180 - (r + s) \hat{o}$$

$$\angle OCA = s \hat{o}$$

±ÉŞĂ ΔOAC $\hat{p} \hat{o}$

$$\frac{OA}{\sin OCA} = \frac{AC}{\sin AOC} = \frac{OC}{\sin OAC}$$

$$\frac{OA}{\sin s} = \frac{AC}{\sin r} = \frac{OC}{\sin(180 - r + s)}$$

$$\frac{OA}{\sin s} = \frac{AC}{\sin r} = \frac{OC}{\sin(r + s)}$$

±ÉŞĂ

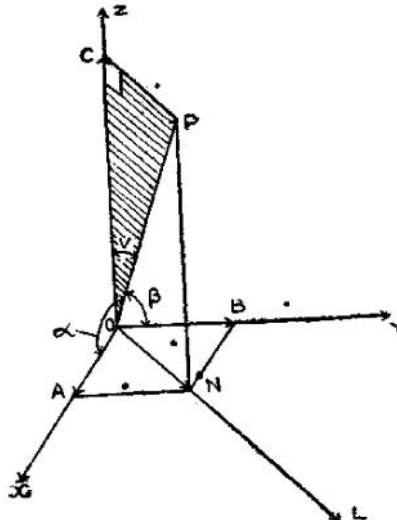
$$OA = \frac{OC \cdot \sin s}{\sin(r + s)}$$

$$\ll \hat{O} \hat{A} \hat{D} F_x = OA = \frac{F \sin s}{\sin(r + s)} \hat{o}.$$

$$F_y = OB = AC = \frac{F \sin r}{\sin(r+s)}$$

1.12 (3) ...

...



A 1-15

« ... OP ... »

$$OP = OC + ON$$

« ... ON ... »

$$ON = OA + OB$$

$$\therefore OP = OA + OB + OC$$

« ... OA, OB, OC ... »

$$F = F_x + F_y + F_z$$

« ... F_x, F_y, F_z ... »

$\vec{F} = F_x \mathbf{i} + F_y \mathbf{j} + F_z \mathbf{k}$

F_x, F_y, F_z (Scalar Components)

$\vec{F} = F \cos r \mathbf{i} + F \cos s \mathbf{j} + F \cos x \mathbf{k}$

$F_x = F \cos r$

$F_y = F \cos s$

$F_z = F \cos x$

$\vec{F} = F_x \mathbf{i} + F_y \mathbf{j} + F_z \mathbf{k}$

$ON^2 = OA^2 + AN^2$

$OP^2 = OC^2 + CP^2$

$OC^2 = OA^2 + OB^2$

$OP^2 = OC^2 + CP^2$

$\therefore F^2 = F_x^2 + F_y^2 + F_z^2$

$\cos^2 r + \cos^2 s + \cos^2 x = 1$

$\vec{F} = F_x \mathbf{i} + F_y \mathbf{j} + F_z \mathbf{k}$

$\frac{\cos r}{F_x} = \frac{\cos s}{F_y} = \frac{\cos x}{F_z} = \frac{1}{F}$

$\vec{F} = F_x \mathbf{i} + F_y \mathbf{j} + F_z \mathbf{k}$

$F = F_x \left(\frac{F_x}{F} \right) + F_y \left(\frac{F_y}{F} \right) + F_z \left(\frac{F_z}{F} \right)$

$= F_x \cos r + F_y \cos s + F_z \cos x$

$F = F_x \cdot 1 + F_y \cdot m + F_z \cdot n$

$\vec{F}_x = i F_x, \vec{F}_y = j F_y, \vec{F}_z = k F_z$

$\vec{F} = F_x \mathbf{i} + F_y \mathbf{j} + F_z \mathbf{k}$

$$\underline{F} = F_x \underline{i} + F_y \underline{j} + F_z \underline{k} \rightarrow \text{ò.}$$

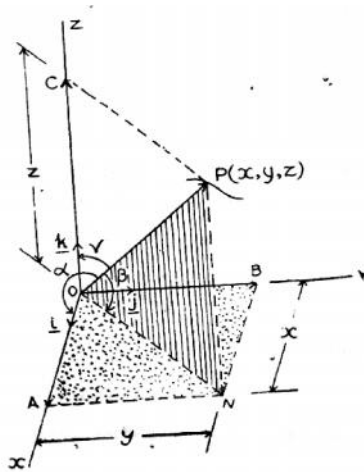
$$\begin{aligned} \text{ŞAÖö } \underline{F} &= F \left(\frac{F_x}{F} \right) \underline{i} + F \left(\frac{F_y}{F} \right) \underline{j} + F \left(\frac{F_z}{F} \right) \underline{k} \\ &= F \cos r \underline{i} + F \cos s \underline{j} + F \cos x \underline{k} \rightarrow \text{ò.} \end{aligned}$$

« øÄÐ, $\underline{F} = F: f \pm y \text{Üö} \text{ Ì Èñ, } \underline{A}_i \text{ö.}$

þí Ì $f \pm y \text{ÄÐ, } \underline{F} \text{ ¼ö°Äö; °ÄüÄÌ ö ¼ö° òì Ì Þ'' ½Ä_i, } \ll \text{'' ÄÖö } \mu \text{ÄÄÌ ö}$
 $\text{¼ö° °Ä_i} \text{ö.}$

1-13 Äö¼ | ÄÇÄö ò òüÇÄ_y çö Äö ¼ö° °Äö Ä_i, Ì ¼ö

O $\pm y \text{È òüÇö'' Äö ÐÄ_i, } \text{òüÇöÄ_i} \text{ Ì | Ì ñ Î « ¼öø OX, OY, OZ } \pm y \text{È}$
 $\text{ý Üì |, } \text{ý Üì | } \text{óì Ì ò¼_i, } \text{üÇ } \underline{a} \text{ý Ü « ÌÍ, } \text{Ç } \pm \text{Ì Ì, } \times \text{ö. Äö¼ | ÄÇÄö}$
 $\text{P } \pm y \text{ÄÐ } \text{ö òüÇöÄ_i, } \text{ö OP } \pm y \text{È « öòì } \text{Ş_i} \text{Ä, } \text{P } \pm y \text{È òüÇöÄ_y}$
 $\text{çö'' Äö¼ö° °Äö'' Ä (Position vector) Ä'' ÄÄÜì Ì ö. O, P Üì Ì Þ'' ¼ÄÄ'' ÄÖö}$
 $\text{¼_i'' Ä } \times \text{r } \pm y \text{È } \text{ö, P } \text{ý çö'' Äö¼ö° °Äö, } \text{Ä¼ö 1-16ö, } \text{öÈÄÄ_i Ü,}$
 $\text{OP} = \underline{r} \text{ö.}$



Ä¼ö 1-16

OP $\pm y \text{È } \text{Ş}_i \text{Ş_j} \text{Ä } X, Y, Z \ll \text{ÍÍ, Ü } \text{¼ý} \ll \text{'' Äì Ì ö } \text{Ş_i} \text{½í, } \text{Ç,}$
 $\text{ÄÈì öŞÄ_iö, } \text{r, s, x } \pm \text{Èì |, } \text{üÇ } \times \text{ö. } X, Y, Z \ll \text{ÍÍ Çö, OP } \pm y \text{È}$
 $\text{Ş}_i \text{Ş_j} \text{öÈý } \text{¼ÇÄüì °ç, } \text{ŞÇ (Projections) P } \pm y \text{È } \text{öüÇöÄ_y} \ll \text{ÍÍ}$
 $\text{¼_i'' Ä } \times \text{Çì} \text{ö. (Coordinates). OA, OB, OC } \text{öÄü'' È OPý } \text{¼Ç}$
 $\text{Äüì °ç, } \text{Ç_i} \text{ì |, } \text{üÇ } \times \text{ö. « öì Ä_i} \text{øÐ, OA=x, OB=y, OC=z } \text{ö.}$

ŞAÖö, OAP $\pm y \text{È } \text{óì } \text{Ş_i} \text{½ Öì } \text{Ş_j} \text{½ ö¼öø,$

$$\frac{OA}{OP} = \cos r \ll \text{¼_i} \text{ÄÐ, } OA = OP \cos s \ll \text{øÄÐ } x = r \cos x \pm y \text{È } \text{ö.}$$

« üÄ_i ŞÈ, $y = r \cos s, z = r \cos x \rightarrow \text{ö.}$

OX, OY, OZ $\pm y \text{È} \ll \text{ÍÍ Çö Ö'' ÈŞÄ (i, j, k) } \pm y \text{È } \mu \text{ÄÄÌ ö ¼ö° °Äö, } \text{Ç}$
 $\ll \text{'' Äì } \times \text{ö.}$

« öì Ä_i} øÐ, $OA = xi, OB = yj, OC = zk \pm y \text{È } \text{ö.}$

P $\pm y \text{È } \text{öüÇöÄ'' ÖöÐ, XOY } \text{¼Çö¼üì } \text{PN } \pm y \text{È } \text{óì Ì òÐì } \text{Ş_i} \text{Ä}$

\vec{y} È $\vec{A} \cdot \vec{A} \times \vec{o}$. N- \vec{O} óÐ OY, OX « \hat{i} , \hat{j} , \hat{k} $\vec{A} \cdot \vec{A} \vec{o}$
 $\vec{S}_i \hat{i} \vec{u} \vec{O} \vec{E} \vec{S} \vec{A} \vec{O} \vec{X}, \vec{O} \vec{Y} \ll \hat{i} \vec{I} \vec{C} \vec{A}, \vec{B} \pm \vec{y} \vec{E} \vec{p} \vec{1} \vec{I} \vec{C} \vec{O} \vec{A} \vec{D} \vec{I} \vec{o}$.
 $\vec{O} \vec{N} \vec{P} \vec{C} \pm \vec{y} \vec{E} \vec{I} \vec{o} \vec{D} \vec{o} \vec{3} \vec{4} \vec{C} \vec{o} \vec{3} \vec{4} \vec{C} \vec{o}$ (Vertical Plane) $\vec{p} \vec{1} \vec{I} \vec{C} \vec{O} \vec{A} \vec{E}$,
 $\vec{O} \vec{P} = \vec{O} \vec{N} + \vec{O} \vec{C} \vec{I} \vec{o}$.

$\vec{O} \vec{A} \vec{N} \vec{B} \pm \vec{y} \vec{E} \vec{C} \vec{o} \vec{1} \vec{4} \vec{o} \vec{3} \vec{4} \vec{C} \vec{o} \vec{3} \vec{4} \vec{C} \vec{o}$, $\vec{p} \vec{1} \vec{I} \vec{C} \vec{O} \vec{A} \vec{E}$,
 $\vec{O} \vec{N} = \vec{O} \vec{A} + \vec{O} \vec{B} \vec{I} \vec{o}$.

$\pm \vec{E} \vec{S} \vec{A}, \vec{O} \vec{P} = \vec{O} \vec{A} + \vec{O} \vec{B} + \vec{O} \vec{C}$
 $\ll \vec{O} \vec{A} \vec{D} \vec{r} = x\vec{i} + y\vec{j} + z\vec{k} \pm \vec{y} \vec{E} \vec{I} \vec{o}$.

$\vec{r} = x\vec{i} + y\vec{j} + z\vec{k} \pm \vec{y} \vec{E} \vec{O} \vec{u} \vec{C} \vec{O} \vec{A} \vec{y} \vec{z} \vec{C} \vec{o} \vec{3} \vec{4} \vec{C} \vec{o} \vec{O} \vec{A} \vec{C} \vec{o} \vec{A}$,
 $\vec{r} = x\vec{i} + y\vec{j} + z\vec{k} \pm \vec{y} \vec{A} \vec{D} \ll \vec{E} \vec{C} \vec{O} \vec{A} \vec{D} \vec{C} \vec{E} \vec{D}$.

$\vec{S} \vec{A} \vec{O} \vec{o}$,

$$\begin{aligned}
 \vec{r} &= x\vec{i} + y\vec{j} + z\vec{k} \\
 &= r \cos \gamma \vec{i} + r \cos \beta \vec{j} + r \cos \alpha \vec{k} \\
 &= r(\cos \gamma \vec{i} + \cos \beta \vec{j} + \cos \alpha \vec{k}) \\
 \therefore r &= r \sqrt{\cos^2 \gamma + \cos^2 \beta + \cos^2 \alpha}
 \end{aligned}$$

$\vec{p} \vec{1} \vec{I} \vec{C} \vec{O} \vec{A} \vec{E} \vec{r} = (\cos \gamma \vec{i} + \cos \beta \vec{j} + \cos \alpha \vec{k}) \pm \vec{y} \vec{A} \vec{D}$, $\vec{r} \pm \vec{y} \vec{E} \vec{3} \vec{4} \vec{C} \vec{o} \vec{O} \vec{A} \vec{C} \vec{o} \vec{A} \vec{I} \vec{o}$
 $\vec{3} \vec{4} \vec{C} \vec{o} \vec{O} \vec{A} \vec{C} \vec{o} \vec{S} \vec{A} \vec{S} \vec{A} \vec{m} \vec{A} \vec{A} \vec{I} \vec{o} \vec{3} \vec{4} \vec{C} \vec{o} \vec{O} \vec{A} \vec{C} \vec{o} \vec{A} \vec{I} \vec{o}$. $\vec{S} \vec{A} \vec{O} \vec{o}$, $\vec{A} \vec{C} \vec{O} \vec{S}_i \vec{S} \vec{A} \vec{S} \vec{A} \vec{I} \vec{o}$ (Pythagoras) $\vec{z} \vec{C} \vec{O} \vec{A} \vec{E}$,

$$\vec{O} \vec{P}^2 = \vec{O} \vec{A}^2 + \vec{O} \vec{B}^2 + \vec{O} \vec{C}^2 \ll \vec{3} \vec{4} \vec{I} \vec{A} \vec{D}, r^2 = x^2 + y^2 + z^2 \pm \vec{E} \vec{x} \vec{o},$$

$$|\vec{r}| = \cos^2 \gamma + \cos^2 \beta + \cos^2 \alpha = 1 \pm \vec{E} \vec{x} \vec{o} \vec{A} \vec{I} \vec{A} \vec{U} \vec{i} \vec{S}_i \vec{A} \vec{I} \vec{o}.$$

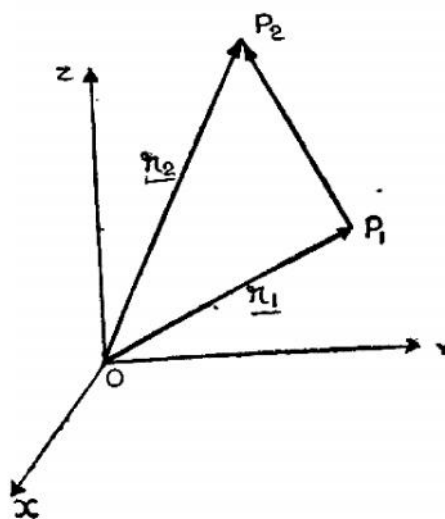
$\vec{A} \vec{A} \vec{o} \vec{3} \vec{4} \vec{I} \vec{A} \vec{C} \vec{O} \vec{A} \vec{C} \vec{o} \vec{P}_1(x_1, y_1, z_1), \vec{P}_2(x_2, y_2, z_2) \pm \vec{y} \vec{E} \vec{O} \vec{u} \vec{C} \vec{O} \vec{S}_i \vec{C} \vec{O} \vec{S} \vec{A} \vec{I} \vec{o}$,
 $\ll \vec{o} \vec{u} \vec{C} \vec{O} \vec{S}_i \vec{C} \vec{O} \vec{S} \vec{A} \vec{I} \vec{o} \vec{z} \vec{C} \vec{o} \vec{3} \vec{4} \vec{C} \vec{o} \vec{O} \vec{A} \vec{C} \vec{o} \vec{u} \vec{O} \vec{I} \vec{E} \vec{S} \vec{A}$,

$$\vec{r}_1 = \vec{O} \vec{P}_1 = x_1 \vec{i} + y_1 \vec{j} + z_1 \vec{k}$$

$$\vec{r}_2 = \vec{O} \vec{P}_2 = x_2 \vec{i} + y_2 \vec{j} + z_2 \vec{k}$$

$\pm \vec{y} \vec{E} \vec{I} \vec{o}$.

$\vec{A} \vec{1} \vec{7} \vec{o} \vec{1} \vec{1} \vec{7} \vec{o} \vec{S}_i \vec{D} \vec{E} \vec{O} \vec{u} \vec{C} \vec{O} \vec{A} \vec{E}$, "« $\vec{E} \vec{N} \vec{E} \vec{C}$ " « $\vec{A} \vec{o} \vec{D} \vec{O} \vec{I} \vec{E} \vec{A} \vec{C} \vec{o}$,



$\vec{A} \vec{1} \vec{7} \vec{o} \vec{1} \vec{1} \vec{7}$

$$\underline{OP}_1 = \underline{P}_1 \underline{P}_2 = \underline{OP}_2 \pm \underline{y} \hat{E}_i \hat{I} \hat{o}.$$

$$\ll \frac{3}{4} \hat{I} \hat{A} \hat{D}, \underline{P}_1 \underline{P}_2 = \underline{OP}_2 - \underline{OP}_1,$$

$$= \underline{r}_2 - \underline{r}_1$$

$$= (x_2 \hat{i} + y_2 \hat{j}) - (x_1 \hat{i} + y_1 \hat{j} + (z_2 - z_1) \hat{k}) \hat{I} \hat{o}.$$

ŞAÖö, $(x_2 - x_1), (y_2 - y_1), (z_2 - z_1) \pm \underline{y} \hat{A} \hat{I} \hat{o}$ $x, y, z \ll \hat{I} \hat{I} \hat{o} \hat{C} \hat{o} \hat{P}_1, \hat{P}_2 \pm \underline{y} \hat{E} \hat{I} \hat{o}$
 $\hat{S}_z \hat{S}_i \hat{D} \hat{E} \hat{y} \frac{3}{4} \hat{C} \hat{A} \hat{U} \hat{o} \hat{C} \hat{I} \hat{o}$. « $\hat{A} \hat{S} \hat{U} \hat{P}_1, \hat{P}_2 \pm \underline{y} \hat{E} \hat{I} \hat{o}$ $\hat{S}_z \hat{S}_i \hat{D} \hat{E} \hat{y} \frac{3}{4} \hat{C} \hat{o} \hat{A} \hat{C} \hat{o} \hat{P}_1$
 $\pm \hat{n} \hat{U}$ (Direction Ratios) $\pm \underline{y} \hat{U} \hat{o} \hat{U} \hat{E} \hat{o} \hat{A} \hat{I} \hat{o}$. $\hat{P}_1, \hat{P}_2 \hat{o} \hat{U} \hat{C} \hat{o} \hat{U} \hat{I} \hat{o} \hat{U} \hat{C}$
 $\frac{3}{4} \hat{I} \hat{A} \hat{D} \pm \hat{E} \hat{I} \hat{I} \hat{o} \hat{I} \hat{I} \hat{o} \hat{P}_1, \hat{P}_2 \pm \underline{y} \hat{E} \hat{I} \hat{o}$ $\hat{S}_z \hat{S}_i \hat{D} \hat{E} \hat{y} \frac{3}{4} \hat{C} \hat{o} \hat{I} \hat{o} \hat{U} \hat{C} \hat{o} \hat{P}_1$
 $\hat{O} \hat{E} \hat{S} \hat{A}$,

$$\cos r = \frac{x_2 - x_1}{d}, \cos s = \frac{y_2 - y_1}{d}, \cos x = \frac{z_2 - z_1}{d} \pm \underline{y} \hat{E}_i \hat{I} \hat{o}.$$

$$1.14 \frac{3}{4} \hat{C} \hat{o} \hat{A} \hat{C} \hat{o} \hat{C} \hat{o} \hat{y} \hat{U} \hat{I} \hat{o} \hat{A} \hat{I} \hat{o} \hat{A} \hat{A} \hat{I} \hat{o} \hat{E} \hat{o} \hat{A} \hat{I} \hat{o} \hat{C} \hat{o} \hat{C} \hat{o} \hat{I} \hat{o} \hat{A} \hat{C} \hat{o} \hat{A} \hat{I} \hat{o} \hat{I} \hat{o} \hat{o} \hat{C} \hat{o}$$

$\hat{i}, \hat{j}, \hat{k} \pm \underline{y} \hat{A} \hat{I} \hat{o}$ $x, y, z \ll \hat{I} \hat{I} \hat{o} \hat{C} \hat{o} \hat{\mu} \hat{A} \hat{A} \hat{I} \hat{o} \hat{C} \hat{o} \hat{A} \hat{C} \hat{o} \hat{C} \hat{o} \hat{I} \hat{o} \hat{E} \hat{o} \hat{I} \hat{o}$. « $\hat{A} \hat{U} \hat{E} \hat{y} \hat{a} \hat{A} \hat{A} \hat{I} \hat{o}$, $\hat{F}_1, \hat{F}_2, \dots, \hat{F}_n \pm \underline{y} \hat{E} \hat{I} \hat{o}$ $\hat{C} \hat{o} \hat{A} \hat{C} \hat{o} \hat{A} \hat{O} \hat{A} \hat{I} \hat{o} \hat{A} \hat{A} \hat{U} \hat{I} \hat{o} \times \hat{o}$.

$$\underline{F}_1 = F_{1x} \hat{i} + F_{1y} \hat{j} + F_{1z} \hat{k}$$

$$\underline{F}_2 = F_{2x} \hat{i} + F_{2y} \hat{j} + F_{2z} \hat{k}$$

$$\underline{\hat{F}}_r = \hat{F}_{rx} \hat{i} + \hat{F}_{ry} \hat{j} + \hat{F}_{rz} \hat{k}$$

$$\underline{\hat{F}}_n = \hat{F}_{nx} \hat{i} + \hat{F}_{ny} \hat{j} + \hat{F}_{nz} \hat{k}$$

$\hat{O} \pm \underline{y} \hat{E} \hat{I} \hat{o} \hat{D} \hat{A} \hat{I} \hat{o} \hat{o} \hat{U} \hat{C} \hat{o} \hat{A} \hat{C} \hat{o}$, $\hat{S} \hat{A} \hat{U} \hat{I} \hat{o} \hat{I} \hat{o} \hat{n} \frac{3}{4} \hat{C} \hat{o} \hat{A} \hat{C} \hat{o} \hat{C} \hat{o} \ll \hat{A} \hat{U} \hat{I} \hat{o} \hat{I} \hat{o} \hat{A} \hat{A} \hat{U} \hat{I} \hat{o} \hat{D}$, « $\hat{A} \hat{U} \hat{E} \hat{y} \hat{I} \hat{I} \hat{o} \hat{A} \hat{A} \hat{I} \hat{o} \hat{E} \hat{I} \hat{o} \hat{I} \hat{o} \hat{I} \hat{o} \hat{O} \hat{E} \hat{O} \hat{o}$.
 $\hat{P} \hat{U} \hat{A} \hat{I} \hat{o} \hat{A} \hat{O} \hat{o} \ll \hat{A} \hat{U} \hat{E} \hat{y} \hat{I} \hat{I} \hat{o} \hat{A} \hat{A} \hat{y} \frac{3}{4} \hat{C} \hat{o} \hat{A} \hat{C} \hat{o} \hat{A} \hat{R} \pm \hat{E} \hat{I} \hat{I} \hat{o} \hat{I} \hat{o} \hat{I} \hat{o} \hat{I} \hat{o}$,

$$\underline{R} = \underline{F}_1 + \underline{F}_2 + \dots + \underline{F}_r + \dots + \underline{F}_n$$

$$\sum_{r=1}^n \underline{F}_r \sin^2 \theta_r = \frac{(A_y B_z - A_z B_y)^2 + (A_z B_x - A_x B_z)^2 + (A_x B_y - A_y B_x)^2}{(A_x^2 + A_y^2 + A_z^2)(B_x^2 + B_y^2 + B_z^2)}$$

$$= \sum_{r=1}^n (F_{rx} \hat{i} + F_{ry} \hat{j} + F_{rz} \hat{k})$$

$$= \left(\sum_{r=1}^n F_{rx} \right) \hat{i} + \left(\sum_{r=1}^n F_{ry} \right) \hat{j} + \left(\sum_{r=1}^n F_{rz} \right) \hat{k} \pm \underline{y} \hat{E}_i \hat{I} \hat{o}.$$

$\hat{i} \hat{j} \hat{k} \frac{3}{4} \hat{C} \hat{o} \hat{C} \hat{o} \hat{o}$, $\underline{R} \hat{y} \hat{I} \hat{o} \hat{U} \hat{U} \hat{o} \hat{C} \hat{o} \hat{R}_x, \underline{R}_y, \underline{R}_z \pm \hat{E} \hat{I} \hat{I} \hat{o} \hat{E} \hat{o} \hat{A} \hat{I} \hat{o} \hat{S} \hat{A} \hat{I} \hat{o} \hat{D}$,

$$\underline{R}_x \hat{i} + \underline{R}_y \hat{j} + \underline{R}_z \hat{k} = \left(\sum_{r=1}^n F_{rx} \right) \hat{i} + \left(\sum_{r=1}^n F_{ry} \right) \hat{j} + \left(\sum_{r=1}^n F_{rz} \right) \hat{k} \pm \underline{y} \hat{E}_i \hat{I} \hat{o}.$$

$\pm \hat{E} \hat{S} \hat{A}$, $R_x = \sum_{r=1}^n F_{rx}; R_y = \sum_{r=1}^n F_{ry}; R_z = \sum_{r=1}^n F_{rz} \pm \underline{y} \hat{E} \hat{o} \hat{A} \hat{y} \hat{A} \hat{I} \hat{o} \hat{U} \hat{o} \hat{C} \hat{o} \hat{I} \hat{o}$.

ŞAüÜÈÄ $\hat{o} \hat{A} \hat{y} \hat{A} \hat{I} \hat{o} \hat{U} \hat{o}$, $\hat{I} \hat{I} \hat{o} \hat{A} \hat{A} \hat{y} \frac{3}{4} \hat{C} \hat{o} \hat{A} \hat{C} \hat{o} \underline{R} \hat{P} \hat{y} \hat{i}, \hat{j}, \hat{k} \frac{3}{4} \hat{C} \hat{o} \hat{C} \hat{o} \hat{o}$

$$= AB \cos \theta \quad \rightarrow \quad \text{ó.}$$

$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$
 \rightarrow
 $|\vec{A}| |\vec{B}| \cos \theta = \vec{A} \cdot \vec{B}$
 \rightarrow
 $\cos \theta = \frac{\vec{A} \cdot \vec{B}}{|\vec{A}| |\vec{B}|}$

$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$
 \rightarrow
 $|\vec{A}| |\vec{B}| \cos \theta = \vec{A} \cdot \vec{B}$
 \rightarrow
 $\cos \theta = \frac{\vec{A} \cdot \vec{B}}{|\vec{A}| |\vec{B}|}$

$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$
 \rightarrow
 $|\vec{A}| |\vec{B}| \cos \theta = \vec{A} \cdot \vec{B}$
 \rightarrow
 $\cos \theta = \frac{\vec{A} \cdot \vec{B}}{|\vec{A}| |\vec{B}|}$

$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$
 \rightarrow
 $|\vec{A}| |\vec{B}| \cos \theta = \vec{A} \cdot \vec{B}$
 \rightarrow
 $\cos \theta = \frac{\vec{A} \cdot \vec{B}}{|\vec{A}| |\vec{B}|}$

$$OL = OA \cos \theta$$

$$= A \cos \theta \quad \rightarrow \quad \text{ó.}$$

$\vec{A} \cdot \vec{B}$

$$\vec{A} \cdot \vec{B} = AB \cos \theta$$

$$= A(B \cos \theta)$$

$$= OA \cdot OM \quad \rightarrow \quad \text{ó.}$$

$$\vec{A} \cdot \vec{B} = BA \cos \theta$$

$$= B(A \cos \theta)$$

$$= OB \cdot OL \quad \rightarrow \quad \text{ó.}$$

$$\vec{A} \cdot \vec{B} = AB \cos \theta = OA \cdot OM = OB \cdot OL \quad \rightarrow \quad \text{ó.}$$

$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$
 \rightarrow
 $|\vec{A}| |\vec{B}| \cos \theta = \vec{A} \cdot \vec{B}$
 \rightarrow
 $\cos \theta = \frac{\vec{A} \cdot \vec{B}}{|\vec{A}| |\vec{B}|}$

$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$
 \rightarrow
 $|\vec{A}| |\vec{B}| \cos \theta = \vec{A} \cdot \vec{B}$
 \rightarrow
 $\cos \theta = \frac{\vec{A} \cdot \vec{B}}{|\vec{A}| |\vec{B}|}$

$$\vec{A} \cdot \vec{B} = AB \cos \theta = BA \cos \theta = \vec{B} \cdot \vec{A} \quad \rightarrow \quad \text{ó.}$$

$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$
 \rightarrow
 $|\vec{A}| |\vec{B}| \cos \theta = \vec{A} \cdot \vec{B}$
 \rightarrow
 $\cos \theta = \frac{\vec{A} \cdot \vec{B}}{|\vec{A}| |\vec{B}|}$

ÍÆÄÜÈ ÞÛ¼Ë °ÄË ÛÏÏ Þ¼ÄÄ ÁÏÛ §,¼½Û Ö ÌÍ §,¼½ÄÉÏ
 («¼ÄÄ „ = 90° ±ÉË)

« Õ ÌÄÏÐ Ä,ß ±ÝÈ¼Ë °ÄË ÛÏÏ ÿÛÏ Ì,¼ÛÛ ÌÍ ð¼É¼Ï Õ. „ Ý Ä¼ÛÛ
 0° ±ÉË Ä,ß = AB cos 0°

$$= AB ±ÝÈÏ Õ.$$

«¼ÄÄ ÑÄ¼Ë °ÄË ÁÏÛ ÞÛ¼Ë °ÄË ÇÛ ±ñ½Û ÌÄÏÏ Ì¼Ë °ÄË
 ±ñ Ä¼ÛÛ ÇÛ ÌÄÏÏ ð¼Ë ÌÍ °ÄÄÏ Õ.

„ Ä¼ÛÛ180° ±ÝÈÏ

$$\underline{A.B} = AB \cos 180^\circ$$

$$= AB(-1)$$

$$= -AB \text{ Ì Õ.}$$

§ÄÛ ±ñ½Û ÌÄÏÏ Ì¼Ë Ä¼ÛÛ B = A ±ÝÛÏÏ ÕÄÏÐ.

$$\underline{A.B} = AA \cos 0^\circ = A^2 ±ÝÈÏ Õ.$$

¼ÄÏ Õ¼Ë °ÄË Ä¼ÛÛ Ä

$$A = \sqrt{\underline{A.A}} ±ÝÈ °ÄËÄÏ¼Û¼Û ð¼ÛÄÄÛÏ ð¼ÛÛ ñ¼ÉÄÄÏ.$$

Ä « ðÄÐ Ò ÌÆÛ¼Ë °ÄË (Null Vector) ÄÏ ÌÄÉË

$$\underline{O.B} = 0 \text{ Ì Õ.}$$

« ÛÄÏ Ò ÄÏ = 0 Ì Õ.

±É §Ä ±ñ½Û ÌÄÏÏ Ì¼Ë Ä¼ÛÛ Ä¼ÛÛ Ì¼Ë °ÄË ÌÆÄÜÈ¼Ë °ÄË ÇÛ Ì
 Õ¼ÛÄÏ Õ.

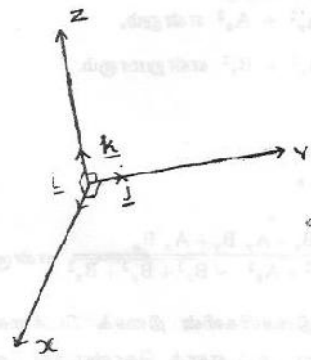
§ÄÛ Ä = Aa, B = Bb, ±ÝÈ « ÄÏ Ì¼Ë a, b ±ÝÈ µÄÄÏ ð¼Ë °ÄË ÇÛ
 Ä¼Û ÌÄÏÏ ÕÄÏ ÕÄÏ ÕÄÏ

$$\underline{A.B} = A \underline{a} . B \underline{b}$$

$$= AB(\underline{a.b}) ±ÝÈÏ Õ.$$

±É §Ä (a, b) = cos „ Ì Õ.

§ÄÛ Ì,¼,¼ ±ÝÄÄ Ä¼Û 1-24Û ÌÄÏÏ Ì¼Ë ðÉÄÄÏÛ Ì¼Ë Ì¼Ë Ì¼Ë
 ÌÍ ð¼Ë « ÄÏ x, y, z « ÌÍ ÇÛ¼Ë °ÄË ÇÛ « ÈÄÏ Ì¼Ë µÄÄÏ ð¼Ë
 °ÄË ÇÛ¼Ë



$$\underline{i} \cdot \underline{i} = 1 \cdot 1 \cos 0 = 1 \rightarrow \bar{1} \bar{0}$$

$$\ll \underline{j} \cdot \underline{j} = 1 = \underline{k} \cdot \underline{k} \rightarrow \bar{1} \bar{0}$$

$$\ll \underline{i} \cdot \underline{j} = \underline{j} \cdot \underline{i} = \underline{k} \cdot \underline{k} = 1 \rightarrow \bar{1} \bar{0}$$

$$\S \text{ÁÖö } \underline{i} \cdot \underline{j} = 1 \cdot 1 \cos 90^\circ = 0 \rightarrow \bar{1} \bar{0}$$

$$\rightarrow \underline{j} \cdot \underline{i} = 0$$

$$\underline{i} \cdot \underline{j} = \underline{j} \cdot \underline{i} = 0$$

$$\underline{j} \cdot \underline{k} = \underline{k} \cdot \underline{j} = 0$$

$$\underline{k} \cdot \underline{i} = \underline{i} \cdot \underline{k} = 0$$

$$\rightarrow \bar{1} \bar{0}$$

$$\underline{A}, \underline{B} \pm \acute{y} \bar{E} \text{ } \underline{A} = A_x \underline{i} + A_y \underline{j} + A_z \underline{k} \quad \underline{B} = B_x \underline{i} + B_y \underline{j} + B_z \underline{k}$$

$$\underline{A} = A_x \underline{i} + A_y \underline{j} + A_z \underline{k}$$

$$\underline{B} = B_x \underline{i} + B_y \underline{j} + B_z \underline{k} \pm \acute{y} \bar{E} \bar{1} \bar{0}$$

$$\ll \underline{A} \cdot \underline{B}$$

$$\begin{aligned} \underline{A} \cdot \underline{B} &= (A_x \underline{i} + A_y \underline{j} + A_z \underline{k}) \cdot (B_x \underline{i} + B_y \underline{j} + B_z \underline{k}) \\ &= A_x B_x (\underline{i} \cdot \underline{i}) + A_x B_y (\underline{i} \cdot \underline{j}) + A_x B_z (\underline{i} \cdot \underline{k}) + A_y B_x (\underline{j} \cdot \underline{i}) + A_y B_y (\underline{j} \cdot \underline{j}) + A_y B_z (\underline{j} \cdot \underline{k}) \\ &\quad + A_z B_x (\underline{k} \cdot \underline{i}) + A_z B_y (\underline{k} \cdot \underline{j}) + A_z B_z (\underline{k} \cdot \underline{k}) \\ &= A_x B_x (\underline{i} \cdot \underline{i}) + A_y B_y (\underline{j} \cdot \underline{j}) + A_z B_z (\underline{k} \cdot \underline{k}) \\ &= A_x B_x + A_y B_y + A_z B_z \rightarrow \bar{1} \bar{0} \end{aligned}$$

$$\S \text{ÁÖö}$$

$$\begin{aligned} A^2 &= \underline{A} \cdot \underline{A} = (A_x \underline{i} + A_y \underline{j} + A_z \underline{k}) \cdot (A_x \underline{i} + A_y \underline{j} + A_z \underline{k}) \\ &= A_x^2 + A_y^2 + A_z^2 \pm \acute{y} \bar{U} \bar{0} \quad B^2 = \underline{B} \cdot \underline{B} = B_x^2 + B_y^2 + B_z^2 \pm \acute{y} \bar{U} \bar{A} \bar{1} \bar{0} \end{aligned}$$

$$\pm \acute{E} \S \text{Á} \quad \cos \alpha = \frac{\underline{A} \cdot \underline{B}}{AB}$$

$$= \frac{A_x B_x + A_y B_y + A_z B_z}{\sqrt{A_x^2 + A_y^2 + A_z^2} \sqrt{B_x^2 + B_y^2 + B_z^2}}$$

$$\pm \acute{y} \bar{E} \bar{1} \bar{0}$$

$$\S \text{ÁÖö } \underline{A}, \underline{B} \pm \acute{y} \bar{E} \text{ } \underline{A} = A_x \underline{i} + A_y \underline{j} + A_z \underline{k} \quad \underline{B} = B_x \underline{i} + B_y \underline{j} + B_z \underline{k} \quad \text{Ó} \cdot \bar{E} \S \hat{A}(l_1, m_1, n_1), (l_2, m_2, n_2)$$

$$\pm \acute{E} \bar{1} \bar{0} \ll \underline{A} \cdot \underline{B} = A_x B_x + A_y B_y + A_z B_z$$

$$l_1 = \frac{A_x}{A} = \frac{A_x}{\sqrt{A_x^2 + A_y^2 + A_z^2}}; l_2 = \frac{B_x}{B} = \frac{B_x}{\sqrt{B_x^2 + B_y^2 + B_z^2}}$$

$$n_1 = \frac{A_z}{A} = \frac{A_z}{\sqrt{A_x^2 + A_y^2 + A_z^2}}; n_2 = \frac{B_z}{B} = \frac{B_z}{\sqrt{B_x^2 + B_y^2 + B_z^2}}$$

Οι $\vec{OC} = \vec{OB} + \vec{BC} = \vec{B} + \vec{C} \rightarrow \vec{0}$.

Β, C $\pm \vec{y} \in \vec{0}$ $\vec{OC} = \vec{OB} + \vec{BC} = \vec{B} + \vec{C} \rightarrow \vec{0}$. OA $\pm \vec{y} \in \vec{0}$ BM, CN $\pm \vec{y} \in \vec{0}$
 | $\vec{OC} = \vec{OB} + \vec{BC} = \vec{B} + \vec{C} \rightarrow \vec{0}$. OA $\pm \vec{y} \in \vec{0}$ OM, MN, ON
 $\pm \vec{y} \in \vec{0}$ $\vec{OC} = \vec{OB} + \vec{BC} = \vec{B} + \vec{C} \rightarrow \vec{0}$.

$$\rightarrow \vec{OC} \cdot \vec{OA} = (\vec{B} + \vec{C}) \cdot \vec{OA} = \vec{OA} \cdot \vec{ON}$$

$$= \vec{OA} \cdot (\vec{OM} + \vec{MN})$$

$$= \vec{OA} \cdot \vec{OM} + \vec{OA} \cdot \vec{MN}$$

$$= \vec{OA} \cdot \vec{B} + \vec{OA} \cdot \vec{C} \rightarrow \vec{0}$$

$\vec{OC} = \vec{OB} + \vec{BC} = \vec{B} + \vec{C} \rightarrow \vec{0}$. OA $\pm \vec{y} \in \vec{0}$ OM, MN, ON
 $\pm \vec{y} \in \vec{0}$ $\vec{OC} = \vec{OB} + \vec{BC} = \vec{B} + \vec{C} \rightarrow \vec{0}$.

$$(\vec{A} + \vec{B}) \cdot (\vec{C} + \vec{D}) = \vec{A} \cdot (\vec{C} + \vec{D}) + \vec{B} \cdot (\vec{C} + \vec{D})$$

$$= \vec{A} \cdot \vec{C} + \vec{A} \cdot \vec{D} + \vec{B} \cdot \vec{C} + \vec{B} \cdot \vec{D}$$

$$\vec{m} \cdot \vec{n} = m \cdot n \cos(\angle \vec{m}, \vec{n}) = mn \cos(\angle \vec{A}, \vec{B})$$

$$= mn \cos(\angle \vec{A}, \vec{B}) \rightarrow \vec{0}$$

1.17 $\vec{C} = \vec{A} \times \vec{B}$ (Vector or cross product of two vectors)

$\vec{C} = \vec{A} \times \vec{B}$ $\vec{C} = \vec{A} \times \vec{B}$ $\vec{C} = \vec{A} \times \vec{B}$ $\vec{C} = \vec{A} \times \vec{B}$ $\vec{C} = \vec{A} \times \vec{B}$

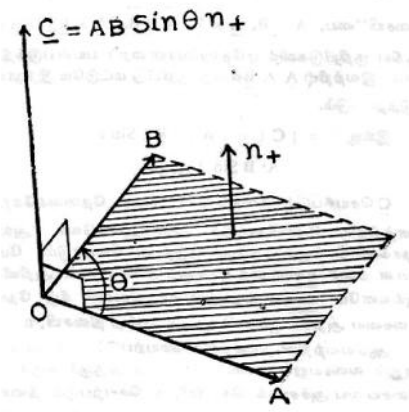


Figure 1-26

\vec{A}, \vec{B} $\vec{C} = \vec{A} \times \vec{B}$ $\vec{C} = \vec{A} \times \vec{B}$ $\vec{C} = \vec{A} \times \vec{B}$ $\vec{C} = \vec{A} \times \vec{B}$

\vec{A}, \vec{B} $\vec{C} = \vec{A} \times \vec{B}$ $\vec{C} = \vec{A} \times \vec{B}$ $\vec{C} = \vec{A} \times \vec{B}$ $\vec{C} = \vec{A} \times \vec{B}$

"İ Üi ì ò | AÖi ì ò ¼°° °Ä°" ·Ä A×B, Ì×Ì, Ì×Ì, [Ì×Ì], Ì×Ì, Ì×Ì →, Ì
Ì ÈÄÏ ¼°° ²§¼Ü | Äi y · Èò ÄÄyÄÌ ò¼° ì ÈÄi Ì. ÞÄüÈò Ì×Ì ±yÈ
Ì ÈÄÏ ÄÖÌ §Ä Þóá Äò ÄÄyÄÌ ò¼°ÄÌ ò.

$$\text{pí ì } C = |C| = |A| |B| \sin, \\ = A.B \sin, \quad \text{ì ò.}$$

Ì | °ÄüÄÌ ò ¼°° °i §, j ò ¼ò §¼ · Äì §, üÄ (A, B) ¼Çò¼Üì §Äð§Ìì Ì
| °í ì ò¼i §Äi « ØÄÐ Ì§Ìì Ì | °í ì ò¼i §Äi ±ì ò¼ø §Äñ Ì ò.
§Äð§Ìì ÜÜÇ ¼°° ° ñ±±yÈ µÄÄÌ ò ¼°° °ÄÄiø « ÈÄÄi òÄÌ ò.
« í ½ §Ä ñ±±yÈ µÄÄÌ ò ¼°° °ÄÄi Ì§Ìì ÜÜÇ ¼°° ° Ä « ÈÄÄi Ì ò.
§ÄÖò Ì±yÈ ¼°° °ÄÄi ñ± « ØÄÐ ñ± ÌÄüÈý ¼°° °, Çò | °ÄüÄÌ ò
±yÄ Ì¼ò ÄÄyÄÖÄi Üò Ä · ÄÄÜì Äiø. ÄÄòÈò ¼°ÖÌ îíÜü ´yÜ Ì
¼°° °ÄÄi Ä « î°i Ì | jñ Ì Ä | °ÄüÄÌ ò ¼°° °ÄÄÖóÐ B | °ÄüÄÌ ò
¼°° ° Ä §Ìì Ì ÍÆÖð§ÄiÐ ¼°ÖÌ §Äð§Ìì Ì | °ÖÖ¼iø Ì | °ÄüÄÌ ò
¼°° ° Ä ñ±Ä · ÄÄÜðÄ¼i ×ò B | °ÄüÄÌ ò ¼°° °ÄÄÖóÐ Ä | °ÄüÄÌ ò
¼°° ° Ä §Ìì Ç ¼°ÖÌ · í ÍÆÜÈÌ ò§ÄiÐ ¼°ÖÌ Ì§Ìì ÄÖÄ¼iø Ì
| °ÄüÄÌ ò ¼°° ° Ä ñ± Ä · ÄÄÜðÄ¼i ×ò Ì, jüÇòÄÌ ò.

¼°ÖÌ §Äð§Ìì Ì | °ÖÖð§ÄiÐ Ä, B, C →, Ä ¼°° °ÄÄi Ü, È, jÄ ÓÜÇý
ÞÄi ò¼Üì ±¼Äi È ÍÆü°Ä Ä §Äüì, jüÄ¼iø Ì | °ÄüÄÌ ò ¼°° ° Äò
¼Çò¼Üý §Äð§Ìì Ì µÄÄÌ ò ¼°° °ÄÄi ñ± ÌÖò B, Ä, C →, Ä ¼°° °ÄÄi Ü
ÄÄi ÍÆÄiÄ¼iø (clockwise rotation) Ì | °ÄüÄÌ ò ¼°° ° Äò ¼Çò¼Üý Ì
§Ìì Ì µÄÄÌ ò ¼°° °ÄÄi ñ± ÌÖò Ì Èò¼ø §Äñ Ì ò.

$$\text{±É§Ä } \underline{A}, \underline{B}, \underline{C} \text{ ±yÄ · Ä } \text{p¼í ÍÆÄi, « · ÄÖð§ÄiÐ } \underline{C} = \underline{A} \wedge \underline{B}$$

$$= (AB \sin,) \underline{n} \pm \text{±É} \times \text{ò} \\ \underline{B}, \underline{A}, \underline{C} \text{ ±yÄ · Ä ÄÄi ÍÆÄi, « · ÄÖð§ÄiÐ} \\ \underline{C} = \underline{B} \wedge \underline{A} \\ = (AB \sin,) \underline{n} \\ = -(AB \sin,) \underline{n} \pm \text{±É} \times \text{ò } \text{ì, jüÇòÄÌ ò.}$$

$$\text{pí ì } \underline{A} \wedge \underline{B} = -(\underline{B} \wedge \underline{A}) \text{ ±yÈ } \text{ì, jüÈÐ.} \\ \text{« ØÄÐ } \underline{A} \wedge \underline{B} \neq (\underline{B} \wedge \underline{A}) \text{ Ì ò.}$$

« ¼i ÄÐ ÞÖ ¼°° °ÄÄi Çý Ì Üi ì ò | AÖi Ì ¼°° °ÄÄi Ü Äi Äi ÜÈ Ä¼°Ä Ä
(Commutative Law)ò ¼°ÖÄÄi | °ÄüÄ¼ÄÄi Ä ±É « È¼ø §Äñ Ì ò.
ÍÆÄüÈ¼i È Ä, B ±yÈ ÞÖ ¼°° °ÄÄi Ü Þ · ½Äi, ÞÖì Äi Èiø « · Ä, Üì Ì
Þ · ¼ÄÄi ÄÖò §, j ½ò ÍÆÄi Ì ò. (« ¼i ÄÐ · °=0). « ò | ÄiøÐ

$$\underline{C} = \underline{A} \wedge \underline{B}$$

$$= (AB \sin 0^\circ) \underline{n}$$

$$= \underline{0} \rightarrow \text{ñ} \text{õ.}$$

±ÉŞĂ pŌ¾ċ'' °Āċ, ū p'' ½Āĵ, « '' Áó¾ċ¼ « ÄüËÿ Ì Úì Ì ô|ÀŌì, ċÍĒĀĵ, ŞĂñ Ĩ õ.

ŞĂŌõ A, B Ì, Ū Ì Ì p'' ¼ĀĈĀ'' ÁŌõ Ş, ĵ ½õ 'Ō | °í Ş, ĵ ½ĀĴÉ ĵ ø (°=90).

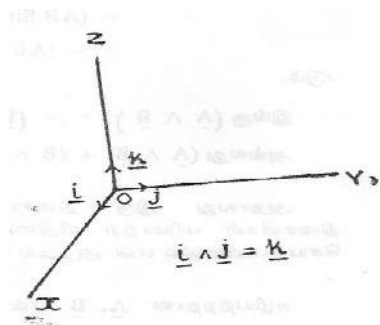
$$\underline{C} = \underline{A} \wedge \underline{B}$$

$$= (AB \sin 90^\circ) \underline{n}$$

$$= AB \underline{n} \pm \text{ýË} \text{ì} \text{õ.}$$

±ÉŞĂ A, B ±ýË pŌ¾ċ'' °Āċ, ū | °í Ì ò¾ĵ, « '' ÁĀ¾üĹ ĵ ĈĀ ĵ ĈĀ¾ċ "A∧B=0" ñ Ĩ õ. « '' Ā, ū p'' ½ĀĴ, « '' ÁĀ¾üĹ ĵ ĈĀ ĵ ĈĀ¾ċ "A∧B=0" ñ Ĩ õ.

1-18 (1) µĀĀĬ ò¾ċ'' °Āċ, ċÿ Ì Úì Ì ô|ÀŌì, ċ'' ĀĬ ĵ Ĵø
 Ā¼õ 1-27ø ĵ ðĒĒĀĴ Ū O ±ýË òúĈĀÿ ĀĒĀĵ, 'ýŪ Ì ĵ ĵ Ū
 | °í Ì ò¾ĵ, - ūĈ ox, oy, oz ±ýË « ĨĬ, '' Ĉ ±Ĩ Ĭ ×õ. « '' Ā, ċÿ
 ¾ċ'' °, '' Ĉ Ó'' ÈŞĂ i, j, k ±ýË µĀĀĬ ò¾ċ'' °Āċ, ū Ĩ ÈĈ, ðĬ õ.



Ā¼õ 1-27

i, j, k ±ýË µĀĀĬ ò¾ċ'' °Āċ, ū ĀĀòĒÈ ò¾ċŌĬ Ó'' ÈòĀĒ (Right Handed Screw Rule) 'Ō ĀĀòĒÈ Óõ'' Ā, ċÿ Ĩ õ (Right Handed Triad). « '' Ā, ū 'Ō ĀĀòĒÈ « '' ÁòĒ Ó'' È'' ĀĬ (Right Handed System of Reference) Ĩ ÈĈ¾ĵ, ×õ Ĩ ĵ ūĈòĀĬ õ.

i · i ±ýË °ĀĀĴÉ µĀĀĬ ò¾ċ'' °Āċ, ċÿ Ì Úì Ì ô|ÀŌì, ċò¾ċ'' °Āċ'' Ā ñ ĀĵŌõŞĀĴĐ « '' Ā, Ū Ì, ċ'' ¼ĀĈĀ'' ÁŌõ Ş, ĵ ½õ ÍĒĀĴĀ¾ĵø

$$\underline{i} \wedge \underline{i} = (1 \cdot 1 \sin 0) \underline{n}$$

$$= 0 \underline{k}$$

$$= \underline{0} \rightarrow \text{ñ} \text{õ.}$$

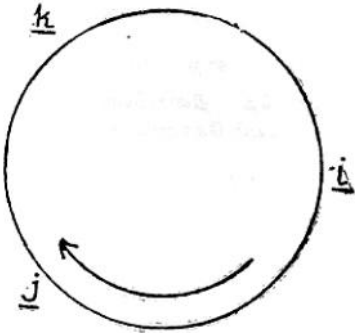
« ùĀĴŞĒ

$$\underline{j} \wedge \underline{j} = 0 = \underline{k} \wedge \underline{k} \rightarrow \text{ñ} \text{õ.}$$

i, j ±ýË pŌ¾ċ'' °Āċ, ū ĀĀòĒÈ ò¾ċŌĬ Ó'' ÈòĀĒ (Right Handed Screw Rule) 'Ō ĀĀòĒÈ Óõ'' Ā, ċÿ Ĩ õ (Right Handed Triad). « '' Ā, ū 'Ō ĀĀòĒÈ « '' ÁòĒ Ó'' È'' ĀĬ (Right Handed System of Reference) Ĩ ÈĈ¾ĵ, ×õ Ĩ ĵ ūĈòĀĬ õ.

$i \wedge j = (1.1 \sin 90^\circ) \underline{n} = \underline{k} \rightarrow \bar{1} \bar{0}$. ($\cdot \cdot i, j$)
 $\underline{j} \wedge i = -\underline{k} \rightarrow \bar{1} \bar{0}$.
 $\pm \underline{E} \underline{S} \underline{A} \quad i \wedge j = \underline{k} = -(j \wedge i) \rightarrow \bar{1} \bar{0}$.
 $\ll \underline{u} \underline{A} \underline{j} \underline{S} \underline{E}$, $j \wedge k = i = -(k \wedge j) \pm \underline{y} \underline{U} \bar{0}$
 $\underline{k} \wedge i = \underline{j} = -(i \wedge k) \pm \underline{y} \underline{U} \bar{0} \rightarrow \bar{1} \bar{0}$.

$\underline{p} \underline{A} \underline{U} \underline{E} \underline{C} \quad \underline{E} \pm \underline{C} \underline{A} \underline{j}$ « $\underline{E} \underline{C} \underline{A} \underline{j}$ $\bar{0}$ $\underline{A} \underline{D} \underline{U} \underline{C} \underline{A} \underline{j}$ $i, j, k \pm \underline{y} \underline{E}$
 $\underline{C} \underline{i} \quad \underline{E} \underline{j} \underline{A} \underline{O} \underline{U} \quad \underline{I} \underline{U} \underline{U} \bar{0} \quad \underline{A} \ll \underline{I} \underline{D} \underline{A} \underline{O} \underline{U} \underline{C} \underline{A} \underline{j} \quad 1-28 \bar{0}$
 $\underline{j} \underline{D} \underline{E} \underline{A} \underline{j} \underline{U} \ll \underline{A} \underline{i} \times \bar{0}$.
 $\underline{A} \underline{D} \underline{U} \underline{C} \underline{A} \underline{j} \underline{p} \underline{O} \ll \underline{I} \underline{D} \underline{A} \underline{O} \underline{U} \underline{C} \underline{A} \underline{j} \quad \underline{C} \pm \underline{I} \underline{D} \underline{E} \underline{j} \underline{A} \underline{O} \underline{U} \underline{I} \underline{E} \underline{O} \bar{0}$
 $\underline{A} \underline{j} \underline{A} \underline{i} \underline{D} \underline{E} \ll \underline{A} \underline{U} \underline{E} \underline{C} \underline{y} \quad \underline{I} \underline{U} \underline{I} \underline{O} \underline{A} \underline{O} \underline{i} \underline{C} \underline{A} \ll \underline{A} \underline{D} \underline{U} \underline{C} \underline{A} \underline{j} \underline{D} \ll \underline{D}$
 $\ll \underline{I} \underline{D} \underline{A} \underline{O} \underline{U} \underline{C} \underline{A} \underline{j} \underline{p} \underline{O} \underline{i} \bar{0}$.



$\underline{A} \underline{D} \underline{U} \underline{C} \underline{A} \underline{j}$ 1-28

$\pm \underline{I} \underline{D} \underline{E} \underline{j} \underline{A} \underline{O} \underline{U} \underline{C} \underline{A} \underline{j}$
 $\underline{k} \wedge i = \underline{j} \rightarrow \bar{1} \bar{0}$.
 $\underline{E} \underline{j} \underline{A} \underline{O} \underline{U} \underline{C} \underline{A} \underline{j} \underline{p} \underline{O} \ll \underline{I} \underline{D} \underline{A} \underline{O} \underline{U} \underline{C} \underline{A} \underline{j} \quad \underline{C} \pm \underline{I} \underline{D} \underline{E}$
 $\ll \underline{A} \underline{U} \underline{E} \underline{C} \underline{y} \quad \underline{I} \underline{U} \underline{I} \underline{O} \underline{A} \underline{O} \underline{i} \underline{C} \underline{A} \ll \underline{A} \underline{D} \underline{U} \underline{C} \underline{A} \underline{j} \underline{D} \ll \underline{D} \underline{A} \underline{O} \underline{U} \underline{C} \underline{A} \underline{j} \underline{p} \underline{O} \underline{i} \bar{0}$.

$1-18 (2) \underline{p} \underline{O} \underline{C} \underline{y} \quad \underline{C} \underline{y} \quad \underline{I} \underline{U} \underline{I} \underline{O} \underline{A} \underline{O} \underline{i} \underline{C} \underline{A} \quad \underline{A} \underline{D} \underline{U} \underline{C} \underline{A} \underline{j} \quad \underline{C} \underline{y}$
 $\underline{A} \underline{j} \underline{A} \underline{C} \underline{A} \underline{j} \quad \underline{1} \underline{2} \underline{i} \quad \underline{C} \underline{A} \underline{j}$

$\underline{A}, \underline{B} \quad \pm \underline{y} \underline{E} \quad \underline{C} \underline{y} \quad i, j, k \quad \underline{C} \underline{A} \underline{j} \quad \underline{A} \underline{D} \underline{U} \underline{C} \underline{A} \underline{j} \underline{D} \ll \underline{A}$
 $\underline{A} = A_x \underline{i} + A_y \underline{j} + A_z \underline{k}$
 $\underline{B} = B_x \underline{i} + B_y \underline{j} + B_z \underline{k}$
 $\pm \underline{y} \underline{U} \underline{I} \underline{E} \underline{C} \underline{y} \quad \underline{O} \underline{A} \underline{I} \bar{0}$.
 $\pm \underline{E} \underline{S} \underline{A} \ll \underline{A} \underline{U} \underline{E} \underline{C} \underline{y} \quad \underline{I} \underline{U} \underline{I} \underline{O} \underline{A} \underline{O} \underline{i} \underline{C} \underline{A}$
 $\underline{C} = \underline{A} \wedge \underline{B}$
 $= (A_x \underline{i} + A_y \underline{j} + A_z \underline{k}) \cdot (B_x \underline{i} + B_y \underline{j} + B_z \underline{k})$
 $= A_x \underline{i} \wedge (B_x \underline{i} + B_y \underline{j} + B_z \underline{k}) + A_y \underline{j} \wedge (B_x \underline{i} + B_y \underline{j} + B_z \underline{k}) + A_z \underline{k} \wedge (B_x \underline{i} + B_y \underline{j} + B_z \underline{k})$
 $= (A_y B_z - A_z B_y) \underline{i} + (A_z B_x - A_x B_z) \underline{j} + (A_x B_y - A_y B_x) \underline{k} \rightarrow \bar{1} \bar{0}$
 $\underline{p} \underline{O} \underline{C} \underline{y} \quad \underline{E} \ll \underline{1} \underline{2} \underline{i} \underline{S} \underline{j} \underline{A} \ll \underline{A} \underline{D} \underline{U} \underline{C} \underline{A} \underline{j} \quad (\text{Determinant}),$

$$\underline{C} = \underline{A} \wedge \underline{B} = (A_y B_z - A_z B_y) \underline{i} + (A_z B_x - A_x B_z) \underline{j} + (A_x B_y - A_y B_x) \underline{k}$$

$$\begin{vmatrix} \underline{i} & \underline{j} & \underline{k} \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$$

$\pm \dot{y} \dot{u} \ddot{o} \dot{\dot{e}} \dot{\dot{a}} \dot{\dot{o}}$.

1-18 (3) $\underline{A}, \underline{B} \pm \dot{y} \dot{e} \frac{3}{4} \dot{\dot{c}} \dot{\dot{o}} \dot{\dot{a}} \dot{\dot{c}} \dot{\dot{u}} \dot{\dot{i}} \dot{\dot{l}} \dot{\dot{p}} \dot{\dot{r}} \frac{1}{4} \dot{\dot{a}} \dot{\dot{c}} \dot{\dot{a}} \dot{\dot{r}} \dot{\dot{a}} \dot{\dot{o}} \dot{\dot{o}} \dot{\dot{s}} \dot{\dot{j}} \frac{1}{2} \dot{\dot{o}} \dot{\dot{r}} \frac{3}{4}, \frac{3}{4} \dot{\dot{c}} \dot{\dot{o}} \dot{\dot{a}} \dot{\dot{c}}$
 $\dot{\dot{l}} \dot{\dot{u}} \dot{\dot{l}} \dot{\dot{o}} \dot{\dot{a}} \dot{\dot{o}} \dot{\dot{i}} \dot{\dot{a}} \dot{\dot{i}} \dot{\dot{o}} \dot{\dot{j}} \dot{\dot{i}} \dot{\dot{r}} \frac{3}{4} \dot{\dot{o}}$

$\underline{i}, \underline{j}, \underline{k} \pm \dot{y} \dot{e} \mu \dot{\dot{a}} \dot{\dot{a}} \dot{\dot{l}} \dot{\dot{o}} \frac{3}{4} \dot{\dot{c}} \dot{\dot{o}} \dot{\dot{a}} \dot{\dot{c}} \dot{\dot{c}} \dot{\dot{o}}, \underline{A}, \underline{B} \dot{\dot{r}} \dot{\dot{a}} \frac{3}{4} \dot{\dot{c}} \dot{\dot{o}} \dot{\dot{a}} \dot{\dot{c}} \dot{\dot{r}} \dot{\dot{c}},$

$$\underline{A} = A_x \underline{i} + A_y \underline{j} + A_z \underline{k}$$

$$\underline{B} = B_x \underline{i} + B_y \underline{j} + B_z \underline{k}$$

$\pm \dot{e} \dot{\dot{l}} \dot{\dot{l}} \dot{\dot{e}} \dot{\dot{a}} \dot{\dot{r}} \times \dot{\dot{o}}$.

$\underline{A}, \underline{B} \dot{\dot{l}} \dot{\dot{u}} \dot{\dot{l}} \dot{\dot{c}} \dot{\dot{r}} \frac{1}{4} \dot{\dot{a}} \dot{\dot{c}} \dot{\dot{a}} \dot{\dot{r}} \dot{\dot{a}} \dot{\dot{o}} \dot{\dot{o}} \dot{\dot{s}} \dot{\dot{j}} \frac{1}{2} \dot{\dot{o}} \dot{\dot{r}} \frac{3}{4}, \dot{\dot{r}} \pm \dot{e} \dot{\dot{l}} \dot{\dot{l}} \dot{\dot{u}} \dot{\dot{c}} \times \dot{\dot{o}}$.

$\underline{A}, \underline{B} \dot{\dot{r}} \dot{\dot{a}} \dot{\dot{a}} \dot{\dot{u}} \dot{\dot{e}} \dot{\dot{n}} \dot{\dot{y}} \frac{3}{4} \dot{\dot{c}} \dot{\dot{o}} \dot{\dot{i}} \dot{\dot{c}} \dot{\dot{a}} \dot{\dot{l}} \dot{\dot{r}} \dot{\dot{r}} \dot{\dot{c}} \dot{\dot{o}} \dot{\dot{r}} \dot{\dot{e}} \dot{\dot{s}} \dot{\dot{a}} (l_1, m_1, n_1), (l_2, m_2, n_2) \pm \dot{e}$

$\dot{\dot{l}} \dot{\dot{u}} \dot{\dot{l}} \dot{\dot{u}} \dot{\dot{c}} \times \dot{\dot{o}}$.

$\pm \dot{e} \dot{\dot{s}} \dot{\dot{a}}$,

$$A^2 = \underline{A} \cdot \underline{A} = A_x^2 + A_y^2 + A_z^2$$

$$B^2 = \underline{B} \cdot \underline{B} = B_x^2 + B_y^2 + B_z^2 \quad \dot{\dot{r}} \dot{\dot{l}} \dot{\dot{o}}$$

$$l_1 = \frac{A_x}{A} = \frac{A_x}{\sqrt{A_x^2 + A_y^2 + A_z^2}}$$

$$l_2 = \frac{B_x}{B} = \frac{B_x}{\sqrt{B_x^2 + B_y^2 + B_z^2}}$$

$$m_1 = \frac{A_y}{A} = \frac{A_y}{\sqrt{A_x^2 + A_y^2 + A_z^2}} \quad ; \quad n_1 = \frac{A_z}{A} = \frac{A_z}{\sqrt{A_x^2 + A_y^2 + A_z^2}}$$

$$m_2 = \frac{B_y}{B} = \frac{B_y}{\sqrt{B_x^2 + B_y^2 + B_z^2}} \quad n_2 = \frac{B_z}{B} = \frac{B_z}{\sqrt{B_x^2 + B_y^2 + B_z^2}}$$

$\dot{\dot{r}} \dot{\dot{l}} \dot{\dot{o}}$

$$\underline{C} = \underline{A} \wedge \underline{B} = (AB \sin \theta) \underline{n} \pm \dot{y} \dot{e} \dot{\dot{a}} \dot{\dot{c}} \dot{\dot{a}} \dot{\dot{i}} \dot{\dot{o}}$$

$$(\underline{C} \cdot \underline{C}) = (\underline{A} \wedge \underline{B}) \cdot (\underline{A} \wedge \underline{B})$$

$$= (AB \sin \theta \underline{n}) \cdot (AB \sin \theta \underline{n})$$

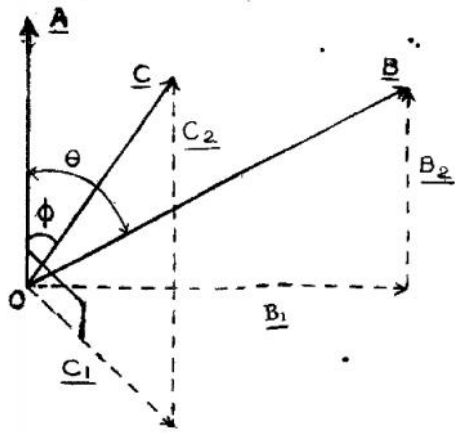
$$= (AB \sin \theta)^2 (\underline{n} \cdot \underline{n})$$

$$= A^2 B^2 \sin^2 \theta$$

$$= (A_x^2 + A_y^2 + A_z^2) (B_x^2 + B_y^2 + B_z^2) \sin^2 \theta \quad \dot{\dot{r}} \dot{\dot{l}} \dot{\dot{o}}$$

ŞAÖö

$$(\underline{C} \cdot \underline{C}) = \left\{ (A_y B_z - A_z B_y) \underline{i} + (A_z B_x - A_x B_z) \underline{j} + (A_x B_y - A_y B_x) \underline{k} \right\}$$



À¼õ 1-30

$$\underline{A} \wedge \underline{B} = (AB \sin \theta) \underline{n}_+ \quad (\theta = \angle \text{between } \underline{A} \text{ and } \underline{B})$$

$$= A(B \sin \theta) \underline{n}_+$$

$$= AB_1 \underline{n}_+ \quad \text{since } \underline{B} \text{ is perpendicular to } \underline{n}_+$$

§ÁÖõ

$$\underline{A} \wedge \underline{B}_1 = (AB_1 \sin 90^\circ) \underline{n}_+$$

$$= AB_1 \underline{n}_+ \quad \text{since } \underline{A} \text{ is perpendicular to } \underline{n}_+$$

$$\underline{A} \wedge \underline{B}_2 = (AB_2 \sin 0^\circ) \underline{n}_+$$

$$= 0 \quad (\because \underline{A} \text{ and } \underline{B}_2 \text{ are parallel})$$

$$\underline{A} \wedge \underline{B} = AB_1 \underline{n}_+$$

$$\underline{A} \wedge \underline{B} = \underline{A} \wedge (\underline{B}_1 + \underline{B}_2) = \underline{A} \wedge \underline{B}_1 \quad \text{since } \underline{A} \wedge \underline{B}_2 = 0$$

∴ $\underline{A} \wedge \underline{B} = AB_1 \underline{n}_+ = A(B \sin \theta) \underline{n}_+ = AB \sin \theta \underline{n}_+$

$$\underline{A} \wedge \underline{C} = (AC \sin \omega) \underline{n}_+ \quad (\omega = \angle \text{between } \underline{A} \text{ and } \underline{C})$$

$$= (AC_1) \underline{n}_+ \quad \text{since } \underline{C} \text{ is perpendicular to } \underline{n}_+$$

$$= (AC_1) \underline{n}_+ \quad \text{since } \underline{A} \text{ is perpendicular to } \underline{n}_+$$

§ÁÖõ

$$\underline{A} \wedge \underline{C}_1 = (AC_1 \sin 90^\circ) \underline{n}_+$$

$$= (AC_1) \underline{n}_+ \quad \text{since } \underline{A} \text{ is perpendicular to } \underline{n}_+$$

$$\underline{A} \wedge \underline{C}_2 = (AC_2 \sin 0^\circ) \underline{n}_+ \quad (\underline{A} \wedge \underline{C}_2 = (AC_2 \sin 0^\circ) \underline{n}_+)$$

$$= 0 \quad (\because \underline{A} \text{ and } \underline{C}_2 \text{ are parallel})$$

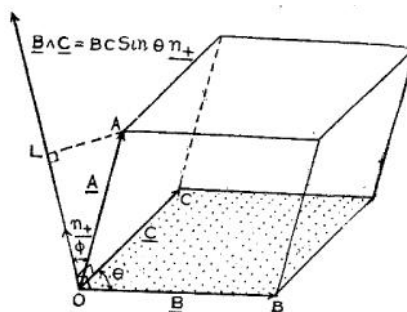
$$\underline{A} \wedge \underline{C} = \underline{A} \wedge (\underline{C}_1 + \underline{C}_2) = \underline{A} \wedge \underline{C}_1 \quad \text{since } \underline{A} \wedge \underline{C}_2 = 0$$

$\pm y \Delta D \sim \tilde{O} \frac{3}{4} \text{ } \circ \hat{A} \hat{C} \hat{A} \hat{O} \hat{o}, \underline{A}(\underline{B} \wedge \underline{C}) \pm y \Delta D \mu \pm \tilde{n} \frac{1}{2} \hat{O} \hat{A} \hat{O} \hat{i} \hat{C} \hat{A} \hat{O} \hat{o} \text{ p r } \hat{i}$
 $\underline{A}(\underline{B} \wedge \underline{C}) \pm y \hat{A} \hat{u} \hat{i} \pm \tilde{n} \hat{A} \hat{O} \hat{O} \hat{A} \hat{O} \hat{I} \hat{S} \hat{A} \hat{C} \hat{A} \hat{O} \hat{o}, \ll \frac{3}{4} \text{ } \hat{E} \hat{O} \hat{i} \hat{U} \hat{O} \hat{I} \pm \tilde{n} \frac{1}{2} \hat{O}$
 $\hat{A} \hat{O} \hat{i} \hat{C} \hat{A} \hat{O} \hat{o} \text{ (Scalar Triple Product) } \pm y \hat{U} \hat{U} \hat{U} \hat{A} \hat{D} \hat{A} \hat{i} \hat{O} \hat{O} \hat{D} \hat{o}. \hat{a} \hat{y} \hat{E} \hat{i} \hat{A} \hat{D}$
 $\hat{A} \hat{C} \hat{A} \hat{O} \hat{o} \pm \hat{i} \hat{O} \hat{A} \hat{C} \hat{A} \hat{O} \hat{o} \pm y \hat{E} \hat{A} \hat{O} \hat{i} \hat{C} \hat{A} \hat{O} \hat{o} \hat{i} \hat{O} \hat{A} \hat{i} \hat{O} \hat{u} \hat{C} \hat{A} \hat{O} \hat{o} \hat{A} \hat{C} \hat{A} \hat{O} \hat{o} \text{ p r } \hat{i} \hat{O} \hat{A} \hat{C} \hat{A} \hat{O} \hat{o}$
 $\pm y \Delta D \sim \tilde{O} \frac{3}{4} \text{ } \circ \hat{A} \hat{C} \hat{A} \hat{i} \hat{O} \hat{o}. \hat{C} \hat{A} \hat{C} \hat{A} \hat{O} \hat{o} \underline{A}(\underline{B} \wedge \underline{C}) \pm y \Delta D \sim \tilde{O} \frac{3}{4} \text{ } \circ \hat{A} \hat{C} \hat{A} \hat{i} \hat{O} \hat{o}$
 $\hat{i} \hat{U} \hat{i} \hat{O} \hat{A} \hat{O} \hat{i} \hat{C} \hat{A} \hat{O} \hat{o} \hat{A} \hat{i} \hat{O} \hat{E} \hat{O} \hat{i} \hat{O} \hat{o}. \text{ p r } \hat{i} \hat{O} \hat{A} \hat{C} \hat{A} \hat{O} \hat{o} \pm y \Delta D \sim \tilde{O} \frac{3}{4} \text{ } \circ \hat{A} \hat{C} \hat{A} \hat{i} \hat{O} \hat{o},$
 $\ll \frac{3}{4} \text{ } \hat{E} \hat{O} \hat{i} \hat{U} \hat{O} \hat{I} \hat{i} \hat{U} \hat{i} \hat{O} \hat{A} \hat{O} \hat{i} \hat{C} \hat{A} \hat{O} \hat{o} \ll \hat{O} \hat{A} \hat{D} \frac{3}{4} \text{ } \circ \hat{A} \hat{C} \hat{O} \hat{A} \hat{O} \hat{i} \hat{C} \hat{A} \hat{O} \hat{o} \text{ (Vector Triple}$
 $\text{product) } \pm y \hat{U} \hat{U} \hat{U} \hat{A} \hat{D} \hat{A} \hat{i} \hat{O} \hat{O} \hat{D} \hat{o}.$

[I È O O (A.B).C, (A.B) ^ C - C A A A i O C u E A]

1.19 (1) O i U O I ± n 1/2 O A O i C A y A C i x A
 A A O 3/4 A C A O, O ± y È O u C A O O A, O B, O C ± y È « O O i S j I u, A, B, C
 - C A 3/4 C A O C i I E O I O. (O B, O C) ± y A A O 3/4 C O 3/4 A A A U i I O.

« O 3/4 C O 3/4 U i I O i I O 3/4 i u x u C n ± ± y È μ A A I O 3/4 C O 3/4 A C (B ^ C) ± y È
 3/4 C O 3/4 A C O A A I O 3/4 C O 3/4 A i I E O I O. O B, O C, O A - C A A U i È
 A C O O C i i (Edges) i i n 1/4 μ ± È p 1/2 A O 3/4 (Paralleloid) A 1/4 O 1-31 O
 i O E A A i U A A A x O. O B, O C, U i I p 1/4 A C A A O O S j 1/2 O 3/4 " ± È i
 i i u C x O. (A, n ±) - C A 3/4 C O 3/4 U i I p 1/4 A C A A O O S j 1/2 O 3/4 W ± È i
 i i u C x O.



A 1/4 O 1-31

È p 1/2 A O 3/4 C « È O 3/4 C O A A O O O B. O C sin η, - I O. « 3/4 y i O i I O D
 - A A O O L = A n ± = O A cos w - I O.

S A O O, B ^ C = (O B. O C sin η) n ± - I O.

± È S A, A (B ^ C) = A (O B. O C sin η) n ±

$$= O B. O C \sin \eta (\underline{A} \cdot \underline{n} \pm)$$

$$O B. O C \sin \eta (O A \cdot \cos w)$$

= È p 1/2 A O 3/4 C A O A y - I O.

A, B, C ± y È 3/4 C O 3/4 A C u y U i i y U i O i I O 3/4 i p O i I A i E i O, " = 90°, w = 0°

$\neg \hat{1} \circ. \ll \hat{o} | \hat{A}_i \emptyset \mathcal{D},$

$$\begin{aligned} \underline{A} \cdot (\underline{B} \wedge \underline{C}) &= OA \cdot OB \cdot OC \\ &= \underset{\text{S}\hat{A}\hat{O}\hat{o}}{\underset{\text{S}\hat{A}\hat{O}\hat{o}}{\underset{\text{S}\hat{A}\hat{O}\hat{o}}{\hat{E} | \circ \hat{u} \hat{A} \circ \frac{3}{4} \hat{y} \hat{A}\hat{O}\hat{A}\hat{E} | \hat{1} \hat{o}.}}} \end{aligned}$$

$\underline{A} \cdot (\underline{B} \wedge \underline{C}) = (\underline{B} \wedge \underline{C}) \cdot \underline{A} = -\underline{A} \cdot (\underline{C} \wedge \underline{B}) = -(\underline{C} \wedge \underline{B}) \cdot \underline{A}$
 $= \underline{B} \cdot (\underline{C} \wedge \underline{A}) = (\underline{C} \wedge \underline{A}) \cdot \underline{B} = -\underline{B} \cdot (\underline{A} \wedge \underline{C}) = -(\underline{A} \wedge \underline{C}) \cdot \underline{B}$
 $= \underline{C} \cdot (\underline{A} \wedge \underline{B}) = (\underline{A} \wedge \underline{B}) \cdot \underline{C} = -\underline{C} \cdot (\underline{B} \wedge \underline{A}) = -(\underline{B} \wedge \underline{A}) \cdot \underline{C}$
 $= \underset{\text{S}\hat{A}\hat{O}\hat{o}}{\underset{\text{S}\hat{A}\hat{O}\hat{o}}{\underset{\text{S}\hat{A}\hat{O}\hat{o}}{\hat{E} | \circ \frac{1}{2} \hat{A} \circ \frac{3}{4} \hat{y} \hat{A}\hat{O}\hat{A}\hat{E} | \hat{1} \hat{o}.}}}$

$\text{p}\hat{r}\hat{i}\hat{l} \quad 12 \quad \text{O} \hat{\cdot} \hat{E} \text{, } \text{C} \hat{\emptyset} \quad \text{O}\hat{i} \hat{U} \hat{\mathcal{D}}\hat{I} \quad \pm \hat{n} \frac{1}{2} \hat{\omega} | \hat{A}\hat{O}\hat{i} \text{, } \text{C} \quad \pm \hat{\emptyset} \frac{3}{4} \hat{o} \hat{A} \hat{\mathcal{D}}\hat{I} \hat{u} \hat{\mathcal{C}} \hat{\mathcal{D}}.$
 $\ll \hat{A} \hat{u} \hat{E} \hat{y} \quad \hat{A} \frac{3}{4} \hat{\omega} \hat{0} \hat{u} \hat{A} \hat{i} \times \hat{o} \quad \hat{\circ} \hat{A} \hat{A} \hat{i} | \hat{1} \hat{o}. \quad \text{S}\hat{A}\hat{O}\hat{o} \quad \hat{0} \hat{u} \hat{\mathcal{C}} \hat{t}, \text{"} \text{"} \quad \hat{1} \hat{U} \hat{i} | \hat{1} \hat{o} | \hat{A}\hat{O}\hat{i} \text{, } \hat{\emptyset}$
 $\hat{1} \hat{E} \hat{c} \text{ - " } \wedge \text{ " } \quad \neg \hat{\mathcal{A}} \hat{A} \hat{u} \hat{\cdot} \hat{E} \hat{A} \hat{O} \hat{o} \hat{A} \hat{o} \hat{A} \hat{E} \hat{A} \hat{j} \hat{u} \hat{E} \hat{\mathcal{A}} \hat{\cdot} \hat{A} \hat{i} \quad \hat{A} \hat{j} \hat{o}. \quad \ll \hat{o} | \hat{A}_i \emptyset \mathcal{D} \hat{A}\hat{O}\hat{A}\hat{y}$
 $\hat{A} \frac{3}{4} \hat{\omega} \hat{A} \hat{\mathcal{C}} \times \hat{A} \hat{j} \hat{U} \hat{A} \frac{3}{4} \hat{\emptyset} \hat{\cdot} \hat{A}. \quad \neg \hat{E} \hat{j} \hat{\emptyset} \pm \hat{\emptyset} \hat{\mathcal{D}} \text{, } \text{C} \hat{\mathcal{Y}} \hat{A} \hat{j} \hat{\cdot} \hat{\circ} \quad \ll \hat{\cdot} \hat{A} \hat{\omega} \hat{0} \hat{\cdot} \hat{E} \text{, } \hat{j} | \hat{u} \hat{A} \frac{1}{4}$
 $\text{S}\hat{A}\hat{n} \hat{1} \hat{o}. \quad (\text{should be preserved.}) \quad \frac{2}{3} \hat{A} \hat{\mathcal{D}} \text{ p}\hat{O} \pm \hat{\emptyset} \hat{\mathcal{D}} \text{, } \hat{\cdot} \hat{\mathcal{C}} \quad \hat{\cdot} \hat{\mathcal{O}} \hat{\mathcal{O}} \hat{\cdot} \hat{E} \text{ p}\hat{1} \hat{o}$
 $| \hat{A} \hat{A} \hat{\cdot} \hat{\omega} \hat{\mathcal{A}} \hat{1} \hat{o} \hat{S} \hat{A} \hat{j} \hat{\mathcal{D}}, \quad \hat{1} \hat{E} \hat{\mathcal{A}} \hat{\emptyset} \hat{A} \hat{j} \hat{u} \hat{E} \hat{o} \quad (\text{change of sign}) \quad \hat{\mathcal{C}} \hat{u} \hat{A} \hat{\cdot} \frac{3}{4} \hat{O} \hat{o}, \text{ p}\hat{O} \hat{\mathcal{O}} \hat{\cdot} \hat{E}$
 $\text{p}\hat{1} \hat{o} | \hat{A} \hat{A} \hat{\cdot} \hat{\omega} \hat{\mathcal{A}} \hat{1} \hat{o} \hat{S} \hat{A} \hat{j} \hat{\mathcal{D}} \hat{1} \hat{E} \hat{\mathcal{C}} \hat{\cdot} \hat{A} \hat{\omega} \hat{0} \hat{o} \hat{A} \hat{\cdot} \frac{3}{4} \hat{O} \hat{o} \text{, } \hat{j} | \frac{1}{2} \hat{A} \hat{j} \hat{o}. \quad \neg \frac{3}{4} \hat{A} \hat{j} \hat{\emptyset}, \quad \text{O}\hat{i} \hat{U} \hat{\mathcal{D}}\hat{I}$
 $\pm \hat{n} \frac{1}{2} \hat{\omega} | \hat{A}\hat{O}\hat{i} \text{, } \text{C} \hat{\cdot} \hat{A} \quad [\underline{A}, \underline{B}, \underline{C}] \pm \hat{y} \hat{U} \hat{o} \hat{1} \hat{E} \hat{\omega} \hat{A} \hat{\mathcal{D}} \hat{A} \hat{E} \hat{i} \text{, } \hat{o}.$

$$\underline{A}, \underline{B}, \underline{C} \pm \hat{y} \hat{E} \hat{a} \hat{y} \hat{U} \frac{3}{4} \hat{\cdot} \hat{\circ} \hat{A} \hat{\mathcal{C}} \text{, } \hat{U} \hat{o} \quad \hat{\cdot} \hat{S} \hat{A} \frac{3}{4} \hat{\mathcal{C}} \hat{\omega} \hat{\mathcal{A}} \hat{\cdot} \hat{A} \hat{O} | \hat{A} \hat{y} \hat{E} \hat{j} \hat{\emptyset}, \quad \hat{E}$$

$\text{p}\hat{\cdot} \frac{1}{2} \hat{u} \hat{A} \hat{\omega} \hat{\mathcal{A}} \hat{y} \hat{A}\hat{O}\hat{A}\hat{y} \hat{1} \hat{E} \hat{\mathcal{A}} \hat{j} | \hat{1} \hat{o}.$
 $\ll \frac{3}{4} \hat{A} \hat{\mathcal{D}} \quad (\underline{B} \wedge \underline{C}) \pm \hat{y} \hat{E} \frac{3}{4} \hat{\cdot} \hat{\circ} \hat{A} \hat{\mathcal{C}} (\underline{B}, \underline{C}) \frac{3}{4} \hat{\mathcal{C}} \hat{\omega} \hat{\mathcal{A}} \hat{u} \hat{l} \hat{1} \hat{1} \hat{o} | \hat{1} \hat{o} \hat{3} \hat{4} \hat{E} \frac{3}{4} \hat{\cdot} \hat{\circ} \hat{A} \hat{\emptyset}$
 $| \hat{\circ} \hat{A} \hat{u} \hat{A} \hat{1} \hat{o}. \quad \underline{A} \pm \hat{y} \hat{E} \frac{3}{4} \hat{\cdot} \hat{\circ} \hat{A} \hat{\mathcal{C}} (\underline{B}, \underline{C}) \frac{3}{4} \hat{\mathcal{C}} \hat{\omega} \hat{\mathcal{A}} \hat{\cdot} \hat{A} \hat{A} \frac{3}{4} \hat{j} \hat{\emptyset}, \quad \underline{A} \cdot (\underline{B} \wedge \underline{C}) \neg \hat{\mathcal{A}} \hat{A} \hat{u} \hat{E} \hat{y}$
 $| \hat{\circ} \hat{A} \hat{u} \hat{A} \hat{1} \hat{o} \frac{3}{4} \hat{\cdot} \hat{\circ} \hat{u} \quad \hat{\cdot} \hat{y} \hat{U} \hat{i} | \hat{u} \hat{y} \hat{U} | \hat{o} | \hat{1} \hat{o} \hat{3} \hat{4} \hat{E} \hat{\cdot} \hat{A} \hat{A} \hat{j} | \hat{1} \hat{o}. \quad \pm \hat{E} \hat{S} \hat{A} \ll \hat{\cdot} \hat{A} \text{, } \text{C} \hat{\mathcal{Y}}$
 $\pm \hat{n} \frac{1}{2} \hat{\omega} | \hat{A}\hat{O}\hat{i} \text{, } \text{C} \quad \underline{A} \cdot (\underline{B} \wedge \underline{C}) = 0 \quad \neg \hat{1} \hat{o}.$

$\underline{A}, \underline{B}, \underline{C} \neg \hat{\mathcal{A}} \frac{3}{4} \hat{\cdot} \hat{\circ} \hat{\mathcal{C}} \hat{\emptyset}, \quad \frac{2}{3} \hat{S} \hat{3} \hat{4} \hat{U} \hat{o} \text{ p}\hat{O} \frac{3}{4} \hat{\cdot} \hat{\circ} \hat{A} \hat{\mathcal{C}} \hat{u} \quad \hat{\circ} \hat{A} \hat{A} \hat{j} \text{, } \text{p}\hat{O} \hat{i} | \hat{A} \hat{j} \hat{E} \hat{j} \hat{\emptyset},$
 $\ll \hat{\cdot} \hat{A} \text{, } \text{C} \hat{\mathcal{Y}} \pm \hat{n} \frac{1}{2} \hat{\omega} | \hat{A}\hat{O}\hat{i} \text{, } \text{C} \hat{1} \hat{E} \hat{\mathcal{A}} \hat{j} | \hat{1} \hat{o}.$

$$\begin{aligned} &\ll \frac{3}{4} \hat{A} \hat{\mathcal{D}} \quad \underline{A} = \underline{B} \quad \pm \hat{E} \hat{\emptyset}, \\ \underline{A} \cdot (\underline{B} \wedge \underline{C}) &= \underline{A} \cdot (\underline{A} \wedge \underline{C}) \\ &= (\underline{A} \wedge \underline{A}) \cdot \underline{C} \\ &= \underline{0} \cdot \underline{C} = 0 \quad \neg \hat{1} \hat{o}. \end{aligned}$$

$\underline{A}, \underline{B}, \underline{C} \neg \hat{\mathcal{A}} \hat{A} \hat{u} \hat{E} \hat{y} \quad \text{O}\hat{i} \hat{U} \hat{\mathcal{D}}\hat{I} \quad \pm \hat{n} \frac{1}{2} \hat{\omega} | \hat{A}\hat{O}\hat{i} \text{, } \hat{\mathcal{A}} \hat{y} \quad \hat{A} \frac{3}{4} \hat{\omega} \hat{\cdot} \hat{A}, \hat{i}, \hat{j}, \hat{k} \pm \hat{y} \hat{E}$
 $\mu \hat{A} \hat{A} \hat{1} \hat{o} \quad \hat{\omega} \hat{\mathcal{A}} \hat{\cdot} \hat{\circ} \hat{A} \hat{\mathcal{C}} \text{, } \hat{\cdot} \hat{\mathcal{C}} \hat{o} \hat{A} \hat{A} \hat{y} \hat{A} \hat{1} \hat{o} \hat{3} \hat{4} \hat{O} \hat{o} \hat{A} \hat{y} \hat{A} \hat{O} \hat{A} \hat{j} \hat{U} \hat{A} \hat{\cdot} \hat{A} \hat{A} \hat{U} \hat{i} \text{, } \hat{A} \hat{j} \hat{o}.$

$\hat{i}, \hat{j}, \hat{k} \pm \hat{y} \hat{E} \hat{A} \hat{A} \hat{o} \hat{0} \hat{E} \hat{1} \hat{1} \hat{o} \frac{1}{4} \hat{\cdot} \hat{A} \hat{o} \hat{0} \quad \text{O} \hat{\cdot} \hat{E} \hat{A} \hat{\emptyset} \quad (\text{Right Handed Frame of Reference}), \quad \underline{A}, \underline{B}, \underline{C} \pm \hat{y} \hat{E} \frac{3}{4} \hat{\cdot} \hat{\circ} \hat{A} \hat{\mathcal{C}} \text{, } \hat{\cdot} \hat{\mathcal{C}}$

$$\begin{aligned} \underline{A} &= A_x \hat{i} + A_y \hat{j} + A_z \hat{k} \\ \underline{B} &= B_x \hat{i} + B_y \hat{j} + B_z \hat{k} \\ \underline{C} &= C_x \hat{i} + C_y \hat{j} + C_z \hat{k} \quad \pm \hat{E} \hat{1} | \hat{u} \hat{\mathcal{C}} \times \hat{o}. \\ &\ll \hat{o} | \hat{A}_i \emptyset \mathcal{D}, \end{aligned}$$

$$\underline{B} \wedge \underline{C} = \begin{pmatrix} \underline{i} & \underline{j} & \underline{k} \\ B_x & B_y & B_z \\ C_x & C_y & C_z \end{pmatrix}$$

$$= (B_y C_z - B_z C_y) \underline{i} + (B_z C_x - B_x C_z) \underline{j} + (B_x C_y - B_y C_x) \underline{k} \quad \rightarrow \text{is } \vec{0}.$$

$$\rightarrow \text{is } \vec{0}, \underline{A} \cdot (\underline{B} \wedge \underline{C}) = (A_x \underline{i} + A_y \underline{j} + A_z \underline{k}) \cdot \{(B_y C_z - B_z C_y) \underline{i} + (B_z C_x - B_x C_z) \underline{j} + (B_x C_y - B_y C_x) \underline{k}\}$$

$$= A_x (B_y C_z - B_z C_y) + A_y (B_z C_x - B_x C_z) + A_z (B_x C_y - B_y C_x)$$

$$\begin{vmatrix} A_x & A_y & A_z \\ B_x & B_y & B_z \\ C_x & C_y & C_z \end{vmatrix} \rightarrow \text{is } \vec{0}.$$

1.20 Orthogonal System (Vector-Product of three vectors)

$\underline{A}, \underline{B}, \underline{C}$ are orthogonal vectors, $\underline{D} = \underline{A} \wedge (\underline{B} \wedge \underline{C})$ is orthogonal to $\underline{A}, \underline{B}, \underline{C}$.

$(\underline{B} \wedge \underline{C})$ is perpendicular to $\underline{B}, \underline{C}$. $\underline{A} \cdot (\underline{B} \wedge \underline{C}) = 0$.

$\therefore \underline{D} = \underline{A} \wedge (\underline{B} \wedge \underline{C})$ is perpendicular to $\underline{A}, \underline{B}, \underline{C}$.

$\ll \underline{D} \cdot \underline{A} = 0, \underline{D} \cdot \underline{B} = 0, \underline{D} \cdot \underline{C} = 0$.

$\ll \underline{D} \cdot \underline{D} = |\underline{D}|^2 = |\underline{A}|^2 |\underline{B} \wedge \underline{C}|^2$.

$$\underline{A} \wedge (\underline{B} \wedge \underline{C}) = m \underline{B} + n \underline{C} \quad \text{is } \vec{0}.$$

1.20(1) $\underline{A} \wedge (\underline{B} \wedge \underline{C})$ is orthogonal to $\underline{A}, \underline{B}, \underline{C}$

$\underline{A}, \underline{B}, \underline{C}$ are orthogonal vectors, $\underline{A} \cdot \underline{B} = 0, \underline{A} \cdot \underline{C} = 0, \underline{B} \cdot \underline{C} = 0$.

$$\underline{A} = A_x \underline{i} + A_y \underline{j} + A_z \underline{k}$$

$$\underline{B} = B_x \underline{i} + B_y \underline{j} + B_z \underline{k}$$

$$\underline{C} = C_x \underline{i} + C_y \underline{j} + C_z \underline{k}$$

$$\therefore \underline{A} \wedge (\underline{B} \wedge \underline{C}) = (A_x \underline{i} + A_y \underline{j} + A_z \underline{k}) \wedge \begin{pmatrix} \underline{i} & \underline{j} & \underline{k} \\ B_x & B_y & B_z \\ C_x & C_y & C_z \end{pmatrix}$$

$$= (A_x \underline{i} + A_y \underline{j} + A_z \underline{k}) \wedge \{(B_y C_z - B_z C_y) \underline{i} + (B_z C_x - B_x C_z) \underline{j} + (B_x C_y - B_y C_x) \underline{k}\}$$

$$= \begin{pmatrix} \underline{i} & \underline{j} & \underline{k} \\ A_x & A_y & A_z \\ B_y C_z - B_z C_y & B_z C_x - B_x C_z & B_x C_y - B_y C_x \end{pmatrix}$$

$$= \{A_y (B_x C_y - B_y C_x) - A_z (B_z C_x - B_x C_z)\} \underline{i}$$

$$\begin{aligned}
& + \{A_z(B_y C_z - B_z C_y) - A_x(B_x C_y - B_y C_x)\} \underline{j} \\
& + \{A_x(B_z C_x - B_x C_z) - A_y(B_y C_z - B_z C_y)\} \underline{k} \\
= & (A_x C_x + A_x C_x + A_x C_x) B_x \underline{i} - A_x B_x C_x \underline{i} \\
& + (A_x C_x + A_x C_x + A_x C_x) B_y \underline{j} - A_y B_y C_y \underline{j} \\
& + (A_x C_x + A_x C_x + A_x C_x) B_z \underline{k} - A_z B_z C_z \underline{k} \\
& - (A_x B_x + A_y B_y + A_z B_z) C_x \underline{i} + A_x B_x C_x \underline{i} \\
& - (A_x B_x + A_y B_y + A_z B_z) C_y \underline{j} + A_y B_y C_y \underline{j} \\
& - (A_x B_x + A_y B_y + A_z B_z) C_z \underline{k} + A_z B_z C_z \underline{k} \\
= & (\underline{A.C})(B_x \underline{i} + B_y \underline{j} + B_z \underline{k}) - (\underline{A.B})(C_x \underline{i} + C_y \underline{j} + C_z \underline{k}) \\
\therefore & \underline{A} \wedge (\underline{B} \wedge \underline{C}) = (\underline{A.C}) \underline{B} - (\underline{A.B}) \underline{C} \quad \square \quad \text{ò.}
\end{aligned}$$

$\underline{A} \wedge (\underline{B} \wedge \underline{C}) \pm \dot{y} \dot{E} \frac{3}{4} \dot{C} \cdot \circ \hat{A} \dot{C} \cdot (\underline{B.C}) \frac{3}{4} \dot{C} \dot{\delta} \frac{3}{4} \dot{U} \dot{I} \quad \text{p} \cdot \frac{1}{2} \hat{A} \dot{I} \cdot \hat{I} \quad | \quad \circ \hat{A} \dot{U} \hat{A} \dot{I} \quad \text{o} \cdot \quad \neg \dot{E} \dot{I} \dot{\delta}$
 $(\underline{A} \wedge \underline{B}) \wedge \underline{C} \pm \dot{y} \dot{E} \frac{3}{4} \dot{C} \cdot \circ \hat{A} \dot{C} \cdot (\underline{A.B}) \frac{3}{4} \dot{C} \dot{\delta} \frac{3}{4} \dot{U} \dot{I} \quad \text{p} \cdot \frac{1}{2} \hat{A} \dot{I} \cdot \hat{I} \quad | \quad \circ \hat{A} \dot{U} \hat{A} \dot{I} \quad \text{o} \cdot \quad \pm \dot{E} \dot{S} \dot{A}$
 $\ll \cdot \cdot \hat{A} \cdot \dot{U} \text{ p} \hat{A} \hat{n} \hat{I} \text{ o} \cdot \circ \hat{A} \dot{A} \dot{I} \cdot \dot{I} \dot{D} \cdot$
 $\neg \frac{3}{4} \dot{A} \dot{I} \dot{\delta} \cdot \underline{A} \wedge (\underline{B} \wedge \underline{C}) \neq (\underline{A} \wedge \underline{B}) \wedge \underline{C}$
 $\ll \frac{3}{4} \dot{I} \hat{A} \dot{D} \frac{3}{4} \dot{C} \cdot \circ \hat{A} \dot{C} \cdot \hat{I} \dot{U} \dot{I} \dot{\delta} | \hat{A} \dot{O} \dot{I} \cdot \dot{C} \cdot \text{p} \hat{A} \dot{U} \cdot \frac{1}{2} \dot{\delta} \hat{I} \quad \dot{U} \dot{D} \hat{I} \hat{I} \dot{S} \circ \dot{I} \cdot \cdot \cdot \hat{A} \dot{C} \dot{I} \dot{I}$
 $\dot{\delta} \hat{D} \hat{A} \hat{O} \hat{A} \frac{3}{4} \dot{C} \cdot \cdot \hat{A} \cdot$

1.20 (2) $\frac{3}{4} \dot{C} \cdot \circ \hat{A} \dot{C} \cdot \hat{O} \hat{o} | \hat{A} \dot{O} \dot{I} \cdot \dot{C} \dot{A} \dot{y} \hat{A} \cdot \dot{C} \cdot \times \cdot \cdot \dot{C} \pm \dot{C} \hat{A} \dot{O} \cdot \cdot \hat{E} \hat{A} \dot{C} \cdot \frac{3}{4} \dot{O} \hat{A} \dot{C} \cdot \frac{3}{4} \dot{C} \cdot$
 $\dot{O} \hat{I} \hat{E} \hat{O} \hat{A} \dot{C} \cdot \frac{1}{4} \hat{I} \dot{\delta} \frac{1}{4} \cdot \hat{A} \dot{O} \cdot \cdot \hat{A} \dot{O} \dot{S} \frac{3}{4} \dot{\delta} \hat{O} | \frac{3}{4} \hat{I} \dot{\delta} \hat{D} \cdot \underline{A}, \underline{B}, \underline{C} \pm \dot{y} \dot{U} \dot{\delta} \frac{3}{4} \dot{C} \cdot \circ \hat{A} \dot{C} \cdot \dot{C} \dot{y}$
 $\hat{A} \cdot \dot{C} \cdot \times \cdot \cdot \dot{C} \ll \cdot \cdot \hat{A} \dot{O} \dot{D} \cdot \frac{3}{4} \dot{C} \cdot \circ \hat{A} \dot{C} \cdot \hat{O} \hat{o} | \hat{A} \dot{O} \dot{I} \cdot \dot{C} \dot{A} \dot{y} \quad \circ \hat{A} \dot{y} \hat{A} \cdot \dot{C} \cdot \frac{1}{4} \pm \dot{C} \hat{A} \dot{O} \cdot \cdot \hat{E} \hat{A} \dot{C} \cdot$
 $\hat{A} \dot{y} \hat{A} \cdot \dot{C} \cdot \dot{U} \dot{U} \hat{A} \cdot \dot{C} \cdot \text{o} \cdot$

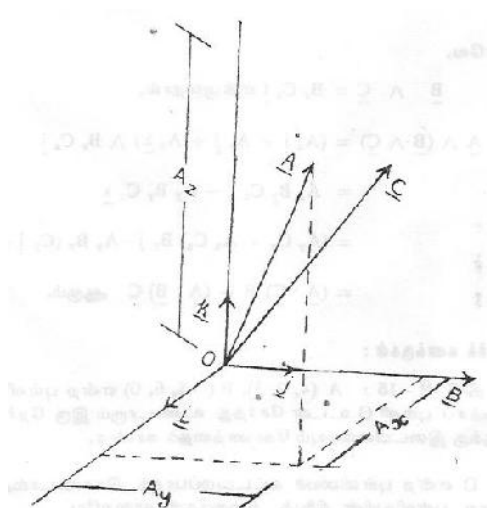


Figure 1-32

$\underline{B} = B_x \hat{i} + B_y \hat{j} + B_z \hat{k}$, $\underline{j} = j_x \hat{i} + j_y \hat{j} + j_z \hat{k}$, $\underline{C} = C_x \hat{i} + C_y \hat{j} + C_z \hat{k}$, $\underline{A} = A_x \hat{i} + A_y \hat{j} + A_z \hat{k}$.

$$\underline{B} = B_y \hat{j}$$

$$\underline{C} = C_y \hat{j} - C_z \hat{k}$$

$$\underline{A} = A_x \hat{i} + A_y \hat{j} + A_z \hat{k}$$

$$\underline{B} \cdot \underline{C} = B_y C_y - C_z^2$$

$$\underline{B} \cdot \underline{A} = A_y B_y$$

$$\underline{B} \wedge \underline{C} = B_y C_z \hat{i} - B_z C_y \hat{j}$$

$$\underline{A} \wedge (\underline{B} \wedge \underline{C}) = (A_x \hat{i} + A_y \hat{j} + A_z \hat{k}) \wedge B_y C_z \hat{i} - A_y B_z C_y \hat{j}$$

$$= A_x B_y C_z \hat{j} - A_y B_z C_y \hat{k}$$

$$= (A_x C_z - A_z C_x) B_y \hat{j} - A_y (B_z C_x - B_x C_z) \hat{k}$$

$$= (\underline{A} \cdot \underline{C}) \underline{B} - (\underline{A} \cdot \underline{B}) \underline{C}$$

1.21 Forces

Forces are vectors acting on a particle. They can be added to find the net force.

1.21.1 Nature of a force

Forces can be classified into different types based on their point of application and direction.

Body forces (e.g., gravity) act on the entire volume of a body. Contact forces (e.g., tension, friction) act at the point of contact. Surface forces act along the surface of a body.

!ÀðÊÃø « " È " Çî °iÇÃ |ÀjÏðÐÃ¼ø « øÄÐ ¾ÈòÀ¾ø Æ" °ÃjÉÐ
§¾" ÅòÃð¼ ¾ç" °Ãø |°ÄüÃî ò -Ãjõ×Ãç" ° |ÀjÏù þÃí î ò ¾ç" °î î
±¾ç-òðÈð¾ø |°ÃøÃî ÇÐ,

§ÄüÛÈÃ ±î òðì |ðî ÇçÉjø Æ" °ÃjÉÐ " Ò î ÈòÃø¼ ¾ç" °" Å
§çjî Ç |°ÃøÃî ÅÐ ÒÃÈj î.

§ÄÏò Æ" ° Ùî î ±ñ Å¾òð, Ùò - ñ î.

|Àðjî Ó" ÈÃø Æ" °Ãý µÃÃî Çjò ±" ¼Ãj î. ÒÃÆèòð « Æî
Ó" ÈÃø « ¾ýÃ¾òð 9.81 çäð¼ý Çj î, Æçð¼ý Ó" ÈÃø Æ" °Ãý
µÃÃî Å×½î ±" ¼Ãj î. « Ð 4.45 çäð¼ý ±" ¼, Ùî î î °Ãj î.

Æ" ° Ùî î ±ñ Å¾òð |°ÄüÃî ò ¾ç" °Ïò - ùÇ¾j" Åjø
« " Å " Çò ¾ç" °Ãç Çjø (vectors) « ÈÃî ÓÈÏò. |ÀjÐÃj " Ò Æ" °" Å
Å" ÅÄÛî « ¾ý ±ñ Å¾òð (magnitude) |°ÃøÃî ò ¾ç" °(Direction)
|°ÃøÃî ò òùÇç (point of application) - Ç" Å §¾" ÅòÃî ò. §ÄüÛÈÃ 1,3
±î òðì |ðî Çç |°ÃøÃî ò òùÇç, ¾ç" °Ãç-ý ÐÃì òðùÇçÃÏò 2,4
±î òðì |ðî Çç |°ÃøÃî òðùÇç ¾ç" °Ãç-ý ÑÈòðùÇçÃÏò « " Å ÇÐ.

1.21.2 Ð, ù, Ùò þÛî, ò |ÀjÏù, Ùò (Particles and Rigid bodies)

þÃó¾ÃÃÃø ÒðÐ, ù, Æ" ° Çjø |°ÄüÃðî þÃí Çî ò |ÀjÏù, ù
±ÐÃj, Òò « " Å Ç" Èððì î |ÀjÐÃj, þÏî î. þÃó¾ÃÃÃø ÒðÐ, ù,
§çjðÃj, ù - Ç" Åü" È ±ÇÃÓ" ÈÃø Æçj, ¼, |ÀjÏù, Ç" Èð" ¾Ïò
Ð, ù Çj, §Äüj, jüÅÐ Æèj. þí î Ð, ù ±ýÅÐ " Ò |ÀjÏçý
½¾ÃÃø - ÒÃðÈÃø(Mathematical model)- î. |ÀjÏù Çý - ÒÃð,
ÃjÇj ½ò - Ç" Å - ñ " ÅÃø |ÀjÇ" ÅÃj « øÄÐ °ÈÃ" ÅÃj, þÏó¾
§Ãj¾Ïò Ýúç" Å Ùî î çüÈÃjÛ « " Å " Çò Ð, ù Çj, î Ò¾§Ãñ î.

±î òðì |ð¼j, µ± ° øî ñ Èý ÆjÇj ½ò, ° °Ãý ççò" ¾
§çj î î §ÃjÐ Æç î °ÈÃ¾j, - ùÇÐ. « ùÃj§È ÆjÉð¾ø íüÈî §çjü, « ¾ý
íüÛòÃj" ¾Ãý ÆjÇj ½òð¼ý "òÃî ò§ÃjÐ Æç î °ÈÃ¾j, çü òÃî ò. §ÄÏò
|¾j î î |ÀjÏù, ù ¾jüòÃjü, Æ" È - ½ç, ù Ó¾ÃÃ þÛî, ç, ù « " Èððò
ç" ÅÃÃø Ð, ù Çj, î Ò¾òÃî.

|ÀjÐÃj, Ð Çý ç" Å " Ò òùÇçjø î Èç, òÃî ò. - Èjø
ç" ¼ò" ÈÃø Ð Çý §çjðÃj, " Çò Æò |ÀjÏ" Çî °i÷¾
ÃÃî °ç" È Ùî î ÆÃýÃî òðò§ÃjÐ Æò |ÀjÏù Ð, ù§Ãjø |°ÃøÃî Æ¾j, î
|jüÇòÃî Æ¾jø ç" ¼î î Æç" Ç× ù, - ñ " ÅÃj, ççÈj ÛÈÃ
Æç" Ç× Çý §¾j, ÆjÇj, î |jüÇòÃî ò. þüÃ¾î, ÒðÐ þÃó¾ÃÃÃý
î Èç §çjü |çÈç Çç ýÈj î.

°Ã °ÃÃî Çç |ÀjÏçjÉÐ, Ð Çj, î Ò¾ÓÈÃ¾ çç" ÅÃÃÏî Æjò.
« ò§ÃjÐ |ÀjÏçjÉÐ |°Ãø, ±¾ç-|°Ãø Æç" ÇÃî î Ð, ù Çý ÈÃj, î
|jüÇòÃî ò. « ó¾ çç" Å Çç Ð, ù ù ýÛî |jýÛ þ½î Æj, ò
Æç" ½î òÃî ò, Ð, ù Ùî î ùç þ" ¼ð |¾j" Å× ù ÆjÈj, Æòò
þÏî î Ûî ÆjÉ¾jø |ÀjÏ" Ç þÛî, ò |ÀjÏçj, î (Rigid Body) Ò¾
§Ãñ î. - óÐÃñ È, ç½ç, òð¼í, ù (frames) þÃó¾Ãò Æj ¾ç, ù - Ç" Å
þÛî, ò |ÀjÏù Ùî î " Ò °Ã ±î òðì |ðî Çj î.

þÃó¾ÃÃÃø ±ýÅÐ |ÀjÏù Çý þÃí, ò" ¾ò ÆüÈç ÙÛ ÇÐ ±Èj
ÛÈòÃð¼Ð. §ÄÏò þÃó¾ÃÃÃø þÃí, ò¾ü î |jü½j, - ùÇ
Æç" °, " Çò ÆüÈòò « ÈÃjò. " Ò çç" ÅÃjÉ òùÇç" Æò |ÀjÛðð " Ò

$\mu\text{O}^{\text{A}^{\text{O}}}$ (« $\frac{3}{4}\text{A}^{\text{D}} \text{S}^{\text{A}} \ll \text{A}^{\text{A}^{\text{O}}}$) $\text{pO}^{\text{O}}\text{A}^{\frac{3}{4}}\text{i}$ i i $\text{u}\text{C}^{\text{O}}\text{A}^{\text{I}} \text{o}$. $\neg \text{E}^{\text{i}}\text{o}$
 $\text{Y}^{\text{i}}\text{A}^{\text{E}} \text{I}^{\text{O}} \frac{1}{4} \text{A}^{\text{O}}\text{A}^{\text{i}} \text{i}$ i i i n $\frac{1}{4}\text{i}$ o « $\text{o}^{\text{i}}\text{A}^{\text{i}}\text{O}^{\text{u}}$ $\mu\text{O}^{\text{A}^{\text{O}}}\text{O}^{\text{O}}\text{A}^{\frac{3}{4}}\text{O}^{\text{A}^{\text{O}}}$ A .
 $\text{pA}^{\text{i}} \text{A}^{\text{A}^{\text{O}}}$, $\text{O}^{\text{A}^{\text{S}}}\text{A}^{\text{I}} \text{O}^{\text{A}^{\text{i}}}$ $\text{O}^{\frac{3}{4}}\text{O}^{\text{A}^{\text{I}}}$ o . $\text{A}^{\text{O}}\text{A}^{\text{E}}\text{y}^{\text{A}^{\text{O}}}$ u
 $\text{u}^{\text{i}}\text{A}^{\text{i}}\text{y}^{\text{E}} \text{O}^{\text{O}} \text{u}^{\text{U}} \text{A}^{\text{C}}\text{A}^{\text{i}}$ i i i i n $\frac{1}{4}\text{A}^{\text{i}}\text{U} - \text{A}^{\text{i}}\text{O}^{\text{O}}\frac{3}{4}\text{A}^{\text{i}}\text{o}$.

1.21.3 (1) $\text{O}^{\frac{3}{4}}\text{O}^{\text{A}^{\text{O}}}$

$\text{pU}^{\text{A}^{\text{O}}}\text{A}^{\text{C}} \text{pO}^{\text{O}}\text{A}^{\text{C}} - \text{A}^{\text{i}}\text{A}^{\text{A}^{\text{i}}}\text{o}$. $\text{y}^{\text{U}} \ll \text{A}^{\text{A}^{\text{O}}}$ $\text{pO}^{\text{I}}\text{i} \text{o}$
 o $\text{A}^{\text{i}}\text{O}^{\text{u}}$, $\text{O}^{\text{E}^{\text{A}^{\text{O}}}}$ $\text{A}^{\text{i}}\text{y}^{\text{U}}$ $\text{A}^{\text{u}}\text{A}^{\text{I}} \text{o}^{\text{A}}$ $\text{A} \pm \text{O}^{\text{S}}\text{A}^{\text{i}}\text{D}^{\text{O}} \ll \text{A}^{\text{A}^{\text{O}}}$ $\text{A}^{\text{A}^{\text{S}}}\text{A}^{\text{S}}\text{A}^{\text{A}}$
 $\text{pO}^{\text{I}}\text{i} \text{o}$. $\text{A}^{\text{u}}\text{E}^{\text{i}}\text{y}^{\text{U}}$, $\text{A}^{\text{i}}\text{E}^{\frac{3}{4}}$ $\text{O}^{\text{S}}\text{A}^{\text{O}}\text{D}^{\frac{1}{4}}\text{y}^{\text{O}}$ $\text{S}^{\text{i}}\text{S}^{\text{i}}\text{D}^{\text{E}}\text{o}$ $\text{pA}^{\text{i}}\text{i} \text{o}$ O
 $\text{A}^{\text{i}}\text{O}^{\text{u}}$, $\text{O}^{\text{E}^{\text{A}^{\text{O}}}}$ y^{U} $\text{A}^{\text{u}}\text{A}^{\text{I}} \text{o}^{\text{A}}$, « $\text{S}^{\frac{3}{4}} \text{S}^{\text{i}}\text{S}^{\text{i}}\text{D}^{\text{E}}\text{o} \ll \text{S}^{\frac{3}{4}} \text{S}^{\text{A}} \text{O}^{\text{D}^{\frac{1}{4}}}\text{y}^{\text{O}}$
 $\pm \text{O}^{\text{S}}\text{A}^{\text{i}}\text{D}^{\text{O}} \text{pA}^{\text{i}}\text{i} \text{o}$. $\text{pU}^{\text{A}^{\text{O}}}$ $\text{A}^{\text{C}}\text{y}^{\text{O}}$ n A^{A} « $\text{y}^{\text{E}}\text{i} \frac{1}{4}$ $\text{u}^{\text{i}}\text{o}$ u
 $\text{A}^{\text{i}}\text{A}^{\text{C}}\text{A}^{\text{i}}$ $\text{A}^{\text{C}}\text{i}$ $\frac{1}{4}\text{A}^{\text{i}}\text{o}$. $\pm \text{I}^{\text{O}}\text{D}^{\text{i}}$ i $\text{O}^{\frac{1}{4}}\text{i}$, S^{A} $\text{O}^{\text{A}}\text{y}^{\text{A}^{\text{D}}}$ A^{i} $\text{O}^{\text{A}}\text{O}^{\frac{1}{4}}$ $\text{A}^{\text{O}}\text{A}^{\text{O}}\text{D}$,
« $\text{O}^{\frac{3}{4}}$ $\text{O}^{\text{A}^{\text{O}}}$ $\text{O}^{\frac{3}{4}}\text{i}$ $\text{O}^{\text{I}} \text{E}^{\text{i}}\text{y}^{\text{E}} \ll \text{O}^{\text{A}^{\text{O}}}$ A . $\text{S}^{\text{A}}\text{O}^{\text{O}}$ $\frac{3}{4}\text{C}^{\text{O}}$ $\text{y}^{\text{E}}\text{O}$ S^{A}
 $\text{S}^{\text{A}} \text{O}^{\frac{3}{4}}\text{O}^{\text{O}}$ y^{U} i n $\text{E}^{\text{O}}\text{i} \text{o}$ $\text{A}^{\text{O}}\text{A}^{\text{O}}\text{D}$ y^{U} $\text{O}^{\text{A}^{\text{A}}}\text{E}^{\text{O}}$, $\text{A}^{\text{i}}\text{o}^{\text{x}}$, u^{U}
 $\text{O}^{\frac{3}{4}}\text{A}^{\text{A}}$ A^{C} $\text{C}^{\text{i}}\text{o}$ $\frac{3}{4}\text{i}$ $\frac{1}{4}$ $\frac{1}{4}\text{A}^{\text{u}}\text{U}$ $\text{pO}^{\text{I}}\text{i} \text{A}^{\text{i}}\text{o}$ « D $\text{u}^{\text{i}}\text{A}^{\text{O}}$, « $\text{S}^{\frac{3}{4}}$
 $\text{S}^{\text{A}} \text{O}^{\frac{3}{4}}\text{O}^{\text{O}}$, $\frac{3}{4}\text{C}^{\text{O}}\frac{3}{4}\text{O}^{\text{O}}$ y^{U} i n $\text{S}^{\frac{1}{4}}\text{A}^{\text{O}}\text{i} \text{o}$. $\neg \text{E}^{\text{i}}\text{o}$ « $\text{U}^{\text{A}}\text{O}^{\frac{3}{4}}\text{O}^{\text{O}}$ $\text{A}^{\text{O}}\text{A}^{\text{O}}\text{y}^{\text{O}}$
 $\text{S}^{\text{A}}\text{O}$ $\text{S}^{\text{A}}\text{u}^{\text{U}}\text{E}^{\text{A}}$ $\text{O}^{\text{E}^{\text{A}^{\text{O}}}}$ u $\text{A}^{\text{u}}\text{A}^{\text{I}} \text{A}^{\frac{3}{4}}\text{O}$ $\frac{3}{4}\text{i}$ $\text{O}^{\text{E}^{\text{A}}}\frac{3}{4}\text{i}$ o « D $\text{u}^{\text{U}}\text{O}$
 $\frac{3}{4}\text{i}$ A^{x} $\text{y}^{\text{E}}\text{A}^{\text{y}}$ $\text{y}^{\text{U}}\text{A}^{\text{I}} \text{o}$. $\pm \text{E}^{\text{S}}\text{A}^{\text{O}^{\frac{3}{4}}}\text{A}^{\text{i}}\text{D}^{\text{A}^{\text{O}}}$ $\text{pU}^{\text{A}^{\text{O}}}$ $\text{u}^{\text{i}}\text{o}$ C^{i}
 u^{A} $\text{E}^{\text{A}^{\text{i}}}$ i i i n $\frac{1}{4}\text{i}$ y , $\text{O}^{\text{E}^{\text{i}}}$ $\frac{1}{2}\text{i}$ $\text{O}^{\text{A}^{\frac{1}{4}}}\text{A}^{\text{O}}$ $\text{u}^{\text{U}}\text{i}$ i i $\text{u}^{\text{C}}\text{O}^{\frac{3}{4}}\text{i}$ $\frac{3}{4}\text{i}$
 $\text{u}^{\text{C}}\text{D}$.

$\text{O}^{\frac{3}{4}}\text{O}^{\text{A}^{\text{O}}}\text{A}^{\text{C}}\text{O}^{\text{O}}\text{D} \pm \text{O}^{\text{i}}\text{A}^{\text{i}}\text{O}^{\text{U}} \text{o} \ll \frac{3}{4}\text{y}^{\text{O}}$ A^{A} A^{O} $\frac{3}{4}\text{i}$ E^{i} S^{A} $\text{A}^{\text{i}}\text{u}^{\text{E}}\text{I}$
 i i $\text{u}^{\text{C}}\text{O}^{\text{E}^{\text{A}}}\text{i}^{\text{D}}$ $\pm \text{y}^{\text{A}}\text{D}$ $\frac{1}{4}\text{i}$ o A^{U} E^{D} . $\text{pU}^{\text{A}^{\text{O}}}$ A^{n} O $\text{A}^{\text{A}}\text{o}$
(inertia) $\pm \text{y}^{\text{U}}$ $\text{U}^{\text{E}}\text{O}^{\text{A}^{\text{I}}}$ o . $\text{S}^{\text{A}}\text{O}^{\text{O}}$, « $\text{o}^{\text{i}}\text{A}^{\text{i}}\text{O}^{\text{u}}$ « $\text{A}^{\text{A}^{\text{O}}}$
(equilibrium) $\text{pO}^{\text{O}}\text{A}^{\frac{3}{4}}\text{i}$ x^{O} $\text{U}^{\text{E}}\text{O}^{\text{A}^{\text{I}}}$ o . « $\frac{3}{4}\text{i}$ A^{D} « $\text{A}^{\text{A}^{\text{O}}}$ A^{i} i A^{A} E ,
 $\frac{3}{4}\text{i}$ $\text{A}^{\text{A}}\text{y}^{\text{O}}$ $\text{A}^{\text{A}^{\text{O}}}$ (Net resultant force) $\text{I}^{\text{E}}\text{A}^{\text{i}}$, $\text{S}^{\text{A}}\text{n}$ $\text{i} \text{o}$ $\pm \text{y}^{\text{A}}$ $\frac{3}{4}\text{O}^{\text{O}}$
 $\text{A}^{\text{A}}\text{O}^{\text{U}}\text{O}^{\text{D}}$ E^{D} .

$\text{A}^{\text{i}}\text{O}^{\text{C}}\text{y}^{\text{S}^{\text{A}}\text{O}}$ $\text{A}^{\text{u}}\text{A}^{\text{I}} \text{o}$ $\text{A}^{\text{A}^{\text{O}}}$ $\text{I}^{\text{E}}\text{A}^{\text{i}}$ pO^{I} $\text{S}^{\text{A}}\text{n}$ $\text{i} \text{o}$ $\pm \text{y}^{\text{E}}$
 $\text{A}^{\text{O}}\frac{3}{4}$ E , $\text{A}^{\text{i}}\text{O}^{\text{u}}$ « $\text{A}^{\text{A}^{\text{O}}}$ $\text{A}^{\text{A}^{\text{O}}}\text{O}^{\text{O}}\text{A}^{\frac{3}{4}}\text{u}^{\text{i}} \text{o}$ $\text{S}^{\text{A}}\text{i}^{\text{D}}\text{A}^{\text{i}}\text{E}^{\frac{3}{4}}\text{O}^{\text{A}}$ $\pm \text{y}^{\text{A}}$ $\frac{3}{4}\text{O}^{\text{O}}$
 $\text{A}^{\text{E}}\frac{3}{4}\text{u}$ i i $\text{u}^{\text{C}}\text{S}^{\text{A}}\text{n}$ $\text{i} \text{o}$. (The net force acting on a rigid body must be
equal to zero is not enough to ensure its equilibrium) equilibrium $\pm \text{y}^{\text{E}}$
 $\neg \text{i}$ A^{i} i o $\text{pA}^{\text{O}}\frac{3}{4}\text{y}$ $\text{A}^{\text{i}}\text{E}^{\text{A}^{\text{O}}}\text{O}^{\text{O}}\text{D}$ $\text{A}^{\text{E}}\text{O}^{\text{A}^{\text{O}}}\text{i}$ $\text{u}^{\text{C}}\text{D}$. $\text{pA}^{\text{O}}\frac{3}{4}\text{y}$ $\text{A}^{\text{i}}\text{E}^{\text{A}^{\text{O}}}$
aequus $\pm \text{y}^{\text{E}}\text{i}$ o equal A^{O} $\pm \text{y}^{\text{U}}\text{o}$, libra $\pm \text{y}^{\text{E}}\text{i}$ o balance $\text{A}^{\text{A}^{\text{O}}}$ $\text{A}^{\text{A}^{\text{O}}}$
 $\text{A}^{\text{i}}\text{O}^{\text{u}}\text{A}^{\text{I}} \text{o}$. $\neg \text{S}^{\text{A}}$ $\text{A}^{\text{i}}\text{O}^{\text{u}}$ « $\text{A}^{\text{A}^{\text{O}}}\text{A}^{\text{i}}$, $\text{pO}^{\text{O}}\text{A}^{\frac{3}{4}}\text{i}$ $\text{O}^{\text{A}^{\text{O}}}$ $\text{A}^{\text{A}^{\text{O}}}$ $\text{pO}^{\text{O}}\text{A}^{\frac{3}{4}}\text{i}$,
 $\text{S}^{\text{A}}\text{u}$ i i $\text{u}^{\text{C}}\text{S}^{\text{A}}\text{n}$ $\text{i} \text{o}$.

$\text{S}^{\text{A}}\text{O}^{\text{O}}$ $\text{A}^{\text{A}^{\text{O}}}$ $\pm \text{y}^{\text{A}}\text{D}$ $\pm \text{y}^{\text{E}}$ $\pm \text{y}^{\text{U}}\text{o}$ $\text{O}^{\frac{3}{4}}\text{O}^{\text{A}^{\text{O}}}\text{A}^{\text{C}}\text{O}^{\text{O}}\text{D}$ $\text{A}^{\text{A}^{\text{O}}}$ $\text{A}^{\text{u}}\text{i}$ $\text{A}^{\text{i}}\text{o}$.

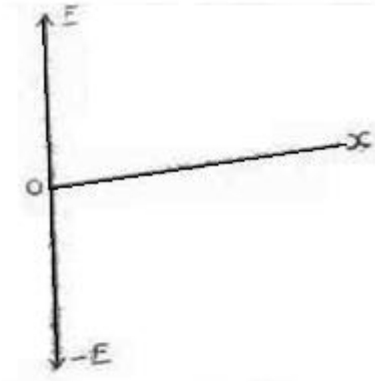
$\text{A}^{\text{A}^{\text{O}}}$ $\pm \text{y}^{\text{A}}\text{D}$ « $\text{A}^{\text{A}^{\text{O}}}$ $\text{A}^{\text{A}^{\text{O}}}$ « $\text{O}^{\text{A}^{\text{D}}}$ $\text{S}^{\text{i}}\text{S}^{\text{i}}\text{D}^{\text{E}}\text{o}$ $\text{A}^{\text{i}}\text{E}^{\frac{3}{4}}$ $\text{O}^{\text{S}}\text{A}^{\text{O}}$
 $\text{A}^{\text{A}^{\text{O}}}\text{O}^{\text{u}}\text{C}$ $\text{A}^{\text{i}}\text{O}^{\text{u}}$ $\text{y}^{\text{E}}\text{O}$ $\text{A}^{\text{u}}\text{A}^{\text{O}}\text{I}$ « o^{i} A^{A} $\text{A}^{\text{i}}\text{u}^{\text{E}}\text{I} \text{o}$ O^{O} A^{i} o .

O^{O} $\text{A}^{\text{A}^{\text{O}}}$ $\text{A}^{\text{A}^{\text{O}}}$ $\text{A}^{\text{u}}\text{i}$ o $\text{A}^{\text{y}}\text{A}^{\text{O}}\text{o}$ $\text{A}^{\text{A}^{\text{A}}}\text{i}$ $\text{u}^{\text{S}^{\frac{3}{4}}}$ $\text{A}^{\text{O}}\text{A}^{\text{I}} \text{o}$:

- (i) $\frac{3}{4}\text{i}$ $\text{O}^{\frac{3}{4}}$ « A^{i} $\text{S}^{\text{i}}\text{A}^{\text{O}}$ $\text{A}^{\text{A}^{\text{O}}}$ $\text{A}^{\text{A}^{\text{O}}}$ $\pm \text{n}$ $\text{A}^{\frac{3}{4}}\text{O}^{\text{O}}$,
- (ii) $\text{pA}^{\text{i}}\text{i} \text{o}$ $\frac{3}{4}\text{O}^{\text{O}}$ (« $\frac{3}{4}\text{i}$ A^{D} $\text{A}^{\text{u}}\text{A}^{\text{I}} \text{o}$ $\text{S}^{\text{i}}\text{I} \text{o}$ $\text{A}^{\text{u}}\text{A}^{\text{I}} \text{o}$ $\frac{3}{4}\text{O}^{\text{O}}$),
- (iii) $\text{A}^{\text{u}}\text{A}^{\text{I}} \text{o}$ $\text{O}^{\text{u}}\text{C}$ (« $\frac{3}{4}\text{i}$ A^{D} $\text{A}^{\text{i}}\text{O}^{\text{u}}$ $\text{y}^{\text{E}}\text{O}$ $\text{A}^{\text{A}^{\text{O}}}$ $\text{A}^{\text{u}}\text{A}^{\text{I}} \text{o}$ $\text{O}^{\text{u}}\text{C}$)

p^{i} i $\text{A}^{\text{A}^{\text{O}}}$ O^{i} i $\pm \text{n}$ $\text{A}^{\frac{3}{4}}\text{O}^{\text{O}}$ $\frac{3}{4}\text{O}^{\text{O}}$ n i $\frac{1}{4}\text{y}^{\text{A}^{\frac{3}{4}}}\text{i}$ o « D O $\frac{3}{4}\text{O}^{\text{O}}$ A^{C} (vector)
 $\text{I} \text{o}$.

| Áð;ñ Ó ËÄØ, Ä° °Äÿ ±ñ Á¾ÙÒ ÆÈð¾Ä « Ä,Ø §Ä;Ä; Ö Ä° °
 (Kgf) ±ÿÉ ÓÄ Ä° ° « Ä;ÖÖ « ØÄÐ | Áð;ñ ¼ÿ ±ÿÉ ÓÄÄ° °
 « Ä;ÖÖ Ä° °ÄÄü; òÄÍ ò. Ä° °Ä¾ ÄÇ; - ÄÄØ¾° °¼ÿ ÜÈÄ Ðñ Í
 §±§;ö¾;ÖÖ « ¾ÄÐ O A ±ÿÉ « òðÌ ÈÖÙÇ §±§;ö¾;ÖÖ
 Ä° °Ä;ÉÐ Ì ÈÇ; ôÄÍ ò. Ä° ° | °ÄüÄÍ ò §±§;î Ä° °ÄüÉ¾;×ö, « ¾Ø
 Ä° ° ÇØÄ; ÜÈÄ¾;×ö (sliding) - ùÇÐ. Ä° ° | ÇÄ¾° ° Ä Ö ±ÿÉ
 Íð¾ Äôðò òùÇÄØ ÿÿÜ; ÿÿÜ; |°Í ò¾; Ä° °ÄôÄÍ ò ox.oy.oz ±ÿÉ
 « ÍÏ Ü¼ÿ Ä° ° | °ÄüÄÍ ò §;î¾;Ï ò §;½Í Çÿ Ç;ÖÖ
 « ÈÄ;Ä;ö. §ÄÖÖ Ä° ° | ÇÄ¾° °, Ä° °Ä¾ð¾Ø Ðñ Í §±§;öÉÿ
 ÑÈÖÄÍ¾ÄØ Ä° °ÄôÄÍ ò « òðÌ ÈÄ;Ø Ì ÈÇ; ôÄÍ ò.



A½ 1-41

ÞÖÄ° ° Çÿ ±ñ Á¾ÙÒ ù °Ä;×ö, | °ÄüÄÍ ò §;î ÿÿÉ;×ö, - É;ð
 | °ÄüÄÍ ò¾° ° ù ÿÿÜ; ÿÿÜ; ±¾Ä;×ö ÞÖÍ Ä;É;ð, « Ä;ü Ö
 Ð Çÿ§ÄØ | °ÄüÄÍ ò §Ä;Ð ±¾Ç;Ä¾; ö;Ç;÷ Ä° ° Ç× Ç Ä½ 1.41Ø
 ;ðÈÄ;ü - ñ Í Äñ Í ò. « ò§Ä;Ð Ð Çÿ§ÄØ | °ÄüÄÍ ò ÇÄÄ° °Äÿ
 |¾; ÄÄÿ ÍÄØ¾° °Ä;Ì ò. ±É§Ä òùÇÇ; « Ä¾Ç; ÄÄØ ÞÖÍ ÇÉÐ.

° | Ä;Ö Çò Ð Ç; Ì ÖÐò§Ä;Ð Ä° ° Ç Èððò Ð ÇØ
 | °ÄüÄÍ Ä¾;ð, « Ä;ü ÓÖÙÇÄ ÄÆ§Ä | °ØÖÖ Ä° ° Ç;Ì ò. (Concurrent
 forces). « ò§Ä;Ð Ä° ° ù ù;Ä;ÿÿÿ ±ñ Á¾ÙÒö, | °ÄüÄÍ ò¾° °ÖÖ
 « ÈÄ;ö òÄð¾;ð ÄÐÍ ò §Ä;ÐÄ;É¾;Ì ò.

1.21.3 (2) ÞÄñ ¼ÄÐ Ä¾

ÞÐ Ä° ° Ä « ÇÄÍ Ä¾ü; -¾ÄØ;Ç; ÇÉÐ. ° | Ä;ÖÇÿÄÐ | °ÄüÄÍ ò
 Ä° °Ä;ÉÐ, « ò;Ä;ÖÇÿ Ç;È, « ¾Ø ²üÄÍ ò ÓÍ ò - ÇÄüÉÿ
 |ÄÖÍ ò |¾; Ä;ð « ÇÄ¾öÄÍ ÇÉÐ. ÞüÄ¾Äÿ ÄüÈ ÄÇ; Ì;ü
 ÞÄÍ ÄÄØ ÄÍ¾ÄØ¾ÄôÄÍ ò.

1.21.3 (3) ãÿÿ;ÄÐ Ä¾

ÞüÄ¾ÄÇÖðÄ° ° ù¾ÉÇðÍ | °ÄüÄÍ Ä¾° ° Ä. « Ä ±ò§Ä;Ðò
 ÞÄÖ ¼Ä; §Ä « ÄòÐ, ÿÿÜ Äü;É;ÿÿÿ ±ñ Á¾ÙÒðÌ Í °Ä;×ö, §Ä
 §±§;öÉØ, ±¾Ç; ±¾Ç;¾° ° ÇÖÖ | °ÄüÄÍ ÿÿÈ ±ÿÄ¾ « ÈÄÄ;ö.
 ÞÄÖ ¼ÄÖÙÇ Ä° ° ù ÞÄñ Í ò Ó§Ä;Ðò §Ä;Ä;ÖÇØ | °ÄüÄÍ ÄÐ
 Þ° ° Ä. -¾Ä;ð « Ä;Ç;Ø °Ä;Ä ÄÄ ÇÄ; ÖÈÄ;Ð.

$\vec{S}_A \cdot \vec{A}_i \hat{y} \hat{A} \hat{D} \cdot \hat{A}_i \hat{o} \hat{A} \hat{D} \hat{I} \hat{u} \hat{C} \hat{l} \hat{n} \hat{I} \hat{y} \hat{U} \ll \frac{3}{4} \hat{y} \pm \frac{1}{4} \hat{l} \hat{l} \hat{i} \hat{o} \hat{A} \hat{A}_i \hat{E}$
 $\hat{A} \hat{C} \hat{o} \hat{o} \hat{A} \hat{S}_A \hat{y} \hat{A} \hat{D} \hat{l} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \hat{D} \hat{C} \hat{E} \hat{D} \cdot \hat{S}_A \hat{o} \hat{S}_A \hat{i} \ll \hat{u} \hat{A} \hat{C} \hat{o} \hat{i} \hat{l} \pm \frac{3}{4} \hat{C} \hat{A}_i \hat{E} \hat{D} \hat{o}$
 $\hat{o} \hat{A} \hat{A}_i \hat{E} \hat{D} \hat{A}_i \hat{E} \hat{A} \hat{C} \hat{o} \hat{o} \hat{y} \hat{E} \hat{l} \hat{n} \hat{E} \hat{y} \hat{A} \hat{D} \hat{A} \hat{C} \hat{C} \hat{A} \hat{l} \hat{C} \hat{E} \hat{D} \cdot \ll \hat{i} \hat{l} \frac{1}{2} \hat{S}_A \hat{S}_A \hat{o} \hat{A} \hat{y}$
 $\ll \hat{E} \hat{A} \hat{u} \hat{S} \hat{C} \frac{3}{4} \hat{u} \hat{U} \hat{o} \hat{S}_A \hat{i} \hat{D} \ll \frac{3}{4} \hat{u} \hat{l} \hat{i} \hat{o} \hat{A} \hat{A}_i \hat{E} \hat{A} \hat{C} \hat{o} \hat{o} \hat{y} \hat{E} \ll \hat{E} \hat{A}_i \hat{E} \hat{D}$
 $\frac{3}{4} \hat{u} \hat{U} \hat{A} \hat{A} \hat{S} \hat{A} \hat{o} \hat{l} \hat{o} \hat{D} \hat{C} \hat{E} \hat{D} \cdot \hat{A} \hat{u} \hat{E} \hat{o} \hat{l} \frac{3}{4} \hat{i} \hat{l} \hat{A} \hat{C} \hat{o} \hat{A} \hat{D} \frac{1}{4} \hat{l} \hat{A}_i \hat{O} \hat{u} \cdot \hat{A} \hat{u} \hat{E} \hat{i}$
 $\hat{l} \hat{u} \hat{S} \hat{C} \hat{l} \hat{i} \hat{l} \hat{C} \hat{p} \hat{O} \hat{i} \hat{l} \hat{o} \hat{S}_A \hat{i} \hat{D} \hat{l} \hat{C} \hat{u} \hat{o} \frac{3}{4} \hat{C} \hat{l} \hat{o} \hat{A} \hat{C} \hat{o} \hat{i} \hat{l} \hat{i} \hat{o} \hat{A} \hat{A}_i \hat{E} \hat{A} \hat{C} \hat{o} \hat{o} \hat{A} \hat{i} \hat{A} \hat{C} \hat{E}_i \hat{E} \hat{D}$
 $\hat{S}_A \hat{o} \hat{S}_C \hat{l} \hat{i} \hat{l} \hat{C} \hat{A} \frac{3}{4} \hat{C} \hat{o} \hat{A} \hat{o} \hat{l} \hat{A}_i \hat{O} \hat{C} \hat{y} \hat{S}_A \hat{o} \hat{A} \hat{C} \hat{C} \hat{A} \hat{l} \hat{C} \hat{E} \hat{D} \cdot \hat{l} \hat{A}_i \hat{E} \hat{C} \hat{A} \hat{n} \hat{E} \hat{i} \hat{o} \hat{l} \hat{A} \hat{o} \frac{3}{4} \hat{C} \hat{y}$
 $\hat{l} \hat{A}_i \frac{3}{4} \hat{C} \hat{A} \hat{o} \hat{o} \text{ (tyre)} \hat{A}_i \frac{3}{4} \hat{A} \hat{y} \hat{S}_A \hat{u} \hat{A} \hat{o} \hat{A} \hat{o} \hat{l} \hat{o} \hat{D} \hat{C} \hat{E} \hat{D} \hat{O} \hat{y} \hat{S}_E \hat{l} \hat{l} \hat{C} \hat{l} \hat{C} \hat{u} \hat{o} \frac{3}{4} \hat{C} \hat{l} \hat{o}$
 $\hat{A} \hat{C} \hat{o} \hat{i} \hat{l} \hat{i} \hat{o} \hat{A} \hat{A}_i \hat{E} \hat{A} \hat{C} \hat{o} \hat{o} \hat{A} \cdot \hat{l} \hat{A}_i \hat{E} \hat{C} \hat{A} \hat{n} \hat{E} \hat{p} \hat{A} \hat{i} \hat{l} \hat{o} \frac{3}{4} \hat{C} \hat{o} \hat{i} \hat{l} \pm \frac{3}{4} \hat{C} \hat{o} \hat{D} \frac{3}{4} \hat{C} \hat{o} \hat{A} \hat{o}$
 $\frac{3}{4} \hat{A} \hat{A} \hat{y} \hat{A} \hat{i} \hat{o} \times \hat{A} \hat{C} \hat{o} \hat{o} \hat{l} \hat{A}_i \frac{3}{4} \hat{C} \hat{A} \hat{o} \hat{o} \frac{3}{4} \hat{C} \hat{y} \hat{S}_A \hat{o} \hat{l} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \hat{D} \hat{C} \hat{E} \hat{D} \cdot$

$\hat{A} \hat{C} \hat{o} \hat{o} \hat{u} \hat{S} \hat{o} \hat{i} \hat{E} \hat{A}_i \hat{S}_A \hat{z} \hat{u} \hat{A} \hat{I} \hat{A} \frac{3}{4} \hat{i} \hat{o} \ll \hat{A} \hat{u} \hat{E} \hat{o} \pm \hat{u} \hat{A} \hat{C} \hat{o} \hat{o} \hat{S}_A \hat{u} \hat{l} \hat{l} \hat{n} \frac{1}{4}$
 $\hat{A} \hat{o} \times \hat{o} \hat{l} \hat{A}_i \hat{O} \hat{C} \hat{o} \hat{l} \hat{S} \frac{3}{4} \hat{A} \hat{o} \hat{A} \hat{I} \hat{C} \hat{E} \hat{S} \frac{3}{4} \hat{i} \ll \hat{u} \hat{A} \hat{C} \hat{o} \hat{o} \hat{i} \hat{l} \hat{o} \frac{3}{4} \hat{i} \hat{y} \hat{o} \hat{C} \hat{E} \hat{o} \hat{A} \hat{C} \hat{o} \hat{l} \hat{o}$
 $\ll \hat{C} \hat{l} \hat{o} \hat{A} \frac{1}{4} \hat{S}_A \hat{n} \hat{i} \hat{o} \cdot \hat{l} \hat{O} \hat{l} \hat{A}_i \hat{O} \hat{u} \hat{A} \hat{u} \hat{E} \hat{o} \hat{l} \hat{A}_i \hat{O} \hat{u} \hat{U} \frac{1}{4} \hat{y} \text{ "n" } \hat{l} \hat{E} \hat{o} \hat{A} \hat{D} \frac{1}{4} \hat{l} \hat{A} \hat{o}$
 $\pm \frac{3}{4} \hat{C} \hat{o} \hat{l} \hat{A} \hat{o} \hat{C} \hat{l} \hat{C} \hat{u} \hat{o} \frac{3}{4} \hat{C} \hat{l} \hat{o} \hat{S}_A \hat{i} \hat{D} \ll \hat{D} \text{ "2n" } \hat{A} \hat{C} \hat{o} \hat{o} \hat{U} \hat{i} \hat{l} \hat{A} \hat{C} \hat{o} \hat{o} \hat{u} \hat{C} \hat{l} \hat{l} \hat{O} \hat{u} \hat{C} \hat{D} \cdot$
 $\ll \hat{A} \hat{u} \hat{E} \hat{o} \hat{l} \hat{E} \hat{o} \hat{A} \hat{D} \frac{1}{4} \hat{l} \hat{A}_i \hat{O} \hat{C} \hat{y} \hat{S}_A \hat{o} \hat{l} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \text{ "n" } \hat{A} \hat{C} \hat{o} \hat{o} \hat{C} \hat{o} \frac{3}{4} \hat{i} \hat{y}$
 $\hat{S}_A \hat{u} \hat{l} \hat{l} \hat{u} \hat{C} \hat{S}_A \hat{n} \hat{i} \hat{o} \cdot \ll \frac{3}{4} \hat{i} \hat{A} \hat{D} \hat{l} \hat{E} \hat{o} \hat{A} \hat{D} \frac{1}{4} \hat{l} \hat{A}_i \hat{O} \hat{o} \hat{C} \hat{o} \frac{3}{4} \hat{E} \hat{o} \hat{A} \hat{I} \hat{o} \frac{3}{4} \hat{C} \text{ (isolate)}$
 $\hat{A} \hat{u} \hat{E} \hat{o} \hat{l} \hat{A}_i \hat{O} \hat{u} \hat{u} \ll \frac{3}{4} \hat{y} \hat{S}_A \hat{o} \hat{l} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \hat{D} \hat{o} \hat{O} \hat{E} \hat{A} \hat{C} \hat{o} \hat{o} \hat{C} \hat{o} \frac{3}{4} \hat{i} \hat{y} \hat{A} \hat{o} \times \hat{i} \hat{l}$
 $\pm \hat{l} \hat{o} \hat{D} \hat{i} \hat{l} \hat{l} \hat{u} \hat{C} \hat{S}_A \hat{n} \hat{i} \hat{o} \cdot \hat{p} \hat{u} \hat{A} \hat{C} \hat{o} \hat{l} \hat{A}_i \hat{O} \hat{o} \hat{C} \hat{o} \frac{3}{4} \hat{E} \hat{o} \hat{A} \hat{I} \hat{o} \frac{3}{4} \hat{C} \ll \frac{3}{4} \hat{y} \hat{S}_A \hat{o}$
 $\hat{l} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \hat{O} \hat{E} \hat{A} \hat{C} \hat{o} \hat{o} \hat{C} \hat{i} \hat{l} \hat{E} \hat{o} \hat{A} \hat{C} \hat{l} \hat{A} \frac{3}{4} \hat{C} \hat{o} \hat{A} \hat{C} \hat{i} \hat{o} \hat{A} \frac{1}{4} \hat{i} \hat{u} \hat{l} \hat{A}_i \hat{D} \hat{o} \hat{A} \hat{C} \hat{o}$
 $\hat{O} \hat{i} \hat{C} \hat{y} \hat{E} \hat{E} \cdot \ll \frac{3}{4} \hat{u} \hat{l} \hat{O} \frac{3}{4} \hat{A} \hat{o} \frac{3}{4} \hat{E} \hat{o} \hat{A} \hat{I} \hat{o} \frac{3}{4} \hat{C} \hat{o} \hat{A} \hat{D} \frac{1}{4} \hat{l} \hat{A}_i \hat{O} \hat{C} \hat{y} \pm \hat{o} \hat{A} \hat{i} \hat{S} \hat{l} \hat{o} \frac{1}{4}$
 $\text{ (Outline) } \hat{A} \hat{A} \hat{o} \frac{3}{4} \hat{C} \hat{o} \hat{l} \hat{S}_A \hat{n} \hat{i} \hat{o} \cdot \hat{A} \hat{C} \hat{E} \hat{l} \ll \hat{o} \hat{l} \hat{A}_i \hat{O} \hat{u} \hat{A} \hat{u} \hat{E} \hat{o} \hat{l} \hat{A}_i \hat{O} \hat{u} \hat{U} \frac{1}{4} \hat{y} \hat{l} \hat{A} \hat{o}$
 $\pm \frac{3}{4} \hat{C} \hat{o} \hat{l} \hat{A} \hat{o} \hat{C} \hat{A} \hat{C} \hat{o} \hat{l} \hat{o} \hat{O} \hat{u} \hat{C} \hat{l} \hat{u} \hat{l} \hat{A}_i \hat{y} \hat{E} \hat{O} \hat{o} \ll \hat{o} \hat{l} \hat{A}_i \hat{O} \hat{C} \hat{y} \hat{S}_A \hat{o}$
 $\hat{l} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \hat{O} \hat{E} \hat{A} \hat{C} \hat{o} \hat{o} \hat{U} \hat{i} \hat{l} \hat{l} \hat{C} \hat{A} \frac{3}{4} \hat{C} \hat{o} \hat{A} \hat{C} \hat{o} \hat{l} \hat{E} \hat{C} \hat{l} \hat{S}_A \hat{n} \hat{i} \hat{o} \cdot \ll \hat{o} \hat{S}_A \hat{i} \hat{D}$
 $\hat{C} \hat{l} \frac{1}{4} \hat{l} \hat{o} \hat{A} \hat{A} \frac{1}{4} \hat{o} \frac{3}{4} \hat{C} \hat{o} \hat{l} \hat{o} \frac{3}{4} \hat{A} \hat{u} \hat{E} \hat{l} \hat{A}_i \hat{O} \hat{u} \hat{A} \hat{C} \hat{i} \hat{o} \hat{A} \frac{1}{4} \hat{o} \text{ (free body diagram)}$
 $\pm \hat{y} \hat{U} \hat{l} \hat{A} \hat{A} \hat{o} \cdot$

1.21.3 (4) $\frac{3}{4} \hat{A} \hat{u} \hat{E} \hat{l} \hat{A}_i \hat{O} \hat{u} \hat{A} \hat{A} \frac{1}{4} \hat{A} \hat{C} \hat{i} \hat{l} \hat{U} \hat{i} \hat{l} \hat{l} \hat{O} \hat{A} \pm \hat{l} \hat{o} \hat{D} \hat{i} \hat{l} \hat{o} \hat{D} \hat{i} \hat{l} \hat{u}$
 (free body diagrams some illustrations)

$\hat{l} \hat{O} \hat{l} \hat{A}_i \hat{O} \hat{C} \hat{y} \pm \frac{1}{4} \ll \hat{o} \hat{l} \hat{A}_i \hat{O} \hat{C} \hat{y} \hat{O} \hat{A} \hat{C} \hat{A} \hat{E} \hat{o} \hat{o} \hat{O} \hat{u} \hat{C} \hat{C} \hat{A} \hat{o} \hat{l} \hat{u} \hat{S} \hat{C} \hat{l} \hat{i} \hat{l} \hat{C} \hat{A}$
 $\hat{l} \hat{o} \hat{D} \frac{3}{4} \hat{C} \hat{o} \hat{A} \hat{o} \hat{l} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{A} \frac{3}{4} \hat{i} \hat{A} \hat{A} \hat{o} \hat{A} \hat{I} \hat{o} \cdot \hat{A} \hat{u} \hat{E} \hat{o} \hat{l} \frac{3}{4} \hat{i} \hat{l} \hat{A} \hat{C} \hat{o} \hat{A} \hat{D} \frac{1}{4} \hat{l} \hat{n} \hat{E} \hat{y}$
 $\pm \frac{1}{4} \text{ (w)} \hat{l} \hat{u} \hat{S} \hat{C} \hat{l} \hat{i} \hat{l} \hat{O} \hat{o} \hat{A} \hat{u} \hat{E} \hat{y} \hat{p} \hat{O} \hat{o} \hat{O} \text{ (T)} \hat{S}_A \hat{o} \hat{S}_C \hat{l} \hat{i} \hat{l} \hat{O} \hat{o}$
 $\hat{A} \frac{1}{4} \hat{o} \text{ 1-42} \hat{o} \hat{l} \hat{o} \hat{E} \hat{A} \hat{A} \hat{E} \hat{l} \hat{E} \hat{C} \hat{l} \hat{o} \hat{A} \hat{I} \hat{o} \cdot$



A/4o 1-42

$\hat{l} \hat{O} \hat{l} \hat{A}_i \hat{O} \hat{u} \hat{A} \hat{E} \hat{A} \hat{E} \hat{o} \hat{A}_i \hat{E} \frac{3}{4} \hat{A} \hat{A} \hat{y} \hat{S}_A \hat{o} \hat{l} \hat{A} \hat{i} \hat{o} \hat{A} \hat{D} \hat{E} \hat{O} \hat{i} \hat{l} \hat{o} \hat{S}_A \hat{i} \hat{D} \frac{3}{4} \hat{A} \hat{A} \hat{y}$
 $\hat{O} \hat{E} \hat{A} \hat{C} \hat{o} \hat{o} \hat{A} \cdot \hat{l} \frac{3}{4} \hat{i} \hat{l} \hat{o} \hat{O} \hat{u} \hat{C} \hat{C} \hat{A} \hat{o} \hat{l} \frac{3}{4} \hat{A} \hat{i} \hat{l} \hat{i} \hat{l} \hat{o} \hat{i} \hat{l} \hat{o} \frac{3}{4} \hat{i} \hat{E} \hat{S}_A \hat{u} \hat{O} \hat{E} \frac{3}{4} \hat{C} \hat{o} \hat{A} \hat{o}$
 $\hat{l} \hat{A}_i \hat{O} \hat{C} \hat{y} \hat{A} \hat{D} \hat{l} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{A}_i \hat{U} \hat{A} \hat{A} \frac{3}{4} \hat{o} \hat{S}_A \hat{n} \hat{i} \hat{o} \cdot \hat{A} \hat{i} \hat{o} \times \hat{A} \hat{C} \hat{o} \hat{o} \hat{A}_i \hat{E} \hat{D} \cdot \hat{l} \hat{A}_i \hat{O} \hat{u}$
 $\hat{p} \hat{A} \hat{i} \hat{l} \hat{o} \frac{3}{4} \hat{C} \hat{o} \hat{i} \hat{l} \pm \frac{3}{4} \hat{C} \hat{o} \hat{D} \frac{3}{4} \hat{C} \hat{o} \hat{A} \hat{o} \hat{l} \hat{E} \hat{C} \hat{l} \hat{o} \hat{A} \hat{I} \hat{o} \cdot$

$\mu = \frac{1}{2} \frac{W}{T_1 + T_2}$

$\mu = 1.43$

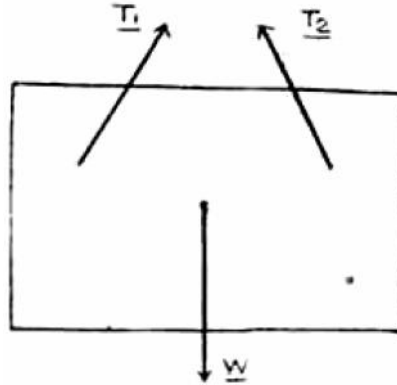


Fig. 1-43

$\mu = 1.44$

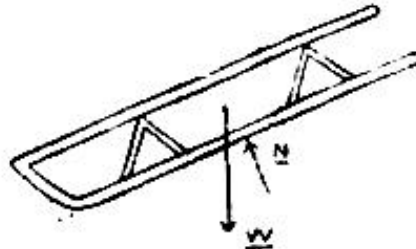
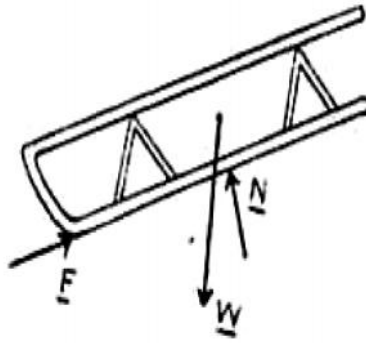


Fig. 1-44

$\mu = 1.45$



À¼õ 1-45

1.21.3 (4) çä ð¼Éý ðÀÀÊòð À¼ (Newton's law of gravitation)

Þ çä ð¼Éý ã ý È ÁÐ À¼ | °ÄÜÀÎ Á¼ ÀÇì Ç ÙÈÀÇ ò. Þ Ò
 | Àì Òù Ç Þ ½òÐì ðÎ Á¼üì - ½÷ò¼ÈÇÄÏ ÙÈÄ ° Î | Àì Òù
 (perceptible medium) ðÄÁý È « Á ü ý Ùì | ý Ù | °Ä | À¼Äì È Á¼°
 À¼°° Äò | ÄÜÙÇÉ ±ýÈ À¼° Ä çä ð¼ý ñ Î ÀÈò¼ì ÷. Þ ÐŞÄ
 çä ð¼Éý ðÀÀÊòð À¼Äì ò. ŞÄÖò ÞÜÀ¼ì Á¼°° Ä¼È Ð
 | Àì Òù Ç Î (Ð ù Ç) Ş°÷ì ò Ş÷÷ì ðÈø | °ÄÜÀÎ ò « ¼ý ±ñ Á¼òò
 | Àì Òù Ù ¼Ä ç È ±ñ Çý (masses) | ÀÒì ò | ¼ì ÁÄý ÞÒÄÈì Ì
 ±¼°Ä¼°¼òò ÞÒì Ì | Äý Ùò çä ð¼Éý ðÀÀÊòð À¼ ÜÙ ÇÐ.

Þ Ò Ð ù Çý (| Àì Òù) ç È Ç Ö ÈŞÄ $m_1, m_2 ±É × ò$, « Á Ù Ì Ì
 Þ ¼ÄÄ ÁÒò | ¼ì Á Á $r ±É × ò$ | ùÇ « Á ü ù | Äý Èý ŞÄø
 | °ÄÜÀÎ ò Á¼°° Ä¼ý ±ñ Á¼òò Ä¼È Ð ½ì ÇÄì $F = \frac{G \cdot m_1 \cdot m_2 ±ý Ù}{r^2}$
 « ÈÇÄ òÄÎ ò.

Þ Ì $G ±ý ÁÐ Á¼òð Óø Ì ò ùÇ$ (universal) ð÷òðÄ¼°° Ä¼ý
 Á¼« Ç Ä Ì ÈÇ Ì ò Ä¼ÈÄ.

Çý Á¼òò Ä¼°° ÈÇ¼ì È¼ø Þ Ò | Àì Òù Ù Ì Ì Þ ¼ŞÄ « ÁÒò
 °Ä°÷òò Ä¼°° Ì ÈòÄ¼ò¼ì « ÇÄø ÞÒòÄ¼üì | Àì Òù Çø
 ¼¼ì Á¼¼ý Èý ç È Ä¼ × ò « ¼Ä Äì ÞÒì ŞÄñ ÈÄÖò. ± òÐì ð¼ì
 ðÀÄ¼ý ŞÄøÄÄòÜç | Àì Òù Çý ç È ù ðÀÄ¼ý ç È Ò¼ý
 °ÄÇ òŞÄì Ð Ä¼°° ÈÇÄ Ä¼È¼ø | Àì Òù Çý ŞÄø | °ÄÜÀÎ ò ðÀÀÊòð
 Ä¼°° Ä¼ × ò Ì ÈòÄ¼ò¼ì « ÇÄø ùÇÐ.

1.21.3(4.1) ðÀÀø $\mu =$ Þ¼ò¼ý ðÀÀÊòð ÓÎ ò ð¼ì | Ì ¼ø

m ç ÈÒùÇ Ò Ð Ç ðÀÀÄòÄ¼ý ŞÄø ± Ì ò × ò. ðÄ¼ Äì
 Ş¼ÇÄì Ì | Ì ñ Î « ¼ý ç È, - Äò - ÇÄÜÈ Ò ÈŞÄ M, R
 $±É Ì Ì ùÇ × ò$. « òŞÄì Ð Ð Ù Ì ò ðÀÇ Ì ò Þ ¼ÄÄ ÁÒò Á¼°° Ä¼°°
 $F = \frac{G \cdot M \cdot m}{R^2} ±ý È °Äý Äì ð¼ø Á¼ ÄÄÜì òÄÎ ò.$

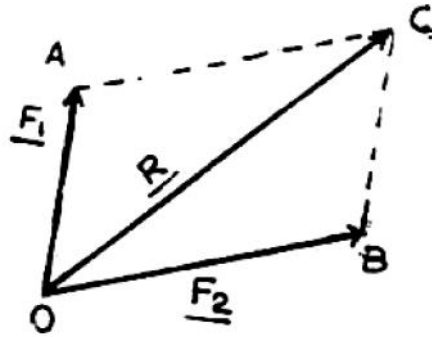
ŞÄÖò Ð Çý ± ¼, « òÐ Çý ÁÐ | °ÄÜÀÎ ò ðÀÀÊòð Ä¼°° Ä¼¼ø,
 çä ð¼Éý ÞÄñ ¼ì ÁÐ À¼òÄÈ,

$$F = W = mg - \text{Ì ò.}$$

$$±É ŞÄ $g = \frac{F}{m} = \frac{G \cdot M}{R^2} - \text{Ì ò.$$$

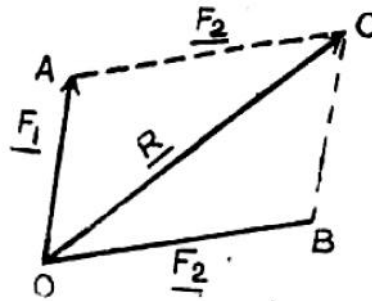
$\vec{R} = \vec{F}_1 + \vec{F}_2$ (Resultant force)

$\vec{R} = \vec{F}_1 + \vec{F}_2$



À¼õ 1-46

$\vec{R} = \vec{F}_1 + \vec{F}_2$ (free vectors)



À¼õ 1-47

$\vec{R} = \vec{F}_1 + \vec{F}_2$

$$\vec{F}_1 = \vec{OA}$$

$$\vec{F}_2 = \vec{OB} = \vec{AC}$$

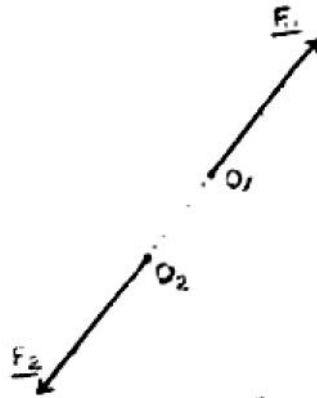
$$\therefore \vec{F}_1 + \vec{F}_2 = \vec{OA} + \vec{AC}$$

$\vec{R} = \vec{OC}$

$\vec{R} = \vec{OC}$

Final resultant force

1.23 (2) | Áöõ Á II



Á¼õ 1-48

$\underline{F}_1, \underline{F}_2 \pm \acute{y} \acute{E}$ pÖÁ º ù Ó | Á; ÖÇ « º | Á; Ö Ç « º Á¼Ç
 º º ÁÁÇ pÖì î | º öÁ¼; É;ø « º Á ù ±ñ Á¼öð º Çî º ÁÁ; ×ö, ±¼Ç ò
 ¼Ç º ÇÇ | º ÄüÄöî ö pÁñ î ö º ŠÁ (same) | º ÄüÄî ö Š; ð º ¼ö
 | ÄüÜüÇÉ Á; ×ö pÖì º ŠÁñ î ö. (Á¼õ 1.48 º ö Á; ÷ì º)
 | º ù º Á¼ ÁÉ,

« øÄÐ $\underline{F}_1 = -\underline{F}_2$
 $\underline{F}_1 = \underline{F}_2 = 0$
 « ¼; ÄÐ $\underline{R} = 0$

±É ŠÁ pí ì | ¼; ì ÄÄý Á º í ÁÇ; ÇÉÐ.

– ¼; Á;ø | ÁöÁö º Á ù ìö, ìö Ó òüÇÁÇ « º ÁÖö Á º ù òüÇ º Á
 « º Á¼Ç º ÁÁÇ º º ÁöÁ¼üì « º ÄüÉý | ¼; ì ÄÄý Á º í ÁÇ; º
 ŠÁñ î | ÁýÄ º ¼; Á º ÁÄÜì º ýÉÉ.

1.23 (3) | Áöõ Á III

ù | Á; Ö | º ÄÖì ì ö « ¼üì º ÁÁ; É ±¼Ç î | º Äø – ñ î. pÐ
 º äö¼Éý äýÉ; ÄÐ Á¼; Á; ì ö. \underline{w} ± º ¼öüÇÐö, – Öñ º ¼
 ÁÉÁóüÇÐÁ; É, pÖöòì ñ î º ýÜ Áö¼¼Çö¼Ç º Á; öÄÉÖöÁ¼; º
 | ùÇ×ö. ì ñ Éý ± º ¼, ¼Ç ò º ¼ö | ¼; ì ö òüÇÁÇ º ùŠ; ì ù Ç
 | º ÄüÄî ÇÉÐ. ì ñ î « º Á¼Ç º º ÁÁÇ ÖöÁ¼; Öö, « ¼ý ± º ¼ º ùŠ; ì ù Ç
 | º ÄüÄî Á¼; Öö « ¼üì î º ÁÁ; É \underline{R} ±ýÉ Á º ýÜ | ¼; ì ö òüÇÁÇ
 ŠÁøŠ; ì ù Ç | º ÄüÄ¼ ŠÁñ ÉÄ º º Á º ÄüÄî º ÇÉÐ.

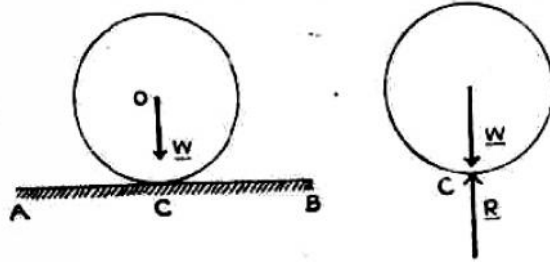


Figure 1-49

ΣF_y = 0
 $W + R = 0$

$R = -W$ (reaction)

1.23 (4) The principle of Transmissibility of a force

« sliding vector »

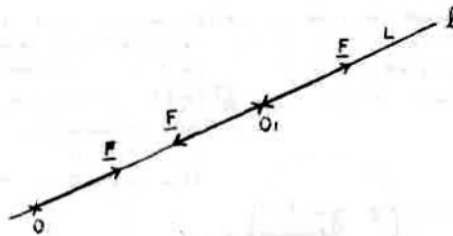


Figure 1-50

« sliding vector »

« sliding vector »

$$\{F\}_{O_1} = \{F\}_{O_2} + \{-F\}_{O_1}$$

$$\{F\}_{O_1} = \{F\}_{O_2}$$

□

1.25 $\vec{F}_1, \vec{F}_2 \sim \vec{F}$ (Equivalence of forces)

\vec{F}_1, \vec{F}_2 (two sets of forces) $\vec{F} \ll \vec{F}_1, \vec{F}_2$ (instantaneous) $\vec{F} \ll \vec{F}_1, \vec{F}_2$ (necessary), $\vec{F} \ll \vec{F}_1, \vec{F}_2$ (sufficient) $\vec{F} \ll \vec{F}_1, \vec{F}_2$
 (i) $\vec{F} \ll \vec{F}_1, \vec{F}_2$
 (ii) $\vec{F} \ll \vec{F}_1, \vec{F}_2$

$\vec{F} \ll \vec{F}_1, \vec{F}_2$ $\vec{F} \ll \vec{F}_1, \vec{F}_2$ $\vec{F} \ll \vec{F}_1, \vec{F}_2$ $\vec{F} \ll \vec{F}_1, \vec{F}_2$

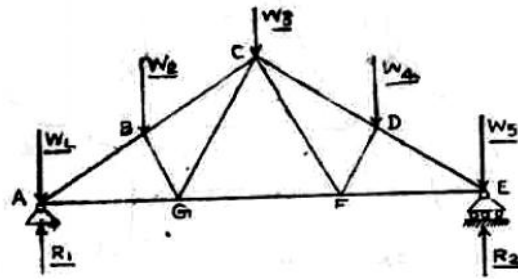
1.26 $\vec{F}_1, \vec{F}_2, \dots, \vec{F}_n \sim \vec{F}$ (Resultant of a set of forces)

$\vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$
 $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$
 $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$

$\vec{F}_1, \vec{F}_2, \vec{F}_3, \dots, \vec{F}_i, \dots, \vec{F}_n \pm \vec{F} \ll \vec{F}_1, \vec{F}_2, \vec{F}_3, \dots, \vec{F}_i, \dots, \vec{F}_n$
 $\vec{F} \ll \vec{F}_1, \vec{F}_2, \vec{F}_3, \dots, \vec{F}_i, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \vec{F}_3, \dots, \vec{F}_i, \dots, \vec{F}_n$
 $\vec{F} \ll \vec{F}_1, \vec{F}_2, \vec{F}_3, \dots, \vec{F}_i, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \vec{F}_3, \dots, \vec{F}_i, \dots, \vec{F}_n$
 $\vec{F} \ll \vec{F}_1, \vec{F}_2, \vec{F}_3, \dots, \vec{F}_i, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \vec{F}_3, \dots, \vec{F}_i, \dots, \vec{F}_n$

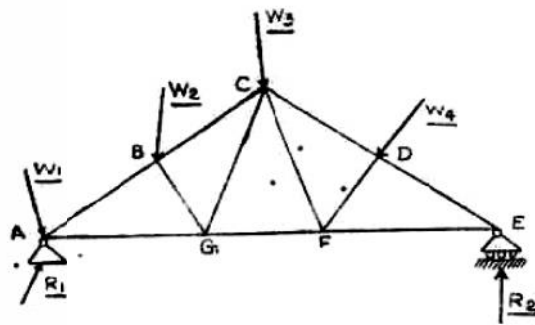
1.27 $\vec{F}_1, \vec{F}_2, \dots, \vec{F}_n \sim \vec{F}$ (coplanar force system)

$\vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$
 $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$
 $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$
 $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\vec{F} \ll \vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$



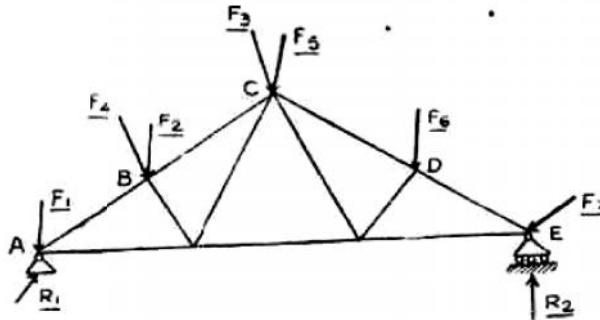
À¼õ 1-51

À¼õ 1.52ø À¸¸ ¸, Ç¸¸ É ò Ð ò ¸ Ò ¼Ç ò ¼Ç ò þ¸ ½Ä Ò È ¼jÉ « ¸¸ Á ò ¸¸ Á ò | Ä Ò Ü ò Ç É.



À¼õ 1-52

À¼õ 1.53ø ¸ Ò ¸ ¸ Ä ¼Ç Ä¸¸ ¸, ù ¸ Ò SÄj, j, x ò, Ä Ò È ¸¸ Ä ¸ Ò SÄj, j, « ¸¸ Ä Äj ¼É Äj, x ò ¸ Ò Ç É.



À¼õ 1-53

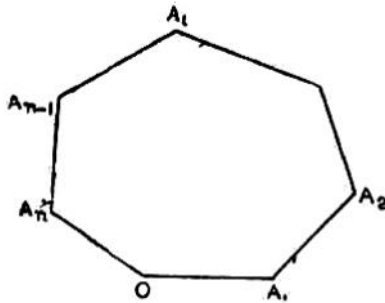
1.27 (1) | ¼j | Ä Äý (Resultant)

| j, | Î ì ò Ä Ò ¼Ä¸¸ ¸, Ç¸¸ | ¼j | ¼Ç | Ä¸ ± Ç ¼j, x ò ¸j ¸ Ä ò Ð Ä Äj, x ò - ù Ç « ¸¸ Á ò | ¼j | Ä Äý ± É ò Ä | ò. | ¼j | Ä Äý ¸ Ò ù ¸¸ È (single) Ä¸¸ ¸ Äj, ¸ Ò | Ä Ä¸¸ ½Äj, (couple) « ø Ä Ð ¸ Ò ¼É ò ¼Ä¸¸ ¸ Ä¸¸ ¸ Ò ¼Ä | Ä Ä¸¸ ½Äj, (single force together with a couple) « ¸¸ Ä Äj, ò.

Ä¸¸ ¸, Ç¸¸ ¸ý Èj, Î S ò ò Ð ò | ¼j | Ä Ä¸¸ É ò | Ä Ò È | ò ò Ö¸¸ È | ò ò | ¼j | ò ò (composition) « ø Ä Ð | Î ì, ò (reduction) ± É ò | Ä Ä¸¸.

1.27 (2) $\vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ (polygon of forces)

ஒரு பலகோண வகை $\vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ க்கு $\vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\pm \vec{E}$ இல் உள்ளிருந்து \vec{R} க்கு $\vec{R} = \vec{F}_1 + \vec{F}_2 + \dots + \vec{F}_n$ ஆகும். \vec{R} \vec{O} க்கு $\vec{R} = \vec{OA}_n$ ஆகும்.



படி 1-54

பலகோண வகை 1.54-ல் $\vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ $\pm \vec{E}$ இல் உள்ளிருந்து \vec{R} க்கு $\vec{R} = \vec{F}_1 + \vec{F}_2 + \dots + \vec{F}_n$ ஆகும். \vec{R} \vec{O} க்கு $\vec{R} = \vec{OA}_n$ ஆகும்.

$$\vec{OA}_2 = \vec{OA}_1 + \vec{A}_1\vec{A}_2 = \vec{F}_1 + \vec{F}_2$$

$$\vec{OA}_3 = \vec{OA}_2 + \vec{A}_2\vec{A}_3 = \vec{F}_1 + \vec{F}_2 + \vec{F}_3$$

$$\vec{OA}_n = \vec{OA}_{n-1} + \vec{A}_{n-1}\vec{A}_n = \vec{F}_1 + \vec{F}_2 + \dots + \vec{F}_{n-1} + \vec{F}_n = \vec{R}$$

\vec{R} \vec{O} க்கு $\vec{R} = \vec{OA}_n$ ஆகும். \vec{R} \vec{O} க்கு $\vec{R} = \vec{OA}_n$ ஆகும்.

பலகோண வகை (Statics), $\vec{F}_1, \vec{F}_2, \dots, \vec{F}_n$ (free vectors) \vec{R} \vec{O} க்கு $\vec{R} = \vec{OA}_n$ ஆகும்.

$$\vec{OA}_1 + \vec{A}_1\vec{A}_2 = \vec{OA}_2$$

$$\vec{OA}_2 + \vec{A}_2\vec{A}_3 = \vec{OA}_3$$

$$\vec{OA}_{n-1} + \vec{A}_{n-1}\vec{A}_n = \vec{OA}_n = \vec{R}$$

பலகோண வகை $\vec{R} = \vec{OA}_n$,

$$\vec{OA}_1 + \vec{A}_1\vec{A}_2 + \vec{A}_2\vec{A}_3 + \dots + \vec{A}_{n-1}\vec{A}_n = \vec{OA}_n$$

« $\vec{R} = \vec{OA}_n$,

$$\vec{OA}_n = \vec{OA}_1 + \vec{A}_1\vec{A}_2 + \dots + \vec{A}_{n-1}\vec{A}_n,$$

$$\vec{R} = \vec{F}_1 + \vec{F}_2 + \dots + \vec{F}_n,$$

$$\vec{R} = \sum_{i=1}^n \vec{F}_i$$

$\vec{R} = \vec{OA}_n$.

$\vec{A} \cdot \vec{C} = |\vec{A}| |\vec{C}| \cos \alpha$ (where α is the angle between \vec{A} and \vec{C}).
 $\vec{A} \cdot \vec{A} = |\vec{A}|^2$.
 $(\vec{A} + \vec{B}) \cdot \vec{C} = \vec{A} \cdot \vec{C} + \vec{B} \cdot \vec{C}$.
 $\vec{A} \cdot (\vec{B} + \vec{C}) = \vec{A} \cdot \vec{B} + \vec{A} \cdot \vec{C}$.
 $(\vec{A} \cdot \vec{B}) \vec{C} = \vec{A} (\vec{B} \cdot \vec{C})$.
 $\vec{A} \cdot (\vec{B} \times \vec{C}) = \vec{B} \cdot (\vec{C} \times \vec{A}) = \vec{C} \cdot (\vec{A} \times \vec{B})$.
 $\vec{A} \cdot (\vec{A} \times \vec{B}) = 0$.
 $(\vec{A} \times \vec{B}) \cdot (\vec{A} \times \vec{B}) = |\vec{A}|^2 |\vec{B}|^2 \sin^2 \alpha$.
 $(\vec{A} \times \vec{B}) \cdot \vec{C} = |\vec{A}| |\vec{B}| |\vec{C}| \cos \beta$ (where β is the angle between $\vec{A} \times \vec{B}$ and \vec{C}).

$\vec{A} + \vec{B} = \vec{B} + \vec{A}$ (Commutative law of addition)
 $(\vec{A} + \vec{B}) + \vec{C} = \vec{A} + (\vec{B} + \vec{C})$ (Associative law of addition)

$\vec{A} \cdot \vec{B} = \vec{B} \cdot \vec{A}$
 $(\vec{A} \cdot \vec{B}) \vec{C} = \vec{A} (\vec{B} \cdot \vec{C})$
 $\vec{A} \cdot (\vec{B} \times \vec{C}) = \vec{B} \cdot (\vec{C} \times \vec{A}) = \vec{C} \cdot (\vec{A} \times \vec{B})$

$\vec{A} \cdot (\vec{A} \times \vec{B}) = 0$
 $(\vec{A} \times \vec{B}) \cdot (\vec{A} \times \vec{B}) = |\vec{A}|^2 |\vec{B}|^2 \sin^2 \alpha$
 $(\vec{A} \times \vec{B}) \cdot \vec{C} = |\vec{A}| |\vec{B}| |\vec{C}| \cos \beta$

$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \alpha$
 $\vec{A} \cdot \vec{A} = |\vec{A}|^2$
 $(\vec{A} + \vec{B}) \cdot \vec{C} = \vec{A} \cdot \vec{C} + \vec{B} \cdot \vec{C}$
 $\vec{A} \cdot (\vec{B} + \vec{C}) = \vec{A} \cdot \vec{B} + \vec{A} \cdot \vec{C}$

1.28 Resolution of coplanar concurrent forces

$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \alpha$
 $\vec{A} \cdot \vec{A} = |\vec{A}|^2$
 $(\vec{A} + \vec{B}) \cdot \vec{C} = \vec{A} \cdot \vec{C} + \vec{B} \cdot \vec{C}$
 $\vec{A} \cdot (\vec{B} + \vec{C}) = \vec{A} \cdot \vec{B} + \vec{A} \cdot \vec{C}$

$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \alpha$
 $\vec{A} \cdot \vec{A} = |\vec{A}|^2$
 $(\vec{A} + \vec{B}) \cdot \vec{C} = \vec{A} \cdot \vec{C} + \vec{B} \cdot \vec{C}$
 $\vec{A} \cdot (\vec{B} + \vec{C}) = \vec{A} \cdot \vec{B} + \vec{A} \cdot \vec{C}$

$\vec{R} = \vec{F}_1 + \vec{F}_2 + \dots + \vec{F}_n$

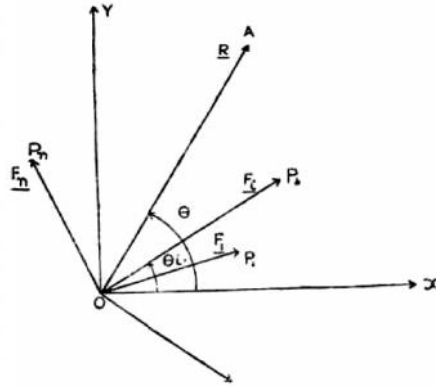


Fig. 1-55

$\underline{R} = \sum_{i=1}^n \underline{F}_i$ - is the resultant of the forces $\{F_i\}$ acting on the point O . The components F_{ix}, F_{iy} are the projections of the force F_i on the axes Ox, Oy .

The components F_{ix}, F_{iy} are the projections of the force F_i on the axes Ox, Oy (component), F_{ix}, F_{iy} are the projections of the force F_i on the axes Ox, Oy (projections).

The components F_{ix}, F_{iy} are the projections of the force F_i on the axes Ox, Oy .

$$\underline{OP}_i = \underline{ON}_i + \underline{N}_i \underline{P}_i$$

$$\underline{F}_i = \underline{F}_{ix} + \underline{F}_{iy}$$

$$= F_{ix} \underline{i} + F_{iy} \underline{j}, i=1, 2, \dots, n$$

is the resultant of the forces $\{F_i\}$ acting on the point O .

The components F_{ix}, F_{iy} are the projections of the force F_i on the axes Ox, Oy .

$$\sum_{i=1}^n \underline{F}_i = \sum_{i=1}^n (F_{ix} \underline{i} + F_{iy} \underline{j})$$

$$= \sum_{i=1}^n F_{ix} \underline{i} + \sum_{i=1}^n F_{iy} \underline{j}$$

The components F_{ix}, F_{iy} are the projections of the force F_i on the axes Ox, Oy .

$$\underline{R} = \underline{R}_x + \underline{R}_y$$

$$= R_x \underline{i} + R_y \underline{j}$$

is the resultant of the forces $\{F_i\}$ acting on the point O .

The components F_{ix}, F_{iy} are the projections of the force F_i on the axes Ox, Oy .

$$R_x \underline{i} + R_y \underline{j} = \left(\sum_{i=1}^n F_{ix} \right) \underline{i} + \left(\sum_{i=1}^n F_{iy} \right) \underline{j}$$

$\vec{R} = \sum_{i=1}^n \vec{F}_i$; $R_x = \sum_{i=1}^n F_{ix}$; $R_y = \sum_{i=1}^n F_{iy}$

$R^2 = R_x^2 + R_y^2$
 $= \left(\sum_{i=1}^n F_{ix} \right)^2 + \left(\sum_{i=1}^n F_{iy} \right)^2$

$\tan \alpha = \frac{R_y}{R_x}$
 $\frac{\sin \alpha}{R_y} = \frac{\cos \alpha}{R_x} = \frac{1}{R}$

$F_{ix} = F_i \cos \alpha_i$; $F_{iy} = F_i \sin \alpha_i$

$R_x = \sum_{i=1}^n F_{ix} = \sum_{i=1}^n F_i \cos \alpha_i$
 $R_y = \sum_{i=1}^n F_{iy} = \sum_{i=1}^n F_i \sin \alpha_i$

1.29 $\vec{R} = \sum_{i=1}^n \vec{F}_i = 0$

- (i) $\vec{R} = 0$
- (ii) $\vec{R} = 0$
- (iii) $\vec{R} = 0$

$\vec{R} = \sum_{i=1}^n \vec{F}_i = 0$

$\vec{R} = 0$

$$= \sqrt{\left(\sum_{i=1}^n F_{ix}\right)^2 + \left(\sum_{i=1}^n F_{iy}\right)^2 + \left(\sum_{i=1}^n F_{iz}\right)^2} \text{-----1}$$

$\underline{R} = \pm y \in \left\{ \frac{3}{4} \right\} \text{AA} \dot{y} \dot{A} \dot{c} \cdot \circ \dot{A} \dot{c} \dot{y} \left| \circ \dot{A} \dot{u} \dot{A} \dot{I} \circ \dot{S}_{,i} \dot{I} \right., x, y, z \ll \hat{I} \dot{I} \dot{U} \frac{1}{4} \dot{y} \text{ " } x \text{ " } y \text{ " } z$
 $\pm y \in \dot{S}_{,i} \dot{I} \frac{1}{2} \dot{I} \dot{S} \ll \dot{A} \dot{O} \dot{A} \frac{3}{4} \dot{I} \dot{S} \emptyset, R_x = R \cos \alpha_x; R_y = R \cos \alpha_y; R_z = R \cos \alpha_z \pm y \in \dot{I} \dot{O}$
 $\rightarrow \frac{3}{4} \dot{A} \dot{I} \dot{O}, \frac{\cos \alpha_x}{R_x} = \frac{\cos \alpha_y}{R_y} = \frac{\cos \alpha_z}{R_z} = \frac{1}{R} \rightarrow \dot{I} \dot{O} \text{-----2}$

$\pm \dot{E} \dot{S} \dot{A}, \left\{ \frac{3}{4} \right\} \text{AA} \dot{y} \dot{A} \dot{c} \cdot \circ \dot{A} \dot{c} \dot{y} \pm \dot{n} \dot{A} \frac{3}{4} \dot{O} \dot{O} \dot{O}, \left| \circ \dot{A} \dot{u} \dot{A} \dot{I} \circ \frac{3}{4} \dot{c} \cdot \circ \dot{O} \dot{O} (1), (2) \pm y \in \right.$
 $\circ \dot{A} \dot{y} \dot{A} \dot{I} \dot{S}, \dot{C} \dot{I} \dot{O} \dot{A} \dot{A} \dot{U} \dot{I} \dot{S}, \dot{O} \dot{A} \dot{I} \dot{S}, \dot{y} \dot{E} \dot{E} \dot{S}, \dot{U} \circ \dot{A} \dot{c} \dot{c} \cdot \dot{A} \dot{A} \dot{O} \dot{O} \dot{A} \frac{3}{4} \dot{I} \dot{S} \emptyset \underline{R} = 0$
 $\rightarrow \dot{I} \dot{O}.$

$\ll \frac{3}{4} \dot{A} \dot{D} \underline{R} = 0$

$\ll \frac{3}{4} \dot{A} \dot{D}$

$$R_x^2 + R_y^2 + R_z^2 = 0$$

$\ll \frac{3}{4} \dot{A} \dot{D}$

$$R_x = 0, R_y = 0, R_z = 0$$

$\ll \frac{3}{4} \dot{A} \dot{D}$

$$R_x = \sum F_{ix} = 0,$$

$$R_y = \sum F_{iy} = 0,$$

$$R_z = \sum F_{iz} = 0,$$

$\rightarrow \dot{I} \dot{O}.$

$\pm \dot{E} \dot{S} \dot{A} \dot{D}, \dot{U} \circ \dot{A} \dot{c} \dot{c} \cdot \dot{A} \dot{A} \dot{O} \dot{O} \dot{A} \frac{3}{4} \dot{I} \dot{S} \dot{E} \dot{I} \dot{O} x, y, z \frac{3}{4} \dot{c} \cdot \circ \dot{S} \dot{O} \dot{A} \dot{c} \cdot \circ \dot{O} \dot{A} \dot{S} \dot{C} \dot{y}$
 $\dot{U} \hat{I} \frac{3}{4} \dot{O} \dot{I} \dot{A} \dot{C} \dot{A} \dot{I} \dot{S} \dot{S} \dot{A} \dot{n} \dot{I} \dot{O}.$

$\dot{S} \dot{A} \dot{O} \dot{O} \underline{R} = 0 \pm y \dot{A} \dot{D} \dot{D}, \dot{U} \ll \dot{A} \frac{3}{4} \dot{c} \dot{c} \cdot \dot{A} \dot{A} \dot{O} \dot{O} \dot{A} \frac{3}{4} \dot{U} \dot{I} \dot{O} \dot{S} \dot{A} \dot{I} \dot{D} \dot{A} \dot{I} \dot{E}$
 (sufficient) $\dot{A} \dot{A} \dot{A} \dot{A} \dot{I} \dot{O}.$

$R=0 \pm \dot{E} \dot{O} \dot{D} \dot{C} \dot{O} \left| \circ \dot{A} \dot{u} \dot{A} \dot{I} \circ \dot{A} \dot{c} \cdot \circ \dot{C} \dot{y} \dot{U} \hat{I} \frac{3}{4} \dot{O} \dot{I} \dot{A} \dot{C} \dot{A} \dot{I} \dot{S} \dot{E} \dot{D} \right. \pm \dot{E} \dot{S} \dot{A}$
 $\dot{p} \dot{A} \dot{n} \frac{1}{4} \dot{A} \dot{D} \left| \dot{A} \dot{O} \dot{O} \dot{A} \dot{A} \dot{y} \dot{A} \dot{I} \dot{A} \dot{A} \dot{I} \dot{S} \dot{D}, \dot{U} \ll \dot{A} \frac{3}{4} \dot{c} \ll \dot{O} \dot{A} \dot{D} \circ \dot{A} \dot{c} \dot{c} \cdot \dot{A} \dot{A} \dot{O} \dot{O} \dot{U} \dot{C} \dot{D}.$

$\pm \dot{E} \dot{S} \dot{A}, \dot{O} \dot{D}, \dot{U} \ll \dot{A} \frac{3}{4} \dot{c} \ll \dot{O} \dot{A} \dot{D} \circ \dot{A} \dot{c} \dot{c} \cdot \dot{A} \dot{A} \dot{O} \dot{O} \dot{I} \dot{S} \dot{S} \dot{A} \dot{n} \dot{E} \dot{A} \dot{D} \dot{O},$
 $\dot{S} \dot{A} \dot{I} \dot{A} \dot{D} \dot{A} \dot{I} \dot{E} \dot{C} \dot{A} \dot{O} \frac{3}{4} \dot{E} \underline{R} = 0 \pm y \dot{A} \frac{3}{4} \dot{I} \dot{O} \dot{A} \dot{A} \frac{1}{4} \dot{A} \dot{C} \dot{I} \dot{S} \dot{O} \dot{E} \dot{A} \dot{O}$

$F_1, F_2, \dots, F_i, \dots, F_n \pm y \in \dot{A} \dot{c} \cdot \circ \dot{U} \dot{O} \pm y \in \dot{O} \dot{U} \dot{C} \dot{A} \dot{O} \left| \circ \dot{A} \dot{u} \dot{A} \dot{D} \dot{I} \ll \dot{O} \dot{U} \dot{C} \dot{c} \cdot \dot{A} \dot{I} \right.$
 $\circ \dot{A} \dot{c} \dot{c} \cdot \dot{A} \dot{A} \dot{O} \dot{O} \dot{I} \dot{O} \dot{S} \dot{A} \dot{I} \dot{D} \dot{A} \dot{c} \cdot \circ \dot{C} \dot{A} \dot{A} \dot{U} \dot{I} \dot{O} \frac{3}{4} \dot{c} \cdot \circ \dot{A} \dot{c} \dot{c} \cdot \dot{C}$
 $\dot{y} \dot{E} \dot{y} \dot{A} \dot{y} \dot{y} \dot{E} \dot{I} \dot{S} \text{ " } \dot{E} \dot{N} \dot{E} \dot{C} \dot{O} \dot{E} \dot{A} \dot{O} \ll \dot{A} \dot{I} \dot{S} \dot{O} \dot{A} \dot{E} \dot{A} \dot{O} \dot{S}_{,i} \frac{1}{2} \dot{O}$
 $\dot{c} \cdot \frac{1}{4} \dot{I} \dot{O} \dot{p} \dot{I} \dot{I} \frac{3}{4} \dot{c} \cdot \circ \dot{A} \dot{c} \dot{c} \cdot \dot{C} \pm \dot{U} \dot{A} \frac{3}{4} \dot{A} \dot{I} \dot{O} \dot{E} \dot{A} \dot{O} \text{ (in any order) } \pm \dot{I} \dot{O} \dot{D}$
 $\dot{y} \dot{E} \dot{y} \dot{A} \dot{y} \dot{y} \dot{E} \dot{I} \dot{S} \ll \dot{A} \dot{O} \frac{3}{4} \dot{S} \dot{A} \dot{I} \dot{O} \dot{O}, \dot{p} \dot{U} \frac{3}{4} \dot{A} \dot{I} \dot{S} \dot{O} \dot{A} \dot{E} \dot{A} \dot{O} \dot{S}_{,i} \frac{1}{2} \dot{S} \dot{A}$
 $\dot{c} \cdot \frac{1}{4} \dot{I} \dot{O} \pm y \dot{A} \frac{3}{4} \dot{O} \dot{O} \ll \dot{E} \frac{3}{4} \dot{O} \dot{S} \dot{A} \dot{n} \dot{I} \dot{O} \dot{S} \dot{A} \dot{O} \dot{O}, \dot{A} \dot{c} \cdot \circ \dot{O} \dot{A} \dot{O} \dot{S}_{,i} \frac{1}{2} \dot{O},$
 $\frac{3}{4} \dot{c} \cdot \circ \dot{A} \dot{c} \dot{C} \dot{y} \dot{U} \hat{I} \frac{3}{4} \dot{A} \dot{O} \left| \frac{3}{4} \dot{I} \dot{A} \dot{O} \dot{A} \frac{3}{4} \dot{I} \dot{A} \dot{A}, \dot{A} \dot{c} \cdot \circ \dot{U} \left| \circ \dot{A} \dot{u} \dot{A} \dot{I} \circ \dot{S}_{,i} \dot{I} \dot{S} \dot{C} \dot{I} \right. \right.$
 $\dot{O} \dot{I} \dot{O} \dot{A} \frac{3}{4} \dot{O} \dot{O} \dot{A} \pm y \dot{A} \frac{3}{4} \dot{O} \dot{O} \dot{A} \dot{E} \dot{A} \dot{S} \dot{A} \dot{n} \dot{I} \dot{O}.$

1.31 $\dot{S} \dot{E} \dot{U} \dot{I} \dot{O} \left| \dot{A} \dot{I} \dot{O} \dot{U} \dot{y} \dot{E} \dot{y} \circ \dot{A} \dot{c} \dot{c} \cdot \dot{A} \right.$

$\dot{O} \dot{S} \dot{E} \dot{U} \dot{I} \dot{O} \left| \dot{A} \dot{I} \dot{O} \dot{C} \dot{y} \dot{A} \dot{D} \left| \circ \dot{A} \dot{u} \dot{A} \dot{I} \dot{y} \dot{E} \dot{A} \dot{I} \dot{S} \frac{3}{4} \dot{U} \left| \dot{A} \dot{I} \dot{O} \dot{A} \dot{c} \cdot \circ \dot{O} \right. \right.$
 $\left. \left| \frac{3}{4} \right\} \frac{3}{4} \dot{c} \ll \dot{O} \left| \dot{A} \dot{I} \dot{O} \dot{C} \dot{E} \dot{D} \dot{A} \dot{O} \dot{O} \dot{A} \dot{O} \dot{A} \dot{E} \pm \dot{I} \dot{I} \dot{O} \dot{A} \dot{I} \left| \frac{3}{4} \dot{U} \left| \dot{A} \dot{I} \dot{O} \dot{O} \dot{U} \dot{C} \dot{A} \dot{S} \dot{A} \right. \right. \right.$

$\sum_{i=1}^n F_i, \underline{M}^R = \sum_{i=1}^n M_i \wedge F_i \pm \underline{y} \hat{A} \hat{A} \hat{A} \hat{U} \hat{i} \hat{i} \hat{o}$.

$\hat{O} \hat{O} \hat{E} \hat{U} \hat{i} \hat{o} \hat{A} \hat{i} \hat{O} \hat{C} \hat{S} \hat{A} \hat{O} \hat{A} \hat{U} \hat{A} \hat{T} \hat{y} \hat{E} \hat{A} \hat{A} \hat{y} \hat{A} \hat{C} \hat{O} \hat{O} \hat{o}$,
 $\hat{A} \hat{A} \hat{y} \hat{A} \hat{E} \hat{A} \hat{C} \hat{O} \hat{O} \hat{o} \hat{A} \hat{i} \hat{S} \hat{A} \hat{U} \hat{A} \hat{i} \hat{O} \hat{O} \hat{U} \hat{C} \hat{A} \hat{O} \hat{A} \hat{E} \hat{C} \hat{O}$,
 $\ll \hat{o} \hat{A} \hat{i} \hat{O} \hat{U} \ll \hat{A} \hat{A} \hat{C} \hat{O} \hat{O} \hat{A} \hat{i} \hat{i} \hat{U} \hat{C} \hat{O} \hat{A} \hat{i} \hat{o}$.

$\pm \hat{E} \hat{S} \hat{A}, \hat{O} \hat{O} \hat{E} \hat{U} \hat{i} \hat{o} \hat{A} \hat{i} \hat{O} \hat{C} \hat{y} \hat{A} \hat{D} \hat{O} \hat{A} \hat{U} \hat{A} \hat{T} \hat{y} \hat{E} \hat{A} \hat{i} \hat{S} \hat{A} \hat{U} \hat{A} \hat{i} \hat{O}$
 $\hat{A} \hat{C} \hat{O} \hat{o} \hat{A} \hat{i} \hat{S} \hat{A} \hat{U} \hat{A} \hat{i} \hat{O} \hat{O} \hat{U} \hat{C} \hat{A} \hat{O} \hat{A} \hat{E} \hat{C} \hat{O} \hat{O} \hat{o} \hat{R} = 0, \underline{M}^R = 0 \hat{O}$.

$\hat{p} \hat{A} \hat{U} \hat{i} \hat{o} \hat{x}, \hat{y}, \hat{z} \hat{A} \hat{i} \hat{C} \hat{O} \hat{O} \hat{D} \hat{O} \hat{A} \hat{i} \hat{C} \hat{x} \hat{C} \hat{i} \hat{o} \hat{A} \hat{i} \hat{O} \hat{D} \hat{O} \hat{A} \hat{C} \hat{O} \hat{A} \hat{i} \hat{o}$.
 $\ll \hat{o} \hat{A} \hat{i} \hat{O} \hat{D}$,

$\underline{R} = R_x \hat{i} + R_y \hat{j} = 0$
 $\ll \hat{A} \hat{i} \hat{C} \hat{i}$

$(i) R_x = \sum_{i=1}^n F_{ix} = 0$

$(ii) R_y = \sum_{i=1}^n F_{iy} = 0$

$(iii) R_z = \sum_{i=1}^n F_{iz} = 0 \pm \hat{y} \hat{E} \hat{C} \hat{A} \hat{O} \hat{A} \hat{i} \hat{E} \hat{U} \hat{o}$,

$M^R_{ox} \hat{i} + M^R_{oy} \hat{j} + M^R_{oz} \hat{k} = 0$

$\ll \hat{A} \hat{i} \hat{A} \hat{D}, (iv) MR_{ox} = \sum_{i=1}^n (y_i F_{iz} - z_i F_{iy}) = 0$

$(v) M^R_{oy} = \sum_{i=1}^n (z_i F_{ix} - x_i F_{iz}) = 0$

$(vi) M^R_{oz} = \sum_{i=1}^n (x_i F_{iy} - y_i F_{ix}) = 0$

$\pm \hat{y} \hat{E} \hat{C} \hat{A} \hat{O} \hat{A} \hat{i} \hat{E} \hat{U} \hat{o} \hat{C} \hat{O} \hat{A} \hat{i} \hat{O} \hat{U} \hat{A} \hat{U} \hat{o}$.

$\hat{p} \hat{A} \hat{U} \hat{i} \hat{o} \hat{C} \hat{O} \hat{O} \hat{E} \hat{U} \hat{i} \hat{o} \hat{A} \hat{i} \hat{O} \hat{U} \hat{O} \hat{A} \hat{C} \hat{O} \hat{O} \hat{A} \hat{i} \hat{O} \hat{S} \hat{A} \hat{A} \hat{i} \hat{E} \hat{D} \hat{o}$
 (Necessary) $\hat{S} \hat{A} \hat{i} \hat{D} \hat{A} \hat{i} \hat{E} \hat{D} \hat{A} \hat{i} \hat{E}$ (Sufficient) $\hat{C} \hat{A} \hat{O} \hat{A} \hat{i} \hat{E} \hat{C} \hat{i} \hat{o}$.

$\hat{p} \hat{u} \hat{A} \hat{O} \hat{A} \hat{i} \hat{D} \hat{A} \hat{i} \hat{E} \hat{O} \hat{A} \hat{C} \hat{O} \hat{O} \hat{A} \hat{i} \hat{E} \hat{C} \hat{O} \hat{A} \hat{A} \hat{y} \hat{A} \hat{i} \hat{O} \hat{D} \hat{A} \hat{U} \hat{S} \hat{U} \hat{A}$
 $\ll \hat{A} \hat{U} \hat{A} \hat{y} \hat{A} \hat{O} \hat{A} \hat{i} \hat{U} \hat{o} \hat{A} \hat{A} \hat{U} \hat{i} \hat{o} \hat{A} \hat{i} \hat{o}$;

I. $\hat{y} \hat{U} \hat{i} \hat{i} \hat{y} \hat{U} \hat{O} \hat{i} \hat{i} \hat{o} \hat{A} \hat{i} \hat{o} \ll \hat{A} \hat{O} \hat{o} \hat{A} \hat{i} \hat{S} \hat{A} \hat{U} \hat{o} \hat{a} \hat{y} \hat{U} \hat{C} \hat{O} \hat{A} \hat{i} \hat{E}$
 $\hat{C} \hat{O} \hat{A} \hat{C} \hat{O} \hat{O} \hat{U} \hat{A} \hat{C} \hat{i} \hat{O} \hat{A} \hat{i} \hat{C} \hat{O} \hat{y} \hat{i} \hat{E} \hat{C} \hat{A} \hat{O} \hat{U} \hat{O} \hat{i} \hat{o} \hat{A} \hat{i} \hat{C} \hat{O} \hat{O} \hat{A} \hat{i} \hat{E} \hat{C} \hat{S} \hat{A} \hat{a} \hat{i} \hat{O} \hat{A} \hat{O} \hat{U} \hat{i} \hat{O} \hat{A} \hat{O} \hat{A} \hat{i} \hat{o} \hat{D}$.

II. $\hat{y} \hat{U} \hat{i} \hat{i} \hat{y} \hat{U} \hat{O} \hat{i} \hat{i} \hat{o} \hat{A} \hat{i} \hat{o} \ll \hat{A} \hat{O} \hat{o} \hat{A} \hat{i} \hat{S} \hat{A} \hat{U} \hat{o} \hat{a} \hat{y} \hat{U} \hat{C} \hat{O} \hat{A} \hat{i} \hat{E}$
 $\hat{C} \hat{O} \hat{U} \hat{A} \hat{U} \hat{E} \hat{C} \hat{O} \hat{U} \hat{A} \hat{C} \hat{i} \hat{O} \hat{A} \hat{i} \hat{C} \hat{O} \hat{y} \hat{i} \hat{E} \hat{C} \hat{A} \hat{O} \hat{U} \hat{O} \hat{i} \hat{o} \hat{A} \hat{i} \hat{C} \hat{O} \hat{O} \hat{A} \hat{i} \hat{E} \hat{C} \hat{S} \hat{A} \hat{a} \hat{i} \hat{O} \hat{A} \hat{O} \hat{U} \hat{i} \hat{O} \hat{A} \hat{O} \hat{A} \hat{i} \hat{o} \hat{D}$.

I. $\hat{U} \hat{U} \hat{U} \hat{o} \hat{C} \hat{A} \hat{O} \hat{A} \hat{i} \hat{E} \hat{U} \hat{o} \hat{O} \hat{E} \hat{S} \hat{A} \hat{O} \hat{E} \hat{U} \hat{i} \hat{o} \hat{A} \hat{i} \hat{O} \hat{U} \hat{i} \hat{i} \hat{p} \hat{O} \hat{O}$
 $\hat{A} \hat{A} \hat{y} \hat{A} \hat{i} \hat{O} \hat{C}$ (Translocation), $\hat{A} \hat{E} \hat{U} \hat{O} \hat{C}$ (Rotation) $\hat{U} \hat{A} \hat{p} \hat{A} \hat{i} \hat{i} \hat{U} \hat{p} \hat{O} \hat{i}$,
 $\hat{O} \hat{E} \hat{A} \hat{i} \hat{A} \hat{y} \hat{A} \hat{i} \hat{O} \hat{U} \hat{C} \hat{O} \hat{A} \hat{i} \hat{o} \hat{D} \hat{y} \hat{E} \hat{E}$.

$\hat{p} \hat{O} \hat{A} \hat{i} \hat{U} \hat{O} \hat{A} \hat{C} \hat{O} \hat{O} \hat{A} \hat{i} \hat{O} \hat{A} \hat{y} \hat{A} \hat{i} \hat{C} \hat{O} \hat{y} \hat{A} \hat{C} \hat{O} \hat{O} \hat{A} \hat{i} \hat{i} \hat{n} \hat{i} \hat{U} \hat{i} \hat{i}$
 $\hat{A} \hat{C} \hat{O} \hat{o} \hat{A} \hat{i} \hat{S} \hat{A} \hat{U} \hat{o} \hat{A} \hat{i} \hat{C} \hat{O} \hat{A} \hat{i} \hat{D} \hat{A} \hat{i} \hat{E} \hat{U} \hat{C} \hat{O} \hat{A} \hat{i} \hat{U} \hat{i} \hat{i}$ (unknown quantities) $\hat{O} \hat{A} \hat{O} \hat{A} \hat{i}$

Ü Ö ÖÉÜÏ ò | Àî ÖÇÝ « .. Ä¾ « ØÄÐ °Äç " Ä" Âö ÄÁ¾| ÄÇÄç
 ÄÄî ðÐì ÜÜð - ð¾ ½ìì Üìì ð¾× ùi ½ÖËÖ. ÞÜ¾ - ð¾
 ½ìì ù Äî×ò ç ÄÄÄî ð¾ Äî ð¾ (Statically determinate
 problems). - Üìì Äç ÄÄî ð¾ Äî ð¾ (Statically indeterminate problems)

1.32. °Äç " ÄÄý Öì Ä Ä" ù (Special cases of Equilibrium).

1.32 (1) Ä" 1 Ü Ö ðüçÄç °ö¾ ýÈ Ä" °, çý |¾ì |¾ (Concurrent System of Forces)

Þìì Ä" °, çý |¾ì |¾ì | Ä Ä" Ç× « ððüç ÄÄ ÄÄ | ° çý È µ÷
 ü" Èð |¾ì ÄÄý Ä" ° (Single resultant force) - Ä¾ì °Äç " Äìì
 \$Äñ ÈÄ çÄ¾" É R=0 - ì ò.

$$\begin{aligned}
 &\ll \text{ÄÐ } R_x i + R_y j + R_z k = 0 \\
 &\ll \text{ØÄÐ } R_x = \sum_{i=1}^n F_{ix} = 0 \\
 &R_y = \sum_{i=1}^n F_{iy} = 0 \\
 &R_z = \sum_{i=1}^n F_{iz} = 0;
 \end{aligned}$$

¾" ° Ä" Âö ÄüÈÄ | Äî Ð - öÄø äî °Ä Ä" Ç" Ä - Ü¾ | °ö¾üì ÄüÈ
 ÄÄç Üð - Ç.

±ì ðÐì |¾ì, 2\$¾ Ü | Äî Ö r ±ý Üð « ìì ÄüÈ Ä" ° ð |¾ì |¾Äý
 ¾Öð¾Äý äî °ÄÄî ò ±ý ÄÄ Äý ÄÖ ç" Ä, Ç" ° ð ðÜçÐ;

- (a) |¾ì ÄÄý Ä" ° äî °ÄÄî - üç ç" Ä.
- (b) |¾ì ÄÄý Ä" ° ±ì ð¾ « ì" ° \$Ä | °ÄøÄî ò \$¾ì |¾ì ò
 ÄüÈÖì ò ç" Ä.
- (c) |¾ì ÄÄý Ä" ° ±ì ð¾ « ììì Þ" ½ÄîÉ | °ÄøÄî ò
 \$¾ì ð" ¼ð | ÄüÈÖì ò ç" Ä.

r ±ý Üð « ììì Þ" ½ÄüÈ¾ì ±ìì ò s ±ý Üð « ìì ÄüÈ Ä" ° ð
 |¾ì |¾Äý ¾Öð¾Äý äî °ÄÄî ò ±ý Ä" ° Äý ÄÖ ç" Ä, Ç" ° 2\$¾ Üð
 ýÜ Ä" ÄÜì ò.

- (a) |¾ì ÄÄý Ä" ° \$Ä äî °ÄÄî ò ç" Ä; « ØÄÐ
- (b) |¾ì ÄÄý Ä" ° r; s ±ý Üð ÞÖ« ìì çý ° \$¾ (through
 both axes) | °ÄüÄî ò \$¾ì ð" ¼ð | ÄüÈÖì ò ç" Ä.

Þö Þ" ½ÄüÈ « ìì Üìì Öîì \$¾ Ä" ° Äî ÉÐ Þ" ½Äî « " ÄÄ
 ÖËÄ¾¾, äýÈ¾¾ (c) ±ý Üð çÄ¾" É s ±ý Üð « ììì ò
 | Äî Öð¾ÄüÈÐ.

x ±ý Üð äýÈÄÐ « ì" ° ÉÐ |¾ì ÄÄý Ä" ° | °ÄøÄî ò \$¾ì ,
 ÞöäýÜ r, s, x ±ý Üð « ìì, " Ç | Ä¾¾¾ ç" Ä « ØÄÐ r, s ±ý Üð
 « ìì, " Ç | Ä¾¾¾ äýÈ¾¾ x ±ý Üð « ììì Þ" ½Äî « " ÄÖð
 ç" Ä ±ý Ä" Ä, Üìì 2È¾¾, ð¾¾¾ì ð¾¾¾ ð¾¾¾ üç¾¾ì |¾ì. \$ÄÖð
 r, s ±ý Üð « ìì ù ÄüÈ ±ì ð¾ Ä" ° ð |¾ì |¾Äý ¾Öð¾Äý
 äî °ÄÄî Ä¾ý, äýÈÄÐ « ìì ÄüÈÖð äî °ÄÄî ò \$Äî |¾ì ÄÄý Ä" °

at°AAj l o.

±E SA, O ðuÇc AAESâ | °AøAÎ o Åc° ð | 3/4j l 3/4c l - jÂ °Açc° Â° Â - U3/4oAÎ ð3/4 Äu| E; O AAEAj E D

$\sum M_r = 0, \sum M_s = 0, \sum M_x = 0; \pm y E_j l o.$

« uÄjSE °Açc° Äi l jÂ çc°3/4° E° Â | ÄÇcÄË A3/4ül Äu| E; O °AyÄj l Çy | 3/4j l 3/4c ÄyAÏÄjÜ pOÏ, sÄñ l o ±E x o çc°ÄÄ Äj o. « °Açc° ÄEAjE;

1. Y « î l ð 3/4c° °Aø Åc° °, U° 1/4Ä Ä, ç: x, Çy l EÄÄø Üð l ð | 3/4j°°, at°AAj AD1/4y, « 3/4Äj D $\sum_{i=0}^0 F_{iy} = 0 \pm y E_j AD1/4y,$

2. Åc° ° ü °ö3/4c l o ðuÇc AAESâ x z 3/46ñ3/4cül p° 1/2Äj, Å° AÏo 3/4Çö3/4cø « ° ÄÄj3/4Dø, p° 1/2ÄÜEDÄTπ d, ø çy Üo pO« î l ü ÄüEç ± l i l o Åc° ° Ü° 1/4Ä 3/4Oö03/4cEπç Çy ç EÄÄø Üð l ð | 3/4j°°, ç ü | Äjy Üo at°AAj, x o, « 3/4j ÄD $\sum Md = 0, \sum M\emptyset = 0, \pm y Üo pOÏ l o SÄj D$ Åc° ° Çy | 3/4j l 3/4c Äj ø 3/4j l o AÎ o çÜEÜi, ç | Äj Oü « ° A3/4c « ø AD °Açc° AAÄOÏ l o.

±E SA, O ðuÇcÄÄ° AÏo Åc° ° Çy | 3/4j l 3/4c l ä y Ü 3/4Eö3/4 °Açc° AÎ ° AyÄj l, ü OÏ, ÄÄj, o S3/4° ÄoAÎ o ±E pÜ3/4Äj, i UEÄj o.

6-2. (2) Å° °, 2; O 3/4Ç Åc° ° ð | 3/4j l 3/4c (Coplanar force system)

O øEUi o | Äj OÇy AD SÄ3/4Çö3/4cø | °AüAÎ çyE ± üA3/4 Åc° ° ð | 3/4j l 3/4cø O° 3/4Eçc° °Äj, sÄj « øAD ° 3/4Eçc° | ÄÄc° 1/2Äj, sÄj ° l i, oA1/4i Ü l o. - s, sÄ, « uÄc° ° ð | 3/4j l 3/4c °Açc° AAÄOÏ, O3/4Äj Ä3/4j, s,

$$R_x = \sum_{i=1}^n F_{ix} = 0, R_y = \sum_{i=1}^n F_{iy} = 0$$

±y EçOÏ, sÄñ l o. pÄñ 1/4j Ä3/4j, | 3/4j l ÄÄy | ÄÄc° 1/2Äj, ° l i, oA1/4j | 3/4y Ä° 3/4 - U3/4oAÎ ð3/4 Åc° ° ð | 3/4j l 3/4c | °AøAÎ o 3/4Çö3/4cül i ° jöøD « ° AÏo Äj SÜ | Äj O r ±y Üo « î l ÄüEç 3/4Oö03/4cE° E ± l i, s, « D $\sum Ma = 0 \pm y Üo pOÏ, sÄñ l o.$

SÄ3/4ÇöD Åc° ° ð | 3/4j l 3/4c l r ±y Üo « î l ÄüEç ± l ðD - ñ 1/4j l o $\sum Ma = 0 \pm y Üo çc°3/4° E i l o A3/4Äj, « uÄc° ° ð | 3/4j l 3/4c « ° AÏo 3/4Çö3/4cSÄ$ Äj S3/4Ü | Äj O ðuÇc ÄüEç ± l i l o « ð | 3/4j l 3/4c Åc° ° Ü° 1/4Ä 3/4Oö0 3/4Eçy Çy l EÄÄø Üð l ð | 3/4j°°, Äo at°Aö3/4cül i °AøAÎ ð3/4Ä3/4j, x o | jüçÄj o.

±E SA, Äj S3/4Ü | Äj O | j l i, oAö1/4 Åc° ° ð | 3/4j l 3/4c l sÄüUEcÄ °Açc° Ä çc°3/4° E° ço AÄyAÎ øDÄ3/4ül Äj O l o 3/4c° ° çö 3/4l ö3/4Äj Ü S3/4=ö | 3/4l ð3/4j ø Åc° ° î l OÏ Äj E °AyÄj l, ço | ÄEAj o. | Äj DÄj, çc° 1/4ö3/4c° °Oö çc° Äi l ðDö3/4c° °Oö Äc, x o z UE3/4j, pOÏ l o.

SÄOö 3/4Oö03/4Eçy ü ± l i l o ðuÇcÄE D çc° AÏo OÏ ÄÄj E D. « öðuÇcÄj E D UEÄÄ° Ä l ° Eö3/4 ±ñ 1/2c°°, Üüç Åc° ° çc° 3/4Oö0 3/4Eçy °AyÄj øEø p1/4o | ÄEö 3/4l 3/4j, x o S3/4=ö | 3/4l i, oAö1/4 sÄñ l o. pÜA3/4 ä y Ü çc° AAÄø °öAö3/4i, Ü o, « 3/4j ÄD,

« ØÄÐ,

$$\left\{ \sum_{i=1}^n F_{ix} = 0, \sum_{i=1}^n F_{iy} = 0, M_{oz}^R = \sum_{i=1}^n (x_i F_{iy} - y_i F_{ix}) = 0, \left[M_o = \sum_{i=1}^n (x_i F_{iy} - y_i F_{ix}) = 0 \right] \right\}$$

pŌÄċ ÷ ÷ ¼ Ĩ ¼ ÄŸ ÜüÜô ÄĪ ¼ Ü Ĩ ċ ¼ ŠÄŌüÇ ÄĒÄ ½ ¼ ÷ ÷ ¼ Ĩ ¼ = 0 ŠÇĪ ÜĒ, Ō ¼ ÇðÐ Äċ ÷ ÇĪ ŠÄ Ĩ ÄŌÄĪ ŸĒ ÄĪ Š¼ Ü Ĩ ÄĪ Ō ¼ Ĩ ¼ ÄŸ Äċ ÷ Ä Ä Ä Ä Ä ÜðÄ¼ ĩ ÷ Ĩ ÄĪ ÐÄĪ ÷ ŠÄĪ ¼ ÄĒÄĪ ÷. ĩ Ĩ Ĩ ÷ Ĩ ÄŌ¼ Ä Ÿ Ç Ĩ Ē ŠÄüĒĒĪ Ō Ō ¼ Ç Äċ ÷ ÷ ¼ Ĩ ¼ Ä Ĩ ÄÄÄŌĪ ÷.

Ō ðĒÜĪ ÷ Ĩ ÄĪ ŌÇŸÄÐ Ō ¼ Ç Äċ ÷ ÷ ¼ Ĩ ¼ ÄŸ ÄŌÄ¼, ŠÄ ŠÇ ÷ ŠĪ ðĒÄŌÄĪ ¼ ä Ÿ Ü ðüÇċ ũ ũ Ĩ ÄĪ Ÿ Ü ÄüĒċ ± Ĩ Ĩ ÷ « ũ Äċ ÷ Ü ¼ Ä ¼ Ō ÷ ¼ ÄŸ ÇŸ Ĩ Ē ÄÄŌ Ü ðĪ ÷ ¼ Ĩ , ¼ Ä ÷ ¼ Ä ÇŠÄ äĪ ÄÄĪ ĒĪ ÷, « ũ Äċ ÷ ÷ ¼ Ĩ ¼ ÄŸ Äċ ÷ ÄÄÄŌĪ ÷.

« ũ ÄĪ ŠĒ ĩ Ĩ ÷ Ĩ ÄŌ¼ Ä Ÿ ũ Ĩ Ē ŠÄĒĒĪ Ō Ō ¼ Ç Äċ ÷ ÷ ¼ Ĩ ¼ ÄŸ Äċ ÷ ÄÄÄŌĪ ÷;

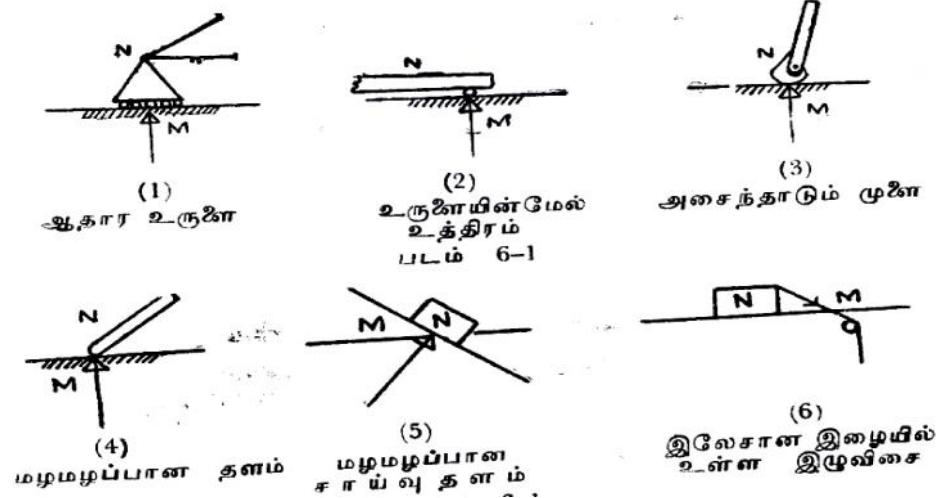
Ō ðĒÜĪ ÷ Ĩ ÄĪ ŌÇŸÄÐ Ō ¼ Ç ÷ ¼ ÇŠÄ Ō Äċ ÷ ÷ ¼ Ĩ ¼ ÄŸ ÄŌÄ¼, ¼ Š¼ Ü ÷ pŌ ðüÇċ ÇÇ ũ Ĩ ÄĪ Ÿ Ü ÄüĒċ ± Ĩ Ĩ ÷ ¼ Ō ÷ ¼ ÄŸ ÇŸ Ĩ Ē ÄÄŌ Ü ðĪ ÷ ¼ Ĩ , ¼ Ä ÷ ¼ Ä ÇŠÄ äĪ ÄÄĪ ĨĪ ÷, « ðüÇċ ÇĪ Š ÷ ÷ ð ũ Ĩ ¼ Ĩ ÷ ŠĪ ðĒĒ Äċ ÷ Ü ¼ Ä Ä Ä Ä Ä ÇŸ Ü ðĪ ÷ ¼ Ĩ äĪ ÄÄĪ ĨĪ ÷ pŌĪ Ĩ ÄĒċ, « ũ Äċ ÷ ÷ ¼ Ĩ ¼ ÄŸ Äċ ÷ ÄÄÄŌĪ ÷."

Ō ¼ Ç « ÄŌðĪ Ĩ Ō¼ ± ¼ Ç-¼ Ĩ Ĩ ¼ ÷ Ç (reactions) Ō Ĩ ÄĪ Ōü ÄüĒċ Ĩ ÄĪ Ōü Ü ¼ Ÿ « ØðÐÄ¼ ÷ ð « ØÄÐ Äċ ½ Ĩ ŌÄĪ Ä¼ ÷ ð ¼ ÷ ¼ Ÿ;

¼ ¼ Ō ÄÄŌ ± ũ ÄŌ¼ Ō Ĩ ÄĪ ŌÜ ÷ pŌ ÄĪ ÄĪ ½ Ĩ Ç ÷ ÄüÜüÇ « ÄŌ ÄĪ ÷ ÷ ¼ ÄĪ Ð. pŌ ÷ ¼ ŠÄĪ ¼ Ō ũ Ä Ō ¼ ÄĪ ÇŸ Ĩ ¼ Ĩ ¼ ÄŸ (roof trusses), Ō ¼ ÄĪ ũ (beams) Ĩ ÄÄüĒŸ Äċ ÷ Ä Ä Ä Ä Ä Ä ÜĪ ÷ Ĩ ÄĪ ŌðĪ « Ä ũ pŌ ÄĪ ÄĪ ½ « ÄŌ ÄŌ ÷ ŌĒÜüÇ ¼ Ĩ Ĩ Ĩ ŌÄĪ ÷. pũ ÄŌ¼ « ÄŌ Ō ÇÇ ðĒÄċ ÷ Ç Ē ðð ÷ pŌ ÄĪ ÄĪ ½ Ĩ Ç ÷ ÄüĒĪ ¼ Ĩ Ō (two dimensional forces), Äċ ÷ ÄĪ Ĩ ± Ĩ ¼ Ĩ ÄĪ ŌÇŸ ¼ Ç ÷ ¼ ÇŠÄŠÄ Ĩ ÄŌÄĪ Ä¼ Ĩ ũ Ĩ ŌÇŠÄĪ Ĩ.

pŌ ÄĪ ÄĪ ½ « ÄŌ ÄĪ ÄĪ ðĒ Ĩ ÄĪ Ōü ÇÇ Ĩ ÄüÄĪ ÷ ± ¼ Ç-¼ Ĩ Ĩ Äċ ÷ Ç ÷ ÄŸ ÄŌÄĪ Ü 3 Ĩ ¼ Ĩ ¼ Ç Ĩ Ō ÄĪ ÷ ð « ĒÄÄĪ ÷.

1. Ĩ ¼ Ĩ ¼ ŠĪ ðĒĒ Ō ÄŌÄĪ ÷ Äċ ÷ Ĩ Ĩ Ĩ ÄÄĪ Ē ± ¼ Ç-¼ Ĩ Ĩ ÷;
pŌ Ĩ ¼ Ĩ ¼ ÄŌ « ÄÄĪ ÜĒÄ Ĩ ¼ ÄĪ ÜĪĪ (supports) Ō Ç ũ (rollers), « Ō Ō ¼ Ĩ Ō Ō ĒĪ ð ¼ ũ (rockers), ÄĒÄĒŌÄĪ Ē ÄŌ ũ (smooth surfaces) ± Ÿ ÄÄ Ō Ō Ä ± Ĩ ðÐĪ ðĪ ÇĪ ÷. « ÄüĒŸ « ÄŌðĪ ũ Ä¼ ÷ 1.80 ÷ ðĒÄÄĪ Ü pŌĪ ÷.
Ō¼ Ō Ĩ Ÿ Ĩ ± Ĩ ð¼ Ĩ Ĩ Ĩ ÇÇ Ĩ ± Ÿ Ü ÷ Ĩ ÄĪ Ō Ç Ĩ ¼ ÄĪ ÄŌÄÄĒ Ĩ ÷ ÷ ¼ ÄĪ ÷. ± Ē ŠÄ Ĩ ¼ ÄĪ Ē Äċ ÷ ¼ ð ÷ pũ ÄŌ¼ Ĩ ¼ ÄĪ ÜĪĪ (M) Ĩ ¼ ÄĪ Ĩ ŠÄ ± ¼ Ç-¼ Ĩ Äċ ÷ Ĩ ÄÄĪ ŠÄ¼ Ÿ Ä¼ ÷ ¼ ÷ ðĒÄÄĪ Ü « ÄŌ ÷. pũ ÄŌ¼ ± ¼ Ç-¼ Ĩ Äċ ÷ Ĩ ÄĪ ŠĪ ðĒĒ ŠÄŌ ŠĪ Ĩ Ĩ « ØÄÐ ũ ŠĪ Ĩ Ĩ ± Ĩ ÷ ¼ Ĩ ÄĪ ŌÇŸ Äċ ÷ Ä « ÄŌðĪ Ĩ ¼ ũ ÄÄĪ Ü Ĩ ÄĪ ŌÄĪ ÷.

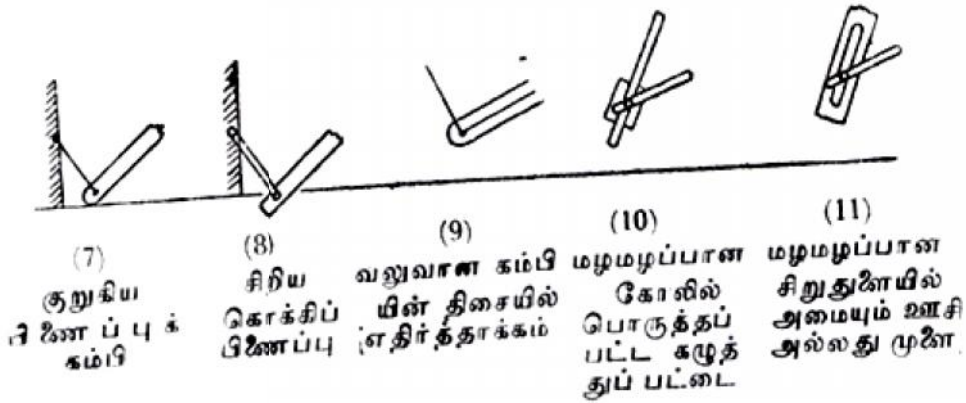


À¼õ 1-80

5ÅÐ ±Ī òÐì | ðËø ±¾¾¼ì ò -- ±ý Ū ò | À; ŒÇý ŠÀø °ì ò x ¾Çò¾üì ì | ò¾¼Ë¾¾ °Àø | °ÄüĀĪ ò.

6ÅÐ ±Ī òÐì | ðËø ÆĪ \$¾Ū | À; Œ¾¼ì ò p ÆĀÉÐ ÇÇò¾üì µ= pØ Å" ° " À; Ī É Ç ŠĀñ Ī ò.

Ī Ū ÇĀ Å" ½òòì òÅç Ū (Short Cables), °ËĀ |¾¼ì ò Å" ½òòì Ū (Short links) ÅÖĀ; É òÅç Ū (Cables) ÅĒÅĒòĀ; É \$¾¼Ëø | À; Œò¾¼òÅĒ¼ ØòÐò ÅĒ" ¼ ÅĒÅĒòĀ; É °Û Ð " ÇĀĀ" ÅÖò ° ò « øĀÐ Œ" ÉĀ;ø Ī ò¾¼ò Å" ½ì òÅĒ¼ Œ" É (Pin in a smooth slot) - ÇĀ" Å Ū ò pò¾¼ì ¾Āç p¼ò; ÅŪò. « ÅüËý « " Åòòì Ç" É ò¾¼òò ±¾¾¼ì , Å" °Åý ±ñ Å¾¼òò ÅĒ ò¾¼ý |¾¼Ā¾¾¼ì |¾¼ÛÇòĀĪ ò.



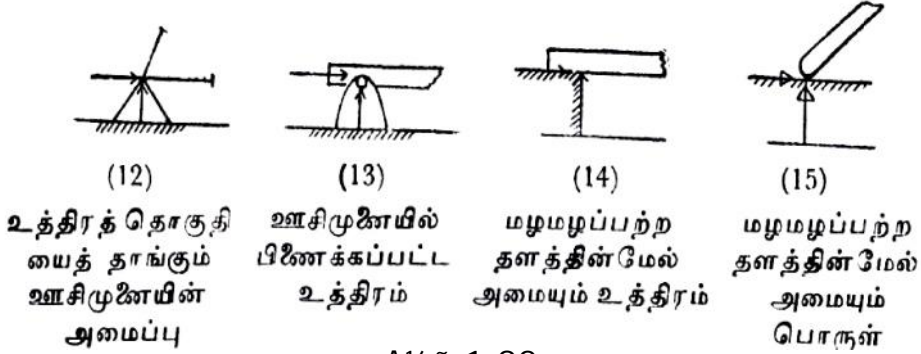
À¼õ 1-81

Ī Ū ÇĀ p ò ½òòì òÅç, °ËĀ |¾¼ì ò Å" ½òòì, ÅÖĀ; É òÅç Çý¾¾¾ °Àç ±¾¾¼ì ò, ÅĒÅĒòĀ; É \$¾¼Ëø | À; Œò¾¼òÅĒ¼ ØòÐò ÅĒ" ¼ ÅĒÅĒòĀ; É °Û Ð " ÇĀĀ" ÅÖò ° ò « øĀÐ Œ" Ç pò¾¼ì « " Åòòì Ç" É ò¾¼òò ±¾¾¼ì , Å" °Åý ±ñ Å¾¼òò ÅĒ ò¾¼ý |¾¼Ā¾¾¼ì |¾¼ÛÇòĀĪ ò.

2. |¾¼Ā¾¾¼ì \$¾¼Ëø | °ÄüĀĪ ò Å" °ì Ĩ °ĀĀ; É ±¾¾¼ì ò.

pò¾¼ì ¾Āç " ÅĀì Ū ÉĀ -¾¼ĀĪ Ū Ĩ | À; Œò¾¼òÅĒ¼ ÅĒÅĒòĀ; É

ஓர் சட்டம் « ஓர் ஓர் எ ஓர் (smooth pin fixed in position), ஓர் 1/2 ஓர் (hinges), ஓர் (rough surfaces) – ஓர் ஓர் 1.82 ஓர்.

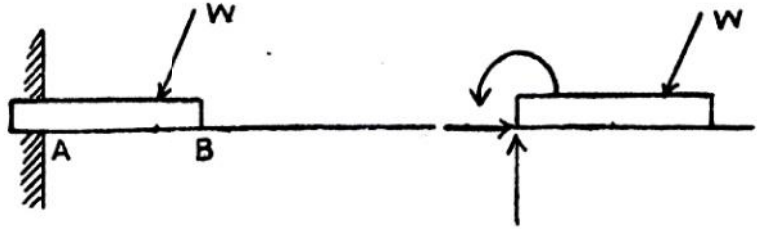


Aஓர் 1-82

ஓர் ஓர் – ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் « ஓர் ஓர் ஓர்
 ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் 1/2 ஓர் ஓர் ஓர் – ஓர் ஓர் ஓர்
 « ஓர் ஓர் ஓர் ஓர் ஓர் 1/2 ஓர் ஓர் ஓர் 1/2 ஓர் ஓர் ஓர்.

ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர்
 ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர்
 ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர்

3. ஓர் ஓர் ஓர் ஓர் ஓர் 1/2 ஓர் ஓர் ஓர் ஓர்
 ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர்
 ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர்
 ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர்
 ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர்
 ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர்
 « ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர்
 – ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர்
 – ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர்



(16) பொருத்தப்பட்ட வளைவுச் சட்டம் அல்லது உத்திரம்
 Aஓர் 1-83

– ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர்
 ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர்
 ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர் ஓர்

$\vec{a} = \vec{y} \hat{e}_2 = \vec{S} \hat{e}_1 + \vec{A} \hat{e}_3 = \vec{S} \hat{e}_1 + \vec{A} \hat{e}_3$.

1.32 (3) $\vec{A} = 3 \hat{e}_1 + \vec{A} \hat{e}_3$; $\vec{A} \hat{e}_3 = \vec{A} \hat{e}_3$ (Parallel forces in space):

$\vec{A} \hat{e}_3 = \vec{A} \hat{e}_3 = \vec{A} \hat{e}_3$ (Parallel forces in space):

$\vec{A} \hat{e}_3 = \vec{A} \hat{e}_3 = \vec{A} \hat{e}_3$ (Parallel forces in space):

$\vec{y} \hat{e}_2 = \vec{y} \hat{e}_2 = \vec{y} \hat{e}_2$ (Parallel forces in space):

$\vec{S} \hat{e}_1 = \vec{S} \hat{e}_1 = \vec{S} \hat{e}_1$ (Parallel forces in space):

$$M_{ox} = \sum_{i=1}^n y_i F_{iz} = 0$$

$$M_{oy} = - \sum_{i=1}^n x_i F_{iz} = 0 \quad \pm \vec{E} \times \vec{o} = \vec{y} \hat{e}_2 \times \vec{S} \hat{e}_1 = \vec{A} \hat{e}_3$$

$\vec{A} \hat{e}_3 = \vec{A} \hat{e}_3 = \vec{A} \hat{e}_3$ (Parallel forces in space):

$\vec{A} \hat{e}_3 = \vec{A} \hat{e}_3 = \vec{A} \hat{e}_3$ (Parallel forces in space):

$\vec{A} \hat{e}_3 = \vec{A} \hat{e}_3 = \vec{A} \hat{e}_3$ (Parallel forces in space):

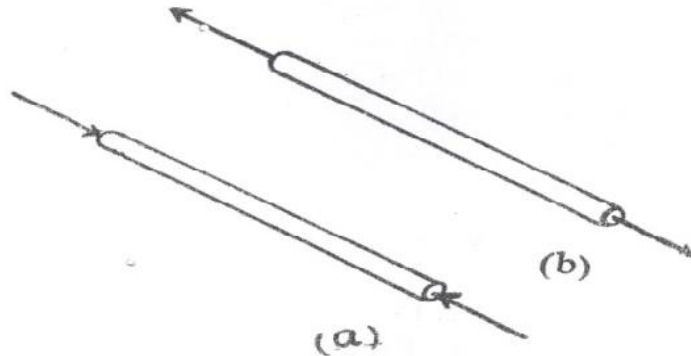
$\vec{A} \hat{e}_3 = \vec{A} \hat{e}_3 = \vec{A} \hat{e}_3$ (Parallel forces in space):

1.32 (4) $\vec{A} = 4 \hat{e}_1$; $\vec{A} \hat{e}_3 = \vec{A} \hat{e}_3$ (Body in Equilibrium with Two Forces);

$\vec{A} \hat{e}_3 = \vec{A} \hat{e}_3 = \vec{A} \hat{e}_3$ (Body in Equilibrium with Two Forces):

$\vec{A} \hat{e}_3 = \vec{A} \hat{e}_3 = \vec{A} \hat{e}_3$ (Body in Equilibrium with Two Forces):

$\vec{A} \hat{e}_3 = \vec{A} \hat{e}_3 = \vec{A} \hat{e}_3$ (Body in Equilibrium with Two Forces):

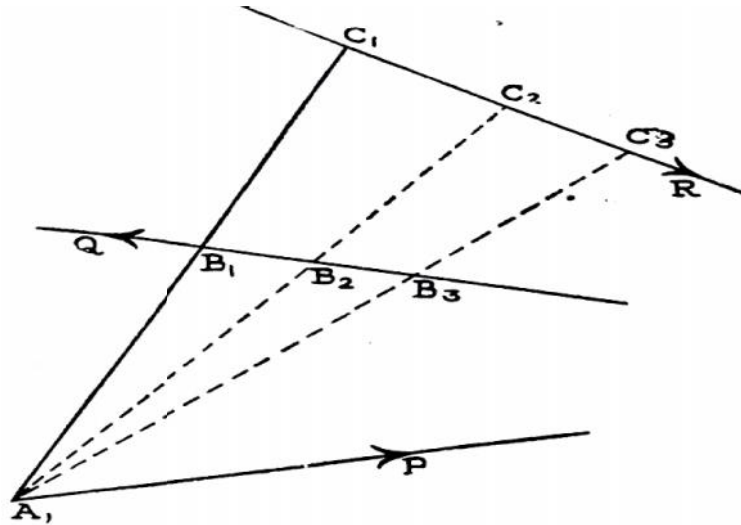


A1-84

(a) $\pm y \bar{U} \circ \ll \dots \hat{A} \circ \hat{A} \circ \hat{O} \hat{U} \hat{C} \circ \hat{U} \hat{3/4} \hat{n} \hat{E} \hat{\theta} \mid \circ \hat{A} \hat{U} \hat{A} \hat{I} \hat{\theta} \circ \hat{A} \hat{U} \hat{\theta} \pm \hat{3/4} \hat{O} \hat{A} \hat{j} \hat{E}$
 $\hat{A} \hat{C} \hat{\circ} \hat{u} \mid \hat{z} \hat{O} \hat{i} \hat{A} \hat{C} \hat{\circ} \hat{C} \hat{j} \hat{x} \hat{o}$ (Compressive forces). (b) $\pm y \bar{U} \bar{o}$
 $\ll \dots \hat{A} \circ \hat{A} \circ \hat{O} \hat{U} \hat{C} \circ \hat{U} \hat{3/4} \hat{n} \hat{E} \hat{\theta} \mid \circ \hat{A} \hat{U} \hat{A} \hat{I} \hat{\theta} \circ \hat{A} \hat{U} \hat{\theta} \pm \hat{3/4} \hat{O} \hat{A} \hat{j} \hat{E}$ $\hat{A} \hat{C} \hat{\circ} \hat{u}$
 $\hat{p} \hat{O} \hat{A} \hat{C} \hat{\circ} \hat{C} \hat{j} \hat{x} \hat{o}$ (Tensile forces) $\mid \hat{z} \hat{U} \hat{C} \hat{o} \hat{A} \hat{I} \hat{\theta}$.

1.32 (5) $\hat{A} \hat{\circ} \hat{5} \mid \hat{\theta} \hat{E} \hat{U} \hat{i} \hat{\theta} \mid \hat{A} \hat{j} \hat{O} \hat{C} \hat{y} \hat{A} \hat{D} \mid \circ \hat{A} \hat{U} \hat{A} \hat{I} \hat{y} \hat{E} \hat{a} \hat{y} \hat{U} \hat{A} \hat{C} \hat{\circ} \hat{o}$
 $\mid \hat{3/4} \hat{j} \hat{3/4} \hat{C} \hat{y} \hat{A} \hat{j} \hat{C} \hat{\circ} \hat{A}$ (Equilibrium of Three Forces)
 $\hat{O} \mid \hat{A} \hat{j} \hat{O} \hat{C} \hat{y} \hat{A} \hat{D} \mid \circ \hat{A} \hat{U} \hat{A} \hat{I} \hat{y} \hat{E} \hat{a} \hat{y} \hat{U} \hat{A} \hat{C} \hat{\circ} \hat{u} \ll \hat{3/4} \hat{E} \hat{i} \circ \hat{A} \hat{j} \hat{C} \hat{\circ} \hat{A} \hat{A} \hat{\theta}$
 $\hat{A} \hat{o} \hat{3/4} \hat{O} \hat{i} \hat{l} \hat{A} \hat{j} \hat{E} \hat{j} \hat{\theta} \ll \hat{A} \hat{\circ} \hat{O} \hat{3/4} \hat{C} \hat{o} \hat{3/4} \hat{A} \hat{\circ} \hat{A} \hat{A} \hat{\theta} \hat{A} \hat{n} \hat{I} \hat{\theta}$.
 $\hat{\S} \hat{A} \hat{O} \hat{o} \ll \hat{o} \hat{a} \hat{y} \hat{U} \hat{A} \hat{C} \hat{\circ} \hat{u} \hat{1/4} \hat{A} \mid \circ \hat{A} \hat{U} \hat{A} \hat{I} \hat{\theta} \hat{\S} \hat{j} \hat{I} \hat{u} \hat{\circ} \hat{O} \hat{U} \hat{C} \hat{A} \hat{\theta}$
 $\hat{o} \hat{o} \hat{3/4} \hat{O} \hat{i} \hat{\S} \hat{A} \hat{n} \hat{I} \hat{\theta} \ll \hat{\theta} \hat{A} \hat{D} \hat{\circ} \hat{A} \hat{\circ} \hat{3/4} \hat{C} \hat{o} \hat{3/4} \hat{\theta} \hat{p} \hat{\circ} \hat{1/2} \hat{A} \hat{j} \hat{p} \hat{O} \hat{i} \hat{z}$
 $\hat{\S} \hat{A} \hat{n} \hat{I} \mid \hat{A} \hat{y} \hat{A} \hat{\circ} \hat{3/4} \hat{O} \hat{o} \hat{z} \hat{U} \hat{A} \hat{A} \hat{j} \hat{\theta}$.

$\hat{p} \hat{A} \hat{u} \hat{\circ} \hat{E} \hat{A} \hat{y} \hat{A} \hat{O} \hat{A} \hat{j} \hat{U} \hat{z} \hat{U} \hat{A} \hat{A} \hat{j} \hat{\theta}$; $\mid \hat{A} \hat{j} \hat{O} \hat{C} \hat{y} \hat{A} \hat{D} \mid \circ \hat{A} \hat{U} \hat{A} \hat{I} \hat{y} \hat{E} \hat{a} \hat{y} \hat{U}$
 $\hat{A} \hat{C} \hat{\circ} \hat{u} \hat{\circ} \hat{C} \hat{O} \hat{o} \hat{p}, \hat{q}, \hat{r} \pm \hat{E} \hat{i} \mid \hat{z} \hat{U} \hat{z} \hat{p}, \hat{q} \pm \hat{y} \hat{A} \hat{A} \hat{U} \hat{E} \hat{C} \hat{U} \hat{\circ} \hat{1/4} \hat{A} \mid \circ \hat{A} \hat{U} \hat{A} \hat{I} \hat{\theta} \hat{\S} \hat{j} \hat{I} \hat{z} \hat{C} \hat{\theta}$
 $\hat{O} \hat{\circ} \hat{E} \hat{\S} \hat{A} \hat{A}, \hat{B}, \hat{1} \pm \hat{y} \hat{E} \hat{z} \hat{\S} \hat{3/4} \hat{U} \hat{\theta} \hat{p} \hat{O} \hat{O} \hat{U} \hat{C} \hat{z} \hat{\circ} \hat{C} \hat{o} \hat{A} \hat{1/4} \hat{o} \hat{1.85} \hat{\theta} \hat{z} \hat{\theta} \hat{E} \hat{A} \hat{A} \hat{j} \hat{U} \hat{\pm} \hat{I} \hat{i} \hat{z}$
 $\ll \hat{u} \hat{A} \hat{C} \hat{\circ} \hat{u} \hat{a} \hat{y} \hat{U} \hat{\theta} \circ \hat{A} \hat{j} \hat{C} \hat{\circ} \hat{A} \hat{A} \hat{A} \hat{O} \hat{o} \hat{A} \hat{3/4} \hat{j} \hat{\theta} \ll \hat{A} \hat{U} \hat{E} \hat{U} \hat{l} \hat{\circ} \hat{O} \hat{A} \hat{O} \hat{D} \ll \hat{o} \mid \hat{A} \hat{j} \hat{O} \hat{\circ} \hat{C}$
 $\hat{A}, \hat{B}, \hat{1} \pm \hat{y} \hat{U} \hat{\theta} \hat{\S} \hat{j} \hat{I} \hat{A} \hat{U} \hat{E} \hat{C} \hat{3/4} \hat{O} \hat{o} \hat{D} \hat{3/4} \hat{\theta} \hat{O} \hat{E} \hat{A} \hat{j} \hat{D}$. $\hat{E} \hat{j} \hat{\theta} \hat{p}, \hat{q} \pm \hat{y} \hat{U} \hat{\theta} \hat{A} \hat{C} \hat{\circ} \hat{u}$
 $\hat{p} \hat{i} \hat{\S} \hat{j} \hat{\theta} \hat{\circ} \hat{1/4} \hat{o} \hat{o} \hat{3/4} \hat{O} \hat{i} \hat{y} \hat{E} \hat{E}$. $\hat{z} \hat{\S} \hat{A} \ll \hat{A} \hat{U} \hat{E} \hat{U} \hat{l} \ll \hat{o} \mid \hat{A} \hat{j} \hat{O} \hat{\circ} \hat{C} \hat{A}, \hat{B}, \hat{1} \pm \hat{y} \hat{U} \hat{\theta} \hat{\S} \hat{j} \hat{I}$
 $\hat{A} \hat{U} \hat{E} \hat{C} \hat{3/4} \hat{O} \hat{o} \hat{D} \hat{3/4} \hat{U} \hat{l} \hat{A} \hat{C} \hat{\circ} \hat{C} \times$ (resultant) $\hat{z} \hat{D} \hat{o} \hat{3/4} \hat{E} \hat{C} \hat{o} \hat{3/4} \hat{E} \hat{C} \hat{A} \hat{j} \hat{o} \hat{z} \hat{C} \hat{\circ} \hat{1/4} \hat{A} \hat{j} \hat{D}$. $\hat{p} \hat{3/4} \hat{E} \hat{j} \hat{\theta}$
 $\hat{a} \hat{y} \hat{E} \hat{j} \hat{o} \hat{A} \hat{C} \hat{\circ} \hat{o} \hat{i} \hat{l} \hat{o} \hat{A}, \hat{B}, \hat{1} \pm \hat{y} \hat{U} \hat{\theta} \hat{\S} \hat{j} \hat{I} \hat{A} \hat{U} \hat{E} \hat{C} \hat{3/4} \hat{O} \hat{o} \hat{D} \hat{3/4} \hat{U} \hat{l} \hat{A} \hat{C} \hat{\circ} \hat{C} \times \hat{A} \hat{j} \hat{D} \hat{o}$
 $\hat{p} \hat{O} \hat{o} \hat{3/4} \hat{\theta} \hat{O} \hat{E} \hat{A} \hat{j} \hat{D}$ (A1-84 1.85)

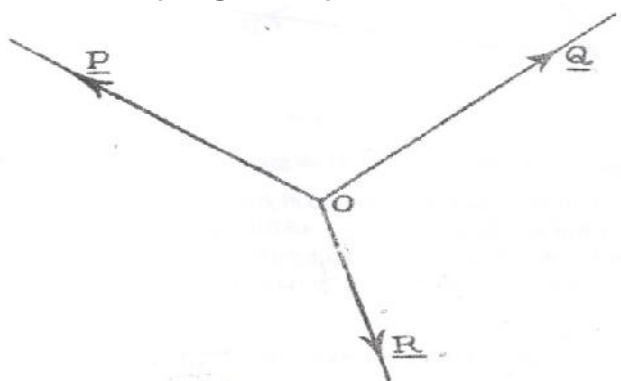


A1-85

\rightarrow $\text{SA}_{A_1, B_1} \pm \text{y} \cup \circ \text{S}_{, i} \hat{I} \text{ R} \pm \text{y} \hat{A} \cdot \text{3/4} \hat{I} \circ \text{3/4} \hat{I} \text{, SAñ } \hat{I} \hat{o} . \text{p} \text{DS} \hat{A}_i \hat{A}_{B_2, B_3}$
 $\pm \text{y} \cup \circ \text{ò} \hat{u} \text{C} \text{, } \text{C} \hat{o} \hat{A} \text{CÉD } | \circ \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \text{ S}_{, i} \text{ ðÉø } \pm \hat{I} \hat{o} \hat{A} \text{3/4} \hat{I} \hat{A} \text{y}_{A_1 B_2, A_1 B_3}$
 $\pm \text{y} \cup \circ \text{S}_{, i} \hat{I} \text{, } \hat{u} \text{ R} \text{ } \hat{I} \circ \text{3/4} \hat{I} \text{, SAñ } \hat{I} \hat{o} . \rightarrow \text{3/4} \hat{A}_i \text{ø } \text{R} \rightarrow \text{ÉD } \hat{A}_i \text{ } \hat{a} \hat{A} \hat{A}_i \text{, } \hat{o}$
 $\hat{A} \text{CÉD } | \circ \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \text{ S}_{, i} \text{ ðÉy } \circ \text{1/4} \hat{I} \hat{I} | \circ \text{ø} \text{ö} \text{ } \text{3/4} \hat{C} \hat{o} \text{3/4} \hat{C} \hat{o} \text{ } \ll \text{ } \hat{A} \hat{A} \hat{S} \hat{A} \hat{n} \hat{I} \hat{o} .$
 $\ll \text{3/4} \hat{I} \hat{A} \text{D } \hat{o}, \text{R} \pm \text{y} \hat{A} \hat{A} \hat{u} \hat{E} \text{y} | \circ \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \text{ S}_{, i} \hat{I} \text{, } \hat{u} \text{ A}_1 \hat{I} \hat{I} \text{ } \circ \text{1/4} \hat{I} \hat{I} | \circ \text{ø} \text{ö} \text{ } \hat{O}$
 $\text{3/4} \hat{C} \hat{o} \text{3/4} \hat{C} \hat{o} \ll \text{ } \hat{A} \hat{A} \hat{S} \hat{A} \hat{n} \hat{I} \hat{o} .$

$\rightarrow \text{É} \text{ø } \hat{A}_i \pm \text{y} \hat{A} \text{D } \text{P} \hat{A} \text{CÉD } | \circ \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \text{ S}_{, i} \text{ ðÉø } \hat{u} \text{C} \hat{A}_i \text{ } \text{3/4} \hat{U} | \hat{A}_i \hat{O} \text{ ð} \hat{u} \text{C} \hat{C} .$
 $\rightarrow \text{3/4} \hat{A}_i \text{ø } \text{S} \hat{A} \hat{u} \hat{U} \text{E} \hat{A} \text{ } \text{3/4} \hat{C} \hat{o} \text{ } \text{P} \hat{A} \text{CÉD } | \circ \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \text{ S}_{, i} \text{ ðÉø } \hat{u} \text{C} \hat{A}_i \text{ } \text{3/4} \hat{U} | \hat{A}_i \hat{O}$
 $\text{ò} \hat{u} \text{C} \hat{C} \hat{I} \text{ } \circ \text{1/4} \hat{I} \hat{I} | \circ \text{ø} \text{ö} . \rightarrow \text{S} \hat{A} \text{ } \text{P} \hat{A} \text{Cø } \text{ } \hat{u} \text{C} \text{ } \hat{u} \hat{A}_i \text{O} \hat{u} \text{C} \hat{C} \hat{A} \hat{E} \hat{C} \hat{A}_i \text{, } \times \hat{o}$
 $| \circ \text{ø} \text{ö} .$

$\ll \text{3/4} \hat{I} \hat{A} \text{D} \ll \text{ } \hat{o} \text{3/4} \hat{C} \hat{o} \text{ } \text{P} \hat{A} \text{CÉD } | \circ \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \text{ S}_{, i} \text{ ð } \text{ } \text{1/4} \hat{O} \hat{o} \text{ } | \text{ } \hat{I} \text{ñ } \hat{I} \hat{u} \text{C} \hat{D} . \text{S} \hat{A} \hat{O} \hat{o}$
 $\ll \hat{o} \hat{a} \text{ } \text{y} \hat{U} \hat{A} \text{ } \circ \text{ } \hat{U} \hat{o} \text{ } \text{ } \hat{O} \hat{u} \text{C} \hat{C} \hat{A} \text{ø } \text{ } \hat{o} \text{3/4} \hat{C} \hat{o} \text{ } \text{S} \hat{A} \hat{n} \hat{I} \hat{o} \ll \text{ } \text{ø} \hat{A} \text{D } \text{p} \text{ } \text{1/2} \hat{A}_i \text{, } \text{p} \hat{O} \hat{i} \text{,}$
 $\text{S} \hat{A} \hat{n} \hat{I} | \hat{A} \text{y} \hat{A} \cdot \text{3/4} \hat{O} \hat{o} \text{, } \hat{u} \hat{A} \hat{O} \hat{A}_i \hat{U} \text{ } \hat{C} \hat{U} \hat{A} \hat{A}_i \hat{o} .$



A1-86

$\ll \text{3/4} \hat{u}_{, i} \text{ } \text{P, Q, R} \pm \text{y} \cup \circ \hat{A} \text{ } \circ \text{, } \hat{u} \text{ } \hat{O} \text{ } \text{3/4} \hat{C} \hat{o} \text{3/4} \hat{C} \hat{o} \text{ } | \circ \hat{A} \hat{u} \hat{A} \hat{O} \hat{I} \text{ } \hat{O} \text{, } \text{ðÉU} \hat{i} \text{ } \hat{o}$
 $| \hat{A}_i \hat{O} \cdot \text{C} \hat{I} \text{ } \hat{A} \hat{I} \text{C} \cdot \hat{A} \hat{A} \text{ø } \hat{A} \hat{O} \hat{A} \text{3/4} \hat{I} \hat{I} \text{ } | \text{ } \hat{I} \text{ñ } \hat{I} \text{u} \text{ } .$
 $\text{ } \text{O} \text{3/4} \hat{A}_i \hat{A} \text{3/4} \hat{I} \ll \text{ } \hat{u} \hat{A} \text{C} \text{ } \circ \text{ } | \hat{C} \text{ø } \hat{A}_i \hat{o} \text{p} \text{ } \text{1/2} \hat{A} \hat{u} \hat{E} \hat{E} \hat{A}_i \hat{A} \text{y} \ll \text{ } \hat{A} \hat{u} \hat{U} \hat{u} \hat{A}_i \text{ } \text{3/4} \hat{U} \hat{o}$
 $\text{p} \hat{A} \hat{n} \hat{I} \hat{A} \text{C} \text{ } \circ \text{ } \hat{u} \text{ } \text{ } \hat{o} \text{3/4} \hat{C} \hat{o} \text{3/4} \hat{C} \hat{o} \text{ } \text{S} \hat{A} \hat{n} \hat{I} \hat{o} . \ll \text{ } \hat{A} \text{, } \text{C} \text{ } \text{P, Q} \pm \text{É} \hat{I} \text{ } | \text{ } \hat{I} \text{ñ } \hat{I} \text{u} \text{ } .$
 $\text{p} \hat{A} \hat{u} \hat{E} \hat{C} \hat{U} \cdot \text{1/4} \hat{A} | \circ \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} .$

$\mathbb{S}_i \hat{I} \cup \Lambda_{1/4} \bar{o} \ 1.86 \ \varnothing \ \mathbb{S}_i \bar{o} \hat{E} \hat{A} \hat{A}_i \hat{U} \ O \ \hat{A} \varnothing \ \circ \acute{o} \frac{3}{4} \hat{I} \ \bar{o} \ . \ p \hat{o} \ | \ \hat{A}_i \varnothing \frac{3}{4} \ \underline{P, Q}$
 $\pm \acute{y} \hat{A} \hat{E} \hat{A} \hat{U} \hat{E} \acute{y} \ \frac{1}{3} \hat{I} \ \hat{A} \hat{A} \acute{y} \ \hat{O} \hat{A} \hat{E} \hat{S} \hat{A} \ \hat{I} \ \circ \varnothing \hat{O} \hat{o} \ \hat{A}_i \ \hat{S} \frac{3}{4} \hat{U} \ | \ \hat{A}_i \hat{O} \ \hat{A} \hat{C} \ \circ \hat{A}_i \frac{3}{4} \varnothing$
 $\hat{S} \hat{A} \hat{n} \hat{I} \ \bar{o} \ . \ \neg \ \hat{E}_i \varnothing \ \underline{P, Q, R} \ \pm \acute{y} \hat{U} \hat{o} \ \hat{A} \hat{C} \ \circ \ \hat{u} \ \circ \hat{A} \hat{C} \ \hat{A} \hat{A} \varnothing \ p \hat{O} \hat{o} \frac{3}{4} \hat{A}_i \varnothing \ \underline{P, Q}$
 $\pm \acute{y} \hat{A} \hat{E} \hat{A} \hat{U} \hat{E} \acute{y} \ \frac{1}{3} \hat{I} \ \hat{A} \hat{A} \acute{y} \ \underline{R} \ \pm \acute{y} \hat{A} \ \hat{I} \ \circ \hat{A} \hat{o} \hat{A} \hat{I} \ \hat{o} \ \frac{3}{4} \varnothing \ \hat{S} \hat{A} \hat{n} \hat{I} \ \bar{o} \ .$

$\neg \ \hat{E}_i \varnothing \ \hat{S} \hat{A} \ \hat{I} \ \circ \hat{A} \hat{U} \hat{A} \hat{I} \ \bar{o} \ \mathbb{S}_i \bar{o} \hat{E} \varnothing \ p \hat{O} \hat{o} \frac{3}{4} \hat{A} \hat{y} \hat{E} \hat{C} \ p \hat{O} \ \hat{A} \hat{C} \ \circ \ \hat{u}$
 $\acute{y} \ \hat{E} \ | \ \hat{A}_i \hat{y} \hat{U} \ \circ \hat{A} \hat{A}_i \hat{I} \ \hat{S} \ \hat{O} \hat{E} \hat{A}_i \hat{D} \ . \ \neg \ \hat{S} \hat{A} \ \underline{R} \ \acute{y} \ \hat{I} \ \circ \hat{A} \hat{U} \hat{A} \hat{I} \ \bar{o} \ \mathbb{S}_i \hat{I} \ \bar{o} \ O \ \hat{A} \hat{E} \hat{C}$
 $\hat{I} \ \circ \varnothing \hat{A} \ \hat{S} \hat{A} \hat{n} \hat{I} \ \bar{o} \ .$

$p \hat{A} \hat{n} \ \frac{1}{4} \hat{A} \frac{3}{4} \hat{I} \ \underline{P, Q} \ \pm \acute{y} \hat{U} \hat{o} \ \hat{A} \hat{C} \ \circ \ \hat{u} \ p \ \frac{1}{2} \hat{A}_i \ \ll \ \hat{A} \hat{A} \hat{D} \hat{I} \ \bar{o} \ . \ \ll \ \hat{A} \hat{U} \hat{E} \acute{y}$
 $\frac{1}{3} \hat{I} \ \hat{A} \hat{A} \acute{y} \ \hat{A} \hat{C} \ \circ \hat{O} \hat{o} \ \ll \ \hat{A} \ \hat{U} \hat{I} \hat{I} \ p \ \frac{1}{2} \hat{A}_i \ \hat{p} \hat{O} \hat{I} \hat{I} \ \bar{o} \ . \ \neg \ \hat{E}_i \varnothing \ \hat{a} \hat{y} \hat{U}$
 $\hat{A} \hat{C} \ \circ \ \hat{U} \hat{o} \ \circ \hat{A} \hat{C} \ \hat{A} \hat{A} \hat{A} \hat{O} \hat{A} \hat{A} \frac{3}{4} \hat{I} \varnothing \ \underline{R} \ \pm \acute{y} \hat{A} \hat{D} \ \underline{P, Q} \ \pm \acute{y} \hat{A} \hat{A} \hat{U} \hat{E} \acute{y}$
 $\frac{1}{3} \hat{I} \ \hat{A} \hat{A} \acute{y} \ \hat{A} \hat{C} \ \circ \hat{I} \hat{I} \hat{I} \ \circ \hat{A} \hat{E}_i \ | \ \hat{A} \frac{3}{4} \hat{O} \hat{A}_i \ \times \hat{o} \ \ll \ \hat{o} \ | \ \frac{3}{4} \hat{I} \ \hat{A} \hat{A} \hat{E} \acute{y} \ \hat{I} \ \circ \hat{A} \hat{U} \hat{A} \hat{I} \ \bar{o}$
 $\mathbb{S}_i \bar{o} \hat{E} \hat{O} \hat{o} \ \ll \ \hat{A} \hat{A} \ \hat{S} \hat{A} \hat{n} \hat{I} \ \bar{o} \ . \ \neg \ \hat{S} \hat{A} \ \underline{R} \ \pm \acute{y} \hat{E} \ \hat{A} \hat{C} \ \circ \hat{A} \hat{y} \ \frac{3}{4} \hat{C} \ \circ \ \underline{P, Q} \ \pm \acute{y} \hat{U} \hat{o}$
 $\hat{A} \hat{C} \ \circ \ \hat{C} \hat{y} \ \frac{3}{4} \hat{C} \ \circ \hat{I} \hat{I} \ p \ \frac{1}{2} \hat{A}_i \ \hat{p} \hat{O} \hat{I} \ \hat{S} \hat{A} \hat{n} \hat{I} \ \bar{o} \ .$

$\pm \hat{E} \hat{S} \hat{A} \ \underline{P, Q, R} \ \pm \acute{y} \hat{U} \hat{o} \ \hat{A} \hat{C} \ \circ \ \hat{I} \ \hat{C} \hat{o} \hat{A}_i \hat{o} \ \acute{y} \hat{U} \hat{I} \ | \ \hat{S}_i \hat{y} \hat{U} \ p \ \frac{1}{2} \hat{A}_i \hat{I} \ \bar{o} \ .$
 $\hat{O} \ \bar{o} \hat{E} \hat{U} \hat{I} \ \hat{o} \ | \ \hat{A}_i \hat{O} \hat{u} \hat{A} \hat{D} \ \hat{S} \hat{A} \ \frac{3}{4} \hat{C} \hat{o} \frac{3}{4} \hat{S} \hat{A} \ \hat{a} \hat{y} \hat{U} \ \hat{A} \hat{C} \ \circ \ \hat{u} \ \hat{I} \ \circ \hat{A} \hat{U} \hat{A} \hat{D} \hat{I}$
 $\ll \ \hat{I} \ \circ \hat{A} \hat{C} \ \hat{A} \hat{A} \varnothing \ \hat{A} \hat{o} \frac{3}{4} \hat{O} \hat{o} \frac{3}{4} \hat{I} \varnothing \ \ll \ \hat{A} \ \hat{O} \ \hat{O} \hat{u} \hat{C} \hat{A} \varnothing \ \circ \acute{o} \frac{3}{4} \hat{I} \ \hat{S} \hat{A} \hat{n} \hat{I} \ \bar{o} \ .$
 $\neg \ \frac{3}{4} \hat{A}_i \varnothing \ \circ \hat{A} \hat{C} \ \hat{A} \ \hat{C} \hat{A} \hat{o} \frac{3}{4} \hat{E} \ \hat{u} \ \hat{O} \ \frac{3}{4} \hat{E} \hat{O} \ \hat{D} \ \hat{C} \hat{U} \ \frac{1}{4} \hat{A} \ \circ \hat{A} \hat{C} \ \hat{A}$
 $\hat{C} \hat{A} \hat{o} \frac{3}{4} \hat{E} \ \hat{U} \hat{I} \hat{I} \ \hat{I} \hat{I} \hat{I} \ | \ \hat{A} \hat{y} \hat{A} \ \frac{3}{4} \hat{O} \hat{o} \ \ll \ \hat{E} \hat{O} \varnothing \ \hat{S} \hat{A} \hat{n} \hat{I} \ \bar{o} \ .$

$\neg \ \hat{S} \hat{A} \ p \hat{A}_i \hat{A} \hat{A} \hat{E} \hat{D} \ (\text{Lami's theorem}) \ \hat{S} \frac{3}{4} \hat{U} \hat{E} \hat{o} \ \frac{3}{4} \hat{o} \ \hat{A} \hat{A} \hat{y} \hat{A} \hat{I} \ \hat{o} \ \frac{3}{4} \hat{S} \hat{A}_i$
 $\ll \ \varnothing \hat{A} \hat{D} \ \ll \ \hat{u} \hat{A} \hat{C} \ \circ \ \hat{C} \ \acute{y} \hat{U} \hat{I} \ | \ \hat{S}_i \hat{y} \hat{U} \ \hat{I} \ \hat{O} \hat{I} \hat{I} \ \hat{o} \ \frac{3}{4} \hat{I} \ \ll \ \hat{A} \hat{O} \hat{o} \ p \hat{O} \ \frac{3}{4} \hat{C} \hat{o}$
 $\hat{A} \hat{C}_i \hat{O} \hat{S} \frac{3}{4} \hat{I} \ \ll \ \varnothing \hat{A} \hat{D} \ \hat{O} \ \hat{A} \ \hat{A} \hat{A} \frac{1}{4} \ \ll \ \hat{A} \hat{o} \hat{A} \hat{y} \ \hat{D} \ \frac{1}{2} \ | \ \hat{S}_i \hat{n} \ \hat{S} \frac{1}{4} \hat{I} \ \hat{S} \hat{A} \hat{n} \hat{E} \hat{A}$
 $\hat{C} \hat{A} \hat{o} \frac{3}{4} \hat{E} \ \hat{C} \hat{o} \ | \ \hat{A} \hat{E} \hat{A}_i \hat{o} \ .$

$\underline{R} = 180\underline{i} - 90\underline{j} + 60\underline{k}$ ±ýÈ ¼c°Âc | °ÄüÄÎ õ ¼c° °ì | ±¼c÷ ¼c° °Âcø μÄÄÌ ò ¼c° °Âc° Äì |, ñ |.

þí ì $\underline{R} = 180\underline{i} - 90\underline{j} + 60\underline{k}$

$$\hat{R} = \frac{\underline{R}}{|\underline{R}|}$$

$$= \frac{180\underline{i} - 90\underline{j} + 60\underline{k}}{\sqrt{180^2 + 90^2 + 60^2}}$$

$$\hat{R} = \frac{6}{7}\underline{i} - \frac{3}{7}\underline{j} + \frac{2}{7}\underline{k}$$

¬ ì õ.

« ¼j ÄÐ, $R = 210r$ ±Éì |, ñ ¼jø, r ±ýÄÐ, \underline{R} ý ¼c° °Âc§Ä§Ä « ° ÄÖõ μÄÄÌ ò ¼c° °ÂcÄì ò. ±É§Ä, \underline{F} ý ±¼c÷ ò ¼c° °° Ä « ÈcÄü ì õ μÄÄÌ ò ¼c° °Âc,

$$-\frac{6}{7}\underline{i} + \frac{3}{7}\underline{j} - \frac{2}{7}\underline{k} \text{ ¬ ì õ.}$$

Äj ¼c; 1-5

\underline{F} ±ýÈ ¼c° °Âc-ý ±ñ Ä¼cõð 490 ±ýÜõ, « Ð | °ÄüÄÎ õ ¼c° °° Ä $\left(\frac{2}{7}\underline{i} + \frac{9}{7}\underline{j} + \frac{6}{7}\underline{k}\right)$ ±ýÈ μÄÄÌ ò ¼c° °Âc « ÈcÄü ì õ ±ýÜõ |, ñ ¼jø, F^3 Ä° ÄÄÜì |.

þí ì $\underline{F} = |\underline{F}| = 490 \pmýÜõ$, « ¼ý ¼c° °° Ä $\underline{f} = \frac{1}{7}(2\underline{i} - 9\underline{j} + 6\underline{k})$ ±ýÈ μÄÄÌ ò ¼c° °ÂcÄj Öõ « ÈcÄ¼jø,

$$\underline{F} = F \underline{f}$$

$$= 490 \left[\frac{1}{7}(2\underline{i} - 9\underline{j} + 6\underline{k}) \right]$$

$$= 70(2\underline{i} - 9\underline{j} + 6\underline{k})$$

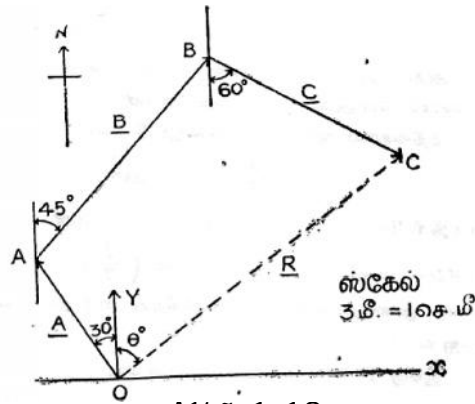
$$= 140\underline{i} - 630\underline{j} + 420\underline{k} \text{ ¬ ì õ.}$$

Äj ¼c; 1-6

° Ö çÄ « ÇÄjÄ÷ (Surveyor) |, ÄcÄÄõ ´ýÈý ±ø° Ä, ü Ä° ÄÄÜì |, Ó¼Äcø ° ì ÈcÄcø¼ ±ø° ÄõðüçÄÄcÖóð, $N30^\circ W$ ±ýÈ ¼c° °Âcø (« ¼j ÄÐ Ä¼¼c° °ÂcÄcÖóð 30° §Äü ì ¼c° °Âcø « øÄÐ Ä¼¼c° °ì ì 80° §Äü ì ¼c° °Âcø) 12 Äð¼÷ | °ýÜ, « í cÖóð $N45^\circ E$; ±ýÈ ¼c° °Âcø $15\sqrt{2}$ Äð¼÷ | ¼j Ä° Äì ¼óð, ÄÈì « í cÖóð $S60^\circ E$ ±ýÈ ¼c° °Âcø $10\sqrt{3}$ Äð¼÷ | °ø cÈj÷. þÜ¼cÄj Äö¼° ¼ó¼ òüçc° ÄÖõ, ÐÄì òðüçc° ÄÖõ §° ò¼cì õ §ÄjÐ, |, ÄcÄÄõ Ä° ÄÄÜì |, òÄì |, ±ýÈjø, « ° Ä, Üì ì üç | ¼j Ä° ÄÖõ,

Ճձի ուղղահայտ եռանկյան կողմերը a, b, c և անկյունները α, β, γ հարաբերակները կոչվում են Կոսինոսի և Տանգենսի թեորեմներ:

Վերջինս a, b, c կապում է α, β, γ անկյունների հետ: $\cos \alpha = \frac{b^2 + c^2 - a^2}{2bc}$ և այլն:



Վերջինս 1-18

քանակները $|A| = A = 12 \text{ կմ} = OA$

$|B| = B = 15 \times \sqrt{2} \text{ կմ}$

$|C| = 10 \times \sqrt{3} \text{ կմ}$

Վեկերի α, β, γ անկյունները α, β, γ անկյունների հետ կապում է $\cos \alpha = \frac{b^2 + c^2 - a^2}{2bc}$ և այլն:

$A_x = -A \sin 30^\circ = -6; B_x = B \sin 45^\circ = 15; C_x = C \sin 60^\circ = 15$

$A_y = A \cos 30^\circ = 6\sqrt{3}; B_y = B \cos 45^\circ = 15; C_y = -C \cos 60^\circ = -5\sqrt{3}$ և այլն:

Երևաքանակները

$R_x = A_x + B_x + C_x$

$R_y = A_y + B_y + C_y$

$= -6 + 15 + 15$

$= 6\sqrt{3} + 15 - 5\sqrt{3}$

$= 24 \text{ կմ} \div$

$= \sqrt{3} + 15$

$= 16.732 \text{ կմ} \div$

Երևաքանակը $R = \sqrt{R_x^2 + R_y^2}$

$= \sqrt{(24)^2 + (16.732)^2}$

$= \sqrt{855.9}$

$= 29.2 \text{ կմ}$

Վեկերի α, β, γ անկյունները α, β, γ անկյունների հետ կապում է $\cos \alpha = \frac{b^2 + c^2 - a^2}{2bc}$ և այլն:

$\tan \alpha = \frac{R_x}{R_y}$

$$= \frac{24}{16.732}$$

$$= 1.434 \pm \hat{y} \hat{e}_j \hat{i} \hat{o}.$$

« $\hat{o} \hat{A} \hat{D}$ » = $55^\circ 7'$ - $\hat{i} \hat{o}$.

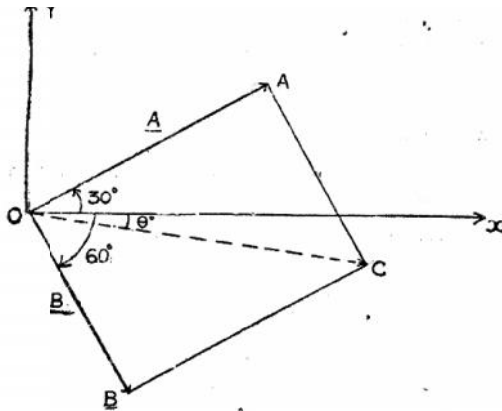
$\pm \hat{E} \hat{S} \hat{A} \hat{O} \hat{C} = 29.2 \hat{A} \hat{D} \hat{1} \hat{4} \hat{d} \hat{i} \hat{v} ; \hat{v}^\circ = 55^\circ 7' - \hat{i} \hat{o}$.

$\hat{i} \hat{E} \hat{o} \hat{o} : \hat{A} \hat{v} \hat{A} \hat{1} \hat{4} \hat{o} \hat{3} \hat{4} \hat{o} \hat{O} \hat{C} \hat{A} \hat{v} \hat{y} \hat{y} \hat{C} \hat{o} \hat{2} \hat{E} \hat{i} \hat{l} \hat{v} \hat{v} \hat{E} \hat{A} \hat{9.8} \hat{i} \hat{o} \hat{A} \hat{f} \hat{v} \hat{x} \hat{o} \hat{v} \hat{v}^\circ = 55^\circ \hat{i} \hat{l} \hat{i}$
 $\hat{o} \hat{A} \hat{A} \hat{j} \hat{x} \hat{o} \hat{p} \hat{O} \hat{o} \hat{A} \hat{v} \hat{3} \hat{4} \hat{i} \hat{j} \hat{n} \hat{v}$.

$\hat{A} \hat{j} \hat{3} \hat{4} \hat{i} \hat{c} \hat{1} \hat{-} \hat{7} \hat{A} \hat{v} \hat{B} \pm \hat{y} \hat{E} \hat{3} \hat{4} \hat{c} \hat{v} \hat{o} \hat{A} \hat{c} \hat{C} \hat{v} \hat{y} \pm \hat{n} \hat{A} \hat{3} \hat{4} \hat{o} \hat{o} \hat{v} \hat{U} \hat{o} \hat{v} \hat{v} \hat{v} \hat{A} \hat{v} \hat{u} \hat{v} \hat{c} \hat{v} \hat{1} \hat{4} \hat{v} \hat{v} \hat{i} \hat{o} \hat{o}$
« $\hat{v} \hat{A} \hat{i} \hat{l} \hat{o} \hat{S} \hat{v} \hat{j} \hat{1} \hat{2} \hat{i} \hat{v} \hat{U} \hat{o} \hat{A} \hat{v} \hat{A} \hat{O} \hat{A} \hat{j} \hat{U} ;$
 $\hat{3} \hat{4} \hat{c} \hat{v} \hat{o} \hat{A} \hat{c} \pm \hat{n} \hat{A} \hat{3} \hat{4} \hat{o} \hat{o} \hat{v} \hat{c} \hat{v} \hat{1} \hat{4} \hat{v} \hat{i} \hat{o} \hat{o} \hat{3} \hat{4} \hat{i} \hat{l} \hat{o}$
 $\hat{S} \hat{v} \hat{j} \hat{1} \hat{2} \hat{o}$

<u>A</u>	48	30°
<u>B</u>	36	-60°

$\hat{p} \hat{v} \hat{1} \hat{2} \hat{v} \hat{A} \hat{A} \hat{3} \hat{4} \hat{c} \hat{v} \hat{A} \hat{o} \hat{A} \hat{A} \hat{y} \hat{A} \hat{i} \hat{o} \hat{3} \hat{4} \hat{c} \hat{v} \hat{v} \hat{A} \hat{v} \hat{C} \hat{v} \hat{y} \hat{1} \hat{3} \hat{4} \hat{i} \hat{l} \hat{A} \hat{A} \hat{y} \hat{3} \hat{4} \hat{c} \hat{v} \hat{o} \hat{A} \hat{c} \hat{v} \hat{A} \hat{i} \hat{j} \hat{n} \hat{v}$
 $\hat{A} \hat{1} \hat{4} \hat{o} \hat{1} \hat{-} \hat{19} \hat{o} \hat{v} \hat{d} \hat{E} \hat{O} \hat{u} \hat{C} \hat{v} \hat{v} \hat{A} \hat{o} \hat{A} \hat{c} \hat{p} \hat{v} \hat{1} \hat{2} \hat{v} \hat{A} \hat{A} \hat{3} \hat{4} \hat{o} \hat{A} \hat{E} \hat{v}$
 $\underline{OA + OB = OC} - \hat{i} \hat{o}$.



$\hat{A} \hat{1} \hat{4} \hat{o} \hat{1} \hat{-} \hat{19}$

$\hat{A} \hat{v} \hat{A} \hat{1} \hat{4} \hat{o} \hat{3} \hat{4} \hat{o} \hat{O} \hat{C} \hat{y} \hat{y} \hat{C} \hat{o} \hat{5} \hat{i} \hat{o} \hat{A} \hat{f} \hat{v} \hat{i} \hat{o}$
 $\pm \hat{E} \hat{S} \hat{A} \hat{1} \hat{3} \hat{4} \hat{i} \hat{l} \hat{A} \hat{A} \hat{y} \hat{3} \hat{4} \hat{c} \hat{v} \hat{o} \hat{A} \hat{c} \hat{R} \hat{y} \pm \hat{n} \hat{A} \hat{3} \hat{4} \hat{o} \hat{o}$
 $= 5 \times 12 = 60 - \hat{i} \hat{o}$.

$\hat{S} \hat{A} \hat{O} \hat{o} \hat{A} \hat{1} \hat{4} \hat{o} \hat{3} \hat{4} \hat{o} \hat{A} \hat{O} \hat{C} = 37^\circ$ ($\hat{2} \hat{E} \hat{i} \hat{l} \hat{v} \hat{v} \hat{E} \hat{A}$)

$\hat{p} \hat{A} \hat{n} \hat{1} \hat{4} \hat{i} \hat{A} \hat{D} \hat{O} \hat{v} \hat{E}$ (Second Method)

$\hat{O} \hat{X} \hat{v} \hat{O} \hat{Y} \hat{v} \hat{i} \hat{l} \hat{v} \hat{C} \hat{o} \hat{i} \hat{j} \pm \hat{y} \hat{E} \hat{\mu} \hat{A} \hat{A} \hat{l} \hat{o} \hat{3} \hat{4} \hat{c} \hat{v} \hat{o} \hat{A} \hat{c} \hat{v} \hat{C} \hat{v} \hat{\pm} \hat{i} \hat{l} \hat{o} \hat{S} \hat{A} \hat{j} \hat{D}$,

$$\underline{A} = 48 \cos 30^\circ \hat{i} + 48 \sin 30^\circ \hat{j}$$

$$= 24\sqrt{3} \hat{i} + 24 \hat{j}$$

$$\underline{B} = 36 \cos 60^\circ \hat{i} - 36 \sin 60^\circ \hat{j}$$

$$\begin{aligned}
&= 18i - 18\sqrt{3}j \\
\therefore \underline{R} &= \underline{A} + \underline{B} \\
&= (24\sqrt{3} + 18)i + (24 - 18\sqrt{3})j \\
R_x &= 24\sqrt{3} + 18, R_y = 24 - 18\sqrt{3} \\
\therefore R^2 = |\underline{R}|^2 &= (24\sqrt{3} + 18)^2 + (24 - 18\sqrt{3})^2 \\
&= 36(4\sqrt{3} + 3)^2 + 36(4 - 3\sqrt{3})^2 \\
&= 3600 \\
\therefore R &= 60
\end{aligned}$$

∠ = ∠(R_x, R) = ∠(24√3 + 18, 24 - 18√3) = ∠(4√3 + 3, 4 - 3√3) = -6.928° = -6°53'

$$\begin{aligned}
\tan \alpha &= \frac{R_y}{R_x} = \frac{24 - 18\sqrt{3}}{24\sqrt{3} + 18} \\
&= \frac{4 - 3\sqrt{3}}{4\sqrt{3} + 3} \\
&= -\frac{1.196}{9.928} \\
&= -0.1205
\end{aligned}$$

∴ ∠ = -6°53'

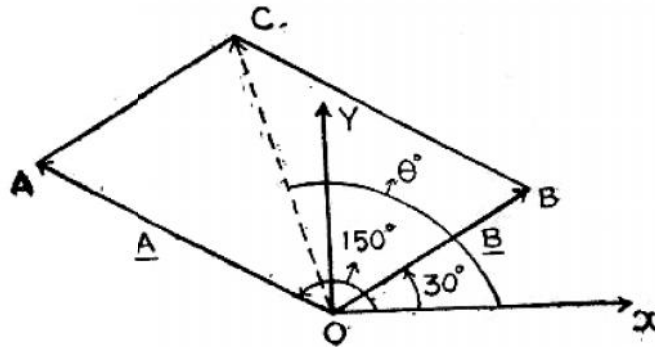
∠ = ∠(A, B) = ∠(12, 8) = 33.7°

Vector	Magnitude	Direction
<u>A</u>	12 [10 ⁻²] Åf	150°
<u>B</u>	8 [10 ⁻²] Åf	30°

∠ = ∠(A, B) = ∠(12, 8) = 33.7°

∠ = ∠(A, B) = ∠(12, 8) = 33.7°

ΣΑΟ = 109° (2Èì Ì ·· ÈĀ) → Ì õ.



Á¼õ 1-20

ρÃñ ¼ĵ ĀĎ ĀĔ;

OX, OY ¼ċ ·· ° ·· Ç ĩ, ĵ ± ŷ È μĀĀ Ì ð ¼ċ ·· ° Āċ, ũ Ā ·· ĀĀ Û Ì Ì Ā ŷ È ĩ ø,

$$\underline{A} = 12(\cos 150\hat{i} + \sin 150\hat{j}) = -6\sqrt{3}\hat{i} + 6\hat{j}$$

$$\underline{B} = 8(\cos 30\hat{i} + \sin 30\hat{j}) = 4\sqrt{3}\hat{i} + 4\hat{j}$$

$$\therefore \underline{R} = \underline{A} + \underline{B}$$

$$= -2\sqrt{3}\hat{i} + 10\hat{j}$$

$$\therefore R_x = -2\sqrt{3}; R_y = 10$$

$$\therefore R = \sqrt{R_x^2 + R_y^2} = \sqrt{(-2\sqrt{3})^2 + 10^2}$$

$$= \sqrt{112} = 4\sqrt{7} = 10.584 [10^{-2}] \text{ ĀĔ}$$

OC ± ŷ È Šċ ÷ Š ĩ Ĩ , x « Ĩ Ĩ ¼ ŷ , " ± ŷ È Š ĩ Ĩ ½ ð ·· ¼ « ·· Ā Ì Ì Ā ŷ È ĩ ø,

$$\tan \theta = \frac{R_y}{R_x} = -\frac{10}{2\sqrt{3}} = -\frac{5\sqrt{3}}{3} = -2.887$$

$$\therefore \theta = 180 - 70^{\circ} 54' = 109^{\circ} 6' \rightarrow \text{Ì õ.}$$

Āĵ ¼ċ ċ 1-9

$N 30^{\circ} W$ ± ŷ È ¼ċ ·· ° Āċ | ° Ā ũ Ā Ĩ õ 34.64 ċ, ċ, ± ·· ¼ Ā ¼ċ ð ũ Ç Ā ± ŷ È

¼ċ ·· ° Āċ Ā, | ¼ ũ Ì ¼ċ ·· ° Āċ | ° Ā ũ Ā Ĩ õ 40 ċ, ċ, ± ·· ¼ Ā ¼ċ ð ũ Ç B ± ŷ È

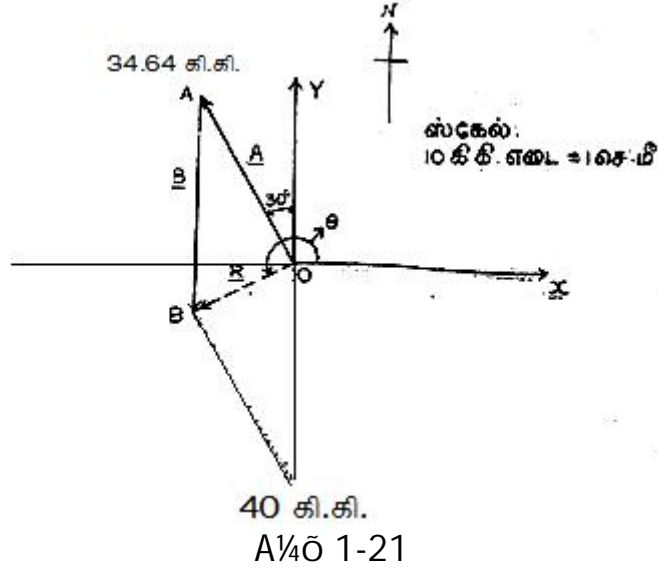
¼ċ ·· ° Āċ ð ¼ ŷ Õ Ì Š ĩ Ĩ ½ Ā ¼ċ ð Ā È ŷ ŭ Š ð ð ð ñ ¼ ĵ Ì õ | ¼ ĵ Ĩ Ā Ā ŷ

¼ċ ·· ° Āċ Ā Ĩ ĩ ñ ··

Ó ¼ċ ĀĔ

"ÑÉċ « È" « ·· Ā ð Ò Ó ·· È Āċ Ā ¼ õ 1-21 ρ ø ĵ ĩ ð È Ā Ā ĵ ŭ

$$\underline{OA} + \underline{AB} = \underline{OB} \rightarrow \text{Ì õ.}$$



\vec{A} மற்றும் \vec{B} ஆகிய இரு வெக்டர்கள் OB பக்கம் $\angle COB = 210^\circ$ எனில் \vec{R} இன் மீட்டர் $|R| = 2 \times 10 = 20$ மீட்டர் எனும் \vec{R} வெக்டர் \vec{A} மற்றும் \vec{B} ஆகிய இரு வெக்டர்களின் கூடுதல் வெக்டர் \vec{R} இன் மீட்டர் $\angle XOB = 210^\circ$ எனில்.

பின்னர் \vec{A} மற்றும் \vec{B} ஆகிய இரு வெக்டர்களின் கூடுதல் வெக்டர் \vec{R} இன் மீட்டர் $\angle XOB = 210^\circ$ எனில்.

i, j ஆகிய இரு வெக்டர்கள் \vec{A} மற்றும் \vec{B} ஆகிய இரு வெக்டர்களின் கூடுதல் வெக்டர் \vec{R} இன் மீட்டர் $\angle XOB = 210^\circ$ எனில், \vec{R} வெக்டர் \vec{A} மற்றும் \vec{B} ஆகிய இரு வெக்டர்களின் கூடுதல் வெக்டர் \vec{R} இன் மீட்டர் $\angle XOB = 210^\circ$ எனில்.

$$\begin{aligned}
 \vec{A} &= 34.64(\cos 120^\circ \underline{i} + \sin 120^\circ \underline{j}) \\
 &= 34.64\left(-\frac{1}{2}\underline{i} + \frac{\sqrt{3}}{2}\underline{j}\right) \\
 &= 17.32(-\underline{i} + \sqrt{3}\underline{j}) \\
 \vec{B} &= 40.00(\cos 270^\circ \underline{i} + \sin 270^\circ \underline{j}) \\
 &= 40.00(0\underline{i} - \underline{j}) \\
 &= -40\underline{j} \\
 \therefore \vec{R} &= \vec{A} + \vec{B} \\
 &= (-17.32\underline{i} - 10\underline{j}) \text{ மீட்டர்} \\
 \therefore R_x &= -17.32; R_y = -10 \\
 \therefore R &= \sqrt{R_x^2 + R_y^2} \\
 &= \sqrt{(-17.32)^2 + (-10)^2} \\
 &= \sqrt{(10\sqrt{3})^2 + (10)^2} \\
 &= \sqrt{300 + 100} \\
 &= 20 \text{ மீட்டர்}
 \end{aligned}$$

$OB \pm y \hat{E} S_{s,i} \hat{I}, x \ll \hat{I} \hat{I} \frac{1}{4} \hat{Y}, " \circ - \hat{u} \zeta S_{s,i} \frac{1}{2} \hat{o} \hat{r} \frac{3}{4} \ll \hat{r} \hat{A} \hat{i} \hat{l} | \hat{A} \hat{y} \hat{E} \hat{i} \hat{o},$

$$\begin{aligned} \tan \theta &= \frac{R_y}{R_x} \\ &= \frac{-10}{-17.32} \\ &= \frac{1}{\sqrt{3}} \end{aligned}$$

$$\begin{aligned} \therefore \theta &= 180^\circ + 30^\circ \\ &= 210^\circ \rightarrow \hat{l} \hat{o}. \end{aligned}$$

Á; ¾; 1-10

ú; ; í ò p¼ô; ÂÂ=î ° ¾; ° Â; Ç; ý |¾; Â Âý ¾; ° Â; Â Â S; i ½ ¾; ° Â; Â¾ôÂÊ ; ñ .

$$A = 420 \text{ Áf}, S75^\circ W.$$

$$B = 400 \text{ Áf}, N45^\circ E.$$

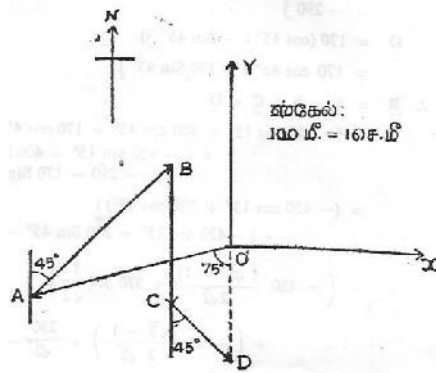
$$C = 290 \text{ Áf}, S$$

$$D = 170 \text{ Áf}, S45^\circ E$$

Ó¾ø ÂÊ

À¼õ 1.22ø ; ðÊôúÇ; Á; Ú, "ÑÉ; « Ê" « ÁôÀø,

$$\underline{OA} + \underline{AB} + \underline{BC} + \underline{CD} = \underline{OD} \rightarrow \hat{l} \hat{o}.$$



À¼õ 1-22

À; Â¼¾ø OD ý ; Çõ 2.4 | °. Áf → ò.

$$\pm \hat{E} \hat{S} \hat{A} |R| = 2.4 \times 100$$

$$= 240 \text{ Áf} \rightarrow \hat{l} \hat{o}.$$

À; Â¼¾ø " = x $\hat{O}D = 270^\circ \rightarrow \hat{l} \hat{o}.$

βÃñ ¼;ÃÐ ÅÆç

$i, j \pm \underline{y} \hat{E} \mu \hat{A} \hat{A} \hat{I} \hat{0} \hat{3} \hat{4} \hat{0} \hat{0} \hat{0} \hat{A} \hat{t} \hat{s} \hat{0} \hat{C} \hat{x}, \hat{y} \hat{\ll} \hat{I} \hat{I} \hat{s} \hat{C} \hat{t} \hat{0} \hat{\ll} \hat{0} \hat{A} \hat{i} \hat{s} \hat{x} \hat{0} \hat{\ll} \hat{0} \hat{I} \hat{A} \hat{i} \hat{0} \hat{D} \hat{,}$

$$\begin{aligned} \underline{A} &= 420(\cos 195^\circ \underline{i} + \sin 195^\circ \underline{j}) \\ &= 420(-\cos 15^\circ \underline{i} - \sin 15^\circ \underline{j}) \\ &= -420 \cos 15^\circ \underline{i} - 420 \sin 15^\circ \underline{j} \end{aligned}$$

$$\begin{aligned} \underline{B} &= 420(\cos 45^\circ \underline{i} + \sin 45^\circ \underline{j}) \\ &= 420 \cos 45^\circ \underline{i} + 400 \sin 45^\circ \underline{j} \end{aligned}$$

$$\begin{aligned} \underline{C} &= 290(-\underline{j}) \\ &= -290 \underline{j} \end{aligned}$$

$$\begin{aligned} \underline{D} &= 170(\cos 45^\circ \underline{i} - \sin 45^\circ \underline{j}) \\ &= 170 \cos 45^\circ \underline{i} - 170 \sin 45^\circ \underline{j} \end{aligned}$$

$$\therefore \underline{R} = \underline{A} + \underline{B} + \underline{C} + \underline{D}$$

$$\begin{aligned} &(-420 \cos 15^\circ + 400 \cos 45^\circ + 170 \cos 45^\circ) \underline{i} + (-420 \sin 15^\circ + 400 \sin 45^\circ - 290 - 170 \sin 45^\circ) \underline{j} \\ &= (-420 \cos 15^\circ + 570 \cos 45^\circ) \underline{i} + (-420 \sin 15^\circ + 230 \sin 45^\circ - 290) \underline{j} \end{aligned}$$

$$= \left(-420 \frac{(\sqrt{3}+1)}{2\sqrt{2}} + 570 \times \frac{1}{2} \right) \underline{i} + \left(-420 \frac{(\sqrt{3}-1)}{2\sqrt{2}} + \frac{230}{\sqrt{2}} - 290 \right) \underline{j}$$

$$= \frac{1}{\sqrt{2}}(360 - 210\sqrt{3}) \underline{i} + \frac{1}{\sqrt{2}}(440 - 210\sqrt{3} - 290\sqrt{2}) \underline{j}$$

$$= -(2.631 \underline{i} + 236.053 \underline{j})$$

$$\therefore R_x = -2.63; R_y = -236.053$$

$$\therefore R = \sqrt{R_x^2 + R_y^2}$$

$$= \sqrt{(-2.63)^2 + (-236.053)^2} \quad \hat{A} \hat{t}$$

$$= 236.05$$

OD ±ýÈ Šs;î x « îí ¼ý " ±ýÈ Šs;î ½ò'' ¾ « '' ÅôÅ¾¼;ø,

$$\tan \theta = \frac{R_y}{R_x}$$

$$= \frac{-236.053}{-2.63}$$

$$= 89.07$$

$$\therefore \theta = 180^\circ + 89^\circ 21'$$

$$= 269^\circ 21' \rightarrow \hat{I} \hat{0}.$$

Å;¾ç;ç 1-11

β¼ô; ÅÃ÷î °ç 30 ÅÐ¼÷ - ùç ¾ç'' °Ãç ´ýÚ, (-2, 2, 1) ±ýÈ ¾ç'' °Ãç ¾¼í s'' çì

$\vec{a} = \frac{1}{\sqrt{2}}\vec{i} + \frac{1}{2}\vec{j} + \frac{1}{2}\vec{k}$

$\vec{a} \cdot \vec{a} = \left(\frac{1}{\sqrt{2}}\right)^2 + \left(\frac{1}{2}\right)^2 + \left(\frac{1}{2}\right)^2 = \frac{1}{2} + \frac{1}{4} + \frac{1}{4} = 1$

$\vec{a} = \frac{1}{\sqrt{2}\sqrt{1}}(-2\vec{i} + 2\vec{j} + \vec{k})$

$\vec{a} = \frac{1}{\sqrt{2}}(-2\vec{i} + 2\vec{j} + \vec{k})$

$\vec{a} = -\frac{2}{\sqrt{2}}\vec{i} + \frac{2}{\sqrt{2}}\vec{j} + \frac{1}{\sqrt{2}}\vec{k} = -\sqrt{2}\vec{i} + \sqrt{2}\vec{j} + \frac{1}{\sqrt{2}}\vec{k}$

$\vec{a} = 30\left(-\frac{2}{\sqrt{2}}\vec{i} + \frac{2}{\sqrt{2}}\vec{j} + \frac{1}{\sqrt{2}}\vec{k}\right)$

$A_x\vec{i} + A_y\vec{j} + A_z\vec{k} = -20\vec{i} + 20\vec{j} + 10\vec{k}$

$A_x = -20, A_y = 20, A_z = 10$

$\vec{a} \cdot \vec{b}$

$\vec{a} = \frac{1}{\sqrt{2}}\vec{i} + \frac{1}{2}\vec{j} + \frac{1}{2}\vec{k}$, $\vec{b} = (-3, 7, 0)$, $\vec{c} = (-5, 10, -6)$

$\vec{a} \cdot \vec{b} = \frac{1}{\sqrt{2}}(-3) + \frac{1}{2}(7) + \frac{1}{2}(0) = -\frac{3}{\sqrt{2}} + \frac{7}{2}$

$\vec{OP} = -3\vec{i} + 7\vec{j} + 0\vec{k}$

$\vec{OQ} = -5\vec{i} + 10\vec{j} - 6\vec{k}$

$\therefore \vec{PQ} = \vec{OQ} - \vec{OP}$

$= (-5\vec{i} + 10\vec{j} - 6\vec{k}) - (-3\vec{i} + 7\vec{j} + 0\vec{k})$

$= -2\vec{i} + 3\vec{j} - 6\vec{k}$

$= 7\left(-\frac{2}{7}\vec{i} + \frac{3}{7}\vec{j} - \frac{6}{7}\vec{k}\right)$

$= 7\vec{f}$

$\vec{f} = -\frac{2}{7}\underline{i} + \frac{3}{7}\underline{j} - \frac{6}{7}\underline{k}$

$l = -\frac{2}{7}, m = \frac{3}{7}, n = -\frac{6}{7}$

$$\underline{F} = F \underline{f}$$

$$= 420 \left(-\frac{2}{7}\underline{i} + \frac{3}{7}\underline{j} - \frac{6}{7}\underline{k} \right)$$

$$= -120\underline{i} + 180\underline{j} - 360\underline{k}$$

$\therefore F_x = -120; \therefore F_y = 180; \therefore F_z = -360$

$\vec{r}_1 = (5, 8, 14)$

$\vec{r}_2 = (7, 3, 0)$

$\vec{PQ} = \vec{r}_2 - \vec{r}_1 = (7, 3, 0) - (5, 8, 14) = (2, -5, -14)$

$\underline{OP} = 5\underline{i} + 8\underline{j} + 14\underline{k}$

$\underline{OQ} = 7\underline{i} + 3\underline{j} + 0\underline{k}$

$\therefore \underline{PQ} = \underline{OQ} - \underline{OP}$

$= (7\underline{i} + 3\underline{j}) - (5\underline{i} + 8\underline{j} + 14\underline{k})$

$= 2\underline{i} - 5\underline{j} - 14\underline{k}$

$= 15 \left(\frac{2}{15}\underline{i} - \frac{5}{15}\underline{j} - \frac{14}{15}\underline{k} \right)$

$= 15\underline{f}$

$\vec{f} = \frac{2}{15}\underline{i} - \frac{5}{15}\underline{j} - \frac{14}{15}\underline{k}$

$l = \frac{2}{15}; m = -\frac{5}{15}; n = -\frac{14}{15}$

$\vec{r}_1 = (5, 8, 14); \vec{r}_2 = (7, 3, 0)$

$$\frac{3A}{5} - \frac{4B}{9} + \frac{C}{3} = 5 \dots\dots\dots(i)$$

$$\frac{B}{9} + \frac{2C}{3} = 14 \dots\dots\dots(ii)$$

$$\frac{4A}{5} + \frac{8B}{9} + \frac{2C}{3} = 4 \dots\dots\dots(iii)$$

±ýÈ °ÁýÀjÎ , ù , ¸· ¼i Ì õ

$$(i) \times 2 + (iii) \rightarrow \frac{6A}{5} - \frac{8B}{9} + \frac{2C}{3} + \frac{4A}{5} + \frac{8B}{9} - \frac{2C}{3} = 10 + 4 \pmýÈjÌ õ.$$

$$\ll \frac{3}{4}j \text{ ÅÐ } \frac{10A}{5} = 14$$

$$\therefore A = 7 \text{ } \neg \text{ } \text{Ì } \text{õ}$$

$$(i) + (iii) \rightarrow \frac{4A}{5} + B = 14 + 4 \pmýÈjÌ õ.$$

$$\begin{aligned} \ll \frac{3}{4}j \text{ ÅÐ} \\ &= 18 - \frac{28}{5} \\ &= \frac{90 - 28}{5} \\ &= \frac{62}{5} \text{ } \neg \text{ } \text{Ì } \text{õ}. \end{aligned}$$

(ii) - ÅÐ °ÁýÀj ðÈÄÏÓÐ

$$\begin{aligned} \frac{2C}{3} &= 14 - \frac{B}{9} \\ &= 14 - \frac{62}{5} \times \frac{1}{9} \\ &= \frac{630 - 62}{45} \\ &= \frac{568}{45} \\ C &= \frac{568}{45} \times \frac{3}{2} \\ &= \frac{284}{9} \end{aligned}$$

$$\therefore A=7; B=\frac{62}{5}; C=\frac{284}{9} \rightarrow \text{I } \checkmark$$

Áj 3/4; 1-16

A (4, 0, 3), B (-8, 6, 0) ±yÈ òùÇç, Çò ÐÀì òòùÇç O - ¼yŞº÷òÐ ñ ¼jì ò pÕ Şç÷ŞçjÎ Ûìì p'' ¼ĀĀ'' ĀŌō Şçj ½ò'' ¼i ñ.

O ±yÈ òùÇç Āî Íð¼'' ĀôĀj ñ ¼jø, A, B ±yÈ òùÇç Ççy çç Āò ¼ç'' °Āç ù Ó'' ÈŞĀ

$$\underline{A} = \underline{OA} = 4\underline{i} + 3\underline{k}; \underline{B} = \underline{OB} = -8\underline{i} + 6\underline{j} \pm yÈ \text{I } \checkmark$$

$\underline{A}, \underline{B}$ ±yÈ ¼ç'' °Āç Ûìì p'' ¼ĀĀ'' ĀŌō Şçj ½ò'' ¼ ±Éì ñ ¼jø, ±ñ ½ò'' ĀŌì ç ĀçĀĀĒ

$$\cos_{\theta} = \frac{\underline{A} \cdot \underline{B}}{AB}$$

$$= \frac{(4\underline{i} + 3\underline{k}) \cdot (-8\underline{i} + 6\underline{j})}{\sqrt{4^2 + 3^2} \sqrt{(-8)^2 + 6^2}}$$

$$= \frac{-32}{5 \times 10} = -0.64 \rightarrow \text{I } \checkmark$$

$$\pm È ŞĀ, \theta = (180^\circ - 50.2^\circ) = 129.8 \rightarrow \text{I } \checkmark$$

Áj 3/4; 1-17.

$\underline{A} = 3\underline{i} - 6\underline{j} - 9\underline{k}$ ±yÈ ¼ç'' °Āç pý Āç'' Ā, $\underline{E} = \frac{1}{3}\underline{i} - \frac{2}{3}\underline{j} - \frac{2}{3}\underline{k}$ ±yÈ µĀĀì ò ¼ç'' °Āç ìì p'' ½ĀĀĒ ¼ç'' °Āçø ñ.

$$\text{Şç'' ĀĀĀĒ Ē Āç'' Ā} \quad \underline{A} \cdot \underline{E} \pm Éì ñ ¼jø,$$

$$\underline{A} \cdot \underline{E}$$

$$= (3\underline{i} - 6\underline{j} - 9\underline{k}) \cdot \left(\frac{1}{3}\underline{i} - \frac{2}{3}\underline{j} - \frac{2}{3}\underline{k} \right) = 11 \rightarrow \text{I } \checkmark$$

Áj 3/4; 1-18

Ûì ñ Ā'' ĀĀ'' Èççø ¼ç'' °Āç Ûìì p'' ¼ĀĀ'' ĀŌō Şçj ½ò'' ¼ ñ.

$$(i) \text{ ¼ç'' °Āç } \underline{u} = 2\underline{i} - \underline{j} - 2\underline{k}, 3\underline{j} - 4\underline{k}$$

$$(ii) (0, 5, 2), (-6, -6, 3) \pm yÈ \text{òùÇç } \underline{u} \text{ ìì } \text{¼Āçç Āò ¼ç'' °Āç } \underline{u}.$$

(iii) A(-2, 6, 3) ±yÈ òùÇç Ā B(-2, 7, 5), C(-1, 6, 1) ±yÈ òùÇç Û ¼yŞº÷òÐ ñ ¼jì ò AB, AC ±yÈ ŞçjÎ ù

(iv) $\left\{\left(\frac{1}{3}\right),\left(-\frac{2}{3}\right),\left(\frac{2}{3}\right)\right\},\left\{\left(\frac{2}{3}\right),\left(\frac{2}{3}\right),\left(\frac{1}{3}\right)\right\}$ ±ýÈ ¾Ë ò ð ¼ì ò ò ò ÇÒ ò ¼À

$S_{ij} \hat{i} \hat{j} \hat{k}$

$\underline{A} = 2\hat{i} - \hat{j} - 2\hat{k}, \underline{B} = 3\hat{j} - 4\hat{k} \pm \hat{y} \hat{E}_i \emptyset$

$\cos_{ij} = \frac{\underline{A} \cdot \underline{B}}{AB} = \frac{(2\hat{i} - \hat{j} - 2\hat{k}) \cdot (3\hat{j} - 4\hat{k})}{\sqrt{4+1+4}\sqrt{9+16}}$

$= \frac{-3+8}{3 \times 5} = \frac{1}{3} \rightarrow \hat{i} \hat{o}$

$\therefore \theta = \cos^{-1}\left(\frac{1}{3}\right) = 70.5^\circ$

(ii) $A(0,5,2), B(-6,-6,3) \pm \hat{y} \hat{E}_i \emptyset$

$\underline{A} = \underline{OA} = 5\hat{j} + 2\hat{k}; \underline{B} = \underline{OB} = -6\hat{i} - 6\hat{j} + 3\hat{k} \rightarrow \hat{i} \hat{o}$

$\therefore \cos_{ij} = \frac{\underline{A} \cdot \underline{B}}{AB} = \frac{(5\hat{j} + 2\hat{k}) \cdot (-6\hat{i} - 6\hat{j} + 3\hat{k})}{\sqrt{25+4}\sqrt{36+36+9}} = \frac{-30+6}{\sqrt{29 \times 9}}$

$= -\frac{8}{3\sqrt{29}} = 0.49517$

$\therefore \theta = (180^\circ - 60.3^\circ) = 119.7^\circ$

(iii) $A(-2, 6, 3), B(-2, 7, 5), C(-1, 6, 1) \pm \hat{y} \hat{E} \hat{O} \hat{U} \hat{C} \hat{U} \hat{i} \hat{l} \hat{i} \hat{A} \hat{Z} \hat{A} \hat{o}$

$\frac{3}{4} \hat{C} \hat{o} \hat{A} \hat{U} \hat{O} \hat{E} \hat{S} \hat{A}$

$\underline{OA} = -2\hat{i} + 6\hat{j} + 3\hat{k}; \underline{OB} = -2\hat{i} + 7\hat{j} + 5\hat{k}; \underline{OC} = -\hat{i} + 6\hat{j} + \hat{k} \rightarrow \hat{i} \hat{o}$

$\therefore \underline{AB} = \underline{OB} - \underline{OA} = \hat{j} + 2\hat{k}$

$\underline{AC} = \underline{OC} - \underline{OA} = \hat{i} - 2\hat{k} \rightarrow \hat{i} \hat{o}$

$\underline{P} = \hat{j} + 2\hat{k}; \underline{Q} = \hat{i} - 2\hat{k} \pm \hat{E} \hat{i} \hat{i} \hat{j} \hat{n} \hat{y} \hat{i} \hat{o}$

$\cos_{ij} = \frac{\underline{P} \cdot \underline{Q}}{PQ} = \frac{-4}{5} = \frac{4}{5} \therefore \theta = (180^\circ - 36.8^\circ)$

$= 143.2^\circ; \rightarrow \hat{i} \hat{o}$

(iv) $\cos_{ij} = l_1 l_2 + m_1 m_2 + n_1 n_2 \pm \hat{y} \hat{E} \hat{Z} \hat{A} \hat{O} \hat{A} \hat{E} \hat{p} \hat{i} \hat{l} \cos_{ij} = \frac{2}{9} - \frac{4}{9} + \frac{2}{9} = 0 \rightarrow \hat{i} \hat{o}$

$\pm \hat{E} \hat{S} \hat{A} \theta = 90^\circ \pm \hat{y} \hat{E} \hat{i} \hat{l} \hat{o}$

$\hat{A}_i \frac{3}{4} \hat{C} \hat{o} \hat{1} - 19 \underline{A} = 16\hat{i} + 3\hat{j}; \underline{B} = -6\hat{i} + 10\hat{k}; \underline{C} = 4\hat{j} \pm \hat{E} \hat{y} \hat{A} \hat{O} \hat{A} \hat{E} \hat{A} \hat{u} \hat{i} \hat{o} \hat{E} \hat{i} \hat{j} \hat{n} \hat{s}$

(i) $\underline{C} \cdot (\underline{A} \cdot \underline{C}) + \underline{B}$

(ii) $-\underline{C} + [\underline{B} \cdot (-\underline{A}) \underline{C}]$

(iii) $\underline{A} \cdot (\underline{B} \wedge \underline{C})$

$$(iv) \underline{A} \wedge (\underline{B} \wedge \underline{C})$$

$$(i) \underline{A} = 16\underline{i} + 3\underline{j}; \underline{B} = -6\underline{i} + 10\underline{k}; \underline{C} = 4\underline{j}$$

$$\therefore (\underline{A} \cdot \underline{C}) = (16\underline{i} + 3\underline{j}) \cdot (4\underline{j}) = 12$$

$$\begin{aligned} \pm \dot{\text{E}} \text{ \AA } \underline{C} (\underline{A} \cdot \underline{C}) + \underline{B} &= 12(4\underline{j}) + (-6\underline{i} + 10\underline{k}) \\ &= -6\underline{i} + 48\underline{j} + 10\underline{k} \quad \rightarrow \text{\AA} \text{ \AA } \end{aligned}$$

$$(ii) [\underline{B} \cdot (-\underline{A}) \underline{C}] = (-6\underline{i} + 10\underline{k}) \cdot (16\underline{i} + 3\underline{j}) = 96$$

$$\begin{aligned} \pm \dot{\text{E}} \text{ \AA } -\underline{C} + [\underline{B} \cdot (-\underline{A}) \underline{C}] \\ &= -4\underline{j} + 96(4\underline{j}) \\ &= 380\underline{j} \quad \rightarrow \text{\AA} \text{ \AA } \end{aligned}$$

$$\begin{aligned} (iii) \underline{A} \cdot (\underline{B} \wedge \underline{C}) &= \begin{vmatrix} 16 & 3 & 0 \\ -6 & 0 & 10 \\ 0 & 4 & 0 \end{vmatrix} \\ &= 16(0 - 14) - 3(0) + 0 = -640 \end{aligned}$$

$$(iv) (\underline{B} \wedge \underline{C}) = \begin{vmatrix} \underline{i} & \underline{j} & \underline{k} \\ -6 & 0 & 10 \\ 0 & 4 & 0 \end{vmatrix}$$

$$= \underline{i}(0 - 40) - \underline{j}(0) + \underline{k}(-24 - 0)$$

$$\begin{aligned} \therefore \underline{A} \wedge (\underline{B} \wedge \underline{C}) &= \begin{vmatrix} \underline{i} & \underline{j} & \underline{k} \\ 16 & 3 & 0 \\ -40 & 0 & -24 \end{vmatrix} \\ &= \underline{i}(-72 - 0) - \underline{j}(-384 - 0) + \underline{k}(0 + 120) \\ &= -72\underline{i} + 384\underline{j} + 120\underline{k} \end{aligned}$$

$$\therefore \underline{A} \wedge (\underline{B} \wedge \underline{C}) = 24(-3\underline{i} + 16\underline{j} + 5\underline{k}) \quad \rightarrow \text{\AA} \text{ \AA }$$

Á; ¼; 1-20 $\underline{A} = 5\underline{i} - 6\underline{j} + 7\underline{k}; \underline{B} = 7\underline{i} - 8\underline{j} + 9\underline{k}; \underline{C} = 3\underline{i} + \underline{j} - 5\underline{k}$ ±ý È ¼; °Å; ù ¯ Ò
¼Ç ò ¼Ä ¯ Á Ò ±É ç Ú ×.

$\underline{A}, \underline{B}, \underline{C}$, ±ý Ä ¯ Å ¯ Ò ¼Ç ò ¼Ä ¯ Á Ò ¼Ü ì; ç Ä ¯ Á ¯ È, $\underline{A} \cdot (\underline{B} \wedge \underline{C}) = 0 \rightarrow \text{\AA} \text{ \AA }$.
±É ŠÄ, Ó ì Ò Ò ±ñ ½ ò; Ì Ò; ç; Ä « ½ Ç; ì ¯ Ä « ¯ Á Ò Ò ±Ø ¼;.

$$\underline{A} \cdot (\underline{B} \wedge \underline{C}) = \begin{vmatrix} 5 & -6 & 7 \\ 7 & -8 & 9 \\ 3 & 1 & -5 \end{vmatrix} \pm \dot{\text{E}} \text{ \AA } \text{\AA} \text{ \AA }$$

$$\ll \pm \dot{\text{E}} \text{ \AA } \text{\AA} \text{ \AA} \text{ \AA} = 5(40 - 9) - 7(30 - 7) + 3(-54 + 56) = 255 - 161 + 6 = 0 \rightarrow \text{\AA} \text{ \AA }$$

±É ŠÄ, $\underline{A}, \underline{B}, \underline{C}$ ±ý Ä ¯ Å ¯ Ò ¼Ç ò ¼Ä ¯ Á Ò ±É È ¼; Ç; ì Ò.

Áj ¼ç 1-21

$A(2,3,5), B(4,-3,-2), C(0,5,4), D(-2,5,-1) \pm \acute{y} \acute{E} \acute{O} \acute{u} \acute{C} \acute{u} \acute{O} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o}$
 $\pm \acute{E} \acute{i} \acute{n}$

$\acute{O} \pm \acute{y} \acute{E} \acute{O} \acute{u} \acute{C} \acute{u} \acute{O} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o}$

$$\underline{OA} = 2\mathbf{i} + 3\mathbf{j} + 5\mathbf{k}, \underline{OB} = 4\mathbf{i} - 3\mathbf{j} - 2\mathbf{k}, \underline{OC} = 5\mathbf{j} + 4\mathbf{k},$$

$$\underline{OD} = -2\mathbf{i} + 5\mathbf{j} - \mathbf{k} \pm \acute{y} \acute{E} \acute{i} \acute{o}. \ll \acute{o} \acute{A} \acute{i} \acute{O} \acute{D},$$

$$\underline{P} = \underline{AB} = \underline{OB} - \underline{OA} = 2\mathbf{i} - 6\mathbf{j} - 7\mathbf{k}$$

$$\underline{Q} = \underline{AC} = \underline{OC} - \underline{OA} = -2\mathbf{i} + 2\mathbf{j} - \mathbf{k}$$

$$\underline{R} = \underline{AD} = \underline{OD} - \underline{OA} = -4\mathbf{i} + 2\mathbf{j} - 6\mathbf{k} \rightarrow \acute{i} \acute{o}.$$

$\underline{P}, \underline{Q}, \underline{R} \pm \acute{y} \acute{E} \acute{O} \acute{u} \acute{C} \acute{u} \acute{O} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o}$

$$\underline{P} \cdot (\underline{Q} \wedge \underline{R}) = 0 \rightarrow \acute{i} \acute{o}.$$

$\pm \acute{E} \acute{S} \acute{A} \acute{O} \acute{i} \acute{U} \acute{o} \acute{I} \pm \acute{n} \frac{1}{2} \acute{o} \acute{A} \acute{O} \acute{i} \acute{C} \underline{P} \cdot (\underline{Q} \wedge \underline{R}) = 0 \acute{y} \acute{A} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o}$
 $\ll \frac{1}{2} \acute{S} \acute{i} \acute{A} \ll \acute{A} \acute{O} \acute{A} \acute{O} \pm \acute{O} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o}$

$$\underline{P} \cdot (\underline{Q} \wedge \underline{R}) = \begin{pmatrix} 2 & -6 & -7 \\ -2 & 2 & -1 \\ -4 & 2 & -6 \end{pmatrix} \pm \acute{y} \acute{E} \acute{i} \acute{o}.$$

$$\ll \frac{3}{4} \acute{y} \acute{A} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o} = 2(-12+2) + 6(12-4) - 7(-4+8) \\ = -20 + 48 - 28 \\ = 0 \rightarrow \acute{i} \acute{o}.$$

$\pm \acute{E} \acute{S} \acute{A} \underline{P}, \underline{Q}, \underline{R} \pm \acute{y} \acute{E} \acute{O} \acute{u} \acute{C} \acute{u} \acute{O} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o}$

$\frac{3}{4} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o}$

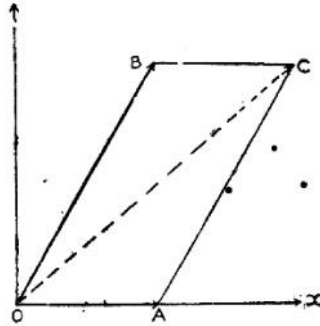
$\ll \frac{3}{4} \acute{A} \acute{D} A, B, C, D \pm \acute{y} \acute{E} \acute{O} \acute{u} \acute{C} \acute{u} \acute{O} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o}$

Áj ¼ç 1-22

25 ç. ç. ± ¼ ò ù ç Áç ° ´ y Ú X « í ° y Áç ° ò ¼ç ° Áç ° | ° Ä ü Ä Í ç È Ð. 50 ç. ç. ± ¼ ò ù ç Ä ü | È Ì Áç °, Ó ¼ç ° ç. ç. Ä ð ¼ ò Ä Í ¼ç ° Áç ° (in the first quadrant) Ð Ä Ì ò ù ç Ä ü Áç ° Ä ç ° Ä X « í í ¼ y 60° ç. ç. ½ ò ° ¼ « Á Ì ò ç ÷ ç. ç. ð È ç | ° Ä ü Ä Í ç È Ð. « ù Áç ° ç. ç. | ¼ | Ä Ä y Áç ° ° Á Ì ç. ç. ç. ç.

Áç ° Ä Ä ¼ Áç ° ç. ç. ò

$\rho \acute{i} \acute{l} \rho \acute{o} \acute{A} \acute{C} \acute{o} \acute{U} \acute{o} \acute{D} \acute{A} \acute{i} \acute{O} \acute{u} \acute{C} \acute{O} \acute{A} \acute{C} \acute{o} \acute{S} \acute{A} \acute{i} \acute{o} \acute{C} \acute{o} \acute{y} \acute{E} \acute{E}. OX, OY \pm \acute{y} \acute{E} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o} \acute{C} \acute{o} \acute{A} \acute{A} \acute{O} \acute{o} \ll \acute{i} \acute{l} \acute{i} \acute{C} \acute{o} \acute{y} \acute{C} \acute{o} \acute{C} \acute{i}, \acute{j} \pm \acute{y} \acute{E} \acute{\mu} \acute{A} \acute{A} \acute{l} \acute{o} \acute{C} \acute{o} \acute{A} \acute{C} \acute{o} \acute{U} \ll \acute{E} \acute{A} \acute{C} \acute{o} \acute{o} \acute{i} \acute{o}.$



Á¼õ 1-33

¾¼ ò¾ « ÇÅÆ ±Í òÐ, Á¼õ 1-33ø ðËÄÄË, x « î°ø OA=2.5 |°.Äf
 - úÇÄ;Ú, A ±ýË òúÇÇ· Äì ì ÈÇ ×õ. X « îÍ¼ý 60° §¼½ð¾ð¾¼í ì õ
 §¼½ðËø, OB=5 |°.Äf |¾¼í· Ä· Ä ì ÈÇ ì õ B ±ýË òúÇÇ· Ä ±Í ì ×õ.
 Þ· ½ Ä Ä¼øÄË, OC ±ýË ã· ÄÄ¼õ |¾¼í ÄÄý ÄÇ· °· Ä « ÈÇÄ ì õ.
 Ä· Ä¼ø¼ø OCý ÇÇõ 6.6 |°.Äf - Ä¾¼ø, |¾¼í ÄÄý ÄÇ· °· Äý
 ±ñ Ä¼ø = 6.6 × 10 = 66 Ç·Ç ±· ¼Äí ì. « Ð |°ÄüÄ ì¾Ç· °, X « îÍ¼ý
 ÇOA=„ = 41° ±ýË §¼½ð¾ð¾¼ « · Äì ÇÈÐ.

ÞÄü ½¾¼ ÄÇì õ;
 Þí ì ÄÇ· °ü

$$F_1 = 25i, F_2 = 50 \cos 60^\circ i + 50 \sin 60^\circ j = 25i + 25\sqrt{3}j \pm ýË ì õ.$$

$$\begin{aligned} R &= F_1 + F_2 \\ &= 25i + 25i + 25\sqrt{3}j \text{ ì õ.} \\ &= 50i + 25\sqrt{3}j \\ R_x &= 50, R_y = 25\sqrt{3} \end{aligned}$$

±É §Ä,

$$\begin{aligned} R^2 &= R_x^2 + R_y^2 \\ &= (50)^2 + (25\sqrt{3})^2 \\ &= 2500 + 1875 \\ &= 4375 \end{aligned}$$

$$\therefore R = \sqrt{4375} = 25\sqrt{7} = 66.13 \text{ Ç·Ç. ±· ¼.}$$

|¾¼í ÄÄý ÄÇ· °, X « îÍ¼ý „ ±ýË §¼½ð¾ð¾¼ « · Ä¼¾¼í ì
 |¾¼í ñ¼ø,

$$\tan „ = \frac{R_y}{R_x} = \frac{25\sqrt{3}}{50} = \sqrt{3} = 0.866 \text{ ì õ.}$$

«¾¼ ÄÐ, „ = 40°55' ì õ.

Ä¾¼Ç 1-22

$\vec{A}_1 = 2.5\hat{i} - 2.5\hat{j}$, $\vec{A}_2 = 25\hat{j}$, $\vec{A}_3 = 50\cos 60^\circ \hat{i} + 50\sin 60^\circ \hat{j}$
 (Negative direction of through X axis) $\vec{A}_4 = 4.4\hat{j}$, $\vec{A}_5 = 4.4\hat{j}$
 $\vec{A}_6 = 4.4\hat{j}$, $\vec{A}_7 = 4.4\hat{j}$, $\vec{A}_8 = 4.4\hat{j}$, $\vec{A}_9 = 4.4\hat{j}$, $\vec{A}_{10} = 4.4\hat{j}$

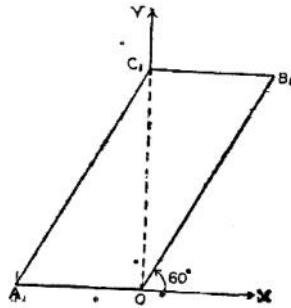


Diagram 1-34

$OA_1 = 2.5$

$\angle B_1 O X = 60^\circ, OB_1 = 5$

$OB_1 C_1 A_1$ is a parallelogram, $OC_1 = 4.4$
 $\vec{A}_1 = -2.5\hat{i}$, $\vec{A}_2 = 25\hat{j}$, $\vec{A}_3 = 50\cos 60^\circ \hat{i} + 50\sin 60^\circ \hat{j}$, $\vec{A}_4 = 4.4\hat{j}$, $\vec{A}_5 = 4.4\hat{j}$, $\vec{A}_6 = 4.4\hat{j}$, $\vec{A}_7 = 4.4\hat{j}$, $\vec{A}_8 = 4.4\hat{j}$, $\vec{A}_9 = 4.4\hat{j}$, $\vec{A}_{10} = 4.4\hat{j}$

$\angle C_1 O X = 90^\circ$

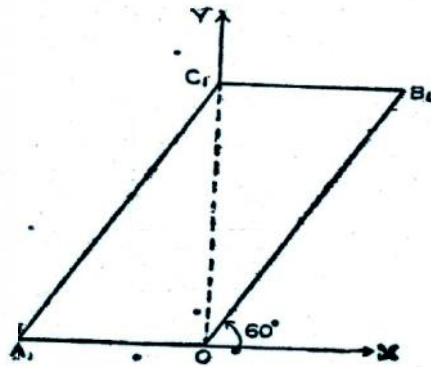


Diagram 1-35

Resultant force $\vec{R} = \vec{F}_1 + \vec{F}_2$

$$\vec{R}_1 = \vec{F}_1 + \vec{F}_2$$

$$= -25\hat{i} + 50\cos 60^\circ \hat{i} + 50\sin 60^\circ \hat{j}$$

$$= -25\hat{i} + 25\hat{i} + 25\sqrt{3}\hat{j}$$

$$= 25\sqrt{3}\hat{j}$$

$$\therefore R_x = 0, R_y = 25\sqrt{3}$$

$$R_1 = \sqrt{R_x^2 + R_y^2} = R_y = 25\sqrt{3} = 43.3$$

$$\tan \theta = \frac{R_y}{R_x} = r = \frac{3}{4} \Rightarrow \theta = 90^\circ - \alpha = 37^\circ$$

Figure 1.23

A 100 kg load is suspended from a horizontal beam by a rope. The rope is attached to the beam at a point 3 m to the left of the load and to a vertical wall at a point 4 m above the load. The weight of the load is 100 kg. Find the tension in the rope and the reaction forces at the wall.

The diagram shows a rectangular load of weight 100 kg. A rope is attached to the top-left corner of the load and extends upwards and to the left, making an angle of 37 degrees with the horizontal. The rope is attached to a vertical wall at a height of 4 m above the load. The load is suspended from a horizontal beam at its top-right corner. The weight of the load acts downwards from its center.

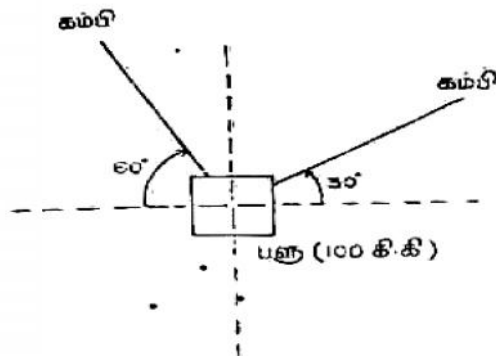


Figure 1-36

The load is a free body. The forces acting on it are: weight (100 kg) acting downwards from the center, tension in the rope acting upwards and to the left from the top-left corner, and reaction forces at the top-right corner (normal force acting to the right and friction force acting upwards).

Free body diagram:

- The weight of the load (100 kg) acts downwards from the center of the load.

$$\sum F = 0$$

The forces acting on the load are: weight (100 kg) acting downwards from the center, tension in the rope acting upwards and to the left from the top-left corner, and reaction forces at the top-right corner (normal force acting to the right and friction force acting upwards).

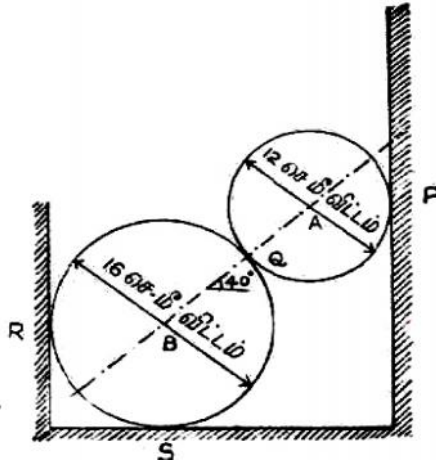
(1) $\sum F_x = 0 \Rightarrow T \cos 37^\circ - R_x = 0$

(2) $\sum F_y = 0 \Rightarrow T \sin 37^\circ + R_y - 100 = 0$

(3) $\sum \tau = 0 \Rightarrow T \sin 37^\circ (4) - 100 (3) = 0$

- The reaction forces at the wall are: normal force R_x acting to the right and friction force R_y acting upwards.

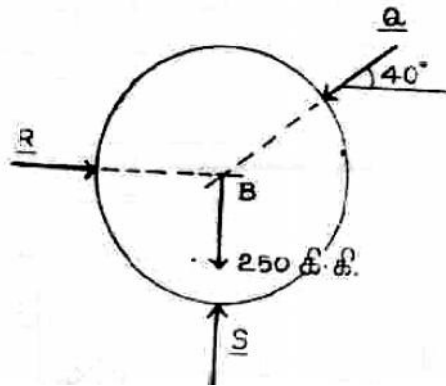
- The tension in the rope is $T = 75 \text{ kg}$.



À¼õ 1-37

ÀÀðÒ ù ´ý Ò È | Áí ý Ú |¼Í ò P,Q,R,S ±ýÈ ÒùÇç Çø çç Øõ Ò Áí ò ×
 Áç ò ò Çõ ÒÈ ò ½òÐ R,S ±ýÚ Á¼í çç B §ç Çò¼ø |ºÄüÄ ò ±¼ç
 Áç ò ò Çì (reactions) §ç ñ .

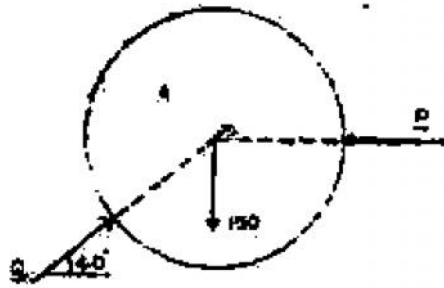
[§ç Çì Çç ±¼ ù, |¼Í ò ÒùÇç Çç « ò ÁÒõ ±¼ç Áç ò Çç È òÐõ Ò
 ¼Çò¼ç Á¼¼í ò |¼Í ò Çç × ò.]
 À¼õ 1-38,1-39 ò ÁüÈø §ç Çõ B, §ç Çõ A ±ýÀ Ò Á¼È òÄ ò¼òÄ Ò Ò
 « ÁüÈý §Áø |ºÄüÄ ò ÒÈÁç ò Ò È ò ÒÄ ò òÄ ò ò Çç. §ç Çõ A Ò Á



À¼õ 1-38

- « ò Á¼çç ÁÄø ò Áì ò Áç ò ò ù Äý ÁÒÁí Ú:
- (i) §ç Çõ Áý ±¼ 150 çç. Þ Á ù ÞÄñ Í ò §ç Çõ Áý ò ÁÄò¼ø
 ò¼ç çç ÈÈ.
 - (ii) ÒÈÁç ò p-
 - (iii) ÒÈÁç ò Q, 40°

Þì Ò Ó¼ø ÞÒÁç ò ù §ç Çõ Áý ò ÁÄò¼ø ò¼ç Ò¼¼ø, « Ð « ò Á¼ç
 çç ÁÄÁÒì , áý Èí ÁÐ Áç ò Çç ò ÁÄòùÇç ÁÈ§Á |ºøÄ§Äñ Í ò. (À¼õ
 (1.39)



Á¼õ 1-39

$$\pm \uparrow \Sigma F_{iy} = 0 \quad \pm \uparrow \Delta D,$$

$$Q \sin 40^\circ - 150 = 0$$

$$Q = \frac{150}{\sin 40^\circ} = 233.5$$

Σ_i Çõ B « Á¼õ Çõ ÁÃø Áì ò Áç ° ù Àý ÁÕÁ; Ú:

(i) Σ_i Çõ Bý ± ¼ 250 ç. ç. ↓

(ii) òÈ Áç ° R →

(iii) òÈ Áç ° S ↑

(iv) òÈ Áç ° Q = 233.5 ∠ 40°

þ Á Ç È ð ò Σ_i Çõ Bý ÁÃø ù Çç ÁÆÇÁ | ° ø ù È È.

$$\pm \uparrow \Sigma F_{iy} = 0 \quad \pm \uparrow \Delta D,$$

$$S - 250 - Q \sin 40^\circ = 0$$

$$S = 250 + Q \sin 40^\circ$$

$$= 250 + 150$$

$$= 400 \text{ ç. ç. } \rightarrow \text{ ò.}$$

$$\Sigma \vec{A} \vec{O} \vec{o} \quad \pm \rightarrow \Sigma F_{ix} = 0 \quad \pm \rightarrow \Delta D,$$

$$R - Q \cos 40^\circ = 0$$

$$R = Q \cos 40^\circ$$

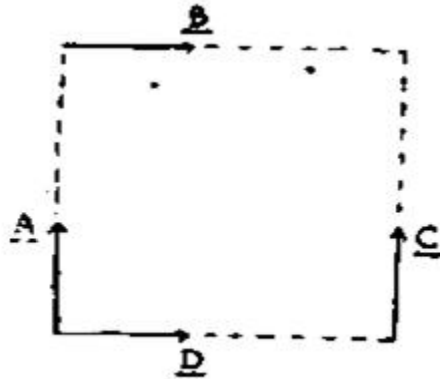
$$= 233.5 \cos 40^\circ$$

$$= 179 \text{ ç. ç. } \rightarrow \text{ ò}$$

Á¼õ 1.25:

°ÁÁ_i ù Ç ç_i ý Ì Áç ° ù, ° ðÃð¾ý Áì í Çç Á¼õ 1.40ø
 ù ðÈÁÁ; Ú ùÁ ù È È. « ÁüÈý |¾ì ÁÁý Áç ° Á Á ÁÁÚ ù.

pril A... C ± uA... S... 3/4i AAy A... ,
 i... oA... A... U... i... A... C... U... A... o.



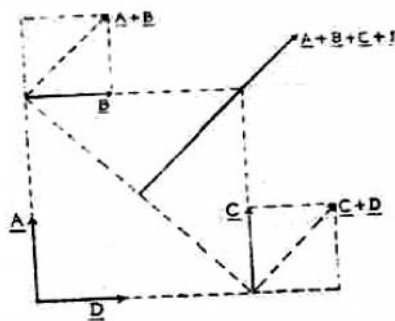
A... 1-40

A... u... A... y... ± n A... a ± E... i... u... x...
 pril 3/4i AAy A... ,

$$\begin{aligned}
 F &= A + B + C + D \\
 &= (A + D) + (B + C) \\
 &= 2(A + D) = 2(B + C) \quad \text{--- } \bar{1} \text{ } \bar{o}. \\
 \therefore F &= |F| = 2\sqrt{|A|^2 + |D|^2} \\
 &= 2\sqrt{a^2 + a^2} \\
 &= 2\sqrt{2a} \\
 &= 2.828a \quad \text{--- } \bar{1} \text{ } \bar{o}.
 \end{aligned}$$

E... u... A... o... S... o... 1/4 o... , 3/4... A... A... A... y... A... o... O... E... C... i... A... E... i... o...
 O... A... A... A... , A, B ± y... E... A... , C... S... i... x... o... « u... A... i... S... E... C, D ± y... E...
 A... o... C... o... S... i... x... o...
 A, B --- A... u... E... y
 « u... A... i... S... E... C, D
 A... o... = C + D --- \bar{1} \bar{o}.

± y... A... i... o...
 --- A... u... E... y
 p... A... U... i... \bar{1}



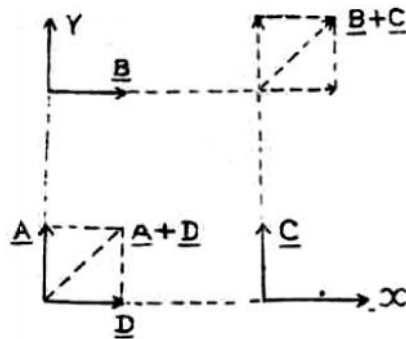
$$\begin{aligned}
 3/4i \text{ AAy} &= A + B \quad \text{--- } \bar{1} \text{ } \bar{o}. \\
 \text{--- } A... u... E... y & \quad 3/4i \text{ AAy} \\
 \text{--- } E... i... & \quad A + B = C + D \\
 & \quad (A + B), (C + D) \\
 3/4i \text{ AAy} & \quad A... o... \\
 p... 1/4 A... , \bar{2} \bar{1} & \quad A... o... 3/4 o... ,
 \end{aligned}$$

A... 1-41

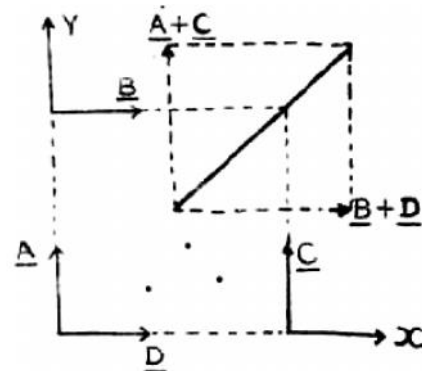
« " $\vec{A}, \vec{u} \parallel \vec{O} \vec{A} \vec{u} \vec{A} \vec{I} \vec{o} \vec{s}, \vec{j} \vec{I} \vec{u} \vec{i} \vec{l} \vec{p} \vec{\cdot} \vec{1} \vec{2} \vec{A} \vec{j}, \times \vec{o}, \ll " \vec{A}, \vec{u} \vec{\cdot} \vec{1} \vec{4} \vec{A} \pm \vec{n}$
 $\vec{A} \vec{3} \vec{4} \vec{o} \vec{o} \vec{s}, \vec{C} \vec{y} \vec{p} \vec{O} \vec{A} \vec{1} \vec{4} \vec{i} \vec{s}, \vec{j}, \times \vec{o} \vec{A} \vec{1} \vec{4} \vec{o} \vec{3} \vec{4} \vec{o} \vec{1} \vec{4} \vec{1} \vec{o}, \vec{j} \vec{o} \vec{E} \vec{A} \vec{A} \vec{E} \ll " \vec{A}, \vec{u} \vec{E} \vec{D}.$

$\vec{p} \vec{A} \vec{n} \vec{1} \vec{4} \vec{j} \vec{A} \vec{3} \vec{4} \vec{j}, (\vec{A}, \vec{D}); (\vec{B}, \vec{C}) \rightarrow \vec{C} \vec{A} \vec{u} \vec{\cdot} \vec{E} \vec{s} \vec{o} \vec{i} \vec{s}, \ll " \vec{A}, \vec{C} \vec{y} \vec{1} \vec{3} \vec{4} \vec{j} \vec{l} \vec{A} \vec{A} \vec{y}$
 $\vec{A} \vec{c} \vec{\cdot} \vec{o} \vec{u} \vec{O} \vec{\cdot} \vec{E} \vec{s} \vec{A} (\vec{A} + \vec{D}), (\vec{B} + \vec{C}) \pm \vec{y} \vec{U} \vec{s}, \vec{y} \vec{E} \vec{E}. \vec{s} \vec{A} \vec{O} \vec{o} (\vec{A} + \vec{D}), (\vec{B} + \vec{C}) \pm \vec{y} \vec{A} \vec{\cdot} \vec{A}, \vec{u} \vec{\cdot} \vec{s} \vec{A}$
 $\vec{1} \vec{o} \vec{A} \vec{u} \vec{A} \vec{I} \vec{o} \vec{s}, \vec{j} \vec{o} \vec{1} \vec{4} \vec{o} \vec{1} \vec{A} \vec{u} \vec{E} \vec{C} \vec{O} \vec{o} \vec{A} \vec{3} \vec{4} \vec{j} \vec{o}, \ll " \vec{A}, \vec{C} \vec{y} \vec{1} \vec{3} \vec{4} \vec{j} \vec{l} \vec{A} \vec{A} \vec{y} \vec{A} \vec{c} \vec{\cdot} \vec{o}$
 $(\vec{A} + \vec{B} + \vec{C} + \vec{D}) \vec{O} \vec{o} \vec{A} \vec{1} \vec{4} \vec{o} \vec{1} \vec{4} \vec{2} \vec{o}, \vec{j} \vec{o} \vec{E} \vec{A} \vec{A} \vec{E} \ll " \vec{s} \vec{3} \vec{4} \vec{s} \vec{2} \vec{s}, \vec{j} \vec{o} \vec{E} \vec{o} \vec{1} \vec{o} \vec{A} \vec{u} \vec{A} \vec{I} \vec{s}, \vec{E} \vec{D}.$

$\vec{a} \vec{y} \vec{E} \vec{j} \vec{A} \vec{3} \vec{4} \vec{j}, \vec{p} \vec{\cdot} \vec{1} \vec{2} \vec{A} \vec{c} \vec{\cdot} \vec{o} \vec{u}, (\vec{A} + \vec{C}) \vec{i} \vec{s}, \vec{C} \vec{O} \vec{o} (\vec{B}, \vec{D}) \vec{i} \vec{s}, \vec{C} \vec{O} \vec{o} \vec{\cdot} \vec{y} \vec{U} \vec{s} \vec{o} \vec{i} \vec{s}, \times \vec{o}.$
 $\ll " \vec{A}, \vec{C} \vec{y} \vec{1} \vec{3} \vec{4} \vec{j} \vec{l} \vec{A} \vec{A} \vec{y} \vec{A} \vec{c} \vec{\cdot} \vec{o} \vec{u} \vec{O} \vec{\cdot} \vec{E} \vec{s} \vec{A} (\vec{A} + \vec{C}), (\vec{B} + \vec{D}) \pm \vec{y} \vec{E} \vec{j} \vec{l} \vec{o}, (\vec{A} + \vec{C}) \pm \vec{y} \vec{E}$
 $\vec{A} \vec{c} \vec{\cdot} \vec{o}, \vec{A}, \vec{C} \vec{A} \vec{c} \vec{\cdot} \vec{o} \vec{u} \vec{1} \vec{o} \vec{A} \vec{u} \vec{A} \vec{I} \vec{o} \vec{s}, \vec{j} \vec{I} \vec{u} \vec{i} \vec{l} \vec{p} \vec{\cdot} \vec{1} \vec{4} \vec{A} \vec{o} \vec{j} \vec{I} \vec{\cdot} \vec{A} \vec{A} \vec{o} \vec{3} \vec{4} \vec{o} \ll " \vec{A} \vec{o} \vec{D} \vec{o},$
 $\ll " \vec{A}, \vec{u} \vec{i} \vec{l} \vec{p} \vec{\cdot} \vec{1} \vec{2} \vec{A} \vec{j}, \times \vec{o}, \ll " \vec{3} \vec{4} \vec{y} \pm \vec{n} \vec{A} \vec{3} \vec{4} \vec{o} \vec{o} \vec{A} \ll " \vec{o} \vec{A} \vec{D} \subseteq \vec{A} \vec{y} \pm \vec{n} \vec{A} \vec{3} \vec{4} \vec{o} \vec{o} \vec{A} \vec{y}$
 $\vec{p} \vec{A} \vec{n} \vec{1} \vec{A} \vec{1} \vec{4} \vec{i} \vec{s}, \vec{j}, \times \vec{o} \vec{p} \vec{O} \vec{o} \vec{A} \vec{\cdot} \vec{3} \vec{4} \vec{i} \vec{s}, \vec{j} \vec{1} \vec{2} \vec{A} \vec{j} \vec{o}. \ll " \vec{u} \vec{A} \vec{j} \vec{s} \vec{E} (\vec{B} + \vec{D}) \pm \vec{y} \vec{E} \vec{1} \vec{3} \vec{4} \vec{j} \vec{l} \vec{A} \vec{A} \vec{y}$
 $\vec{A} \vec{c} \vec{\cdot} \vec{o}, \vec{B} \ll " \vec{o} \vec{A} \vec{D} \vec{D} \vec{A} \vec{c} \vec{\cdot} \vec{o} \vec{A} \vec{o} \vec{s} \vec{A} \vec{j} \vec{o}$



À¼õ 1.42



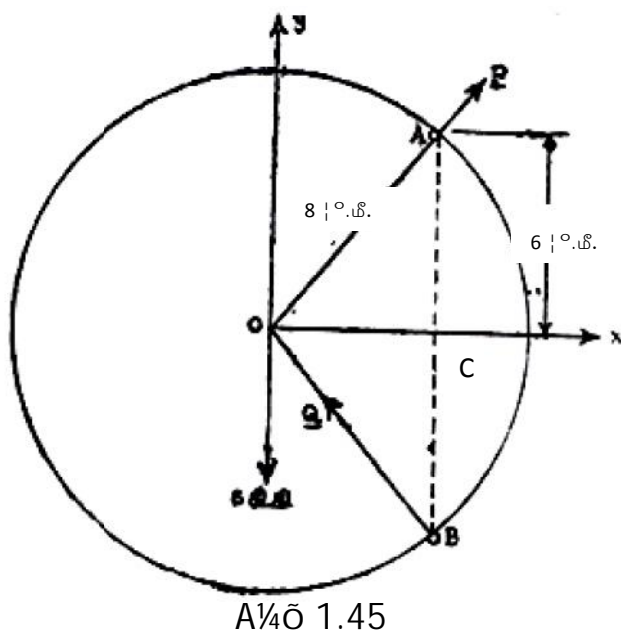
À¼õ 1.43

$\vec{p} \vec{A} \vec{n} \vec{1} \vec{A} \vec{1} \vec{4} \vec{i} \vec{s}, \vec{j}, \times \vec{o} \ll " \vec{A}, \vec{u} \vec{i} \vec{l} \vec{p} \vec{\cdot} \vec{1} \vec{2} \vec{A} \vec{j}, \vec{p} \vec{\cdot} \vec{1} \vec{4} \vec{A} \vec{o} \vec{j} \vec{I} \vec{\cdot} \vec{A} \vec{A} \vec{o} \vec{3} \vec{4} \vec{o} \vec{o}$
 $\ll " \vec{A}, \vec{u} \vec{E} \vec{D}. \pm \vec{E} \vec{s} \vec{A} (\vec{A} + \vec{C}), (\vec{B} + \vec{D}) \rightarrow \vec{C} \vec{A} \vec{u} \vec{E} \vec{y} \vec{1} \vec{3} \vec{4} \vec{j} \vec{l} \vec{A} \vec{A} \vec{y} \vec{A} \vec{c} \vec{\cdot} \vec{o}, \vec{p} \vec{\cdot} \vec{1} \vec{2} \vec{A}$
 $\vec{A} \vec{3} \vec{4} \vec{o} \vec{o} \vec{A} \vec{E} \vec{A} \vec{1} \vec{4} \vec{o} \vec{1} \vec{4} \vec{3} \vec{o}, \vec{j} \vec{o} \vec{E} \vec{A} \vec{A} \vec{E} \vec{1} \vec{o} \vec{A} \vec{u} \vec{A} \vec{I} \vec{o}.$

$\vec{p} \vec{o} \vec{a} \vec{y} \vec{U} \vec{O} \vec{\cdot} \vec{E} \vec{s} \vec{C} \vec{O} \vec{o} \vec{1} \vec{3} \vec{4} \vec{j} \vec{l} \vec{A} \vec{A} \vec{y} \vec{A} \vec{c} \vec{\cdot} \vec{o} \vec{2} \sqrt{2} \vec{a} \pm \vec{y} \vec{E} \pm \vec{n} \vec{A} \vec{3} \vec{4} \vec{o} \vec{\cdot} \vec{A} \vec{o}$
 $\vec{1} \vec{A} \vec{u} \vec{U} \vec{o} \vec{o} \vec{D} \vec{A} \vec{o} \vec{3} \vec{4} \vec{y} \vec{a} \vec{\cdot} \vec{A} \vec{A} \vec{o} \vec{1} \vec{4} \vec{o} \vec{\cdot} \vec{3} \vec{4} \vec{i} \vec{s} \vec{1} \vec{o} \vec{A} \vec{u} \vec{A} \vec{I} \vec{o} \vec{s}, \vec{j} \vec{1} \vec{4} \vec{j}, \times \vec{o} \vec{1} \vec{A} \vec{u} \vec{E} \vec{C} \vec{O} \vec{o} \vec{A} \vec{\cdot} \vec{3} \vec{4}$
 $\ll " \vec{E} \vec{C} \vec{A} \vec{j} \vec{o}.$

Áj 1.26

6 \pm $\frac{1}{4}$ \hat{O} \hat{C} \hat{D} \hat{e} 16 \hat{m} . \hat{A} \hat{O} \hat{C} \hat{D} \hat{A} \hat{E} \hat{p} \hat{O} \hat{o} \hat{d} \hat{A} \hat{O} \hat{A} \hat{C} \hat{A} \hat{A} \hat{y} \hat{U} \hat{A} \hat{B} \hat{y} \hat{U} \hat{o} \hat{O} \hat{u} \hat{C} \hat{C} \hat{o} « \hat{A} \hat{O} \hat{p} \hat{O} \hat{A} \hat{E} \hat{A} \hat{E} \hat{o} \hat{A} \hat{E} \hat{O} \hat{E} \hat{C} \hat{o} \hat{A} \hat{O} \hat{d} \hat{A} \hat{O} \hat{A} \hat{O} \hat{A} \hat{O} \hat{u} \hat{C} \hat{D} . \hat{A} \hat{B} \hat{y} \hat{U} \hat{o} \hat{O} \hat{u} \hat{C} \hat{u} \hat{A} \hat{O} \hat{e} $1.87\hat{o}$ \hat{A} \hat{E} \hat{A} \hat{U} \hat{O} \hat{C} \hat{A} \hat{i} \hat{s} \hat{e} \hat{o} 12 \hat{m} . \hat{A} \hat{f} \hat{A} \hat{A} \hat{o} « \hat{A} \hat{O} \hat{A} \hat{E} \hat{o} \hat{O} \hat{E} \hat{u} \hat{A} \hat{y} \hat{E} \hat{y} \hat{A} \hat{i} \hat{s} \hat{e} \hat{o} \hat{A} \hat{i} \hat{s} \hat{e} \hat{o} .



prí \hat{l} \hat{A} \hat{O} \hat{C} \hat{A} \hat{o} \hat{A} \hat{C} \hat{A} \hat{O} \hat{A} \hat{u} \hat{l} \hat{A} \hat{A} \hat{C} \hat{o} \hat{u} \hat{A} \hat{y} \hat{A} \hat{O} \hat{A} \hat{U} ;

- (1) \hat{A} \hat{C} \hat{A} \hat{o} \hat{y} \hat{A} \hat{O} \hat{C} \hat{D} \hat{A} \hat{E} \hat{o} \hat{A} \hat{A} \hat{o} \hat{O} \hat{A} \hat{C} \hat{u} \hat{s} \hat{e} \hat{i} \hat{s} \hat{e} \hat{o} \hat{A} \hat{O} \hat{A} \hat{E} \hat{O} .
- (2) \hat{A} \hat{o} « \hat{A} \hat{O} \hat{o} \hat{O} \hat{E} \hat{P} \hat{y} \hat{U} \hat{o} $\hat{\mu}$ \hat{A} \hat{C} \hat{A} \hat{O} \hat{A} \hat{C} \hat{A} \hat{o} \hat{O} \hat{A} \hat{y} \hat{U} \hat{o} \hat{A} \hat{C} \hat{A} \hat{o} \hat{A} \hat{O} \hat{A} \hat{O} \hat{D} \hat{C} \hat{E} \hat{D} .
- (3) « \hat{u} \hat{A} \hat{i} \hat{s} \hat{e} \hat{B} \hat{o} « \hat{A} \hat{O} \hat{o} \hat{Q} \hat{y} \hat{U} \hat{o} \hat{A} \hat{C} \hat{A} \hat{o} \hat{B} \hat{O} \hat{y} \hat{U} \hat{o} \hat{A} \hat{C} \hat{A} \hat{o} \hat{A} \hat{O} \hat{A} \hat{E} \hat{O} .

\hat{p} \hat{o} \hat{A} \hat{y} \hat{U} \hat{A} \hat{C} \hat{A} \hat{o} \hat{U} \hat{o} \hat{O} \hat{o} \hat{A} \hat{y} \hat{E} \hat{E} .

\hat{O} \hat{o} \hat{A} \hat{O} \hat{x} \hat{y} \hat{U} \hat{o} \hat{s} \hat{e} \hat{o} \hat{A} \hat{O} , \hat{C} \hat{A} \hat{O} \hat{y} \hat{U} \hat{o} \hat{s} \hat{e} \hat{o} \hat{A} \hat{O} \hat{i} .

$$\angle AOC = \alpha \quad \sin \alpha = \frac{CA}{OA} = \frac{6}{8} = \frac{3}{4} \Rightarrow \alpha = 45^\circ$$

$$\begin{aligned} \therefore \underline{W} &= -6j \\ \underline{P} &= +P \cos \alpha \underline{i} + P \sin \alpha \underline{j} \\ \underline{Q} &= -Q \cos \alpha \underline{i} + Q \sin \alpha \underline{j} \end{aligned}$$

$$\sum F_{iy} = 0 \Rightarrow -6 + P \sin \alpha + Q \sin \alpha = 0 \Rightarrow \dots$$

$$(Q + P) \sin 30^\circ = 6$$

$$(Q + Q) \times \frac{3}{4} = 6$$

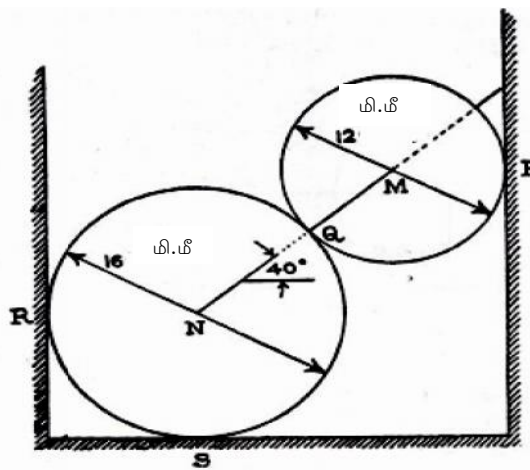
$$2Q \times \frac{3}{4} = 6$$

$$Q = 4 \text{ t}$$

$$P = +4 \text{ t}$$

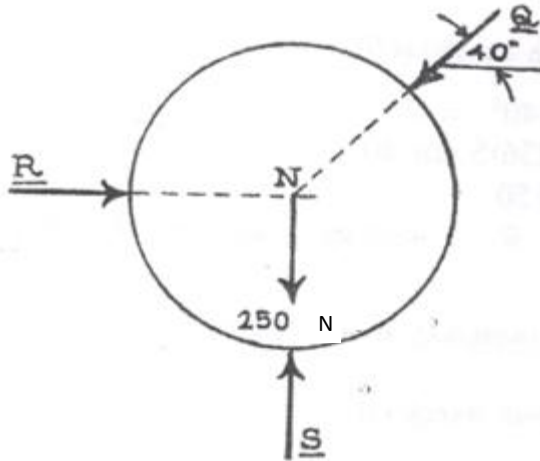
Áj 3/4; 1.27

150 t. \pm 1/40 uC M \pm y U o - O C O o, 250 t. \pm 1/40 uC N \pm y U o
 - O C O o A 1/4 o 1.46 o i o E A A j U 3/4 j i o A i y E E. P, Q, R, S
 \pm y U A 1/4 i C o « A O o 3/4 i A o A A o u A E A e o A j p O o A 3/4 j o, N
 \pm y U o - O C A y S A o R, S \pm y U A 1/4 i C o i o A u A i o \pm 3/4 C 3/4 i i s
 A c o C i j n
 - O C C y i 3/4 j i A A y \pm 1/4, \pm 3/4 C 3/4 j i s A c o u \pm o A j o - O 3/4 C o 3/4 o
 « A A 3/4 j i i i i u s.



A 1/4 o 1-46

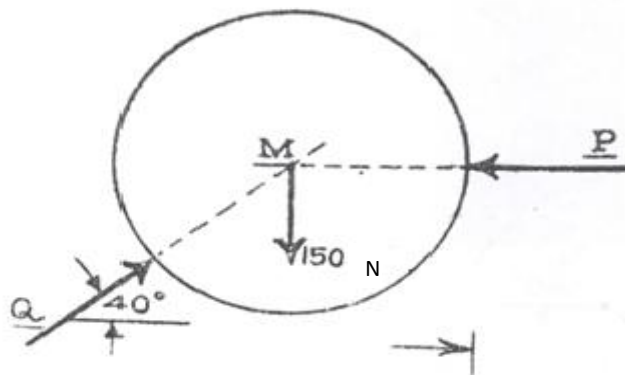
O 3/4 o A E C:
 S 3/4 A o A i o A c o u N \pm E U o i A i O C o i o A u A i A 3/4 j o,
 « o i A i O C o 3/4 E o A i o 3/4 C A 1/4 o 1.47 o i o E A A j U i o A o A i o A c o C i
 i E i x o. « o i A i O C o i o A u A i o A c o u - O O u C t A E S A i o o A 3/4 j o,
 p A n i 3/4 E o 3/4 A c A i o A y A i i s C o 3/4 j y A A A u i s O E O o.



À¼õ 1-47

±ÉŞÀ M ±ýÛõ |À; ÖÇÉÐ ¼ÉÙÀÎ ò¼À « " Áõ" Áõ À¼õ 1.48 ø
 ðÉÁÁÛ ±Í ì ŞÀñ Í õ.
 þí ì õ |°ÄüÀÎ õ (P,Q,150) ±ýÛõ Ä" õ, ù " Ö ¼Çð¼ÇŞÀ " ÖðüÇÇ ÄÆÇŞÀ
 |°ÄüÀÎ õ Ä" õ Ç; ì õ.
 P,Q ±ýÛõ |¼ÇÄ; ì ½ÇÄ; " Ç þÕ ¼ÉÙ¼ °; ÆÈ °ÄÇ" ÄÎ
 °ÄýÄ; Î " Ç; ì ì ì ì Ä" ÄÄÛ; ÖÉÕõ.
 ±ÉŞÀ M ±ýÛõ |À; Öü °ÄÇ" ÄÄÄÖÄ¼; ø. (À¼õ 1.48)

$$\rightarrow + \sum F_{iy} = 0$$



À¼õ 1-48

±ýÛõ °ÄýÄ; Î ,
 $Q \sin 40^\circ - 150 = 0$
 « øÄÐ $Q = 236.5 \text{ Ç.}$
 $\therefore Q = 236.5 \text{ Ç. } (40^\circ)$
 Mý ŞÀø |°ÄøÀÎ , ÇÉÐ

N.

$$\pm y \uparrow \vec{U}_0 \downarrow \vec{A}_i \vec{O} \vec{U} \vec{i} \vec{l} \quad \downarrow \vec{A} \circ \vec{A}_i \vec{C} \vec{C} \vec{A} \ll \vec{A} \hat{o} \vec{A} \vec{C} \vec{C}$$

$$\uparrow + \sum F_{iy} = 0$$

$$S - 250 - Q \sin 40^\circ = 0$$

$$S = 250 + 236.5 \sin 40^\circ$$

$$= 250 + 150$$

$$\therefore S = 400 \text{ zC } \uparrow \pm y \vec{U}_0 \hat{A} \circ \vec{N} \pm y \vec{U}_0 \downarrow \vec{A}_i \vec{O} \vec{C} \vec{C} \vec{C} \downarrow \hat{o} \vec{A} \vec{U} \vec{A} \vec{I} \downarrow \vec{C} \vec{E} \vec{D}$$

$$\vec{S} \vec{A} \vec{O} \vec{o} \vec{N} \pm y \vec{U}_0 \downarrow \vec{A}_i \vec{O} \vec{U} \vec{i} \vec{l} \quad \downarrow \vec{A} \ll \vec{A} \hat{o} \vec{A} \vec{C} \vec{C}$$

$$\left[\begin{array}{c} \rightarrow \\ + \end{array} \right] \sum F_{ix} = 0$$

$$\pm y \vec{U}_0 \circ \hat{A} \hat{y} \vec{A}_i \vec{I} ,$$

$$R - Q \cos 40^\circ = 0$$

$$\ll \frac{3}{4} \text{ j } \vec{A} \vec{D} \quad R = 236.5 \cos 40^\circ = 179 \text{ zC}$$

$$\ll \frac{3}{4} \text{ j } \vec{A} \vec{D} \quad R = 179 \text{ zC} \rightarrow \pm y \vec{U}_0 \hat{A} \circ \vec{N} \pm y \vec{U}_0 \downarrow \vec{A}_i \vec{O} \vec{C} \vec{C} \vec{C} \downarrow \hat{o} \vec{A} \vec{U} \vec{A} \vec{I} \downarrow \vec{C} \vec{E} \vec{D}$$

$$\vec{p} \vec{A} \vec{n} \vec{A} \vec{D} \hat{A} \vec{C} ;$$

$$\vec{p} \vec{O} \downarrow \vec{A}_i \vec{O} \vec{U} \vec{i} \vec{l} \vec{C} \vec{O} \vec{o} \vec{O} \vec{A} \vec{o} \vec{D} \pm \vec{i} \vec{l} \vec{x} \vec{o} . \ll \hat{o} \downarrow \vec{A}_i \vec{O} \vec{D} \circ \vec{A} \vec{C} \vec{C} \downarrow \hat{o} \vec{A} \vec{U} \vec{A} \vec{I} \vec{o}$$

$$\hat{A} \circ \vec{U} \vec{C} \frac{1}{4} \vec{A} \hat{A} \circ \vec{A}_i \vec{l} \vec{o} .$$

$$\vec{p} \vec{u} \vec{A} \vec{A} \hat{o} \vec{o} \vec{i} \vec{l}$$

$$\uparrow + \sum F_{iy} = 0 \pm y \vec{U}_0 \circ \hat{A} \hat{y} \vec{A}_i \vec{I} ,$$

$$S - 150 - 250 = 0$$

$$\ll \frac{3}{4} \text{ j } \vec{A} \vec{D} \quad S = 400 \text{ zC} . \vec{n} \vec{i} \vec{o} .$$

$$\left[\begin{array}{c} \rightarrow \\ + \end{array} \right] \sum F_{ix} = 0 \pm y \vec{U}_0 \circ \hat{A} \hat{y} \vec{A}_i \vec{I}$$

$$R = P \pm y \vec{E}_i \vec{l} \vec{o} .$$

$$M \pm y \vec{U}_0 \downarrow \vec{A}_i \vec{O} \vec{C} \vec{C} \vec{C} \vec{O} \vec{A} \vec{I} \vec{o} \vec{D} .$$

$$\ll \hat{o} \downarrow \vec{A}_i \vec{O} \vec{C} \vec{C} \vec{C} \downarrow \hat{o} \vec{A} \vec{U} \vec{A} \vec{I} \vec{o} \hat{A} \circ \vec{u} \vec{O} \vec{o} \vec{u} \vec{C} \vec{C} \hat{A} \vec{C} \vec{S} \vec{A} \downarrow \hat{o} \vec{A} \vec{o} \vec{A} \vec{o} \vec{I} , \text{ } ^3 \ll \vec{A} \frac{3}{4} \vec{C} \circ \vec{A}_i \vec{C} \vec{C} \vec{A} \hat{A} \vec{C} \vec{C} \vec{A} \vec{I} \vec{y} \vec{E} \vec{E} . \pm \vec{E} \vec{S} \vec{A} \vec{p} \vec{A}_i \vec{A} \vec{C} \vec{A} \vec{y} \vec{A} \vec{C} \vec{O} \vec{A} \vec{E} ,$$

$$\frac{P}{\sin 130^\circ} = \frac{Q}{\sin 90^\circ} = \frac{150}{\sin 140^\circ}$$

$$\therefore P = \frac{150 \sin 50^\circ}{\sin 40^\circ} = 179 \text{ zC}$$

$$\therefore R = P = 179 \text{ zC} . \pm y \vec{E}_i \vec{l} \vec{o} .$$

$\hat{A}_i \frac{3}{4} \vec{C} \vec{C} 1.27$

$$50 \text{ zC} \pm \frac{1}{4} \vec{O} \vec{U} \vec{C} \vec{C} \vec{S} \vec{A} \vec{O} \vec{A}_i \vec{E} \vec{E} \vec{C} \vec{C} \vec{A} \vec{O} \vec{C} \vec{C} \vec{y} \vec{u} \vec{O} \vec{O} \vec{E} \vec{A}_i \vec{E} \vec{D} \vec{O} \text{ zC } \hat{A} \vec{i} \vec{l} \vec{o} \vec{D}$$

$$\vec{I} \vec{A} \vec{O} \frac{1}{4} \vec{y} \vec{45^\circ} \vec{S} \vec{A} \vec{I} \vec{1} \vec{2} \vec{o} \vec{3} \vec{4} \vec{o} \vec{3} \vec{4} \vec{i} \vec{l} \vec{A}_i \vec{U} \vec{A} \vec{C} \vec{C} \vec{1} \vec{2} \vec{i} \vec{o} \vec{A} \vec{o} \vec{I} \vec{U} \vec{C} \vec{D} . \ll \frac{3}{4} \vec{y} \vec{S} \vec{A} \vec{o}$$

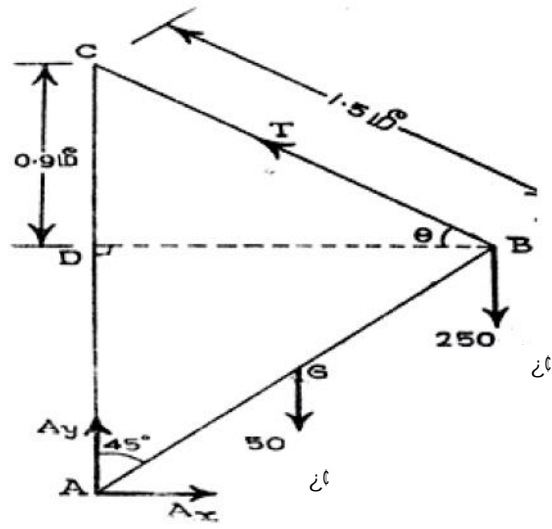
$$\vec{O} \vec{E} \vec{A}_i \vec{E} \vec{D} 1.5 \vec{A} \vec{D} \frac{1}{4} \vec{C} \vec{C} \vec{E} \vec{A} \vec{C} \vec{E} \vec{i} \vec{o} \vec{o} \vec{1} \vec{4} \vec{o} \vec{A} \vec{o} \vec{I} \vec{S} \vec{A} \vec{o} \vec{O} \vec{E} \vec{A} \vec{C} \frac{1}{4} \vec{O} \vec{A} \vec{D} \vec{C} \vec{C} \vec{D} \frac{1}{4} \vec{C} \vec{C} \vec{C} \vec{C} \vec{C} \vec{C} \vec{C}$$

$$\ll \frac{3}{4} \vec{C} \vec{O} \vec{U} \vec{C} \vec{C} \vec{l} \vec{o} \vec{D} \vec{1} \vec{2} \vec{i} \vec{o} \vec{D} \vec{1} \vec{3} \vec{4} \vec{i} \vec{l} \vec{A} \vec{i} \vec{n} \frac{1}{4} \vec{I} \vec{A}_i \vec{C} \vec{C} \ll \vec{A} \vec{O} \vec{o} \vec{U} \vec{C} \vec{C} \vec{A} \vec{C} \vec{C}$$

$$\vec{p} \vec{1} \vec{2} \vec{i} \vec{o} \vec{A} \vec{o} \vec{I} \vec{U} \vec{C} \vec{D} . 250 \text{ zC } \pm \frac{1}{4} \vec{O} \vec{U} \vec{C} \vec{C} \vec{O} \vec{A} \vec{U} \vec{C} \vec{C} \vec{A} \vec{C} \vec{S} \vec{A} \vec{o}$$

$$\vec{O} \vec{E} \vec{A} \vec{A} \vec{O} \vec{o} \vec{D} \vec{1} \vec{3} \vec{4} \vec{i} \vec{l} \vec{A} \vec{C} \vec{O} \vec{A} \vec{o} \vec{I} \vec{U} \vec{C} \vec{D} \pm \vec{E} \vec{C} \vec{C} , \vec{p} \vec{E} \vec{A} \vec{C} \vec{C} \downarrow \hat{o} \vec{A} \vec{o} \vec{A} \vec{I} \vec{o} \vec{p} \vec{O} \hat{A} \circ \hat{A} \circ \vec{1} \vec{2} \vec{A} \hat{A} \vec{C} \vec{C} \downarrow \hat{o} \vec{A} \vec{o} \vec{A} \vec{I} \vec{o} \pm \frac{3}{4} \vec{C} \vec{C} \frac{3}{4} \vec{i} \vec{l} \vec{o} \vec{3} \vec{4} \vec{O} \vec{o} \vec{y} \vec{i} \vec{n} \vec{C} .$$

$\frac{1}{2} \times 1.5 \times 0.9 = 0.675$



A/40 1-49

- (1) $G \hat{=} 50 \downarrow AG=GB$
- (2) $A \hat{=} A_x \rightarrow, A_y \uparrow$
- (3) $B \hat{=} 250 \downarrow$
- (4) $BC \hat{=} T$

...

« ô | À | Ø Ð,

$$A_x - T \cos \theta = 0, \theta = DBC \quad (1)$$

$$A_y + T \sin \theta - 50 - 250 = 0 \quad (2)$$

Missing

...

« ô | À | Ø Ð,

$$\Delta CDB, \sin \theta = \frac{DC}{BC} = \frac{0.9}{1.5} = \frac{3}{5}$$

$$\cos \theta = \frac{DB}{BC} = \frac{1.2}{1.5} = \frac{4}{5}$$

$$\Delta ADB \hat{=} AD = DB = 1.2$$

$$\therefore AB = \sqrt{(1.2)^2 + (1.2)^2} = 1.2 \times \sqrt{2}$$

(3) $\hat{=} \dots$

$$T \times 1.2 \times \sqrt{2} \{ \sin 45^\circ \cos \theta + \cos 45^\circ \sin \theta \}$$

$$= 50 \times 0.6 \times \sqrt{2} \times \frac{1}{\sqrt{2}} + 250 \times 1.2 \times \sqrt{2} \times \frac{1}{\sqrt{2}}$$

$$T \times 1.2 \times \sqrt{2} \left\{ \frac{1}{\sqrt{2}} \times \frac{4}{5} + \frac{1}{\sqrt{2}} \times \frac{3}{5} \right\} = 30 + 300$$

$$1.68T = 330$$

$$T = \frac{330}{1.68}$$

$$= 196.42 \text{ Ն.}$$

(1) Գծ օճյնի ճեղճոճ

$$A_x = T \cos \theta = 196.42 \times \frac{4}{5}$$

$$= 157.136 \text{ Ն.}$$

$$A_y = 300 - T \sin \theta$$

$$= 300 - 196.42 \times \frac{3}{5}$$

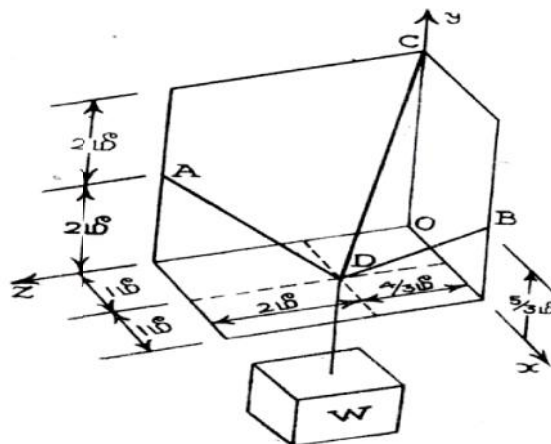
$$= 300 - 117.85$$

$$= 182.15 \text{ Ն.}$$

$$\pm \text{ՋՏ} \quad T = 196 \text{ Ն.} \quad A_x = 157 \text{ Ն.} \quad A_y = 182; \text{ Ն.}$$

Այ՛՛ 1.28.

500 ՏՏ, ՏՏ օճյնի ճեղճոճ 1.50ճ
 ճեղճոճ ԵՃ. BD ճեղճոճ ԵՃ
 ճեղճոճ ԵՃ
 ճեղճոճ ԵՃ
 « ճեղճոճ ԵՃ »



Աճ 1-50

DA, DB, DC ճեղճոճ ճեղճոճ ԵՃ
 ճեղճոճ ԵՃ. D-ճեղճոճ ճեղճոճ ԵՃ
 $\underline{W} = -500j$ ճեղճոճ ԵՃ.

Օ՛՛ ԵՃ ԵՃ ԵՃ ԵՃ ԵՃ ԵՃ « ճեղճոճ »

1/3 i, 2/3 j, 5/3 k

A(0, 2, 10/3); B(2, 5/3, 0); C(0, 4, 0); D(1, 0, 4/3)

$$\underline{DA} = \underline{OA} - \underline{OD} = -i + 2j + 2k$$

$$= 3(-\frac{1}{3}i + \frac{2}{3}j + \frac{2}{3}k)$$

$$\underline{DB} = \underline{OB} - \underline{OD} = (i + \frac{5}{3}j - \frac{4}{3}k)$$

$$= \frac{5\sqrt{2}}{3} \left(\frac{3}{5\sqrt{2}}i + \frac{1}{\sqrt{2}}j - \frac{4}{5\sqrt{2}}k \right)$$

$$= \frac{5\sqrt{2}}{3} \left(\frac{3}{7.07}i + \frac{5}{7.07}j - \frac{4}{7.07}k \right)$$

$$\underline{DC} = \underline{OC} - \underline{OD} = -i + 4j - \frac{4}{3}k$$

$$= \frac{13}{3} \left(-\frac{3}{13}i + \frac{12}{13}j - \frac{4}{13}k \right)$$

$$\therefore \underline{T}_A = \frac{T}{3} (-i + 2j + 2k)$$

$$\underline{T}_B = \frac{T}{7.07} (3i + 5j - 4k)$$

$$\underline{T}_C = \frac{T}{13} (-3i + 12j - 4k)$$

$$\underline{W} = -500j$$

$$\underline{R} = \underline{T}_A + \underline{T}_B + \underline{T}_C + \underline{W}$$

$$= \frac{T}{3} (-i + 2j + 2k) + \frac{T}{7.07} (3i + 5j - 4k) + \frac{T}{13} (-3i + 12j - 4k) - 500j$$

$$= \left(\frac{T}{3} + \frac{3T}{7.07} - \frac{3T}{13} \right) i + \left(\frac{2T}{3} + \frac{T}{7.07} + \frac{T}{13} - 500 \right) j + \left(\frac{2T}{3} - \frac{4T}{7.07} - \frac{4T}{13} \right) k$$

0 = 0, 0 = 0, 0 = 0

R = 0, Rx = 0, Ry = 0, Rz = 0

$$\frac{T}{3} + \frac{3T}{7.07} - \frac{3T}{13} = 0$$

$$\frac{2T}{3} + \frac{T}{7.07} + \frac{T}{13} - 500 = 0$$

$$\frac{2T}{3} - \frac{4T}{7.07} - \frac{4T}{13} = 0$$

1/3 i, 2/3 j, 5/3 k (TA, TB, TC) = 0, 0, 0

$$T_A = 295, T_B = 290, T_C = 106.5$$

$$\underline{T}_B = 290 \left(\frac{3}{7.07}i + \frac{5}{7.07}j - \frac{4}{7.07}k \right)$$

0 = 0, 0 = 0

DB = 290 (3/7.07 i + 5/7.07 j - 4/7.07 k)

$\sum F_x = 0$, $\sum F_y = 0$, $\sum F_z = 0$, $\sum M_x = 0$, $\sum M_y = 0$, $\sum M_z = 0$.
 - $\sum F_x = 0$ \Rightarrow $T_B = 290$ N.

$M_{AC} = n_{AC} \cdot (r_{AD} \wedge \sum F) = 0$

$$\therefore n_{AC} = \frac{2j - \frac{10}{3}k}{\sqrt{\frac{136}{9}}} = \frac{6j - 10k}{\sqrt{136}}$$

$$r_{AD} = i - 2j - 2k$$

$$\sum F = T_B + W$$

$$= \frac{3T_B}{7.07}i + \frac{5T_B}{7.07}j - \frac{4T_B}{7.07}k - 500j$$

$$= \frac{3T_B}{7.07}i + \left(\frac{5T_B}{7.07} - 500\right)j - \frac{4T_B}{7.07}k$$

$$\therefore M_{AC} = \begin{vmatrix} 0 & 6 & -10 \\ 1 & -2 & -2 \\ \frac{3T_B}{7.07} & \left(\frac{5T_B}{7.07} - 500\right) & \frac{-4T_B}{7.07} \end{vmatrix} = 0$$

$\sum M_x = 0 \Rightarrow 6\left(\frac{4T_B}{7.07} - \frac{6T_B}{7.07}\right) - 10\left(\frac{5T_B}{7.07} - 500 + \frac{6T_B}{7.07}\right) = 0$

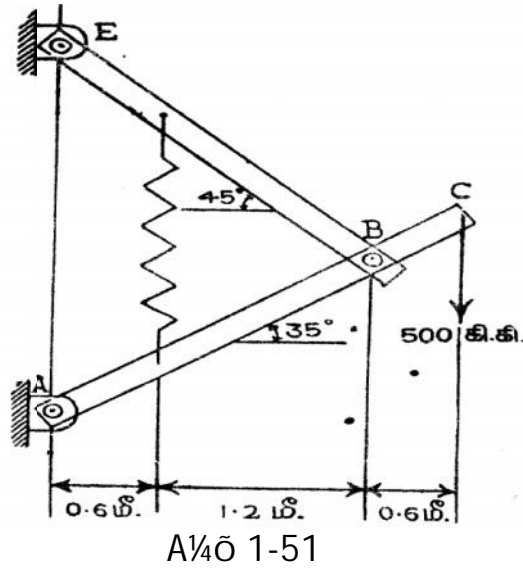
$$6\left(\frac{4T_B}{7.07} - \frac{6T_B}{7.07}\right) - 10\left(\frac{5T_B}{7.07} - 500 + \frac{6T_B}{7.07}\right) = 0$$

$\Rightarrow \frac{3}{4} T_B = 290$ N.

$$\therefore T_B = \frac{290}{7.07} (3i + 5j - 4k)$$

Áj 1.29

$\sum F_x = 0$, $\sum F_y = 0$, $\sum F_z = 0$, $\sum M_x = 0$, $\sum M_y = 0$, $\sum M_z = 0$.
 $\sum F_x = 0 \Rightarrow T_B = 290$ N.



EB 0.8m, E 0.8m, A 0.8m, C 500 mm. AB 35°, EB 45°. A10 1-51

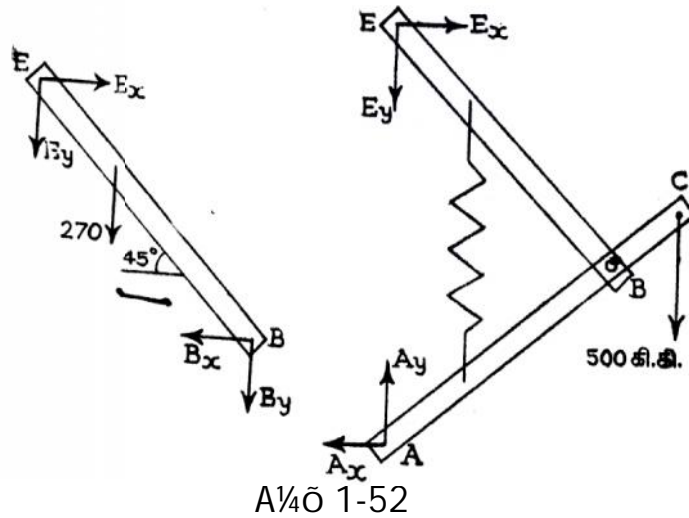


Diagram showing forces E_x , E_y , B_x , B_y , A_x , A_y and a vertical force of 500 mm at point C.

Free body diagram of member EB showing forces E_x , E_y , B_x , and B_y . The angle is 45°.

Free body diagram of member AB showing forces A_x , A_y , B_x , and B_y .

- (4) $\underline{F}_2 = -72 \underline{j} \pm \underline{y} \hat{U} \circ \hat{A} \hat{c} \circ S(8.7, 0) \hat{A} \hat{f} \pm \underline{y} \hat{E} \text{ p} \frac{1}{4} \hat{d} \frac{3}{4} \hat{A} \text{ } | \circ \hat{A} \hat{c} \hat{A} \hat{I} \text{ } \hat{c} \hat{E} \hat{D}.$
 (5) $\underline{F}_3 = -250 \underline{j} \pm \underline{y} \hat{U} \circ \hat{A} \hat{c} \circ T(4.95, 0) \hat{A} \hat{f} \pm \underline{y} \hat{E} \text{ p} \frac{1}{4} \hat{d} \frac{3}{4} \hat{A} \text{ } | \circ \hat{A} \hat{c} \hat{A} \hat{I} \text{ } \hat{c} \hat{E} \hat{D}$
 (6) $\underline{C} = -75 \underline{k} \pm \underline{y} \hat{U} \circ \hat{A} \hat{c} \circ \hat{A} \hat{f} \pm \underline{y} \hat{U} \circ \hat{I} \hat{A} \hat{c} \circ \frac{1}{2} \hat{D} \hat{d} \frac{3}{4} \hat{E} \hat{U} \circ \text{ } | \circ \hat{A} \hat{c} \hat{A} \hat{I} \text{ } \hat{c} \hat{E} \hat{D}.$

$$\underline{R} = \sum \underline{F}_i = 0 \pm \underline{y} \hat{U} \circ \hat{A} \hat{c} \circ \hat{A} \hat{I} \circ \hat{A} \hat{y} \hat{A} \hat{I} \hat{I}$$

$$R_1 + R_2 - 500 - 72 - 250 = 0 \rightarrow \hat{I} \hat{D}, \therefore R_1 + R_2 = 822$$

$$A \hat{U} \hat{E} \hat{c} \hat{A} \hat{c} \circ \hat{U} \circ \frac{1}{4} \hat{A} \hat{c} \hat{O} \hat{d} \frac{3}{4} \hat{E} \hat{y} \text{ } \hat{c} \hat{y} \hat{U} \hat{I} \frac{3}{4} \hat{D}$$

$$= (7.5 \underline{i} \wedge R_2 \underline{j}) + (1.5 \underline{i} \wedge -500 \underline{j}) + (8.7 \underline{i} \wedge -72 \underline{j})$$

$$+ (4.95 \underline{i} \wedge -250 \underline{j});$$

$$= 7.5 R_2 \underline{k} - 2613.9 \underline{k}$$

$\pm \hat{E} \hat{S} \hat{A} \text{ } A \hat{U} \hat{E} \hat{c} \ll \hat{A} \hat{O} \hat{d} \frac{3}{4} \hat{O} \hat{d} \frac{3}{4} \hat{E} \hat{y} \text{ } \hat{c} \hat{y} \hat{I} \hat{E} \hat{A} \hat{c} \hat{A} \hat{c} \hat{U} \hat{D} \hat{I} \hat{D} \text{ } | \frac{3}{4} \hat{I} \text{ } \hat{A} \hat{O} \hat{a} \hat{I} \circ \hat{A} \hat{d} \frac{3}{4} \hat{U} \hat{I} \hat{I} \circ \hat{A} \hat{O} \hat{A} \hat{I} \hat{D} \hat{D} \text{ } .$

$$\ll \hat{O} \hat{I} \hat{A} \hat{I} \hat{D} \hat{D}, 7.5 R_2 \underline{k} - 2613.9 \underline{k} - 75 \underline{k} = 0$$

$$7.5 R_2 = 1451.4$$

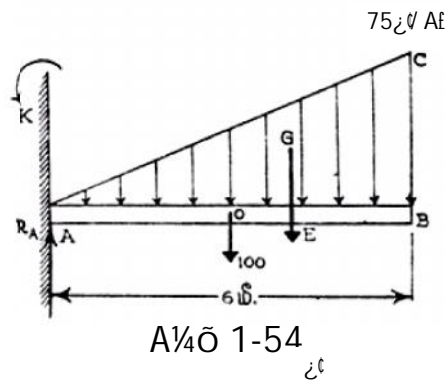
$$R_2 = 358.52 \text{ } \hat{c} \hat{I}.$$

$$\therefore R_1 = 822 - 358.52$$

$$= 463.48 \text{ } \hat{c} \hat{I}.$$

$\pm \hat{E} \hat{S} \hat{A} \text{ } A, B \pm \underline{y} \hat{U} \hat{D} \hat{U} \hat{c} \hat{c} \text{ } \hat{c} \hat{D} \text{ } | \circ \hat{A} \hat{c} \hat{A} \hat{I} \hat{D} \pm \frac{3}{4} \hat{c} \hat{I} \text{ } \hat{A} \hat{c} \hat{I} \text{ } \hat{U} \hat{O} \hat{I} \hat{E} \hat{S} \hat{A}$
 $R_1 = 463.48 \text{ } \hat{c} \hat{I}.$
 $R_2 = 358.52 \text{ } \hat{c} \hat{I}.$

$\hat{A} \hat{I} \hat{c} \hat{I} \text{ } 1.31. A \pm \underline{y} \hat{U} \hat{A} \hat{c} \frac{1}{4} \hat{d} \frac{3}{4} \hat{D} \hat{A} \hat{O} \hat{d} 1.54 \hat{D} \text{ } \hat{I} \hat{D} \hat{E} \hat{A} \hat{O} \hat{A} \hat{I} \hat{E} \text{ } \hat{D} \hat{A} \hat{O} \hat{d} \frac{3}{4} \hat{y} \text{ } \hat{I} \hat{U} \hat{I} \hat{I} \text{ } | \hat{A} \hat{O} \hat{I} \hat{O} \hat{A} \hat{I} \frac{3}{4} \hat{A} \hat{c} \hat{D} \text{ } | \hat{O} \hat{d} \frac{3}{4} \hat{O} \hat{A} \hat{I} \hat{D} \hat{A} \hat{c} \hat{I} \hat{D} \text{ } | \frac{3}{4} \hat{I} \hat{I} \frac{3}{4} \hat{A} \hat{c} \hat{y} \ll \hat{A} \hat{O} \hat{I} \hat{A} \hat{I} \text{ } \hat{I} \hat{D} \hat{D} \text{ } .$
 $\hat{D} \hat{A} \hat{O} \hat{d} \frac{3}{4} \hat{y} \pm \hat{A} \hat{O} \hat{I} \hat{A} \hat{I} \hat{D} \hat{D} \text{ } 100 \text{ } \hat{c} \hat{I} \text{ } \pm \hat{E} \hat{I} \text{ } | \hat{I} \hat{D} \hat{D} \text{ } .$



$\hat{O} \hat{A} \hat{I} \hat{E} \text{ } \hat{D} \hat{A} \hat{O} \hat{d} \frac{3}{4} \hat{I} \hat{O} \hat{A} \hat{c} \hat{I} \hat{D} \hat{D} \hat{A} \hat{O} \hat{d} \frac{3}{4} \hat{O} \hat{I} \hat{I} \hat{D} \hat{A} \hat{c} \hat{I} \text{ } \hat{c} \hat{y} \text{ } | \frac{3}{4} \hat{I} \hat{I} \frac{3}{4} \hat{D}$
 (1) $\ll \frac{3}{4} \hat{y} \pm \hat{A} \hat{O} \hat{I} \hat{A} \hat{I} \hat{D} \hat{D} = 100 \text{ } \hat{c} \hat{I} \hat{A} \hat{f} \hat{I} \hat{D}, 0 \pm \underline{y} \hat{U} \hat{D} \hat{U} \hat{c} \hat{c} \hat{A} \hat{c} \hat{D} \text{ } (AO = OB = 3 \hat{A} \hat{I})$

(2) $\sum \vec{S} \cdot \vec{A}_i = \vec{A}_i \cdot \vec{U} \cdot \vec{A} \cdot \vec{C} = 75 \text{ kN}$ ($\vec{C} = 0.866 \vec{i} - 0.5 \vec{j}$)
 $= \frac{1}{2} \times 75 \times 6 = 225 \text{ kNm}$ ($\vec{C} = 0.866 \vec{i} - 0.5 \vec{j}$)

($G = \vec{y} \cdot \vec{A} \cdot \vec{D} \cdot \vec{A} \cdot \vec{B} \cdot \vec{C}$, $\vec{D} = 0.866 \vec{i} - 0.5 \vec{j}$)

(3) $\sum \vec{R}_A \uparrow = \vec{y} \cdot \vec{E} = 100 \text{ kN}$, $\vec{A} \cdot \vec{C} \cdot \vec{D} \cdot \vec{K} \cdot \vec{y} \cdot \vec{U} = 300 \text{ kNm}$
 $\vec{C} = 0.866 \vec{i} - 0.5 \vec{j}$, $\vec{D} = 0.866 \vec{i} - 0.5 \vec{j}$, $\vec{K} = 0.866 \vec{i} - 0.5 \vec{j}$

$R_A = 100 - 225 = 0 \therefore R_A = 325 \text{ kN}$

$\vec{A} = \vec{y} \cdot \vec{U} = 0.866 \vec{i} - 0.5 \vec{j}$, $\vec{D} = 0.866 \vec{i} - 0.5 \vec{j}$, $\vec{K} = 0.866 \vec{i} - 0.5 \vec{j}$

$K = 100 \times 3 - 225 \times 4 = 0$

$K = 300 + 900 = 1200 \text{ kNm}$

$\vec{A}_i = 1.32 \vec{i} + 1.55 \vec{j}$, $\vec{C} = 0.866 \vec{i} - 0.5 \vec{j}$, $\vec{D} = 0.866 \vec{i} - 0.5 \vec{j}$, $\vec{E} = 0.866 \vec{i} - 0.5 \vec{j}$

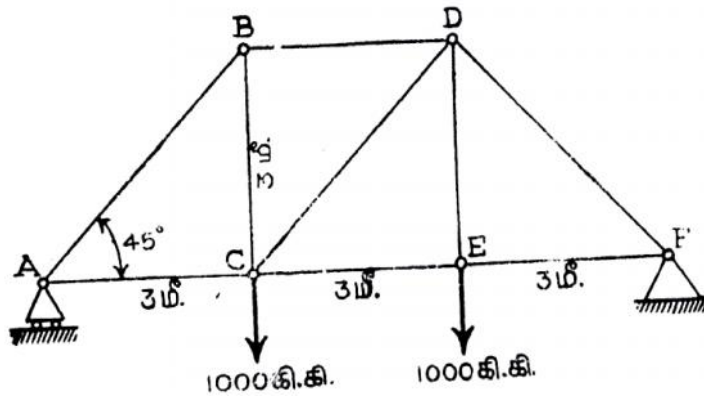


Figure 1-55

Reaction at A: $\vec{R}_A = 1000 \text{ kN}$ ($\vec{C} = 0.866 \vec{i} - 0.5 \vec{j}$)
 Reaction at F: $\vec{R}_F = 1000 \text{ kN}$ ($\vec{D} = 0.866 \vec{i} - 0.5 \vec{j}$)

(i) $\vec{R}_1 = 1000 \text{ kN}$, $\vec{R}_2 = 1000 \text{ kN}$

(ii) $\vec{R}_2 = 1000 \text{ kN}$

(iii) $\vec{C} = 1000 \text{ kN}$

(iv) $\vec{D} = 1000 \text{ kN}$

$\sum F_{iy} = 0 \Rightarrow R_1 + R_2 - 2000 = 0$

$\therefore R_1 = R_2$

Reaction at A: $\vec{R}_1 = R_2 = 1000 \text{ kN}$

$\vec{R}_1 = R_2 = 1000 \text{ kN}$

$\vec{R}_1 = R_2 = 1000 \text{ kN}$

Figure 1-56 shows a free body diagram of a joint. A vertical force of 1000 units acts upwards from the left. A horizontal force of 1000 units acts to the right, labeled AC. A diagonal force of 1414 units acts upwards and to the right, labeled AB. The text above the diagram indicates that the vertical force is 1000 units, the horizontal force is 1000 units, and the diagonal force is 1414 units.

$$\sum F_{iy} = 0, \uparrow +$$

$$-0.707AB + 1000 = 0$$

$$\therefore AB = 1414$$

$$\sum F_{ix} = 0, \rightarrow +$$

$$AC - 0.707AB = 0$$

$$AC = 1000$$

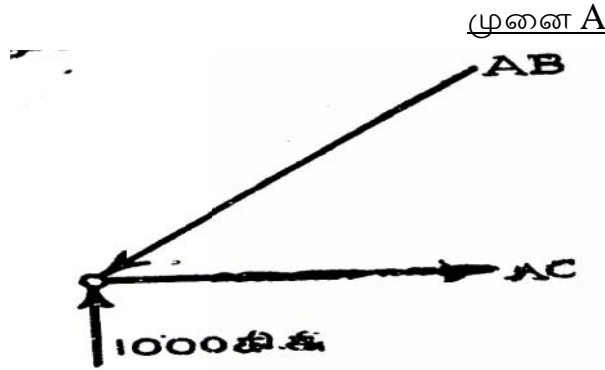


Figure 1-56

Figure 1-56 shows a free body diagram of a joint. A vertical force of 1000 units acts upwards from the left. A horizontal force of 1000 units acts to the right, labeled AC. A diagonal force of 1414 units acts upwards and to the right, labeled AB. The text above the diagram indicates that the vertical force is 1000 units, the horizontal force is 1000 units, and the diagonal force is 1414 units.

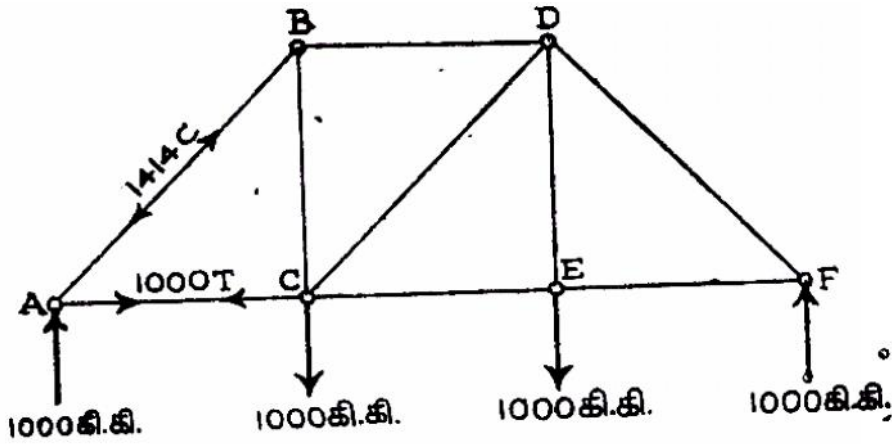
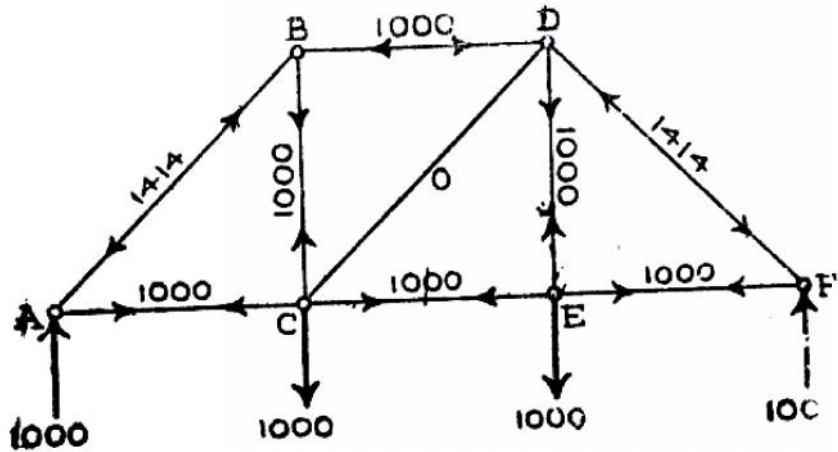


Figure 1-57

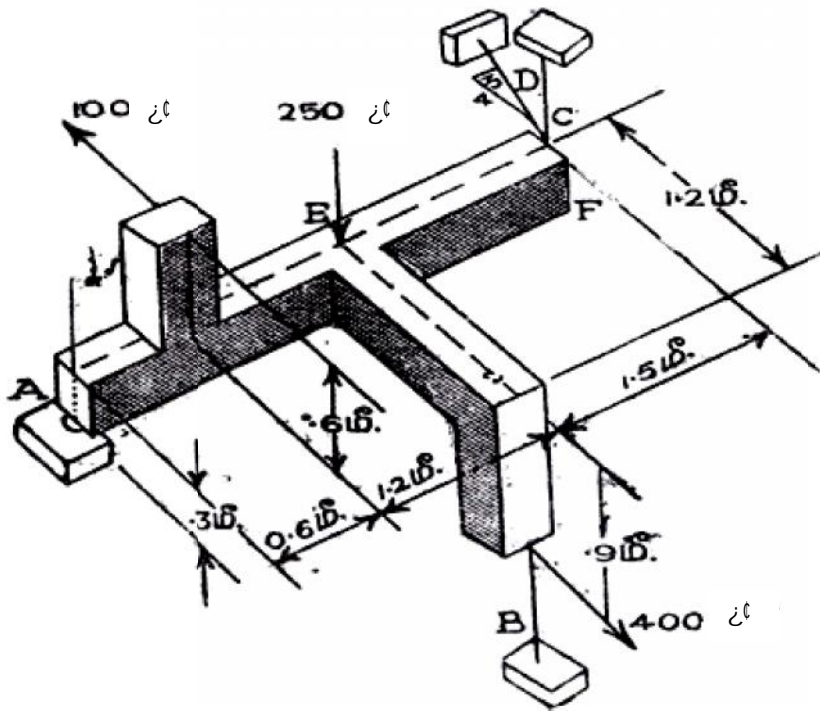
Figure 1-57 shows a truss structure. A vertical force of 1000 units acts upwards at joint A. A horizontal force of 1000 units acts to the right at joint C, labeled AC. A vertical force of 1000 units acts downwards at joint B. A vertical force of 1000 units acts downwards at joint E. A vertical force of 1000 units acts downwards at joint F. A diagonal force of 1414 units acts upwards and to the right at joint C, labeled BC. The text above the diagram indicates that the vertical force at A is 1000 units, the horizontal force at C is 1000 units, and the diagonal force at C is 1414 units.

Figure 1-58 shows a truss structure. A vertical force of 1000 units acts upwards at joint A. A horizontal force of 1000 units acts to the right at joint C, labeled AC. A vertical force of 1000 units acts downwards at joint B. A vertical force of 1000 units acts downwards at joint E. A vertical force of 1000 units acts downwards at joint F. A diagonal force of 1414 units acts upwards and to the right at joint C, labeled BC. The text above the diagram indicates that the vertical force at A is 1000 units, the horizontal force at C is 1000 units, and the diagonal force at C is 1414 units.



À¼õ 1-60

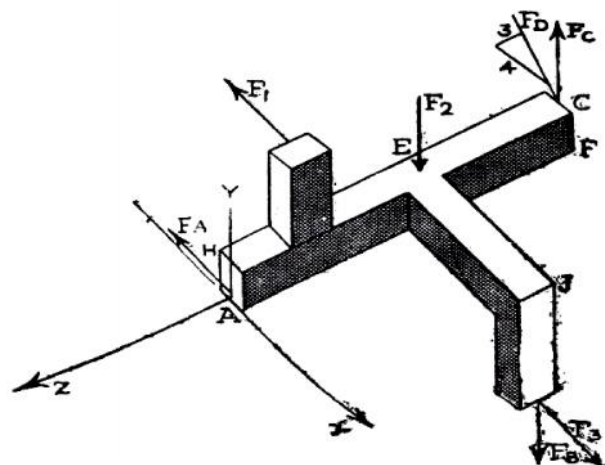
À¼õ 1.33. À¼õ 1.61ø ÷ ðÈÔÛÇ | À¼õÇÉÐ A ±ýÛÁ¼ð¼ø - Åø Ì ÅÄô | À¼õ¼ÄÉ (ball and socket) « " Åô" A ÷¼ÄÄ¼ì | ÷ìñ Î B,C ±ýÛø ðÔ ÅÖÄÉ | °í Ì ðÈÌ ÷øÄÇÖ, Ö,



À¼õ 1-61

D ±ýÛø ÅÖÄÉÐø ð¼ÄÄ" Åôø ÷øÄÄÖø ÷¼í øÄÌ ÷ýÈÐ. « ø|À¼õÇý ±¼ øÈì ½ø øÄø¼¼¼ì | ÷ìñ Î A ±ýÛÁ¼ð¼ø | °ÄüÄø ±¼¼¼ì Åôø, B,C,D ÷øÄÇø | °ÄÄø ðøÄøøü ÷øÄü" È Ä" ÄÄüì.

$\hat{A} \approx 1.62 \hat{i} + \hat{j} + 0.6 \hat{k}$



A ≈ 1.62

The diagram shows a 3D coordinate system with axes x, y, z . The forces are defined as follows:

$$\begin{aligned}
 \underline{F}_A &= A_x \underline{i} + A_y \underline{j} + A_z \underline{k} & \underline{r}_A &= 0 \\
 \underline{F}_B &= -B \underline{j} & \underline{r}_B &= 1.2 \underline{i} - 1.8 \underline{k} \\
 \underline{F}_C &= -B + C & \underline{r}_C &= -3.3 \underline{k} \\
 \underline{F}_D &= D(0.8 \underline{i} - 0.6 \underline{k}) & \underline{r}_D &= 0.3 \underline{j} - 3.3 \underline{k} \\
 \underline{F}_1 &= -100 \underline{i} & \underline{r}_1 &= 0.9 \underline{j} - 0.6 \underline{k} \\
 \underline{F}_2 &= -250 \underline{j} & \underline{r}_2 &= -1.8 \underline{k} \\
 \underline{F}_3 &= 400 \underline{i} & \underline{r}_3 &= -0.6 \underline{j} - 1.8 \underline{k}
 \end{aligned}$$

$$\underline{R} = \sum_{i=1}^n F_i = 0 \pm \hat{y} \hat{U} \hat{o} \hat{o} \hat{A} \hat{y} \hat{A}_i \hat{I}$$

$$\underline{R} = \underline{i}(A_x - 0.8D - 100 + 400) + \underline{j}(A_y - B + C - 250) + \underline{k}(A_z - 0.6D) = 0 \pm \hat{y} \hat{E}_j \hat{I} \hat{o}$$

$$\ll \hat{A} \hat{D} A_x - 0.8D + 300 = 0 \dots \dots \dots (1)$$

$$A_y - B + C - 250 = 0 \dots \dots \dots (2)$$

$$A_z - 0.6D = 0 \dots \dots \dots (3)$$

$$\begin{aligned} \underline{M}_0^R &= \sum_{i=1}^n \underline{r}_i \wedge \underline{F}_i = 0 \pm \underline{y} \hat{U} \hat{o} \circ \hat{A} \hat{y} \hat{A}_i \hat{I} \\ &0 + (1.2\underline{i} - 1.8\underline{k}) \wedge (-3.3\underline{k}) \wedge (C\underline{j}) \\ &+ (0.3\underline{j} - 3.3\underline{k}) \wedge (-0.8D\underline{i} - 0.6D\underline{k}) \\ &+ (0.9\underline{j} - 0.6\underline{k}) \wedge (-100\underline{i}) + (-1.8\underline{k}) \wedge (-250\underline{j}) \\ &+ (-0.6\underline{j} - 1.8\underline{k}) \wedge (400\underline{i}) = 0 \\ &\pm \underline{y} \hat{E}_i \hat{I} \hat{o}. \end{aligned}$$

$$\begin{aligned} &\ll \frac{3}{4} \hat{A} \hat{D} \\ &-1.2B\underline{k} - 1.8B\underline{i} + 3.3C\underline{i} + 0.24D\underline{k} - 0.18D\underline{i} + 0.264D\underline{j} \\ &90\underline{k} + 60\underline{j} - 450\underline{i} + 240\underline{k} - 720\underline{j} = 0 \end{aligned}$$

$$\begin{aligned} &\ll \frac{3}{4} \hat{A} \hat{D} \\ &\underline{i}(-1.8B + 3.3C - 0.18D - 450) + \underline{j}(0.264D + 60 - 720) \\ &+ \underline{k}(-1.2B + 0.24D + 90 + 240) = 0 \end{aligned}$$

$$\ll \frac{3}{4} \hat{A} \hat{D} \quad -1.8B + 3.3C - 0.18D - 450 = 0 \quad (4)$$

$$0.264D + 660 = 0 \quad (5)$$

$$-1.2B + 0.24D + 330 = 0 \quad (6)$$

$$(4)(5)(6) \pm \underline{y} \hat{U} \hat{o} \circ \hat{A} \hat{y} \hat{A}_i \hat{I} \quad \hat{U} \hat{I} \hat{o} \quad \frac{3}{4} \hat{E} \times \hat{s}_i \hat{n} \quad (7)$$

$$\ll \hat{o} \hat{A}_i \hat{D} \quad B = 325 \text{ çł.} \quad (7)$$

$$C = 327.5 \text{ çł.} \quad (8)$$

$$D = 250 \text{ çł.} \quad (9)$$

$$\begin{aligned} &\pm \hat{E} \hat{s} \hat{A} (1) \hat{A} \hat{D} \circ \hat{A} \hat{y} \hat{A}_i \hat{I} \\ &A_x = 0.8D - 300 = 0.8 \times 250 - 300 = -100 \text{ çł.} \quad \rightarrow \hat{I} \hat{o}. \end{aligned} \quad (10)$$

$$\begin{aligned} &\ll \hat{u} \hat{A}_i \hat{s} \hat{E} (2) \hat{A} \hat{D} \circ \hat{A} \hat{y} \hat{A}_i \hat{I} \\ &A_y = 250 + B - C = 250 + 325 - 327.5 = 247.5 \text{ çł.} \quad \rightarrow \hat{I} \hat{o}. \end{aligned} \quad (11)$$

$$\begin{aligned} &\text{p} \hat{U} \frac{3}{4} \hat{A}_i \hat{s} (3) \hat{A} \hat{D} \circ \hat{A} \hat{y} \hat{A}_i \hat{I} \\ &A_z = 0.6D = 0.6 \times 250 = 150 \text{ çł.} \quad \rightarrow \hat{I} \hat{o}. \end{aligned} \quad (12)$$

$$\therefore \underline{F}_A = -100\underline{i} + 247.5\underline{j} + 150\underline{k} \quad (13)$$

$\hat{A} \hat{A} \hat{u} \hat{o} \hat{s} \hat{u}$

1-1 « ÊôÂ'' ¼ « ÂĬ ù (Fundamental Units) ÂĬôô¼ « ÂĬ ù (derived units) ñ Æü'' Èð¼Ĭ ó¼ ±Ĭ òÐĬ ÿĬ ù ¼ý ÂĬĬ ÿ

1-2 ĬĬ Ê, ±'' ¼ p'' Â ù Ĭ Ĭ ùĈ şĂüŪ'' Â'' Â ÂĬĬ Ĭ ÿ

1-3 Âý ÂŌö ÂĬ°Ĭ Çý ÂĬ; ½Ĭ ù ÂĬ'' Â?

(i) « ¼÷ò¼Ĭ (ii) - ó¼ö (iii) şĂ'' Â (iv) şĬ ½ö (v) « Øò¼ö

1-4 ūĬ ĬĬ ö pĂüĂø ÂĬ°Ĭ Çý ÂĬ; ½Ĭ ÿ ĬĬ Ĭ ÿ

(i) şĬ÷şĬ ĬĬ - ó¼ö (Linear Momentum)

(ii) ¼ŌĬ ĬĬ Ōü Ăø 'ý Èý ¼ý É¼òş¼ ş°ĂòÐ'' Âò¼ŌĬ Ĭ ö (ĬĬ Â) ñ üÊø

(iii) ¼ĂĂ « Øò¼ö (Fluid pressure)

(iv) ¼Ōöòò¼ĬÉý

(v) pĂĬ ĬĬ üÊø (Kinetic energy)

(vi) şĬ ½ - ó¼ö (Angular momentum)

$$(i) [şĬ ÷ şĬ ĬĬ - ó¼ö] = [ĬĬ Ê \times ¼Ĭ \circ şĂ \circ] = MLT^{-1}$$

$$(ii) [ĬĬ Â \rightarrow üÊø] = \left[\frac{1}{2} kx^2 \right] = [ML^2T^{-2}]$$

$$(iii) [¼ĂĂ \ll Øò¼ö] = \frac{[şĬ ÷ Ĭ òÐĂĬ \circ]}{[ĂĂòò]} = [ML^{-1}T^{-2}]$$

$$(iv) [¼Ōöòòò¼ĬÉý] = [Ĭ Ĭòò şĬ ĬĬý'' ĬĬö][ĂĬ \circ] = [ML^2T^{-2}]$$

$$(v) [pĂĬ ĬĬ üÊø] = \left[\frac{1}{2} mv^2 \right] = [ML^2T^{-2}]$$

$$(vi) [şĬ ½ - ó¼ö] = [ĬĬö \times şĬ ÷ şĬ ĬĬ - ó¼ö] = [ML^2T^{-1}]$$

1-5 ' Âý ÂŌö °Áý ÂĬĬ Çø ±Ĭ °Áý ÂĬĬ ù ÂĬ; ½Ĭ Çø ÓĂ½üÊ¼Ĭ ùĈÉ ±ĬĬ ĬĬ ŌĂĬ ùĈ¼Ĭ pŌĬ ĬĬ ÉĬø « ¼üĬ ĬĬ ĬĬ ½Ĭ ĬĬ ĬĬ ŪŪ

(i) $v = u + as$

(ii) $T = 2fEI / L$

$T = ¼Ōöòòò¼ĬÉý E = Ăö°Ĭ Ĭ (Ĭ Ĭ / ĂĬ^2)$

$I = ĂĂôĂĈ \times Ĭ Ĭ ĬĬ ĬĬ ĬĬöòòò¼ĬÉý (Area of moment of inertia)$

$L = ĬĬö$

$$(iii) s = ut + \frac{1}{2}at^2$$

$$(iv) y = -\frac{wx}{24EI}(L^2 - 2Lx^2 + x^3)$$

x, y շարժմի փոխարկերի մասին է

$$L = \text{հարկի երկարություն}$$

$$w = \mu \frac{\Delta \rho}{\Delta x} \text{ շարժմի արագություն}$$

$$E = \text{հարկի մոդուլ}$$

$$I = \text{հարկի թափանցանի մոմենտ}$$

$$(v) p = p_a + g \dots h, p, p_a \pm \gamma \Delta h \ll \rho g h, \dots$$

$$g = \text{ճնշման ուժի ուղղություն}$$

$$h = \text{« ճնշման արագություն»}$$

$$\dots = \text{« ճնշման ուժ»}$$

$$(vi) \tau = T \cdot L \left(\frac{a^2 + b^2}{f a^3 b^3 G} \right), \tau = \text{ճնշման ուժի մասին է}$$

$$a, b = \text{հարկի թափանցանի շառվիտներ}$$

$$G = \text{հարկի մոդուլ (modulus of rigidity in kg/m}^2\text{)}$$

$$T = \text{ճնշման ուժի մասին է}$$

$$L = \text{շարժմի երկարություն}$$

1-6 m շարժմի մասին է ճնշման ուժի մասին է $r = \text{հարկի թափանցանի շառվիտ}$ $v = \text{ճնշման ուժի մասին է}$ $p = \text{ճնշման ուժի մասին է}$ $F_r = \text{ճնշման ուժի մասին է}$ $F_r = \text{ճնշման ուժի մասին է}$ $\Delta y = \text{ճնշման ուժի մասին է}$

$$F_r = \frac{mv^2}{r} \text{ մասին է}$$

$\Delta y = \text{ճնշման ուժի մասին է}$ $\Delta y = \text{ճնշման ուժի մասին է}$ $\Delta y = \text{ճնշման ուժի մասին է}$

1-7 $\mu = \text{ճնշման ուժի մասին է}$ $g = \text{ճնշման ուժի մասին է}$ $\text{ճնշման ուժի մասին է}$ $\text{ճնշման ուժի մասին է}$ $\text{ճնշման ուժի մասին է}$

$$T = k \sqrt{\frac{l}{g}} \pm \text{ճնշման ուժի մասին է}$$

$$(i) \text{ ճնշման ուժի մասին է } \{ [T] = [M^a L^b g^c] = [F^a L^{-a+b+c} T^{2a-2c}] \}$$

1-8 $\text{ճնշման ուժի մասին է}$ $\mu = \text{ճնշման ուժի մասին է}$ $\text{ճնշման ուժի մասին է}$ $\text{ճնշման ուժի մասին է}$ $\text{ճնշման ուժի մասին է}$

ŞĂ, ò¼ü ì Ā °ÁýÀ; ð ¼ Ā; Ā; ½í, Çý µ; Āø ¼ðÐĀ ð ¼ô ĀĀýĀĪ ò¼Ā Ā ĀĀŪĪ.

$$\dot{A} \text{ ¼ } \left\{ [v] = [L^{-1}FT^2]^a [F]^b [L]^c = k \sqrt{\frac{fl}{m}} \right\}$$

1-9 òĀĀĒò Ò Ā Ā Ā ĀĀŪĪ ì ò °ÁýĀĪ

$$F = \frac{GM_1M_2}{m^2} \text{ - Ī ò. } G \text{ -ý Ā; Ā; ½í, Çì, ĩ}$$

$$\dot{A} \text{ ¼ } \{ [G] = F^{-1}L^4T^{-4} \}$$

1-10 µ ÷ ĒĀĪÉ ç¼Ā « ĀĀý ¼Ā °ŞĂ, ò (v), « ¼ý « ¼÷ ò¼Ā (...) òĀĀĒò ÓĪ ì ò (g) « Ā ç¼Ā } - ĩ ĀĀŪĪ ĒĪ ò; ðÐŪÇÐ. Ā; Ā; ½í, ŪĪĪ òĀ « ¼ý ç¼Ā Ā Ā ĀĀŪĪ.

$$\dot{A} \text{ ¼ } v = k\sqrt{g}$$

1-11 µ ÷ ĀĀ « ĀĀý ¼Ā °ŞĂ, ò, « ¼ý « ¼÷ ò¼Ā (...) ĀøĪ ĀĪĀĀŞ (Bulk Modulus) (s), [FL⁻²] « Ā ç¼Ā } - ĩ ĀĀŪĪ ĒĪ ò; ðÐŪÇÐ. Ā; Ā; ½í, ŪĪĪ òüĒ¼ĪÉ ç¼Ā Ā Ā ĀĀŪĪ.

$$(\dot{A} \text{ ¼ } v = k \left(\frac{s}{\dots} \right)^{\frac{1}{2}})$$

1-12 ĀĪ ĀĪ òðŪÇ (viscous) ¼ĀĀð¼Ā ±ñ Ā¼Ā ò f - ¼Ā ç¼Ā ĀĀĪÉ Ā Ā Ā ĀĀŪĪ ĀĪĀŪÇ ĀĪĀŪŞĀø ĀĀŪĪ ĀĪĀø ð « ¼ý ¼Ā °ŞĂ, ò (v) ±ñ Ā¼Ā ò (f) Ş, ç¼Ā ŪĪĪ ĀĀĪ òĀĀð (a) ĀĪ ĀĪ òðĪ Āø (Coefficient of viscosity) (y), [ftl⁻²] - ĩ ĀĀŪĪ ĒĪ ò; ðÐŪÇÐ. Ā; Ā; ½í, µ; Āø Ā¼Ā ĀĀĀýĀĪ ò¼Ā ¼Ā °ŞĂ, ò ¼Ā Ā ĀĀŪĪ ì ò °ÁýĀĪ ð ¼Ī ĩ.

$$(\dot{A} \text{ ¼ } \left\{ v = kfa^{\frac{1}{2}}y^{-1} \right\})$$

1-13 Ō Ş, ĩ Ū ÝĪĀĪ ĒĪ ĪüĒĀĀŪĪ ±ĪĪ ò Ş, Āø òĀĀĒò ĀĪĒĀĀ (Gravitational constant) « Ā, Çý ŪĀ ĀĀĒĀĀ ĀĪĪĀĀý « Ā ç¼ĀĪĪ « Ç× (semi major axis) (a) - ĩ ĀĀŪĪ ĒĪ ò; ðÐŪÇÐ. Ā; Ā; ½í, ŪĪĪ òüĒ¼ĪÉ Ş, Āø ç¼Ā ĀĪ ĩ.

$$(\dot{A} \text{ ¼ } ; \left\{ T = KG^{\frac{1}{2}}M^{\frac{1}{2}}a^{\frac{3}{2}} \right\})$$

1-14 ç¼Ā Ō Ç ýĒý ĀĀĒĀø ç¼Ā ūó¼ĀĪ ò ÓŪĪĪ ò¼ĀĒý (T_q) Ī ŪĪĪ ĀĀĪĀĪ ¼ĀĀý ĀĀ¼ð ĪĪĀ× (d) ĀĀĪ ò ĪĪĪĪĪ ĀĀĀ (f) - ĩ ĀĀŪĪ ĒĪ ò; ðÐŪÇÐ. Ā; Ā; ½í, µ; Āø Ā¼Ā ĀĀĀýĀĪ ò¼Ā ÓŪĪĪ ò¼ĀĒý Ā ĀĀŪĪĪ ò °ÁýĀĪ ð ¼Ī ĩ.

[Answer: $35.35i + 25j - 25k$]

1-12 $R_i, (i=1,2,3)$ are direction angles of vector \vec{r} in the first octant. \vec{r} is perpendicular to the plane $x + y + z = 10$. Find \vec{r} .

1-13 Find the direction angles of the vector $\vec{v} = (0.500, -0.707, 0.500)$ in the first octant.

[Answer: $\left\{ \frac{7}{2}i + (1 - \frac{5}{\sqrt{2}})j + \frac{7}{2}k \right\} (10^{-2}) \hat{e}_1$
 $\left\{ -\frac{3}{2}i + (1 + \frac{5}{\sqrt{2}})j + \frac{3}{2}k \right\} (10^{-2}) \hat{e}_2$]

1-14 Find the direction angles of the vector $\vec{a} = (5, 3, 4)$ in the first octant.

[Answer: $A_x = 6, A_y = 5, A_z = -9$]

1-15 Find the direction angles of the vector $\vec{a} = (-1, 5, 4)$ in the first octant.

[Answer: $180, -60, -90$ degrees]

1-16 Find the direction angles of the vector $\vec{v} = \frac{1}{25}(7i - 24k)$ in the first octant.

[Answer: $300(7i - 24k)$ in the first octant]

1-17 Find the direction angles of the vector $\vec{v} = \left(\frac{2}{3}, -\frac{1}{3}, -\frac{2}{3}\right)$ in the first octant.

1-18 Find the direction angles of the vector $\vec{r} = (3.6i - 2.7k)$ in the first octant.

[Answer: $(3.6i - 2.7k)$ in the first octant]

1-19 Find the direction angles of the vector $\vec{v} = (2i + 3j - 6k)$ in the first octant.

[Answer: $(20i + 50j - 60k)$ in the first octant]

1-20 $\vec{A} = 3\hat{i} + 4\hat{j} - 5\hat{k}$, $\vec{B} = 2\hat{i} - 3\hat{j} + 4\hat{k}$, $\vec{C} = 7\hat{i} + 10\hat{j} + 16\hat{k}$, « $\vec{A} \cdot \vec{B}$, « $\vec{A} \cdot \vec{C}$, « $\vec{B} \cdot \vec{C}$, « $\vec{A} \times \vec{B}$, « $\vec{A} \times \vec{C}$, « $\vec{B} \times \vec{C}$, « $\vec{A} \cdot (\vec{B} \times \vec{C})$, « $\vec{B} \cdot (\vec{A} \times \vec{C})$, « $\vec{C} \cdot (\vec{A} \times \vec{B})$.

(1) $\vec{A} = \underline{i} + \underline{j}$

$\vec{B} = -\underline{j} + \underline{k}$ [$\vec{A} \cdot \vec{B}$: 1.414, 0.707*i*, 0.707*k*]

(2) $\vec{A} = 2\underline{i} - 3\underline{k}$

$\vec{B} = \underline{i} + 6\underline{j} - 3\underline{k}$ [$\vec{A} \cdot \vec{B}$: 9, 0.333*i*, +0.667*j* - 0.667*k*]

(3) $\vec{A} = 7 \angle 30^\circ$

$\vec{B} = 7 \angle 150^\circ$ [$\vec{A} \cdot \vec{B}$: 7, *j*]

(4) $\vec{A} = 10 \angle 120^\circ$

$\vec{B} = 10 \angle 45^\circ$ [$\vec{A} \cdot \vec{B}$: 15.9, 0.130*i*, +0.99*j*]

(5) $\vec{A} = 3\underline{i} - 5\underline{j} - 2\underline{k}$

$\vec{C} = -5\underline{i} - 2\underline{j} + 3\underline{k}$, $\vec{B} = 4\underline{i} - 7\underline{j} + 4\underline{k}$ [$\vec{A} \cdot \vec{B}$: 15, $\frac{1}{15}(2\underline{i} - 14\underline{j} + 5\underline{k})$]

(6) $\vec{A} = 6\underline{i} + 8\underline{j}$

$\vec{B} = \underline{i} + 2\underline{j} + 3\underline{k}$

$\vec{C} = 3\underline{i} + 4\underline{j} - 5\underline{k}$ [$\vec{A} \cdot \vec{B}$: $10\sqrt{3}$, $\frac{1}{15\sqrt{3}}(15\underline{i} + 2\underline{j} - 3\underline{k})$]

(7) $\vec{A} = 6\underline{i} + 10\underline{j} + 16\underline{k}$

$\vec{B} = 2\underline{i} - 3\underline{j}$ [$\vec{A} \cdot \vec{B}$: $R = 25.7\underline{i} + 24.7\underline{j} + 16\underline{k}$]

$\vec{C} = 25 \angle 45^\circ$

(8) $\vec{A} = 2\underline{i} + 3\underline{j} + 5\underline{k}$

$\vec{B} = 3\underline{i} - 3\underline{j} - 2\underline{k}$ [$\vec{A} \cdot \vec{B}$: 5, 0.6*i* + 0.8*j*]

$\vec{C} = -2\underline{i} + 4\underline{j} - 3\underline{k}$

1-21 $\vec{A} = 98\hat{i} - 6\hat{j} + 18\hat{k}$, $\vec{B} = 76\hat{i} - 18\hat{j} + 1\hat{k}$, $\vec{C} = 90\hat{i} + 4\hat{j} - 8\hat{k}$, « $\vec{A} \cdot \vec{B}$, « $\vec{A} \cdot \vec{C}$, « $\vec{B} \cdot \vec{C}$, « $\vec{A} \times \vec{B}$, « $\vec{A} \times \vec{C}$, « $\vec{B} \times \vec{C}$, « $\vec{A} \cdot (\vec{B} \times \vec{C})$, « $\vec{B} \cdot (\vec{A} \times \vec{C})$, « $\vec{C} \cdot (\vec{A} \times \vec{B})$.

$\vec{A} \cdot \vec{B} = 98 \cdot 76 - 6 \cdot (-18) + 18 \cdot 1 = 7600 \pm 108 + 18 = 7726$

$\vec{A} \cdot \vec{C} = 98 \cdot 90 + 4 \cdot (-6) - 8 \cdot 18 = 8820 - 24 - 144 = 8652$

$\vec{B} \cdot \vec{C} = 76 \cdot 90 - 18 \cdot 4 + 1 \cdot (-8) = 6840 - 72 - 8 = 6760$

$\vec{C} \cdot (\vec{A} \times \vec{B}) = 90 \cdot (18 \cdot 1 - 18 \cdot (-6)) - (98 \cdot 18 + 76 \cdot 18) = 90 \cdot (18 + 108) - (1764 + 1368) = 90 \cdot 126 - 3132 = 11340 - 3132 = 8208$

[$\vec{A} \cdot \vec{B}$: $R_x = 58, R_y = 90, R_z = 0; l = \frac{58}{\sqrt{11464}}, m = \frac{90}{\sqrt{11464}}; n = 0$]

$R_z = 0; l = \frac{58}{\sqrt{11464}}, m = \frac{90}{\sqrt{11464}}; n = 0$

$\vec{A} \cdot \vec{C} = 98 \cdot 90 + 4 \cdot (-6) - 8 \cdot 18 = 8652$

$$\begin{aligned} \text{(ii)} \quad \underline{A} & \quad A = 150 & (2, -2, 1) \\ \underline{B} & \quad B = 175 & (2, +3, -6) \\ \underline{C} & \quad C = 135 & (-4, -8, -1) \end{aligned}$$

$$[\underline{A}\hat{c} \cdot \underline{1/4}: \underline{R} = 90\underline{i} - 145\underline{j} - 115\underline{k}, R_x = 90, R_y = -145 \\ R_z = -115; l = 0.4373, m = -0.7046; n = -0.5588]$$

$$\begin{aligned} \text{(iii)} \quad \underline{A} & \quad A = 130 & (-5, 12, 0) \\ \underline{B} & \quad B = 100 & (0, -4, 3) \\ \underline{C} & \quad C = 150 & (1, -2, -2) \\ \underline{D} & \quad D = 70 & (-3, 6, 2) \end{aligned}$$

$$[\underline{A}\hat{c} \cdot \underline{1/4}:] \quad \underline{R} = -30\underline{i} + 100\underline{k}, R_x = -30, R_y = 0, R_z = 100, \\ l = -0.2873, m = 0, n = 0.9578$$

$$\begin{aligned} \text{(iv)} \quad \underline{A} & \quad A = 1900 & (18, 1, -6) \\ \underline{B} & \quad B = 1700 & (-8, 0, 15) \\ \underline{C} & \quad C = 2500 & (0, 0, -1) \\ \underline{D} & \quad D = 1500 & (-14, -5, 2) \\ \underline{E} & \quad E = 1300 & (4, 12, -3) \end{aligned}$$

$$\underline{A}\hat{c} \cdot \underline{1/4}: \quad \underline{R} = 800\underline{j} - 1700\underline{k}, R_x = 0, R_y = 800, R_z = -1700, \\ l = 0, m = 0.4255, n = -0.9043$$

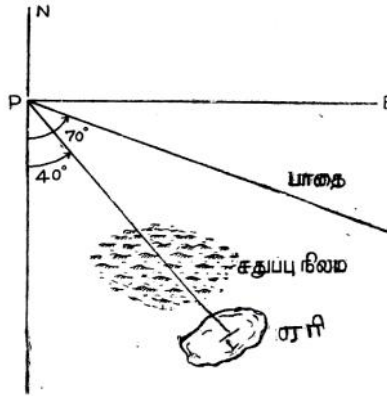
$\underline{1/4}\hat{c} \cdot \underline{A}\hat{c} \quad \pm \tilde{n} \hat{A}\hat{c} \hat{0}\hat{0}$

$\underline{1/4}\hat{c} \cdot \underline{A}\hat{c} \quad \pm \tilde{n} \hat{u}$

$$\begin{aligned} \text{(v)} \quad \underline{A} & \quad A = 380 & (18, 1, -6) \\ \underline{B} & \quad B = 340 & (-8, 0, 15) \\ \underline{C} & \quad C = 500 & (0, 0, -1) \\ \underline{D} & \quad D = 300 & (-14, -5, 2) \\ \underline{E} & \quad E = 260 & (4, 12, -3) \end{aligned}$$

$$\underline{A}\hat{c} \cdot \underline{1/4}: \quad \underline{R} = -340\underline{j} - 340\underline{k}, R_x = 0, R_y = 160, R_z = -340, \\ l = 0, m = 0.4255, n = -0.9043$$

1-22 $\hat{O} \hat{i} \hat{E} \hat{c} \hat{0} \hat{0} \hat{1/4} \hat{0} \hat{u} \hat{C} \hat{P} \hat{A} \hat{c} \hat{0} \hat{0} \hat{D}$, $\hat{A} \hat{E} \hat{c} \hat{1/4} \hat{1/4} \hat{O} \hat{E} \hat{A} \hat{j} \hat{1/4} \hat{0} \hat{D} \hat{0} \hat{1/4} \hat{A} \hat{0} \hat{1/4} \hat{u} \hat{i}$
 $\ll \hat{0} \hat{A} \hat{j} \hat{0}$, $s \hat{4} \hat{0} \hat{E} \pm \hat{y} \hat{E} \hat{1/4} \hat{c} \cdot \underline{A}\hat{c} \hat{0} \hat{2.5} \hat{1/4} \hat{A} \hat{E} \hat{S} \hat{c} \hat{A} \hat{j} \hat{E} \hat{1/4} \hat{1/4} \hat{A} \hat{A} \hat{c} \hat{0} \hat{1/4} \hat{0} \hat{z} \hat{1/4} \hat{u} \hat{C} \hat{D}$.



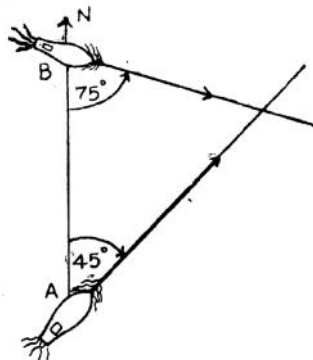
A/4o 1-69

→ Eijø Pø S70°E ±ýÈ ¾c° °Åcø ÁÉ¾÷ ¼ÁiÎ Á¾üì ¾ø ¾ Ö §¿ÁiÉ Ài ¾
 - ùÇÐ. (A/4o 1-69ø ¾iøÉÁÁiÚ). ÁýÁcÉoÁÁý ¾ÖÁý, Ái ¾Ácø
 ±oòùÇÁÁcÖóÐ ¾iç Á Ác ìì ¾Éo¾ ¾¾j ÁÁcø « Ì ÖÉÖó ±Éì ¾ñ
 « o òùÇáì o ¾içì o - ùÇ ¾¾j Á Ácø, « oòùÇÁcø ¾iç « Ácø¾Áì o
 S¾j ½ò ¾Öo ¾ñ

[Ác° ¼ : ¾j Áx = 1.25 ç.Áé,] S20°W

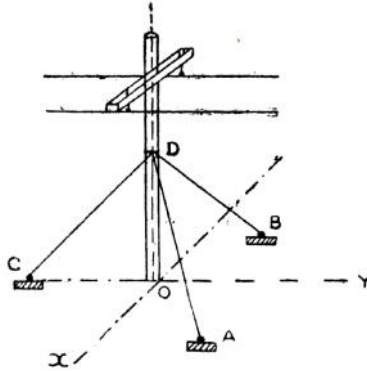
1-23 A ±ýÈ ¾oÁÁý ¾ ÁÁ÷, SÁ¾j÷ ¾c° ÁoÁ¾o¾ø (Radar screen) ¾Éì Ì
 S¿÷ Á¾ ¾c° °Åcø, 30 ç.Áé ¾¾j ÁÁcø B ±ýÈ ¾oÁø, S75°E ±ýÈ ¾c° °Åcø,
 30 ç.Áé SÁ ¾¾j « ÁÌ SÁ ¾¾j ò¾Á¾j ì ¾ñ ¾j÷. « o ÁiøÐ, A ±ýÈ
 ¾oÁø, N45°E ±ýÈ ¾c° °Åcø 20 ç.Áé SÁ ¾¾j « ÁÌ SÁ ¾¾j ò¾Á¾j ì òýÚ
 ì ¾ñ ÉÖó¾Ð. (A/4o 1-70 Á¾o¾ø ¾oÁø Çý ¾¾j ¾i ò¾Á¾j - ùÇ « Áoòì
 ¾i¾oÁoÁi ùÇÐ.) (a) B ±ýÈ ¾oÁø, Áý ¾c° °Åi ¾¾j ì oSÁiÐ, ÁÁcÖóÐ
 ±ùÁçx ¾¾j ÁÁcÖùç ±ýÁ ¾Öo, (b) A ±ýÈ ¾oÁø, B þý ¾c° °Åi
 ¾¾j ì oSÁiÐ, B ±ýÈ ¾oÁø ÁÁcÖóÐ ±ò¾¾j ÁÁcÖùçÐ ±ýÁ ¾Öo
 ¾ñ

[Ác° ¼: (a) 18.8 ç.Áé; (b) 25.3 ç.Áé]



A/4o 1-70

1-24 A/4o 1-71pø, A c° ¼ò ¾c° °Åcø, 10 ç.ç. Ác° °), B (¿c° Ái Ì o¾jý
 ¾c° °Åcø) - ÁÁüÉý ¾¾j Ì ÁÁý Ác° ° C (20 ç.ç. Ác° °) ±ýÈijø, B þý
 ±ñ Á¾o Ácø, C ±ò¾c° °Åcø ò¾Á¾j SÁñ Ì ÁýÁ ¾Öo, Á Á¾
 Áçì o, ¾½ì Áø Ó É - ÁÁüÉý ã ÁÁi ì ¾ñ



À¼õ 1-73

1-27. A rod is supported by a ball-and-socket joint at point D on a vertical shaft. The rod is also supported by a roller support at point B and a pin support at point C. A point A is located on the rod. A coordinate system with x, y, and z axes is shown, with the origin O at the center of the shaft.

$$\left(\begin{array}{l} \text{Angle} = 158.5^\circ, \\ l = 0.0284, m = 0.0172, n = 0.996 \end{array} \right)$$

1-28. A rod is supported by a ball-and-socket joint at point D on a vertical shaft. The rod is also supported by a roller support at point B and a pin support at point C. A point A is located on the rod. A coordinate system with x, y, and z axes is shown, with the origin O at the center of the shaft.

$$\left[\text{Angle} = 54.7^\circ; \frac{1}{\sqrt{3}}, \frac{1}{\sqrt{3}}, \frac{1}{\sqrt{3}} \right]$$

1-29. A rod is supported by a ball-and-socket joint at point D on a vertical shaft. The rod is also supported by a roller support at point B and a pin support at point C. A point A is located on the rod. A coordinate system with x, y, and z axes is shown, with the origin O at the center of the shaft.

$$\left(\text{Angle} = \frac{11}{\sqrt{3}} \right)$$

1-30. A rod is supported by a ball-and-socket joint at point D on a vertical shaft. The rod is also supported by a roller support at point B and a pin support at point C. A point A is located on the rod. A coordinate system with x, y, and z axes is shown, with the origin O at the center of the shaft.

$$A = 3i - 4k; B = 2i - 2j + k$$

(a) The angle between the rod and the x-axis is $82^\circ 20'$.

(b) The angle between the rod and the y-axis is $82^\circ 20'$.

$$\left[\text{Angle} = \frac{2}{3} (b) 82^\circ 20' \right]$$

The force F is supported by a ball-and-socket joint at point D on a vertical shaft. The force is also supported by a roller support at point B and a pin support at point C. A point A is located on the rod. A coordinate system with x, y, and z axes is shown, with the origin O at the center of the shaft.

$$\left[\text{Angle} = \frac{8}{3} \right]$$

1-31 \vec{A} உடன் \vec{B} இன் கோணம் θ , $|\vec{A} + \vec{B}|^2 = \vec{A} \cdot \vec{A} + \vec{B} \cdot \vec{B} + 2\vec{A} \cdot \vec{B} \cos \theta$. \vec{A}, \vec{B} ஆகிய இரு வெக்டர்களுக்கும் $\vec{A} + \vec{B}$ இன் திசைவேகம் \vec{C} ஆகும். $\vec{A} + \vec{B} = \vec{C}$ எனில் $\vec{C} \cdot \vec{C} = (\vec{A} + \vec{B}) \cdot (\vec{A} + \vec{B})$ என்க. $\vec{A} \cdot \vec{A} = 4$, $\vec{B} \cdot \vec{B} = 9$ எனில் $\vec{C} \cdot \vec{C}$ கண்டறியுங்கள்.

1-32 $\vec{A} + 2\vec{B} + 5\vec{C}, 3\vec{A} + 2\vec{B} + \vec{C}, 2\vec{A} + 2\vec{B} + \vec{C}$ ஆகிய மூன்று வெக்டர்கள் $\vec{A}, \vec{B}, \vec{C}$ ஆகிய மூன்று வெக்டர்களுக்கும் செங்குத்தாக உள்ளன. $\vec{A} \cdot \vec{A} = 4$, $\vec{B} \cdot \vec{B} = 9$, $\vec{C} \cdot \vec{C} = 1$ எனில் $\vec{A} \cdot \vec{B}$, $\vec{A} \cdot \vec{C}$, $\vec{B} \cdot \vec{C}$ கண்டறியுங்கள்.

1-33 $\vec{A} = 2\vec{i} - 3\vec{j} + 4\vec{k}, \vec{B} = 7\vec{i} - \vec{j} + 8\vec{k}, \vec{C} = 24\vec{i} + 2\vec{j} + 24\vec{k}$ ஆகிய மூன்று வெக்டர்கள் $\vec{A}, \vec{B}, \vec{C}$ ஆகிய மூன்று வெக்டர்களுக்கும் செங்குத்தாக உள்ளன. $\vec{A} \cdot \vec{A} = 4$, $\vec{B} \cdot \vec{B} = 9$, $\vec{C} \cdot \vec{C} = 1$ எனில் $\vec{A} \cdot \vec{B}$, $\vec{A} \cdot \vec{C}$, $\vec{B} \cdot \vec{C}$ கண்டறியுங்கள்.

1-34 $\vec{A}, \vec{B}, \vec{C}$ ஆகிய மூன்று வெக்டர்கள் $\vec{A} = 2\vec{i} - 3\vec{j} + \vec{k}, \vec{B} = 4\vec{j} - 2\vec{k} + 3\vec{k}, \vec{C} = 3\vec{i} - 4\vec{j}$ ஆகும். $\vec{A}, \vec{B}, \vec{C}$ ஆகிய மூன்று வெக்டர்களுக்கும் செங்குத்தாக உள்ளன. $\vec{A} \cdot \vec{A} = 4$, $\vec{B} \cdot \vec{B} = 9$, $\vec{C} \cdot \vec{C} = 1$ எனில் $\vec{A} \cdot \vec{B}$, $\vec{A} \cdot \vec{C}$, $\vec{B} \cdot \vec{C}$ கண்டறியுங்கள்.

$$\left(\cos^{-1} \left(\frac{5\sqrt{3}}{18} \right) \right)$$

1-35 $2\vec{i} - 2\vec{j} + \vec{k}, 4\vec{i} - 3\vec{k}$ என்ற இரு வெக்டர்கள் \vec{A}, \vec{B} ஆகும். $\vec{A} \cdot \vec{A} = 4$, $\vec{B} \cdot \vec{B} = 9$ எனில் $\vec{A} \cdot \vec{B}$ கண்டறியுங்கள்.

$$\left(\cos^{-1} : 70.5^\circ \right)$$

1-36 $(2, 0, 5), (3, -6, -6)$ ஆகிய இரு வெக்டர்கள் \vec{A}, \vec{B} ஆகும். $\vec{A} \cdot \vec{A} = 4$, $\vec{B} \cdot \vec{B} = 9$ எனில் $\vec{A} \cdot \vec{B}$ கண்டறியுங்கள்.

$$\left(\cos^{-1} : 119.7^\circ \right)$$

1-37 $\vec{A}, \vec{B}, \vec{C}$ ஆகிய மூன்று வெக்டர்கள் $\vec{A} = (3, -2, 6), \vec{B} = (5, -2, 7), \vec{C} = (1, -1, 6)$ ஆகும். $\vec{A}, \vec{B}, \vec{C}$ ஆகிய மூன்று வெக்டர்களுக்கும் செங்குத்தாக உள்ளன. $\vec{A} \cdot \vec{A} = 4$, $\vec{B} \cdot \vec{B} = 9$, $\vec{C} \cdot \vec{C} = 1$ எனில் $\vec{A} \cdot \vec{B}$, $\vec{A} \cdot \vec{C}$, $\vec{B} \cdot \vec{C}$ கண்டறியுங்கள்.

$$\left(\cos^{-1} : 143.2^\circ \right)$$

1-38 $\vec{a} = \left(\frac{2}{3}, \frac{1}{3}, -\frac{2}{3} \right), \vec{b} = \left(\frac{1}{3}, \frac{2}{3}, \frac{2}{3} \right)$ ஆகிய இரு வெக்டர்கள் \vec{a}, \vec{b} ஆகும். $\vec{a} \cdot \vec{a} = 1$, $\vec{b} \cdot \vec{b} = 1$ எனில் $\vec{a} \cdot \vec{b}$ கண்டறியுங்கள்.

$$\left(\cos^{-1} : 90^\circ \right)$$

1-39 $\vec{a} = \vec{i} + \vec{j} + \vec{k}, \vec{b} = \vec{i} + \vec{j} + \vec{k}$ ஆகிய இரு வெக்டர்கள் \vec{a}, \vec{b} ஆகும். $\vec{a} \cdot \vec{a} = 4$, $\vec{b} \cdot \vec{b} = 4$ எனில் $\vec{a} \cdot \vec{b}$ கண்டறியுங்கள்.

$$(1) -6i + 9j + k, 5i + 4j - 6k$$

$$(2) i + 2j + 3k, -16i + 5j + 2k$$

$$(3) 8i - 3j + 5k, -3i + 7j + 9k$$

1-40 $6i + yj - 2k, 9i - 4j + 15k \pm y \hat{E}$ $\frac{3}{4}$ \hat{C} \hat{u} $\hat{y} \hat{U} \hat{i} \hat{j} \hat{y} \hat{U}$ $\hat{i} \hat{o} \hat{i} \hat{o} \frac{3}{4} \hat{i}$
« $\hat{A} \hat{O} \hat{j} \hat{A} \hat{y} \hat{E} \hat{i} \hat{o}, y - \hat{y} \hat{A} \frac{3}{4} \hat{O} \hat{i} \hat{A} \hat{i} \hat{j} \hat{n}$
($\hat{A} \hat{C} \hat{i} \frac{1}{4}; Y = 6$)

1-41 $2x - y + 2z = 1, x - y = 2 \pm y \hat{E}$ $\frac{3}{4}$ \hat{C} \hat{i} $\hat{U} \hat{i} \hat{l}$ \hat{p} $\frac{1}{4} \hat{A} \hat{A} \hat{i} \hat{A} \hat{O} \hat{o}$ $\hat{S} \hat{j} \frac{1}{2} \hat{o} \hat{i} \hat{o} \frac{3}{4} \hat{i}$
 $\hat{j} \hat{n}$
($\hat{A} \hat{C} \hat{i} \frac{1}{4}; 45^\circ$)

1-42 $7x + 4y + 4z + 3 = 0, 2x + y - 2z + 2 = 0 \pm y \hat{E}$ $\frac{3}{4}$ \hat{C} \hat{i} $\hat{U} \hat{i} \hat{l}$ \hat{p} $\frac{1}{4} \hat{A} \hat{A} \hat{i} \hat{A} \hat{O} \hat{o}$
 $\hat{S} \hat{j} \frac{1}{2} \hat{o} \hat{i} \hat{o} \frac{3}{4} \hat{i}$ $\hat{j} \hat{n}$ $\hat{r} \hat{k}$.
($\hat{A} \hat{C} \hat{i} \frac{1}{4}; \cos^{-1}\left(\frac{5}{13}\right)$)

1-43 $7i + 2j + k, 2i - 4j + 3k \pm y \hat{E}$ $\frac{3}{4}$ \hat{C} \hat{i} $\hat{U} \hat{i} \hat{l}$ \hat{p} $\frac{1}{4} \hat{A} \hat{A} \hat{i} \hat{A} \hat{O} \hat{o}$
 $\hat{S} \hat{j} \frac{1}{2} \hat{o} \hat{i} \hat{o} \frac{3}{4} \hat{i}$ $\hat{j} \hat{n}$ $\hat{r} \hat{k}$.
($\hat{A} \hat{C} \hat{i} \frac{1}{4}; 9; 10i - 19j - 6k; 76^\circ, 51'$)

1-44 (i, j, k) $\hat{U} \hat{i} \hat{l}$ \hat{p} $\frac{1}{4} \hat{A} \hat{A} \hat{i} \hat{A} \hat{O} \hat{o}$ $\hat{S} \hat{j} \frac{1}{2} \hat{o} \hat{i} \hat{o} \frac{3}{4} \hat{i}$ $\hat{j} \hat{n}$ $\hat{r} \hat{k}$.
 $\hat{p} \hat{u} \hat{A} \hat{O} \hat{i} \hat{A} \hat{O} \hat{o}$ $\hat{S} \hat{j} \frac{1}{2} \hat{o} \hat{i} \hat{o} \frac{3}{4} \hat{i}$ $\hat{j} \hat{n}$ $\hat{r} \hat{k}$.
($\hat{A} \hat{C} \hat{i} \frac{1}{4}; \frac{1}{\sqrt{33}}(4i + 4j + 4k)$)

1-45 $\underline{A} = i - 3j + 2k, \underline{B} = 2i + 3j - k \pm y \hat{E}$ $\hat{A} \hat{B}$ \hat{y} \hat{A} $\hat{S} \hat{j} \frac{1}{2} \hat{o} \hat{i} \hat{o} \frac{3}{4} \hat{i}$
 $\hat{j} \hat{n}$ $\hat{r} \hat{k}$.
($\hat{A} \hat{C} \hat{i} \frac{1}{4}; -3i + 4k$)

1-46 $\hat{A} \hat{B} \hat{C} \hat{i} \hat{U} \hat{i} \hat{l}$ \hat{p} $\frac{1}{4} \hat{A} \hat{A} \hat{i} \hat{A} \hat{O} \hat{o}$ $\hat{S} \hat{j} \frac{1}{2} \hat{o} \hat{i} \hat{o} \frac{3}{4} \hat{i}$ $\hat{j} \hat{n}$ $\hat{r} \hat{k}$.
 $\hat{A} \hat{B} \hat{C} \hat{i} \hat{U} \hat{i} \hat{l}$ \hat{p} $\frac{1}{4} \hat{A} \hat{A} \hat{i} \hat{A} \hat{O} \hat{o}$ $\hat{S} \hat{j} \frac{1}{2} \hat{o} \hat{i} \hat{o} \frac{3}{4} \hat{i}$ $\hat{j} \hat{n}$ $\hat{r} \hat{k}$.
 $\hat{A} \hat{B} \hat{C} \hat{i} \hat{U} \hat{i} \hat{l}$ \hat{p} $\frac{1}{4} \hat{A} \hat{A} \hat{i} \hat{A} \hat{O} \hat{o}$ $\hat{S} \hat{j} \frac{1}{2} \hat{o} \hat{i} \hat{o} \frac{3}{4} \hat{i}$ $\hat{j} \hat{n}$ $\hat{r} \hat{k}$.

1-47 $\underline{i} - \underline{j} - 2\underline{k}, 2\underline{i} + \underline{j} - \underline{k} \pm y \hat{E}$ $\frac{3}{4}$ \hat{C} \hat{i} $\hat{U} \hat{i} \hat{l}$ \hat{p} $\frac{1}{4} \hat{A} \hat{A} \hat{i} \hat{A} \hat{O} \hat{o}$ $\hat{S} \hat{j} \frac{1}{2} \hat{o} \hat{i} \hat{o} \frac{3}{4} \hat{i}$
 $\hat{j} \hat{n}$ $\hat{r} \hat{k}$.
($\hat{A} \hat{C} \hat{i} \frac{1}{4}; 60^\circ; \frac{1}{\sqrt{3}}(\underline{i} - \underline{j} + 2\underline{k})$)

1-48 $(3\underline{i} + 2\underline{j} - \underline{k}), (-2\underline{i} + 3\underline{j} - 4\underline{k}) \pm y \hat{E}$ $\frac{3}{4}$ \hat{C} \hat{i} $\hat{U} \hat{i} \hat{l}$ \hat{p} $\frac{1}{4} \hat{A} \hat{A} \hat{i} \hat{A} \hat{O} \hat{o}$ $\hat{S} \hat{j} \frac{1}{2} \hat{o} \hat{i} \hat{o} \frac{3}{4} \hat{i}$ $\hat{j} \hat{n}$ $\hat{r} \hat{k}$.

1-48 $\vec{A} = i + 3j - k$, $\vec{B} = 2i + j + 4k$ எனில் $\vec{A} \cdot \vec{B}$ இன் மதிப்பு காண்க. \vec{A} மற்றும் \vec{B} இன் மீட்டர் கோணம் காண்க.

$$\left(\vec{A} \cdot \vec{B}; \cos^{-1} \left(\frac{1}{\sqrt{390}}(-5i + 14j + 13k); \sqrt{390}; 73^\circ 52' \right) \right)$$

1-49 $\vec{A} = i + 3j - k$, $\vec{B} = 2i + j + 4k$ எனில் $\vec{A} \times \vec{B}$ இன் மதிப்பு காண்க. \vec{A} மற்றும் \vec{B} இன் மீட்டர் கோணம் காண்க.

$$\left(\vec{A} \times \vec{B}; \cos^{-1} \left(\frac{\sqrt{2}}{10}(4i - 3j + 5k); \frac{5\sqrt{2}}{2} \right) \right)$$

1-50 $\vec{A} = 12i + 13j + 10k$, $\vec{B} = 5i - 9j + 7k$ எனில் (a) $\vec{A} \cdot \vec{B}$ (b) $\vec{A} \times \vec{B}$ இன் மதிப்பு காண்க.

(b) (a) இன் மதிப்பை \vec{A} மற்றும் \vec{B} இன் மீட்டர் கோணம் காண்க. (c) \vec{A} மற்றும் \vec{B} இன் மீட்டர் கோணம் காண்க. (d) \vec{A} மற்றும் \vec{B} இன் மீட்டர் கோணம் காண்க.

$$\left(\begin{array}{l} (a) 18i - 34j - 173k \\ \vec{A} \cdot \vec{B}; (b) \frac{1}{\sqrt{63846}}(18i - 34j - 173k) \\ (d) 0.9973 \end{array} \right)$$

1-51 $\vec{A} = i + 2j + 2k$, $\vec{B} = 3i - 2j + k$ எனில் $\vec{A} \cdot \vec{B}$ இன் மதிப்பு காண்க. \vec{A} மற்றும் \vec{B} இன் மீட்டர் கோணம் காண்க.

$$\left(\vec{A} \cdot \vec{B}; 5\sqrt{5} \right)$$

1-52 $\vec{A} = i + 2j + 2k$, $\vec{B} = 3i - 2j + k$ எனில் $\vec{A} \times \vec{B}$ இன் மதிப்பு காண்க. \vec{A} மற்றும் \vec{B} இன் மீட்டர் கோணம் காண்க.

- (1) $\vec{A} = 3i - 4j + 5k$, $\vec{B} = -6i + 8j - 10k$
- (2) $\vec{A} = -35i + 15j - 10k$, $\vec{B} = 7i - 3j + 2k$
- (3) $\vec{A} = i + j + k$, $\vec{B} = 7i + 7j + 7k$
- (4) $\vec{A} = -i - j - 5k$, $\vec{B} = -4i + 4j - 4k$
- (5) $\vec{A} = 4i + 3j - 5k$, $\vec{B} = 20i + 15j - 25k$
- (6) $\vec{A} = -i - 2j - 3k$, $\vec{B} = 3i - 6j + 9k$

1-53 $2i - 3j + 4k$, $i + bj + ck$ எனில் $\vec{A} \cdot \vec{B} = 0$ எனில் b மற்றும் c இன் மதிப்புகள் காண்க.

$$\left(\vec{a} = \frac{1}{4}; b = -\frac{3}{2}; c = 2 \right)$$

1-54 $\vec{a} = \frac{1}{4}\hat{i} + \frac{3}{4}\hat{j} + \hat{k}$, $\vec{b} = \frac{1}{2}\hat{i} + \hat{j} + \hat{k}$, $\vec{c} = \hat{i} + \hat{j} + \hat{k}$ எனில் $\vec{a}, \vec{b}, \vec{c}$ ஆகிய மூன்று வெக்டர்கள் மீட்டர் கோணம் என்ன?

$$(1) 2\hat{i} + 3\hat{j} + 4\hat{k}, -\hat{i} + 5\hat{j} + 2\hat{k} \left[\vec{a} = \frac{1}{4}; \sqrt{30} \right]$$

$$(2) \hat{i} - 2\hat{j} + 3\hat{k}, 3\hat{i} + \hat{j} - 2\hat{k} \left[\vec{a} = \frac{1}{4}; \sqrt{171} \right]$$

$$(3) \hat{i} + 2\hat{j} + 3\hat{k}, 3\hat{i} + 2\hat{j} + \hat{k} \left[\vec{a} = \frac{1}{4}; 4\sqrt{6} \right]$$

$$(4) 8\hat{i} + 3\hat{j} + 5\hat{k}, 2\hat{i} + \hat{j} + \hat{k} \left[\vec{a} = \frac{1}{4}; \sqrt{12} \right]$$

1-55 A(1, 2, 3), B(-1, 1, 2), C(2, 3, -1) ஆகிய மூன்று வெக்டர்கள் மீட்டர் கோணம் என்ன? $\vec{a} = \frac{1}{2}\hat{i} + \hat{j} + \hat{k}$ எனில் \vec{a} ஆகிய மூன்று வெக்டர்கள் மீட்டர் கோணம் என்ன?

$$\left(\vec{a} = \frac{1}{2}; \frac{1}{2}\sqrt{107} \right)$$

1-56 A(1, 2, 3)B(-2, -3, 4)C(4, 5, 6) ஆகிய மூன்று வெக்டர்கள் மீட்டர் கோணம் என்ன? $\vec{a} = \frac{1}{2}\hat{i} + \hat{j} + \hat{k}$ எனில் \vec{a} ஆகிய மூன்று வெக்டர்கள் மீட்டர் கோணம் என்ன?

$$\left(\vec{a} = \frac{1}{2}; 3\sqrt{6} \right)$$

1-57 A(0, 0, 0)B(1, 1, 1)C(2, 1, 3) ஆகிய மூன்று வெக்டர்கள் மீட்டர் கோணம் என்ன? $\vec{a} = \frac{1}{\sqrt{6}}(\hat{i} - \hat{j} - \hat{k})$ எனில் \vec{a} ஆகிய மூன்று வெக்டர்கள் மீட்டர் கோணம் என்ன?

$$\left(\vec{a} = \frac{1}{\sqrt{6}}(2\hat{i} - \hat{j} - \hat{k}); \frac{\sqrt{6}}{2} \right)$$

1-58 $4\hat{i} + 3\hat{j} - 5\hat{k}, -2\hat{i} + \hat{j} + 6\hat{k}, 2\hat{i} + 4\hat{j} + \hat{k}$ ஆகிய மூன்று வெக்டர்கள் மீட்டர் கோணம் என்ன? $\vec{a} = \frac{1}{\sqrt{6}}(\hat{i} - \hat{j} - \hat{k})$ எனில் \vec{a} ஆகிய மூன்று வெக்டர்கள் மீட்டர் கோணம் என்ன?

1-59 $\vec{a} = \frac{1}{2}\hat{i} + \hat{j} + \hat{k}$, $\vec{b} = \hat{i} + \hat{j} + \hat{k}$, $\vec{c} = \hat{i} + \hat{j} + \hat{k}$ எனில் $\vec{a}, \vec{b}, \vec{c}$ ஆகிய மூன்று வெக்டர்கள் மீட்டர் கோணம் என்ன?

$$(\vec{a} \cdot \vec{b})(\vec{a} \cdot \vec{c}) \equiv (\vec{a} \cdot \vec{a})(\vec{b} \cdot \vec{c}) - (\vec{a} \cdot \vec{c})(\vec{a} \cdot \vec{b})$$

1-60 $\vec{a} = \frac{1}{2}\hat{i} + \hat{j} + \hat{k}$, $\vec{b} = \hat{i} + \hat{j} + \hat{k}$, $\vec{c} = \hat{i} + \hat{j} + \hat{k}$ எனில் $\vec{a}, \vec{b}, \vec{c}$ ஆகிய மூன்று வெக்டர்கள் மீட்டர் கோணம் என்ன?

$$\vec{a} \cdot \vec{b} = \vec{c}, \vec{b} \cdot \vec{c} = \vec{a} \quad \pm \vec{y} \vec{E} \emptyset,$$

$$\vec{a} \cdot \vec{c} = 0, \vec{b} \cdot \vec{c} = 0, \vec{c} \cdot \vec{a} = 0, \vec{a} \cdot \vec{a} = \vec{c} \cdot \vec{c}, \pm \vec{E} \vec{I} \vec{O} \vec{I}.$$

$$\vec{b} \cdot \vec{b} = 1$$

1-61 $(\underline{A} - \underline{B}) \wedge (\underline{A} + \underline{B}) = 2(\underline{A} \wedge \underline{B}) \pm \vec{E}$ နှင့် \vec{A} ညီမျှသည်။

(\vec{A} ဖြစ်လျှင် $\underline{A}, \underline{B} \pm \vec{E}$ နှင့် \vec{A} နှစ်ခုစလုံး « နှစ် ဝက်စီယံ \vec{A} နှင့် \vec{B} မှာ $\vec{A} \wedge \vec{B}$ ဖြစ်သည်။)

1-62 $\underline{R} \pm \vec{y} \wedge \underline{D} = \vec{O}$ နှင့် \vec{A} (position vector) $\pm \vec{y} \in \vec{0}$,
 $(\underline{i} \wedge \underline{R}) \cdot (\underline{R} \wedge \underline{j}) = (\underline{i} \cdot \underline{R})(\underline{R} \cdot \underline{j}) \pm \vec{E} \cdot \vec{1}$

1-63 \vec{O} ဝက်စီယံ $\vec{A}, \vec{B}, \vec{C} \pm \vec{y} \in \vec{0}$ « \vec{O} ဝက်စီယံ $\vec{A}, \vec{B}, \vec{C}$ နှစ်ခုစလုံး $\vec{A}, \frac{1}{2}(\underline{A} \wedge \underline{B} + \underline{B} \wedge \underline{C} + \underline{C} \wedge \underline{A}) \pm \vec{y} \in \vec{0}$ နှင့် \vec{A} နှစ်ခုစလုံး $\pm \vec{y} \in \vec{0}$ $\vec{A} = \vec{A} \cdot \vec{A} \vec{u}_1, \vec{A} \cdot \vec{A} \vec{u}_1, \vec{A} \cdot \vec{A} \vec{u}_1$
 « $\vec{A} \cdot \vec{A} \vec{u}_1 = -2\vec{i} + 3\vec{j} + 5\vec{k}, \vec{i} + 2\vec{j} + 3\vec{k}, 7\vec{i} - \vec{k} \pm \vec{y} \in \vec{0}$ နှင့် \vec{A} နှစ်ခုစလုံး $\vec{A} = \vec{A} \cdot \vec{A} \vec{u}_1, \vec{A} \cdot \vec{A} \vec{u}_1 = \vec{0}, \vec{A} \cdot \vec{A} \vec{u}_1 = \vec{0}$ နှင့် \vec{A} နှစ်ခုစလုံး $\vec{A} = \vec{A} \cdot \vec{A} \vec{u}_1, \vec{A} \cdot \vec{A} \vec{u}_1 = \vec{0}$

1-64 $\vec{A} \wedge \vec{B} \wedge \vec{C} = \vec{0}$ နှင့် $\vec{A} \cdot \vec{B} \cdot \vec{C} = 0$ ဖြစ်သည်။ $\vec{A} \cdot \vec{B} \cdot \vec{C} = 0$ ဖြစ်သည်။ $\vec{A} \cdot \vec{B} \cdot \vec{C} = 0$ ဖြစ်သည်။

(i) $\underline{A} = 3\underline{i} - 3\underline{j} + 5\underline{k}, \underline{B} = 6\underline{i} + 4\underline{j} - 2\underline{k},$
 $\underline{C} = 3\underline{i} - 2\underline{j} - 2\underline{k}$

$\vec{A} \cdot \vec{B} \cdot \vec{C} : -72, -6(6\underline{i} + 4\underline{j} - 5\underline{k})$

(ii) $\underline{A} = \underline{i} + \underline{j} + \underline{k}, \underline{B} = \underline{i} + 2\underline{j} + 3\underline{k},$
 $\underline{C} = 3\underline{i} + \underline{j} - 5\underline{k}$

$\vec{A} \cdot \vec{B} \cdot \vec{C} : -4, 37\underline{i} + 26\underline{j} + 15\underline{k}$

(iii) $\underline{A} = \underline{i} - \underline{k}, \underline{B} = 3\underline{i} + 4\underline{j} + 5\underline{k},$
 $\underline{C} = -6\underline{j} - 7\underline{k}$

$\vec{A} \cdot \vec{B} \cdot \vec{C} : 20, 21\underline{i} + 16\underline{j} + 21\underline{k}$

(iv) $\underline{A} = 3\underline{i} + 2\underline{j} + 4\underline{k}, \underline{B} = 2\underline{i} - \underline{j} + \underline{k},$
 $\underline{C} = 6\underline{i} + 7\underline{j} - \underline{k}$

$\vec{A} \cdot \vec{B} \cdot \vec{C} : 78, 8\underline{i} - 84\underline{j} + 36\underline{k}$

(v) $\underline{A} = \underline{i} - 2\underline{j} + \underline{k}, \underline{B} = \underline{i} + 2\underline{j} - 3\underline{k},$
 $\underline{C} = 6\underline{i} + 4\underline{j} - 3\underline{k}$

$\vec{A} \cdot \vec{B} \cdot \vec{C} : 28, 31\underline{i} + 14\underline{j} - 3\underline{k}$

1-65 $\vec{A} \wedge \vec{B} \wedge \vec{C} = \vec{0}$ နှင့် $\vec{A} \cdot \vec{B} \cdot \vec{C} = 0$ ဖြစ်သည်။ $\vec{A} \cdot \vec{B} \cdot \vec{C} = 0$ ဖြစ်သည်။

- (1) $2i - 3j + 5k, 3i + 4j - k, 16i - 7j + 23k$
- (2) $i + 3j - 2k, 7i - 2j + 3k, 25i + 6j + k$
- (3) $3i - 7j - 2k, -4i + 5j + 3k, 9i - 34j - 5k$
- (4) $6i - j + 5k, 5i + 7j - 3k, 7i + 38j - 30k$
- (5) $4i - 2j + 59k, -3i + 4j + 7k, 5i - 6j + 2k$
- (6) $18i + 8j + 6k, 4i + 3j + 2k, i - 2j - k$
- (7) $-2i + 3j + k, 3i - 4j - 2k, -i + 2k$

1-66 $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{u} \vec{v} \vec{w}$ $\frac{1}{2} \vec{a} \cdot \vec{b} \cdot \vec{c} \cdot \vec{d}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\pm \vec{E} \vec{I} \vec{J} \vec{K}$
 (i) $A(-13, 17, -1) B(-6, 3, 2) C(3, -2, 4) D(5, 7, 3)$
 (ii) $A(-1, 1, -1) B(1, 1, -1) C(3, -1, -1) D(3, -2, -1)$

1-67 $A(3, 0, 1) B(1, -5, 1) C(6, 0, 2) D(4, -3, 2) \pm \vec{y} \vec{E}$ $\vec{u} \vec{v} \vec{w}$ $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$
 $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$

1-68 $A(-5, 0, 1) \pm \vec{y} \vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{u} \vec{v} \vec{w}$ $\vec{A} \vec{B} \vec{C} \vec{D}$ (Parallelepiped) $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$
 $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$
 $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$

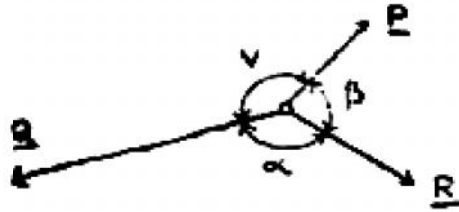
1-69 $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{u} \vec{v} \vec{w}$ $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$
 $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$

1-70 $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{u} \vec{v} \vec{w}$ $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$
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$\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{u} \vec{v} \vec{w}$ $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$
 $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$

1.71 $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{u} \vec{v} \vec{w}$ $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$
 $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$

1.72. $\vec{P} \vec{Q} \vec{R}$ $\vec{u} \vec{v} \vec{w}$ $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$
 $\vec{A} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$ $\vec{A} \vec{O} \vec{B} \vec{C} \vec{D}$

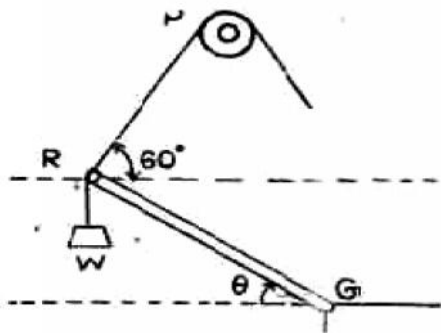


À¼õ 1.74

3.28ø §, ðÊÂÐŞÀ¡ø ´Õ Ð, Çø | °ÄüÄÍ §, ýËË. Ð, ü °Ä, Ç´ ÄÄÄÖÌ Ì | ÁËø, $\frac{P}{\sin r} = \frac{Q}{\sin s} = \frac{R}{\sin x}$ ±ýÚ çãÄñ §. þüÄ´ ÄÄ´ È ç´ ÈŞÄüÈðÀð¼¡ø, Ð, ü °Ä, Ç´ ÄÄÄÖÌ §, ¼¡ §, ¼¡ ±ýÚ - Ä¡ø, §.

1.73 27Äð¼÷ çÇÓúÇ ÄÜ ´ýÚ 21Äð¼÷ þ´¼| ÄÇð | ¼¡´ ÄÄø | Ä¡Öð¼ÄðÍ úÇ | §, Ì çÇø ð¼ðÄðÍ, ÄüËý ´Õ ÑÉÄÄÖóÐ 9Äð¼÷ | ¼¡´ ÄÄø 200 §, ç ±´¼ÖúÇ ÄÜ ´ýÚ | ¼¡Í Ä¼ðÄðÍ ÄÜ, | §, Ì çÇø - Ä äýÜø 9Äð¼÷, 18Äð¼÷, 21Äð¼÷ ÄÌ Í´ ÇÖ´¼Ä´ Ö ÓÌ §, ½ð´¼ «´ ÄÌ ýËË. ÄÜ ×Ì ðÖÈÖÓúÇ ÄüËý ÄÌ ¼ç Çø | °ÄüÄÍ ðøÄ´ °, ÇÌ §, ñ §. [Ä´¼: 182.1 §, ç, Ä´°; 123.5 §, ç, Ä´°]

1.74 250 §, ç ±´¼ÖúÇ Ä¡Äø ´ýÚ WRPýÈ ÄÖÄ¡É §, ðÄ (Cable) ´ýÈø À¼õ 3-29ø §, ðÊÄÄ¡Ü P ±ýÈ §, ðÄÄý ÄÆÄ¡, ð | ¼¡Í, Ä¼ðÄðÍ úÇÐ. §, ðÄ´ Ä GR ÓðÍ ´ýË¡ø (strut) ´Õ ÄÌ §, ¼üÇðÄðÍ, GR ø 150 §, ç, ç. | çÖÌ ø (compression) 2üÄÍ §, ÈÐ. « ð¼ý 60° §, ½ð´¼ «´ Äð¼Ä¡Üø - úÇÐ. (À¼õ 1.75)

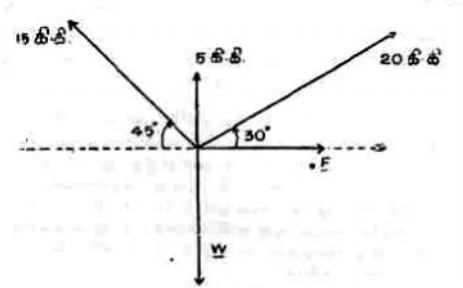


À¼õ 1.75

- (i) GR ±ýÈ ÓðÍ §, ç ¼¡ §, ðÍ¼ý «´ ÄÌ Ì ø §, ½ðø ð ±ýË¡ø «¼ý þÖ Ä¼Öø´ Ç §, ñ
- (ii) RPÄø | °ÄüÄÍ ðøÄ´ °Äý ±ñ Ä¼Ö´ ÄÖø §, ñ §.

[\vec{A} : $\frac{1}{4}(1) - 3.55^\circ, 63.55^\circ(2) 299.40, 133.68$ t. t.]

1.75 \vec{O} \vec{D} \vec{u} , \vec{A} \vec{o} 1.76 \vec{D} \vec{E} \vec{A} \vec{U} \vec{A} \vec{C} \vec{i} \vec{o} \vec{A} \vec{C} \vec{A} \vec{A} \vec{o}
 \vec{A} \vec{i} \vec{o} \vec{A} \vec{D} \vec{u} \vec{C} \vec{D} $\ll \frac{3}{4} \vec{y} \pm \frac{1}{4} \vec{A}$ \vec{O} \vec{o} , \vec{E} $\vec{y} \pm \vec{n}$ \vec{A} \vec{C} \vec{i} \vec{o} \vec{A} \vec{O} \vec{o} \vec{j} \vec{n} .



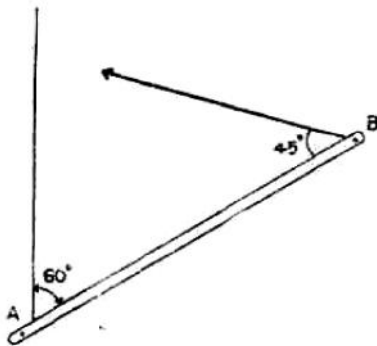
\vec{A} \vec{o} 1.65

[\vec{A} : $\frac{1}{4}: 25.605$ t. t. ; 3.89 t. t.]

1.76 10 t. t. $\pm \frac{1}{4} \vec{O}$ \vec{u} \vec{C} \vec{A} \vec{O} \vec{n} $\frac{1}{4}$, \vec{C} $\frac{1}{4} \vec{O}$ \vec{C} \vec{i} \vec{o} $\frac{1}{4} \vec{y}$ $30^\circ 60^\circ$ \vec{S} \vec{j} $\frac{1}{2} \vec{i}$ \vec{C}
 $\ll \vec{A}$ \vec{i} \vec{o} \vec{p} \vec{O} \vec{A} \vec{E} \vec{A} \vec{E} \vec{o} \vec{A} \vec{i} \vec{E} (Smooth) \vec{o} \vec{i} \vec{o} $\times \frac{3}{4} \vec{C}$ \vec{i} \vec{U} \vec{i} \vec{l} \vec{p} $\frac{1}{4} \vec{A}$ \vec{o} $\ll \vec{A}$ $\frac{3}{4} \vec{C}$
 \vec{C} \vec{A} \vec{A} \vec{o} \vec{A} \vec{i} \vec{o} \vec{A} \vec{D} \vec{u} \vec{C} \vec{D} . \vec{O} \vec{n} $\frac{1}{4}$ \vec{o} \vec{i} \vec{o} $\times \frac{3}{4} \vec{C}$ \vec{i} \vec{C} \vec{o} $\frac{3}{4} \vec{i}$ \vec{A} \vec{C} $\frac{1}{4} \vec{o}$ $\frac{3}{4} \vec{o}$.
 $\frac{3}{4} \vec{C}$ \vec{i} \vec{C} \vec{y} $\pm \frac{3}{4} \vec{C}$ \vec{i} \vec{A} \vec{o} \vec{A} \vec{C} \vec{i} \vec{o} , \vec{C} \vec{i} \vec{j} \vec{n} .

[\vec{A} : $\frac{1}{4}: 5$ t. t. , $5\sqrt{3}$ t. t.]

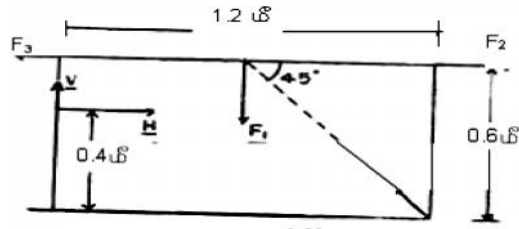
1.77 500 t. t. $\pm \frac{1}{4} \vec{O}$ \vec{u} \vec{C} \vec{S} \vec{A} \vec{A} \vec{i} \vec{E} \vec{A} \vec{B} $\pm \vec{y}$ \vec{E} \vec{o} $\frac{3}{4} \vec{A}$ \vec{o} (Beam) \vec{y} \vec{U} $\frac{3}{4}$ $\frac{1}{4} \vec{A}$ \vec{u} \vec{U}
 \vec{A} \vec{A} \vec{o} \vec{i} \vec{E} \vec{O} \vec{A} \vec{i} \vec{U} \vec{o} , \vec{B} \vec{o} \vec{O} \vec{A} \vec{u} \vec{E} \vec{i} \vec{o} \vec{A} \vec{o} 1.77 \vec{o} \vec{j} \vec{D} \vec{E} \vec{O} \vec{u} \vec{C} \vec{A} \vec{E} $\frac{3}{4} \vec{i}$ \vec{o} \vec{A} \vec{i} \vec{C} \vec{E} \vec{D} .
 $\frac{3}{4} \vec{O}$ \vec{o} $\frac{3}{4} \vec{E}$ \vec{y} \vec{O} \vec{E} \vec{A} \vec{o} \vec{A} \vec{A} \vec{y} \vec{A} \vec{i} \vec{o} $\frac{3}{4} \vec{i}$ \vec{A} \vec{o} \vec{A} \vec{A} \vec{o} \vec{i} \vec{o} \vec{A} \vec{u} \vec{A} \vec{i} \vec{o} \vec{A} \vec{C} \vec{i} \vec{o} , \vec{B} \vec{A} \vec{o} \vec{i} \vec{o} \vec{A} \vec{u} \vec{A} \vec{i} \vec{o}
 \vec{p} \vec{O} \vec{A} \vec{C} \vec{i} \vec{o} \vec{A} \vec{A} \vec{u} \vec{i} \vec{o} \vec{E} \vec{i} \vec{j} \vec{n} .



\vec{A} \vec{o} 1.77

[\vec{A} : $\frac{1}{4}: 514.2$ t. t. , $37^\circ 7'$; 306.3 t. t.]

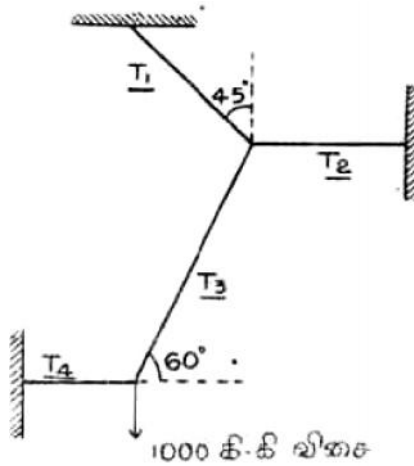
1.78 \vec{p} \vec{U} \vec{i} \vec{O} \vec{u} \vec{C} \vec{j} \vec{o} \vec{u} \vec{A} \vec{o} $\frac{3}{4} \vec{C}$ \vec{o} \vec{y} \vec{U} \vec{o} \vec{A} \vec{o} 1.78 \vec{o} \vec{j} \vec{D} \vec{E} \vec{O} \vec{u} \vec{C} \vec{A} \vec{E}
 $6 \vec{A}$ \vec{C} \vec{i} \vec{o} \vec{C} \vec{i} \vec{o} \vec{A} \vec{C} \vec{i} \vec{o} \vec{A} \vec{A} \vec{o} \vec{A} \vec{i} \vec{o} \vec{A} \vec{D} \vec{u} \vec{C} \vec{D} .



À¼õ 1.78

$|V|/|H|$ ý Á¼õ Æî ÿñ ÆýÀüÈÃ ÅÆç Çì Í Õì Áì ÅÇì Ì .
 [Åç¼: $\frac{1}{3}$]

1.79 1000 çç (Åç °) ±¼õÇ Æì Õç Ç Å¼õ 1.79ø ðÈÄÆ, òÆç ù ¼ì Ì ÿËý. òÆçÇø ÆüÄí ò þØÅç ° Çì ÿñ .



À¼õ 1.79

[Åç¼: $T_1 = 1414 \text{ çç}$

$T_1 = 1578 \text{ çç}$

$T_1 = 1154.67 \text{ çç}$

$T_1 = 577.33 \text{ çç}$]

1.80 Æõ ðüÇÆø ÆüÄí ò Åç ° Çý Æì Ì ÿç ùÄÕÄì Õ:

$F_1 = 8.4i - 6.0k \text{ çç}$

$F_2 = 10.0j - 5k \text{ çç}$

$F_3 = -5.4i + 7.0j + 14.6k \text{ çç}$

þ Å Õì Ì ÆüÄí Æì Ì Æý Åç ° Æî ÿñ .

[Åç¼: $3.0i + 17.0j + 3.6k$]

1.81 $\vec{O} \vec{D}, \vec{u}$ $P=2.2\vec{j}+5.5\vec{k}, Q=-8.4\vec{j}-1.9\vec{i}, R \pm \vec{y} \vec{E}$ $\vec{A} \vec{C} \vec{o}, \vec{C} \vec{j} \vec{o}$ $|\vec{O} \vec{A} \vec{u} \vec{A} \vec{d} \vec{I} \vec{o}|$,
« $\vec{A}, \vec{u} \vec{i} \vec{l}$ $\vec{o} \vec{j} \vec{C} \vec{C}, \vec{A} \vec{j} \vec{E}$ $6.5\vec{i}-4.1\vec{j}+8.3\vec{k} \pm \vec{y} \vec{E}$ $|\vec{3/4} \vec{i}| \vec{A} \vec{A} \vec{y}$ $\vec{A} \vec{C} \vec{o}$ $\vec{A} \vec{O} \vec{o}$
 $|\vec{A} \vec{u} \vec{E} \vec{O} \vec{i} \vec{l}|$ $|\vec{A} \vec{y} \vec{E} \vec{j} \vec{o}|$ $R \pm \vec{y} \vec{E}$ $\vec{A} \vec{C} \vec{o}$ $\vec{A} \vec{A} \vec{A} \vec{A} \vec{u} \vec{i}$ \vec{u} .
 $[\vec{A} \vec{C} \vec{o} \vec{1/4}: 8.4\vec{i}+2.1\vec{j}-2.8\vec{k}]$

1.82 $\vec{o} \pm \vec{y} \vec{E}$ $\vec{O} \vec{u} \vec{C} \vec{A} \vec{o}$ « $\vec{A} \vec{O} \vec{C} \vec{O} \vec{i} \vec{l} \vec{o}$ $\vec{O} \vec{D}, \vec{C} \vec{o}$ $\vec{A} \vec{C} \vec{o} \vec{i}$ $\vec{1/2} \vec{o}$ $\vec{y} \vec{U}$
 $|\vec{O} \vec{A} \vec{u} \vec{A} \vec{d} \vec{I} \vec{o}|$ « $\vec{3/4} \vec{u} \vec{l}$ $\vec{O} \vec{A} \vec{A} \vec{j}$ $|\vec{3/4} \vec{i}| \vec{A} \vec{A} \vec{y}$ $\vec{A} \vec{C} \vec{o}$ $|\vec{O} \vec{A} \vec{u} \vec{A} \vec{I} \vec{o}|$ $\vec{S}, \vec{j} \vec{i}$ (5,2,-14)
 $\pm \vec{y} \vec{E}$ $\vec{3/4} \vec{o}$ $\vec{A} \vec{C} \vec{o}$ $\vec{C} \vec{O} \vec{o}$ $|\vec{A} \vec{u} \vec{U} \vec{u} \vec{C} \vec{D}|$ $\vec{1/2} \vec{o}$ $\vec{3/4} \vec{o}$ $\vec{u} \vec{C} \vec{A} \vec{o}$ \vec{u}
 $\vec{A} = \vec{A} \left(\frac{2}{3} \vec{i} - \frac{2}{3} \vec{j} + \frac{1}{3} \vec{k} \right)$, $\vec{A} = (0.6\vec{j} - 0.8\vec{k})$ $\vec{C} = -110\vec{k}$ $\vec{C} \vec{a} \vec{d} \vec{1/4} \vec{i}$ $\vec{u} \pm \vec{y} \vec{E} \vec{j} \vec{o}$ $|\vec{3/4} \vec{i}| \vec{A} \vec{A} \vec{y}$
 $\vec{A} \vec{C} \vec{o} \vec{i} \vec{l}$ $|\vec{A} \pm \vec{n}$ $\vec{A} \vec{3/4} \vec{O} \vec{O}$, A, B \vec{u} $\vec{A} \vec{A} \vec{u} \vec{E} \vec{y}$ $\vec{A} \vec{3/4} \vec{O} \vec{O}$, $\vec{C} \vec{i}$ $\vec{j} \vec{i} \vec{n}$ \vec{u} .
 $\vec{A} \vec{C} \vec{o} \vec{1/4}: |\vec{3/4} \vec{i}| \vec{A} \vec{A} \vec{y}$ $\vec{A} \vec{C} \vec{o} \vec{A} \vec{y} \pm \vec{n}$ $\vec{A} \vec{3/4} \vec{O} \vec{O} = \frac{1980}{7} \vec{C} \vec{a} \vec{d} \vec{1/4} \vec{y} \vec{u}$;

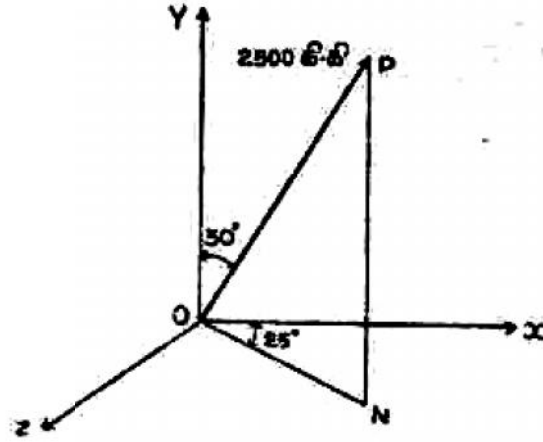
$$A = \frac{990}{7} \vec{C} \vec{a} \vec{d} \vec{1/4} \vec{y} \vec{u}; B = 220 \vec{C} \vec{a} \vec{d} \vec{1/4} \vec{y} \vec{u}$$

1.83 $\vec{O} \vec{D}, \vec{C} \vec{o}$ $\vec{u} \vec{i}$ $\vec{j} \vec{i}$ \vec{o} $\vec{A} \vec{C} \vec{o}$ $\vec{C} \vec{y}$ $\vec{1/2} \vec{o}$ $|\vec{O} \vec{A} \vec{u} \vec{A} \vec{I} \vec{o}| \vec{E} \vec{D}$. « $\vec{3/4} \vec{u} \vec{l}$ \vec{i} $\vec{O} \vec{A} \vec{A} \vec{j} \vec{E}$
 $|\vec{3/4} \vec{i}| \vec{A} \vec{A} \vec{y}$ $\vec{A} \vec{C} \vec{o}$ $\vec{A} \vec{i}$ $\vec{j} \vec{i} \vec{n}$ \vec{u} .
 $\vec{A} = -3.0\vec{i} + 4.2\vec{j}$
 $\vec{B} = -2.5\vec{i} + 5.0\vec{k}$
 $\vec{C} = 7.3\vec{i} - 2.7\vec{j} + 4.0\vec{k}$

$[\vec{A} \vec{C} \vec{o} \vec{1/4}: 1.8\vec{i} + 1.5\vec{j} + 9\vec{k}]$

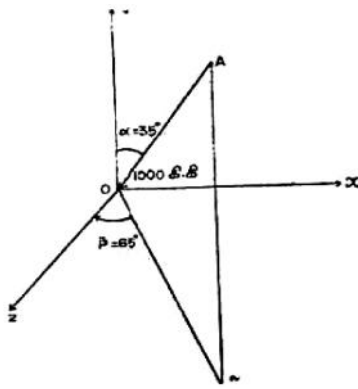
1.84 $75 \vec{C}, \vec{C}$ $\pm \vec{1/4} \vec{O} \vec{u} \vec{C}$ $\vec{A} \vec{A} \vec{i}$ \vec{o} $\vec{1/4}$ $\vec{y} \vec{U}$ $\vec{a} \vec{y} \vec{U}$ $\vec{o} \vec{A} \vec{C} \vec{C} \vec{O} \vec{o} \vec{D}$ $|\vec{3/4} \vec{i}|$
 $\vec{A} \vec{C} \vec{O} \vec{A} \vec{d} \vec{I} \vec{u} \vec{C} \vec{D}$ $\vec{o} \vec{A} \vec{C} \vec{u}$ « $\vec{A} \vec{O} \vec{o}$ $\vec{S}, \vec{j} \vec{i}$ $\vec{C} \vec{y}$ $\vec{3/4} \vec{o}$ $\vec{A} \vec{C} \vec{o}$ $\vec{C} \vec{a} \vec{d} \vec{1/4} \vec{u}$ (direction
ratios) $\vec{O} \vec{i} \vec{E} \vec{S} \vec{A}$ $(-2, 6, 3), (-5, -14, 2), (4, 0, 3) \pm \vec{y} \vec{E} \vec{j} \vec{o}$ $\vec{o} \vec{A} \vec{C} \vec{C} \vec{o}$ $|\vec{O} \vec{A} \vec{u} \vec{A} \vec{I} \vec{o}|$ $\vec{p} \vec{O}$
 $\vec{A} \vec{C} \vec{o}$ $\vec{C} \vec{y}$ $\pm \vec{n}$ $\vec{A} \vec{3/4} \vec{O} \vec{O} \vec{i}$ $\vec{C} \vec{i}$ $\vec{j} \vec{i} \vec{n}$ \vec{u} . $[\vec{A} \vec{C} \vec{o} \vec{1/4}: 78.4 \vec{C}, \vec{C}, 72.0 \vec{C}, \vec{C}, 58.357 \vec{C}, \vec{C}]$

1.85 $\vec{A} \vec{1/4} \vec{o}$ 1.69 \vec{o} 2500 \vec{C}, \vec{C} $\vec{A} \vec{C} \vec{o}$ $\vec{O} \vec{P} \pm \vec{y} \vec{E}$ $\vec{S} \vec{C} \vec{d}$ $\vec{S}, \vec{j} \vec{o} \vec{E} \vec{o}$ $|\vec{O} \vec{A} \vec{u} \vec{A} \vec{I} \vec{o}| \vec{E} \vec{D}$.
(a) $\vec{A} \vec{C} \vec{o}$ $\vec{A} \vec{y}$ x, y, z $\vec{g} \vec{A} \vec{C} \vec{x}$ $\vec{C} \vec{i}$ $\vec{j} \vec{i} \vec{n}$ \vec{u} .
(b) $\vec{A} \vec{C} \vec{o}$ $\vec{A} \vec{y}$ $|\vec{O} \vec{A} \vec{u} \vec{A} \vec{I} \vec{o}|$ $\vec{S}, \vec{j} \vec{i}$ x, y, z « $\vec{I} \vec{I} \vec{i}$ $\vec{u} \vec{1/4} \vec{y}$ « $\vec{A} \vec{i} \vec{l} \vec{o}$
 $\vec{S}, \vec{j} \vec{i}$ $\vec{1/2} \vec{i}$ $\vec{C} \vec{O} \vec{o}$ $\vec{j} \vec{i} \vec{n}$.
 $\vec{A} \vec{C} \vec{o} \vec{1/4}: (a) 1133, 2165, 528 \vec{C}, \vec{C}, \vec{A} \vec{C} \vec{o}$ \vec{O} ;
(b) $63.1^\circ, 30^\circ, 77.8^\circ]$



À¼õ 1.69

1.86 À¼õ 1.70 ø Ÿ; ðĖĀĀĖ 1000 Ÿ; Ć. Ć. ĀĆ' ° Oø Ÿ; ĩ Ÿ; ðĀĎĪ ò, A0³ Š ĩ°ĀüĀĪ ò Š; ĩ¼; x ò ĩ; ĩñ ¼ ĄĖĀø ĩ°ĀüĀĪ Ÿ; ĘĐ r=35°, s=65° ±ýĖ; ø,



À¼õ 1.70

(a) ĀĆ' °Āý x,y,z Ā; Ć; x Ÿ; ĆŠ ĩñ

(b) « Đ ĩ°ĀüĀĪ ò Š; ĩ¼ x,y,z Ÿ; Ć' ° Ÿ; ĩñ « ĩ ĩ ò Š; ĩ¼ ĩ Ÿ; ĆŃ ò ĩñ

ĀĆ' ¼: (a) -2600, -4100, -1212 Ÿ; Ć. Ć. ĀĆ' °

(b) 121°20', 145°, 104°;

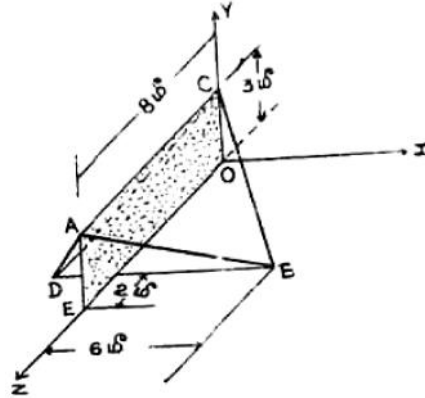
1.87 400 Ÿ; Ć. Ć. ĀĆ' ° Ÿ; Ÿ; ĐĀĪ Ÿ; ððüĈĀý ĀĖŠĀ y,z « ĩ ĩ Ÿ; ĩñ Ó' ĖŠĀ 80°, 40° Š; ĩ¼ ĩ Ÿ; Ć « ĩ ĩ ò Š; ĩ ðĖø ĩ°ĀüĀĪ Ÿ; ĘĐ. ĀĆ' °Āý x Ā; Ć; x ĀĆ' ±ñ ĩ¼; ðŃĪ ĩ ĀýĖ; ø ĀĆ' °Āý x,y,z Ā; Ć; x Ÿ; ĆŃ ò « Đ ĩ°ĀüĀĪ ò Š; ĩ¼ x « ĩ°ø Ÿ; ĩ ò Š; ĩ¼ ð' ĄŃŃ ĩñ Ÿ; .

[ĀĆ' ¼: 92,694,2778.8 Ÿ; Ć. Ć. ĀĆ' °, 45°44']

1.88 Ÿ; ĀĆ' ° ĐĀĪ Ÿ; ððüĈĀý ĀĖĀ; x ò x,y « ĩ ĩ Ĉý Ó' ĖŠĀ 125°, 65° Š; ĩ¼ ĩ Ÿ; Ć ð ĩ ĩ ò Š; ĩ ðĖŃŃ ĩ°ĀüĀĪ Ÿ; ĘĐ. ĀĆ' °Āý Ā; Ć; x 320 Ÿ; Ć. Ć. ±ýĖ; ø ĀĆ' °Āý ±ñ Ā¼ŃŃ ĀŃŃ, ĩ°ĀüĀĪ ò Š; ĩ¼ x « ĩ ĩ ĩñ « ĩ ĩ ò Š; ĩ¼ ð' ĄŃŃ ĩñ Ÿ; .

[Áċ' ¼: 456 ċ. ċ., 45°26' 45'44']

1.89 pŌōðì ōÀċ ū, °ċĠ Āñ Ī ì ū Ā' Ā - ū ĆĀüÈjø Āj÷òð Ĩ°ōĀòĀð¼ ĨĀ÷òĀĪ ¾ċ 1.71 ū j ðĒĀĒĒ

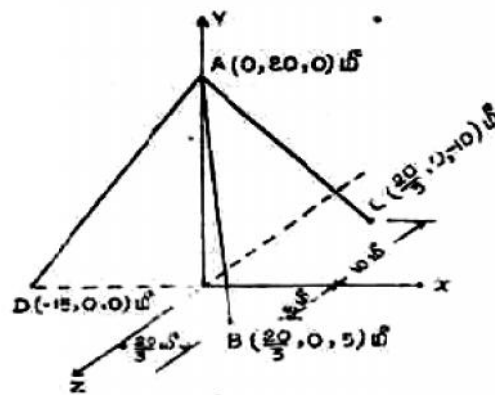


Ā¼ō 1-81

ĀŌĀjĒ ōĀċ Ćjø ċŪĀòĀðĪ ūĆĐ. 350 ċ. ċ. Āċ' °ŌüĆ pø Āċ' ° A,B ±ýĒ ōĀĆĈ Ĩ°ĀüĀĪ ĨĀýĒø ĨĀ÷ò ĀĪ ¾ĆĈ A ±ý ŪĀċ¼ò¾ĆĈ ĀĀýĀĪ ð¾òĀĪ ō Āċ' °ĀĈ x,y, ½Āċ x, ū ĆĪ Ĩñ .
[Āċ' ¼: 300, -150, -100 ċ. ċ.]

Óó¾Ć ½ì Ĉ BC ±ýĒ ōĀċ ū Ĩ°ĀüĀĪ ō pø Āċ' ° 450 ċ. ċ. Āċ' ° ±ýĒjø, ĨĀ÷ò ĀĪ ¾ĆĈ C ±ýĒ p¼ò¾ĆĈ Ĩ°ĀüĀĪ ō Āċ' °Āý x,y,z Āċ x ĆĪ Ĩñ .
[Āċ' ¼: 300, -150, -300 ċ. ċ. Āċ' °]

1.90 Ū¼Ī Ā Ĩ°ċ ĀĪ ĨĒĪ ō A ±ýĒ ðüĆĀĈ, « Đ °ĪĪĀø - ¾xō - ¾ĪĪ ūĆ ū ĆĈ (guy wires)



Ā¼ō 1-82

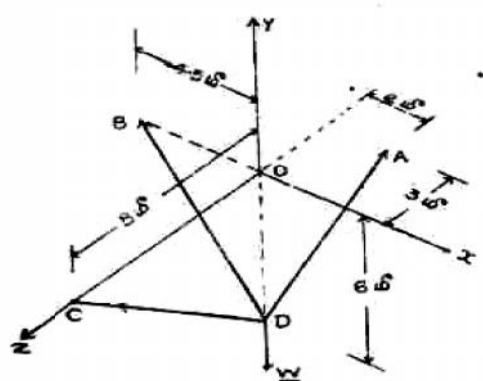
1.90 $1.82 \text{ } \delta$ $\vec{A}_i \cdot \vec{O} = \frac{3}{4} \delta \vec{A} \vec{O} \vec{I} \cdot \vec{u} \vec{C} \vec{E}$. $\vec{A} \vec{U} \cdot \vec{u} \text{ } AB, AC \rightarrow \vec{A} \vec{A} \vec{U} \vec{E} \vec{O}$
 $\vec{A} \vec{U} \vec{A} \vec{I} \vec{O} \text{ } p \vec{O} \vec{A} \vec{C} \vec{O} \vec{u} \text{ } \vec{O} \vec{E} \vec{S} \vec{A} \text{ } 2600 \text{ } \vec{C} \vec{C} \vec{A} \vec{C} \vec{O} \text{ } 1750 \text{ } \vec{C} \vec{C} \vec{A} \vec{C} \vec{O} \text{ } \pm \vec{y} \vec{E} \vec{i} \vec{o}$,
 « $\vec{A} \vec{u} \text{ } p \vec{A} \vec{n} \vec{I} \vec{O} \text{ } A \vec{o} \text{ } \vec{z} \vec{C} \vec{u} \vec{o} \vec{D} \vec{o} \vec{A} \vec{C} \vec{O} \text{ } \vec{C} \vec{y} \text{ } \frac{3}{4} \vec{i} \vec{A} \vec{A} \vec{E} \vec{i} \vec{n} \vec{s}$.
 [$\vec{A} \vec{C} \vec{O} \text{ } \frac{1}{4} \text{ } 1300 \vec{i} - 3900 \vec{j} - 150 \vec{k} \text{ } \vec{C} \vec{C} \vec{A} \vec{C} \vec{O}$]

1.91 $1.91 \text{ } \delta$ $3-37 \text{ } \delta$ $AC \pm \vec{y} \vec{E} \vec{A} \vec{u} \vec{E} \vec{O} \text{ } \vec{A} \vec{U} \vec{A} \vec{I} \vec{O} \text{ } p \vec{O} \vec{A} \vec{C} \vec{O} \text{ } 3500 \text{ } \vec{C} \vec{C}$
 $\pm \vec{y} \vec{E} \vec{O} \vec{i} \vec{l} \vec{o} \vec{S} \vec{A} \vec{i} \vec{D} \text{ } AB, AD \pm \vec{y} \vec{E} \vec{A} \vec{U} \vec{C} \vec{O} \text{ } \vec{A} \vec{U} \vec{A} \vec{I} \vec{O} \vec{A} \vec{C} \vec{O} \text{ } \vec{C} \vec{A} \vec{o} \text{ } \vec{A} \vec{U} \vec{A} \vec{I} \vec{O}$
 $p \vec{o} \vec{a} \vec{y} \vec{U} \text{ } p \vec{O} \vec{o} \vec{D} \vec{A} \vec{C} \vec{O} \text{ } \vec{C} \vec{y} \text{ } \frac{3}{4} \vec{i} \vec{A} \vec{A} \vec{y} \vec{A} \vec{C} \vec{O} \text{ } \vec{O} \vec{i} \vec{l} \vec{o} \frac{3}{4} \vec{i} \text{ } p \vec{O} \vec{o} \vec{A} \frac{3}{4} \vec{i} \vec{l}$
 $\vec{i} \vec{n} \vec{I} \vec{i} \vec{n} \vec{s}$.
 ($\vec{A} \vec{C} \vec{O} \text{ } \frac{1}{4} \text{ } 6500 \text{ } \vec{C} \vec{C} \vec{C}$, $5000 \text{ } \vec{C} \vec{C} \vec{O}$)

1.92 $100 \text{ } \vec{C} \vec{C} \vec{A} \vec{C} \vec{O} \text{ } \pm \frac{1}{4} \vec{O} \vec{u} \vec{C} \vec{O} \text{ } \vec{O} \text{ } \vec{i} \vec{l} \vec{o} \vec{D} \vec{A} \vec{C} \vec{i} \vec{l} \text{ } (\text{Chandelier}) \vec{O} \vec{i} \vec{l} \vec{s}$
 « $\vec{A} \vec{o} \frac{3}{4} \vec{a} \vec{y} \vec{U} \vec{O} \vec{i} \vec{C} \vec{A} \vec{C} \vec{O} \vec{u} \text{ } \vec{A} \vec{i} \vec{y} \vec{U} \vec{o} \text{ } \vec{O} \vec{i} \vec{l} \vec{o} \vec{D} \vec{o} \frac{3}{4} \vec{C} \vec{O} \vec{O} \frac{1}{4} \vec{y} \vec{S} \vec{i} \frac{1}{2} \vec{o} \frac{3}{4} \vec{o}$
 $\frac{3}{4} \vec{i} \vec{C} \vec{A} \vec{i} \vec{U} \text{ } \frac{3}{4} \vec{i} \vec{A} \vec{O} \vec{A} \vec{O} \vec{I} \vec{u} \vec{C} \vec{D}$. $\vec{O} \vec{i} \vec{C} \vec{A} \vec{C} \vec{O} \vec{u} \text{ } \vec{A} \vec{i} \vec{y} \vec{E} \vec{O} \vec{o} \text{ } \vec{A} \vec{U} \vec{A} \vec{I} \vec{O}$
 $p \vec{O} \vec{A} \vec{C} \vec{O} \vec{A} \vec{y} \pm \vec{n} \vec{A} \frac{3}{4} \vec{o} \vec{D} \vec{s} \vec{C} \vec{i} \vec{i} \vec{n} \vec{s}$.

1.93 $Z \ll \vec{i} \vec{O} \vec{y} \vec{A} \vec{C} \vec{O} \text{ } \vec{o} \frac{3}{4} \vec{C} \vec{O} \vec{A} \vec{C} \vec{O} \text{ } \vec{A} \vec{U} \vec{A} \vec{I} \vec{O} \text{ } 2.5 \text{ } \vec{C} \vec{C} \vec{A} \vec{C} \vec{O} \text{ } \vec{A} \vec{a} \vec{y} \vec{U} \text{ } \vec{O} \vec{D} \vec{I} \vec{C} \vec{O}$
 (Stiuts) $\vec{A} \vec{U} \vec{A} \vec{I} \vec{O} \vec{A} \vec{C} \vec{O} \vec{u} \text{ } \vec{O} \vec{A} \vec{z} \vec{C} \vec{A} \vec{A} \vec{C} \vec{O} \vec{A} \vec{i} \vec{y} \vec{E} \vec{E}$. $\vec{O} \vec{D} \vec{I} \vec{u} \text{ } (0,5,-12) \text{ } (3,0-4)$
 $(2,-2,1) \pm \vec{y} \vec{E} \vec{A} \vec{C} \vec{O} \text{ } \vec{C} \vec{O} \vec{A} \vec{C} \vec{O} \text{ } \vec{C} \vec{o} \text{ } \vec{A} \vec{u} \vec{E} \vec{A} \vec{C} \vec{O} \text{ } \vec{C} \vec{O} \text{ } \ll \vec{A} \vec{o} \vec{D} \ll \vec{A} \vec{C} \vec{O}$
 $\vec{A} \vec{U} \vec{A} \vec{I} \vec{O} \text{ } p \vec{O} \ll \vec{o} \vec{A} \vec{D} \text{ } p \vec{U} \vec{i} \vec{A} \vec{C} \vec{O} \text{ } \vec{C} \vec{y} \text{ } (\text{tensile or Compressive forces})$
 $\pm \vec{n} \vec{A} \frac{3}{4} \vec{o} \vec{D} \vec{u} \text{ } \vec{O} \vec{E} \vec{S} \vec{A} \text{ } P, Q, R \pm \vec{y} \vec{E} \vec{o} \text{ } \vec{O} \vec{D} \vec{I} \vec{C} \vec{O} \text{ } \vec{A} \vec{U} \vec{A} \vec{I} \vec{O} \vec{A} \vec{C} \vec{O} \text{ } \vec{C} \vec{i}$
 $\vec{i} \vec{n} \vec{s} \text{ } \pm \vec{A} \vec{u} \vec{E} \vec{O} \text{ } p \vec{O} \ll \vec{o} \vec{A} \vec{D} \text{ } p \vec{U} \vec{i} \vec{A} \vec{C} \vec{O} \text{ } \vec{u} \text{ } \vec{z} \vec{C} \vec{u} \vec{y} \vec{E} \vec{E} \pm \vec{y} \vec{U} \vec{o} \vec{i} \vec{n} \vec{s}$.
 ($\vec{A} \vec{C} \vec{O} \text{ } \frac{1}{4} \text{ } p = 4.15 (-p \vec{O} \vec{A} \vec{C} \vec{O}) \vec{C} \vec{C} \vec{C}$
 $Q = 2.66 (p \vec{U} \vec{i} \vec{A} \vec{C} \vec{O}) \vec{C} \vec{C} \vec{C}$
 $R = 2.40 (p \vec{O} \vec{A} \vec{C} \vec{O}) \vec{C} \vec{C} \vec{O}$)

1.94 $1.94 \text{ } \delta$ $DA, DB, DC \pm \vec{y} \vec{E} \vec{o} \vec{A} \vec{C} \vec{u} \text{ } D \vec{o} \vec{u} \vec{S} \vec{z} \vec{i} \vec{l} \vec{C} \text{ } \vec{A} \vec{U} \vec{A} \vec{I} \vec{O} \vec{W} \vec{C} \vec{C} \vec{A} \vec{U} \vec{A} \vec{i}$
 $\vec{O} \vec{A} \vec{z} \vec{C} \vec{A} \vec{A} \vec{C} \vec{O} \vec{A} \vec{i} \vec{y} \vec{E} \vec{E}$. $DB \vec{o} \vec{A} \vec{U} \vec{A} \vec{I} \vec{O} \text{ } p \vec{O} \vec{A} \vec{C} \vec{O} \text{ } 100 \text{ } \vec{C} \vec{C} \vec{C} \pm \vec{y} \vec{E} \vec{i} \vec{o} \text{ } \vec{A} \vec{U} \vec{A} \vec{y}$
 $\pm \frac{1}{4} \vec{A} \vec{O} \vec{o} \text{ } DA, DC \rightarrow \vec{A} \vec{A} \vec{u} \vec{E} \vec{O} \text{ } \vec{A} \vec{U} \vec{A} \vec{I} \vec{O} \text{ } p \vec{O} \vec{A} \vec{C} \vec{O} \text{ } \vec{C} \vec{y} \pm \vec{n} \vec{A} \frac{3}{4} \vec{o} \vec{D} \vec{s} \vec{C} \vec{O} \vec{o}$
 $\vec{i} \vec{n} \vec{s}$.
 [$\vec{A} \vec{C} \vec{O} \text{ } \frac{1}{4} \text{ } 327.5, 210.0, 112.5 \text{ } \vec{C} \vec{C} \vec{C}$]



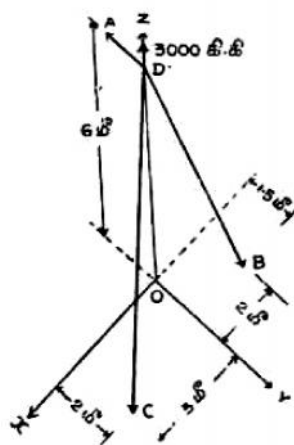
$1.94 \text{ } \delta$

1.95 $1.95 \text{ } \delta$ $DC \vec{o} \vec{A} \vec{C} \vec{O} \text{ } \vec{A} \vec{U} \vec{A} \vec{I} \vec{O} \text{ } p \vec{O} \vec{A} \vec{C} \vec{O} \text{ } 225 \text{ } \vec{C} \vec{C} \vec{C} \pm \vec{y} \vec{E} \vec{i} \vec{o} \text{ } W, T_{DA}, T_{DB}$
 $\rightarrow \vec{A} \vec{A} \vec{u} \vec{E} \vec{O} \vec{A} \frac{3}{4} \vec{o} \vec{D} \vec{s} \vec{C} \vec{i} \vec{i} \vec{n} \vec{s}$.
 [$\vec{A} \vec{C} \vec{O} \text{ } \frac{1}{4} \text{ } 655, 420, 200 \text{ } \vec{C} \vec{C} \vec{C}$]

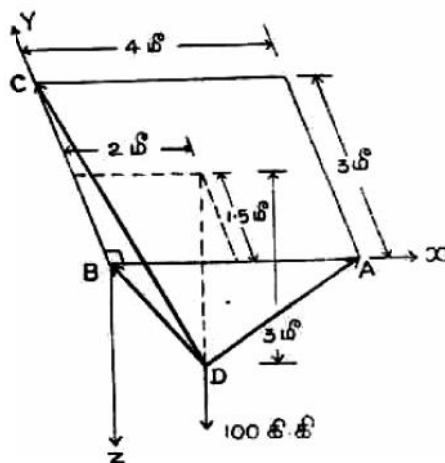
1.96. 3-38ø ùšžì ĩ | °ÄüÄî õ ÄÜ Äŷ ± ĩ ¼ 131 ŷ, ŷ ±ŷËø DA, DB, DC
 → (ÄÜËø | °ÄüÄî õ pø Äŷ ° ŷŷ ±ñ Ä¾00, ŷŷ ĩ ñ.
 [Äŷ ¼ 80, 40, 45, ŷ, ŷ, ŷ]

1.97. D±ŷË òüŸÄø « Î ò¾ Äî ò¾0ÜŸ Ä¾õ 1.78ø ïðÉÄÄ; Ü
 3000 ŷ, ŷ Äŷ °ÄîÉð šÄøšžì ĩ | °ÄüÄî, DA, DB, DC ±ŷË òÄŸ Ÿø
 žž ø õ pø Äŷ ° ŷŷ ° Î | °ÄüÄî D ±ŷË òüŸÄø ÄŸ ÄÄø « ŷ Ä, Éð
 ±ŷËËø òÄŸ Ÿø žž ø õ pø Äŷ ° ŷŷ ±ñ Ä¾00, ŷŷ ĩ ñ.
 [Äŷ ¼ 850, 1950, 1400 ŷ, ŷ, ŷ]

1.98. « Î ò¾ Äî ò¾0ÜŸ Ä¾õ 1.84ø D ±ŷË òüŸÄø ùšžì ĩ | °ÄüÄî õ
 100 ŷ, ŷ, ŷ ± ĩ ¼ ÜŸ.



Ä¾õ 1-84



Ä¾õ 1-85

ÄÜ ŷ Ä DA, DB, DC, → Ä ÄÜ Ÿø | °ÄüÄî õ pø Äŷ ° ü °ÄŸ ÄÄø
 ŷ Ä, ŷËË ±ŷËø pø Äŷ ° ŷŷ ±ñ Ä¾00, ŷŷ ĩ ñ.
 [Äŷ ¼ 62.4, 20.8, 45.8 ŷ, ŷ, ŷ]

À¼õ 1-89

1.109. G, J ±ý ÛÁ¼ð¾¼ø | À; Õð¾¼ðÀðÏ ùÇ ° °Ó· ÉÂø À· ½ì ðÀð¼ (pin connection) °ð¼ð |¾¼í¾¼Áý « ·· Áðð (structure) À¼õ 1-90 ðÈÄÄjÛ - ùÇð, G, J ±ý ÛÁ¼ð¾¼ø | °ÁøÁÏ ð ±¾¼¾¼ì Á· ° ·· ÇÕø GH ±ý Ûø °ð¼ðÁ¾¼Áø H, M ±ý ÛÁ¼í Çø « ·· ÁÕø ° °Ó· Éð¾¼ì Á· ° ·· ÇÕø (pin reaction) ðñ ·· K ±ý ÛÁ¼ð¾¼ø |¾¼í¾¼Á¼ðÀðÏ ùÇ ÀÛ ·· Á 150 ç, ç ±Éì |¾¼ì ·· |¾¼í¾¼ « ·· ÁðÀø - ùÇ °ð¼í¾¼ý ±¾¼ ·· Çò ÒÈì¾¼

$$(\text{Á· } ¼ : \underline{F}_G = 175 \left(\frac{3}{\sqrt{34}} i + \frac{5}{\sqrt{34}} j \right) \text{ ç, ç}$$

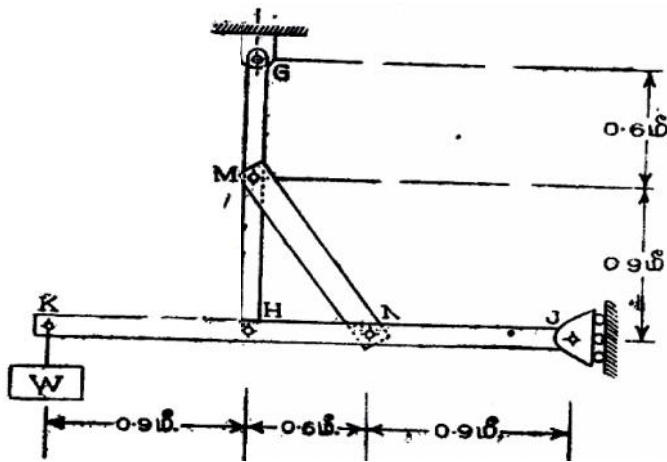
A ÁÆÇÁ

À¼õ

$$\underline{F}_H = 380(0.158i - 0.9872j) \text{ ç, ç}$$

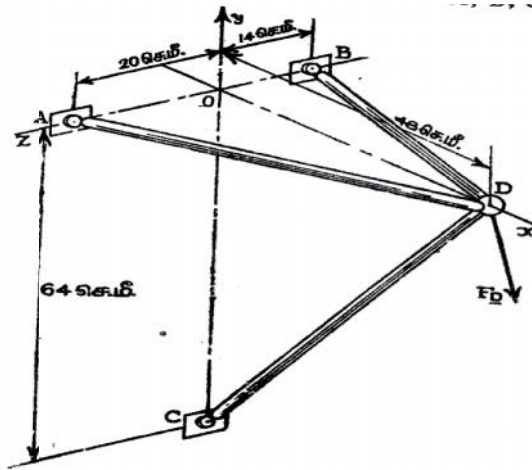
$$\underline{F}_j = -90 \text{ ç, ç}$$

$$\underline{F}_M = 270.5 \left(\frac{2}{\sqrt{13}} i + \frac{3}{\sqrt{13}} j \right) \text{ ç, ç}$$



À¼õ 1-90

1.110. Í Á:Á¾¼Áø -¾¼ÁÄj ð¾¼í¾¼Á¼ðÀðÏ ùÇ AD, BD, CD ±ý Ûø ÁÖÄj É ðÕððì ðÁç ù A, B, C ±ý Ûø



À¼õ 1-91

ÒÙÇÇ Çø ÁóÈì ÷ Ñ ½ç ã ðí ò; À; Õò¼ø (ball and socket joint) « Áò ÷ Çø | ÀÜÜ D ±ý Ü Á¼ò¼ø À¼õ 1.91 ì ðÈÄÄ; Ü ÞÜì Á; ò Áç ½ì ò Ò ðí ùÇÐ. D ±ý Ü ò òÙÇÇ ÁÈÇÄ $F_D = (75i - 600j - 300k)$ ç. ç. ç. Áç °Á; ÉÐ | °ÁøÁÍ ÇÈÐ. CD, AD ±ý Ü ò òðò ÁÍ ¾ç Çø | °ÁøÁÍ ò Áç ° çì ÷ ñ .

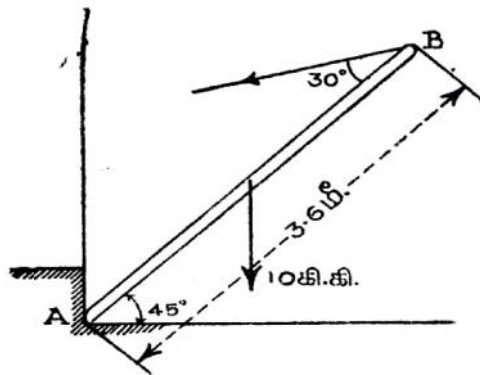
(Áç ¼: $F_{CD} = 750(0.6i + 0.8j)$ ç. ç. ç.

$F_{AD} = -693(-0.923i + 0.385j)$ ç. ç. ç. ÞÜÄÑ Í Áç ° Ü ò D ÁÈÇÄ | °ÁøÁÍ ÷ ÈÈ.)

1.111. 3.6 Åð¼÷ ÇÓÙÇÐò 10 ç. ç. ± ¼òÙÇÐÄ; É µ÷ Á; × ð ¼ (joist) Á À¼õ 1.92 ò ì ðÈÄÄ; Ü ÁÈÇÄ ÷ « ¾ý ÇÁøÑÈÇø ò¼ò Ò ðí ùÇ Áç Ü ´ý È ÞøðÐ Æ÷òÐ ÇÈý. A ±ý Ü Á¼ò¼ø ÷ ÜÁÍ ò ±¾ç÷¾çì Áç ° Áò ò ÁüÈø | °ÁøÁÍ ò ÞøÁç ° Áò ò ÷ ñ .

(Áç ¼ AÄø 13.785 ç. ç. ç.

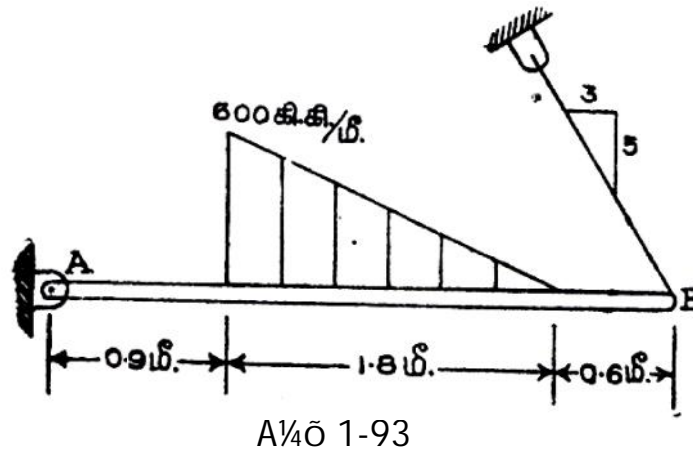
±60°27' ÷ ±ý Ü ò ±¾ç÷¾çì Áç ° BÄø ÞøÁç ° 5√2 ç. ç. ç.



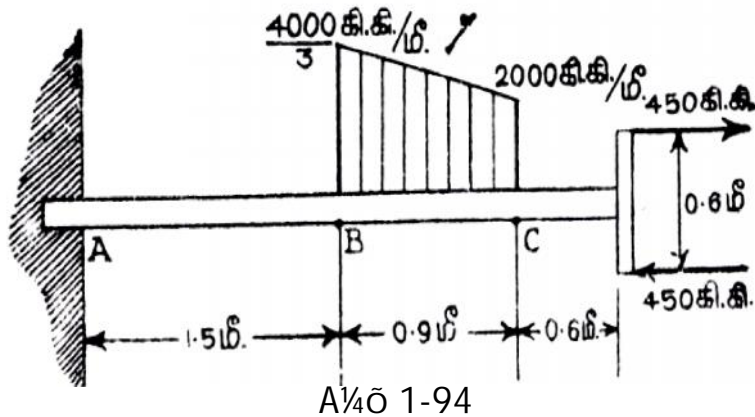
À¼õ 1-92

1.112. À¼õ 1.113ø ì ðÈÄÄ; Ü ç ¼Ä; ì ç¼ì ò ò¼Äò¼ý ÇÁø | °ÁøÁÍ ò ±øÄ; ÞøÁç ° Çò ÷ ñ . ò¼Äò¼ý ± ¼ Äò ÒÈì ½ç .

(Answer: $F_A = 366 \text{ kg}$; $M_A = 1.93 \text{ kg-m}$ at A
 $F_B = 318 \text{ kg}$; $M_B = 0.34 \text{ kg-m}$ at B)



1.113. A cantilever beam is shown in Fig. 1.94. It is subjected to a triangular load of 4000 kg/m at the free end and a point load of 450 kg at the fixed end. The beam is 1.5m long. Find the reactions at the fixed end.

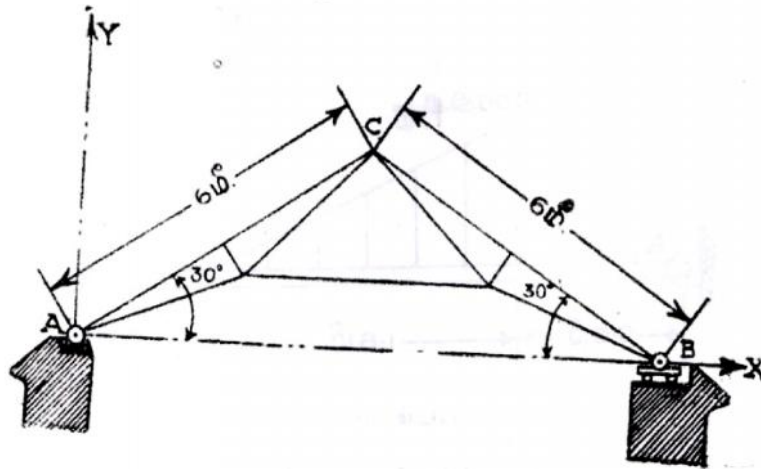


→ The beam is fixed at A. The reactions at A are F_A and M_A . The beam is subjected to a triangular load and a point load. The beam is 1.5m long. Find the reactions at the fixed end.

- (1) F_A and M_A at A
- (2) F_B and M_B at B
- (3) F_C and M_C at C

- (Answer: (a) $F_A = 900 \text{ kg}$; $M_A = 1980 \text{ kg-m}$
 (b) $F_B = 900 \text{ kg}$; $M_B = 630 \text{ kg-m}$
 (c) $F_C = 0 \text{ kg}$; $M_C = 270 \text{ kg-m}$)

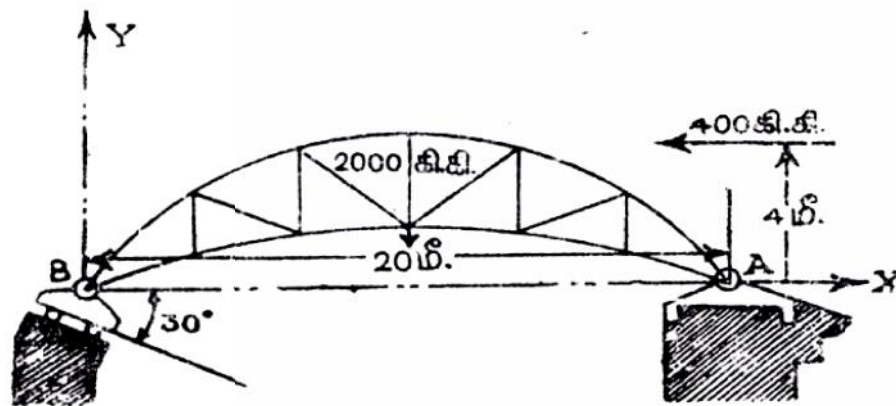
1.114. 2000 кг. м. в. $\frac{1}{4}$ м. в. $\frac{1}{2}$ м. в. ABC \pm γ \bar{U} δ $^{\circ}$ \bar{A} \bar{E} $-$ δ $\frac{3}{4}$ м. в. $\frac{3}{4}$ м. в. \bar{y} \bar{U} A \pm \bar{y} \bar{E} \bar{O} \bar{E} \bar{A} \bar{O} \bar{A} \bar{O} $\bar{1.95}$ м. в. $\bar{\delta}$ \bar{E} \bar{A} \bar{A} \bar{U} \bar{A} \bar{C} $\bar{1}$ $\bar{2}$ м. в. \bar{o} \bar{A} \bar{O} \bar{I} \bar{o} \ll $\frac{3}{4}$ м. в. \bar{B} \pm \bar{y} \bar{U} \bar{o} \bar{A} \bar{U} \bar{E} \bar{O}



А/О 1-95

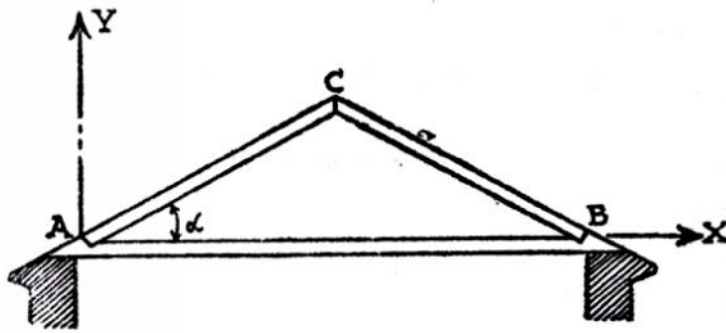
\bar{O} \bar{E} \bar{C} $\bar{1}$ $\bar{4}$ м. в. \bar{x} \bar{U} \bar{C} $\bar{3}$ $\bar{4}$ м. в. \bar{y} \bar{E} \bar{o} $-$ \bar{o} \bar{n} \bar{I} $\bar{1}$ \bar{o} \bar{A} \bar{o} $\bar{3}$ $\bar{4}$ м. в. $-$ \bar{O} \bar{C} \bar{A} \bar{y} \bar{S} \bar{A} \bar{o} \bar{A} \bar{i} \bar{O} \bar{o} $\bar{3}$ $\bar{4}$ м. в. \bar{O} \bar{U} \bar{C} \bar{D} . $AC = BC = 6$ м. в. $\angle CAB = 30^{\circ}$ \pm \bar{E} \times \bar{o} $^{\circ}$ \bar{A} \bar{E} \bar{A} \bar{C} $\bar{1}$ $\bar{4}$ м. в. \bar{A} \bar{U} \bar{E} \bar{D} \bar{o} 160 кг. м. в. \pm $\bar{1}$ \bar{o} \bar{O} \bar{U} \bar{C} $\bar{3}$ $\bar{4}$ м. в. \bar{U} \bar{A} \bar{C} $\bar{1}$ \bar{o} \bar{y} \bar{U} (a uniformly distributed wind load of 160kg) AC \pm \bar{y} \bar{U} \bar{o} $-$ δ $\frac{3}{4}$ м. в. \bar{U} \bar{o} \bar{A} \bar{U} \bar{i} $\bar{1}$ \bar{o} \bar{i} $\bar{1}$ \bar{o} $\frac{3}{4}$ м. в. \bar{A} \bar{U} \bar{A} \bar{A} $\bar{3}$ $\bar{4}$ м. в. \times \bar{o} $\bar{1}$ $\bar{2}$ м. в. \bar{I} \bar{A} \bar{B} \bar{O} \bar{E} \bar{C} \bar{o} $\bar{1}$ $\bar{2}$ м. в. \bar{o} \pm $\frac{3}{4}$ м. в. \bar{A} \bar{C} $\bar{1}$ \bar{o} \bar{C} \bar{i} $\bar{1}$ $\bar{2}$ м. в. \bar{A} \bar{C} $\bar{1}$ $\bar{4}$: ($R_B = 1046$ кг. м. в.) ; $F_{AX} = 800$ кг. м. в. ; $F_{Ay} = 1092$ кг. м. в.)

1.115. 20 м. в. $\frac{1}{4}$ м. в. $\bar{1}$ $\bar{2}$ м. в. \bar{C} \bar{O} \bar{o} , 2000 кг. м. в. \pm $\bar{1}$ \bar{o} \bar{O} \bar{U} \bar{C} \bar{A} \bar{C} \bar{x} $-$ δ $\frac{3}{4}$ м. в. \bar{A} \bar{i} \bar{y} \bar{U} A \pm \bar{y} \bar{U} \bar{A} \bar{C} $\bar{1}$ \bar{o} $\bar{3}$ $\bar{4}$ м. в. \bar{A} \bar{O} \bar{A} \bar{O} $\bar{1.96}$ м. в. $\bar{\delta}$ \bar{E} \bar{A} \bar{A} \bar{U} \bar{A} \bar{C} $\bar{1}$ $\bar{2}$ м. в. \bar{o} \bar{A} \bar{O} \bar{I} \bar{U} \bar{C} \bar{D} . \bar{C} $\bar{1}$ $\bar{4}$ $\bar{3}$ \bar{C} \bar{o} \bar{D} $\frac{1}{4}$ м. в. 30° \bar{S} $\bar{1}$ $\bar{2}$ м. в. \bar{o} \bar{i} \bar{C} \bar{A} \bar{o} \bar{A} \bar{U} \bar{E} $\frac{3}{4}$ м. в. $\bar{1}$ $\bar{2}$ м. в. \bar{y} \bar{E} \bar{o} $-$ \bar{o} \bar{n} \bar{I} $\bar{1}$ \bar{o} \bar{A} \bar{o} $\bar{3}$ $\bar{4}$ м. в. $-$ \bar{O} \bar{C} \bar{C} \bar{y} \bar{S} \bar{A} \bar{o} \ll $\frac{3}{4}$ м. в. \bar{B} \pm \bar{y} \bar{E} \bar{A} \bar{U} \bar{E} \bar{O} \bar{N} \bar{E} \bar{C} \bar{A} \bar{i} \bar{O} \bar{o} $\bar{3}$ $\bar{4}$ м. в. \bar{U} \bar{C} \bar{D} . AB \bar{A} \bar{A} \bar{O} \bar{o} \bar{D} 4 м. в. $\frac{1}{4}$ м. в. \bar{A} \bar{A} \bar{o} $\bar{3}$ $\bar{4}$ м. в. \bar{O} \bar{o} AB \bar{I} $\bar{1}$ $\bar{2}$ м. в. \bar{A} \bar{i} \bar{E} $\frac{3}{4}$ м. в. \bar{A} \bar{O} \bar{o} \bar{A} \bar{H} \bar{o} $\bar{1}$ $\bar{2}$ м. в. \bar{U} \bar{E} \bar{E} \bar{D} $-$ δ $\frac{3}{4}$ м. в. \bar{y} \bar{S} \bar{A} \bar{o} 400 кг. м. в. \ll \bar{C} \bar{x} \bar{U} \bar{C} \bar{A} \bar{C} $\bar{1}$ \bar{o} \bar{y} \bar{E} \bar{i} \bar{A} \bar{o} \bar{A} \bar{O} \bar{A} \bar{i} \bar{o} \bar{D} $\bar{1}$ $\bar{2}$ м. в. \bar{E} \bar{o} \bar{O} \bar{O} \bar{i} $\bar{1}$ $\bar{2}$ м. в. \bar{y} \bar{S} \bar{A} \bar{o} \pm $\frac{3}{4}$ м. в. \bar{A} \bar{C} $\bar{1}$ \bar{o} \bar{C} \bar{i} $\bar{1}$ $\bar{2}$ м. в. \bar{A} \bar{C} $\bar{1}$ $\bar{4}$: $F_{Ax} = 224$ кг. м. в. ; $F_{Ay} = 920$ кг. м. в. ; $R_B = 1247$ кг. м. в.



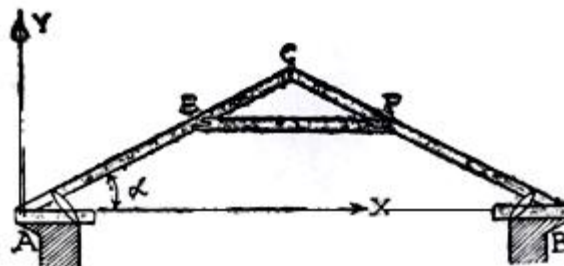
А/О 1-96

1.116. 5 $\text{Å} \div \text{C} \text{O} \text{U} \text{C} \text{p} \text{O} \text{A} \text{r} \text{u} \text{C} \pm \text{y} \text{U} \text{A} \text{C} \text{O} \text{A} \text{C} \text{r} \text{1} \text{2} \text{i} \text{o} \text{A} \text{D} \text{I} \text{o}$
 « $\text{u} \times \text{o} \text{A} \text{D} \text{3} \text{4} \text{I} \text{3} \text{4} \text{A} \text{y} \text{p} \text{O} \text{O} \text{E} \text{U} \text{o} \text{A} \text{1} \text{o} \text{1.97} \text{o} \text{,} \text{i} \text{o} \text{E} \text{A} \text{A} \text{U} \text{AB} \pm \text{y} \text{U} \text{o}$
 $\mu \div \text{C} \text{1} \text{4} \text{A} \text{O} \text{1} \text{4} \text{A} \text{i} \text{y} \text{E} \text{o} \text{A} \text{i} \text{O} \text{o} \text{A} \text{D} \text{I} \text{o} \text{u} \text{C} \text{E} \text{.} \text{U} \text{A} \text{A} \text{y} \text{r} \text{o} \text{A} \text{r} \text{u} \text{C}$
 $\text{C} \text{1} \text{4} \text{o} \text{A} \text{C} \text{o} \text{U} \text{i} \text{r} = \tan^{-1}(0.5) \pm \text{y} \text{E} \text{S} \text{,} \text{i} \text{1} \text{2} \text{i} \text{o} \text{A} \text{O} \text{U} \text{C} \text{E} \text{.} \text{r} \text{o} \text{A} \text{U} \text{o} \text{D}$
 $\text{u} \text{A} \text{i} \text{y} \text{E} \text{y} \text{A} \text{A} \text{o} \text{U} \text{C} \text{A} \text{O} \text{o} \text{180} \text{C} \text{,} \text{C} \text{1} \text{4} \text{o} \text{U} \text{C} \text{A} \text{U} \text{A} \text{A} \text{A} \text{3} \text{4} \text{i} \text{C} \text{,} \text{A}$
 $\pm \text{y} \text{U} \text{A} \text{C} \text{O} \text{A} \text{C} \text{O} \text{A} \text{A} \text{I} \text{o} \text{A} \text{C} \text{r} \text{1} \text{2} \text{i} \text{o} \text{C} \text{i} \text{,} \text{i} \text{n} \text{.}$
 (A $\text{C} \text{r} \text{1} \text{4} \text{:} F_C = 180 \text{C} \text{,} \text{C} \text{,} F_{Ax} = 180 \text{C} \text{,} \text{C} \text{; } F_{Ay} = 180 \text{C} \text{,} \text{C} \text{.}$



A10 1-97

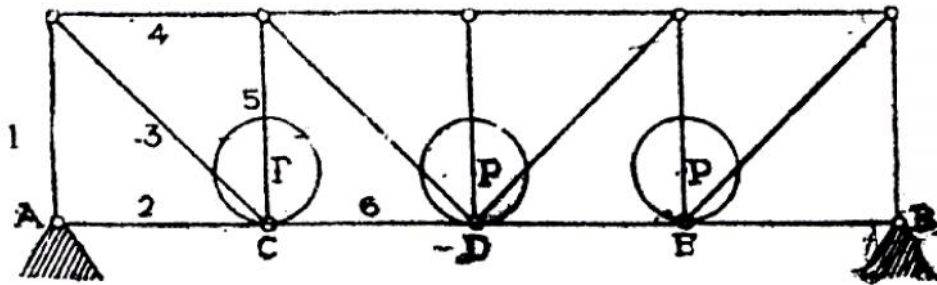
1.117. $\text{u} \text{A} \text{i} \text{y} \text{U} \text{o} \text{4} \text{A} \text{D} \text{1} \text{4} \text{C} \text{O} \text{U} \text{C} \text{AC,BC} \pm \text{y} \text{U} \text{o} \text{A} \text{A} \text{i} \text{o} \text{D} \text{1} \text{4} \text{i} \text{C} \text{i}$
 $\text{,} \text{i} \text{n} \text{1} \text{4} \mu \div \text{U} \text{A} \text{r} \text{o} \text{A} \text{D} \text{3} \text{4} \text{A} \text{y}$



A10 1-988

« $\text{E} \text{O} \text{E} \text{u} \text{A, B} \pm \text{y} \text{U} \text{A} \text{C} \text{O} \text{A} \text{C} \text{O} \text{A} \text{A} \text{O} \text{o} \text{I} \text{A} \text{o} \text{A} \text{i} \text{3} \text{4} \text{C} \text{O} \text{A} \text{i} \text{O} \text{o} \text{A} \text{D} \text{I} \text{o}$
 $\text{EF} \pm \text{y} \text{U} \text{o} \text{C} \text{1} \text{4} \text{A} \text{O} \text{1} \text{4} \text{A} \text{i} \text{y} \text{E} \text{i} \text{o} \text{3} \text{4} \text{i} \text{,} \text{o} \text{A} \text{D} \text{I} \text{o} \text{,} \text{A} \text{1} \text{o} \text{1.98} \text{o} \text{,} \text{i} \text{o} \text{E} \text{A} \text{A} \text{U}$
 $\text{C} \text{U} \text{o} \text{A} \text{C} \text{A} \text{i} \text{o} \text{A} \text{D} \text{I} \text{o} \text{u} \text{C} \text{D} \text{.} \text{AC, BC} \text{o} \text{D} \text{1} \text{4} \text{i} \text{C} \text{y} \text{A} \text{A} \text{o} \text{U} \text{C} \text{C} \text{O}$
 $\text{160} \text{C} \text{,} \text{C} \text{1} \text{4} \text{o} \text{U} \text{C} \text{A} \text{U} \text{A} \text{A} \text{y} \text{A} \text{i} \text{o} \text{A} \text{I} \text{y} \text{E} \text{E} \text{.} \text{A} \text{i} \text{o} \text{x} \text{A} \text{C} \text{r} \text{1} \text{2} \text{i} \text{o}$
 $\text{O} \text{E} \text{i} \text{,} \text{1} \text{2} \text{i} \text{o} \text{A} \text{A} \text{A} \text{3} \text{4} \text{i} \text{,} \text{x} \text{o} \text{,} \text{U} \text{A} \text{A} \text{y} \text{r} \text{o} \text{A} \text{r} \text{u} \text{C} \text{r} = \tan^{-1}(0.5) \pm \text{E} \text{x} \text{o} \text{AC} = 3 \text{EC} \pm \text{E} \text{x} \text{o}$
 $\text{,} \text{i} \text{n} \text{I} \text{A} \text{A} \text{A} \text{A} \text{O} \text{o} \text{I} \text{A} \text{o} \text{A} \text{i} \text{3} \text{4} \text{A} \text{y} \text{3} \text{4} \text{C} \text{o} \text{D} \text{1} \text{4} \text{i} \text{,} \text{A} \text{C} \text{r} \text{1} \text{2} \text{i} \text{o} \text{EF} \text{o} \text{C} \text{,} \text{O} \text{o} \text{p} \text{O} \text{A} \text{C} \text{r} \text{1} \text{2} \text{i} \text{o}$
 $\text{A} \text{A} \text{u} \text{E} \text{i} \text{,} \text{i} \text{n} \text{.}$
 (A $\text{C} \text{r} \text{1} \text{4} \text{:} R_A = 160 \text{C} \text{,} \text{C} \text{,} T = 480 \text{C} \text{,} \text{C} \text{.}$

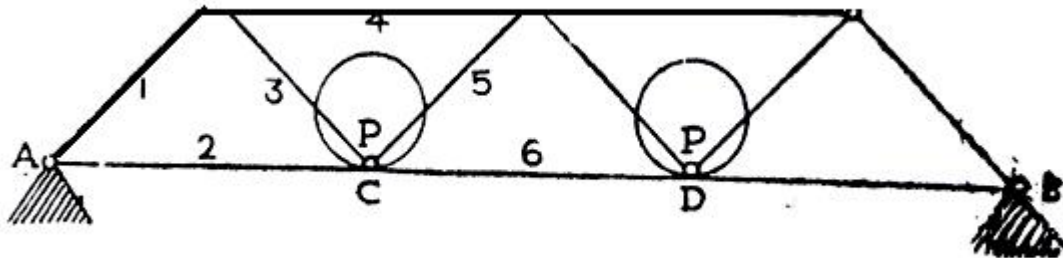
1.118. $\text{C, D, E} \pm \text{y} \text{U} \text{A} \text{C} \text{O} \text{A} \text{C} \text{O} \text{A} \text{u} \text{u} \text{A} \text{i} \text{y} \text{E} \text{O} \text{o} \text{o} \text{,} p = 2000 \text{C} \text{,} \text{C} \text{1} \text{4} \text{o} \text{U} \text{C}$
 $\text{A} \text{U} \text{A} \text{o} \text{3} \text{4} \text{i} \text{A} \text{A} \text{n} \text{1} \text{2} \text{A} \text{i} \text{O} \text{U} \text{C} \text{A} \text{i} \text{A} \text{r} \text{o} \text{A} \text{D} \text{3} \text{4} \text{I} \text{3} \text{4} \text{y} \text{E} \text{y} \text{A} \text{E} \text{A} \text{A} \text{o} \text{D} \text{A} \text{1} \text{o}$
 $\text{1.99} \text{o} \text{,} \text{i} \text{o} \text{A} \text{D} \text{I} \text{o} \text{u} \text{C} \text{D} \text{.} \text{o} \text{i} \text{O} \text{3} \text{4} \text{A} \text{i} \text{x} \text{r} \text{o} \text{A} \text{A} \text{U} \text{o} \text{D} \text{u} \text{(inclined web members)}$
 $\text{C} \text{1} \text{4} \text{o} \text{D} \text{1} \text{4} \text{y} \text{45} \text{S} \text{,} \text{i} \text{1} \text{2} \text{i} \text{o} \text{3} \text{4} \text{o} \text{3} \text{4} \text{i} \text{I} \text{y} \text{E} \text{E} \text{.} \text{A} \text{i} \text{O} \text{E} \text{A} \text{i} \text{A} \text{i} \text{n} \text{I}$
 $\text{1, 2, 3, 4, 5, 6,} \pm \text{y} \text{U} \text{p} \text{A} \text{i} \text{A} \text{O} \text{1} \text{4} \text{U} \text{o} \text{D} \text{C} \text{O} \text{A} \text{A} \text{I} \text{o} \text{A} \text{C} \text{r} \text{1} \text{2} \text{i} \text{o} \text{C} \text{i} \text{,} \text{i} \text{n} \text{.}$



A14õ 1-99

$(\check{A}^{\check{C}} \cdot \check{1} / 4 ; S_1 = -3000 \text{ kN} (\text{p} \check{U} \check{i} \text{ } \check{A}^{\check{C}} \cdot \check{0}) ; S_2 = 0$
 $S_3 = +4250 \text{ kN} (\text{p} \check{O} \check{A}^{\check{C}} \cdot \check{0}) ; S_4 = -3000 \text{ kN}$
 $S_5 = -1000 \text{ kN}, \quad S_6 = +3000 \text{ kN}$

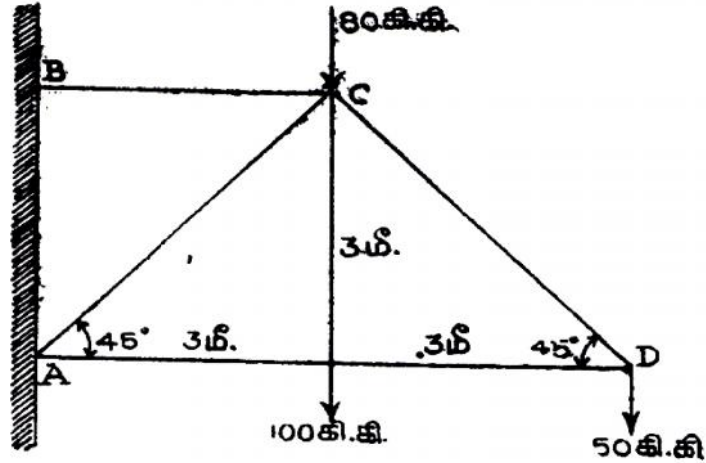
1.119. A14õ 1.100ø ; i ðÊÄ ÀjA - ð¾Ä | Àj ý Ú C, D ± ý È p¼í ; Çø p=2000 kN ± ¼ÖùÇ pÖ °ÄÄj È



A14õ 1-100

AÜ ·· Àð ¾j í Ì ÇÈÐ. °j 0¾ Äj × - ð¾Ä - Úôð ù Ç · ¼¾Ç ðD¼ ý 45°
 $S_1 = 1/2 P$; Ç · ñ ¼j Ì ý È È ; Ä È Ç Ä Ì Ö · È · Ä Ì · Ä j ñ Í
 ÄÄ ý Ä Ì ð¾ôÄ ð¾ ÄÜ Ä ý ; Ä 1/2 Äj ; 1, 2, 3, 4, 5, 6 ± È Ì Ì È Ç ; ðÄ ð Ì ù Ç
 - Úôð Çø Çø ð¾ Ä · ° ; Çj ; ñ ·
 $\check{A}^{\check{C}} \cdot \check{1} / 4 : S_1 = -3000 \text{ kN} (\text{p} \check{U} \check{i} \text{ } \check{A}^{\check{C}} \cdot \check{0}) ; S_2 = 0$
 $S_3 = +4250 \text{ kN} ; S_4 = -3000 \text{ kN}$
 $S_5 = -1000 \text{ kN}, \quad S_6 = +3000 \text{ kN}$

1.120. Ä ·· Ç × °ð¾ - ð¾Ä | ¾j Ì ¾Ç (Cantilever truss) ý Ú A14õ 1.101ø ; i ðÊÄÄj Ú ã ý Ú ÄÜ Ä · È ð¾í ; ÄÄj Úö A, B ± ý ÜÄ¼ø¾ø ÄüÈÇ

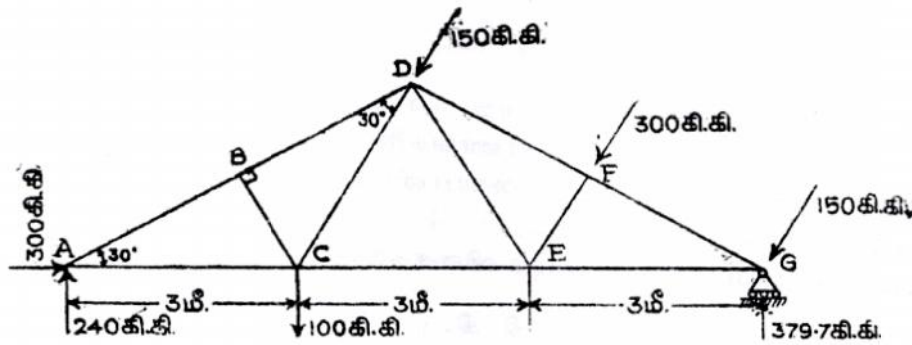


À¼õ 1-101

ÞÙì òÀõĪ ò (clamped) - ùÇÐ. ÞÀü ½¼ ÓĒĒ Āì Ē Ąĵñ Ī - ò¼ĀĪ ò¼ĀĪ Çø ðüĀĪ ò Āċċ ċċ ÇĪ ċĵñ ċ.

$$\begin{aligned}
 (\text{Āċċ } ¼_1: & S_1 = -2820 \text{ ċċċ} & S_2 = +2000 \text{ ċċċ} \\
 & S_3 = +2820 \text{ ċċċ} & S_4 = -4000 \text{ ċċċ} \\
 & S_5 = 0 & S_6 = +4000 \text{ ċċċ}
 \end{aligned}$$

1.121. ÛĒ Ā - ò¼ĀðĪ ¼ĪĪ ¼ĪĪ ĀĵÛ À¼õ 1.102ø ĵĵðĒĀĪÛ Ā ±ÿĒ ÓĒĒĒ Āċċ ½Ī òĀõĪ ò Ġ±ÿĒ ÓĒĒĒ - Óċ ċÿĒÿŞĀø ĪĪ Ò¼ĀðĪ ò 4 ĀÛĒ Āð ¼ĪĪ ĀĀĪÛð - ùÇÐ. ÞÀü ½¼ ÓĒĒ Āð ĀĀÿĀĪ ò¼ċ - ò¼ĀðĪ ¼ĪĪ ¼ċ - Ûððĵ ċÿĪĪÿĒĒø ċċø Āċċ ċċ ÇĪ ċĵñ ċ.



À¼õ 1-102

1.122. À¼õ 1.103ø ĵĵðĒĀĪÛ - ùÇ ċċċċċ ĒĒĒĒ Āð ĪĀüĒ (pin connected) - ò¼ĀðĪ ¼ĪĪ ¼ĪĪ ĀĵÛ - Ûððĵ ċÿĪĪÿĒĒø ðüĀĪ ò Āċċ ċċ ĀĪ ċĵñ ċ.

$$\text{Āċċ } ¼_1, \quad F_{AB} = 288 \text{ ċċċ} \text{ (ÞÙì Ąċċ ċ)}$$

$$F_{BC} = 57.7 \text{ kN (Tension)}$$

$$F_{CD} = 57.7 \text{ kN (Compression)}$$

$$F_{BD} = 173 \text{ kN (Compression)}$$

$$F_{BE} = 173 \text{ kN (Compression)}$$

$$F_{CE} = 202 \text{ kN (Tension)}$$

$$F_{AC} = 144 \text{ kN (Tension)}$$

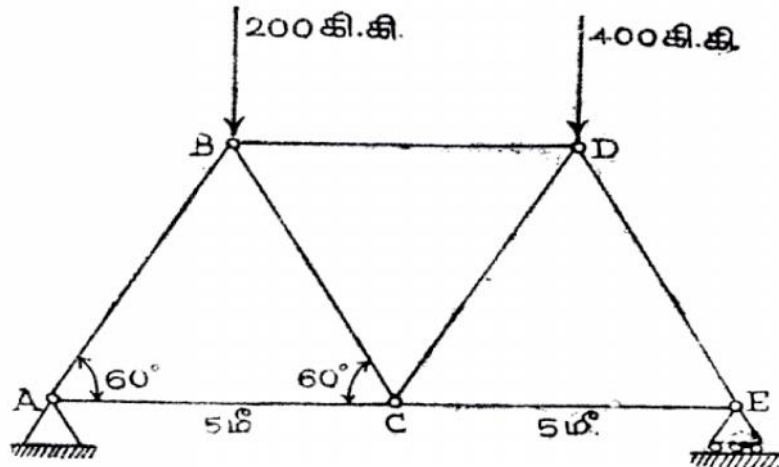


Figure 1-103

1.123. Figure 1.104 shows a truss structure with nodes A, B, C, D, E, F, G, H. Node A is a pin support, and node H is a roller support. The bottom chord consists of segments AC, CE, EG, and GH, each 3m long. The top chord consists of segments AB, BE, EF, and FH. The height of the truss is 4m. Vertical loads of 400 kN, 600 kN, and 800 kN are applied at nodes C, E, and G respectively.

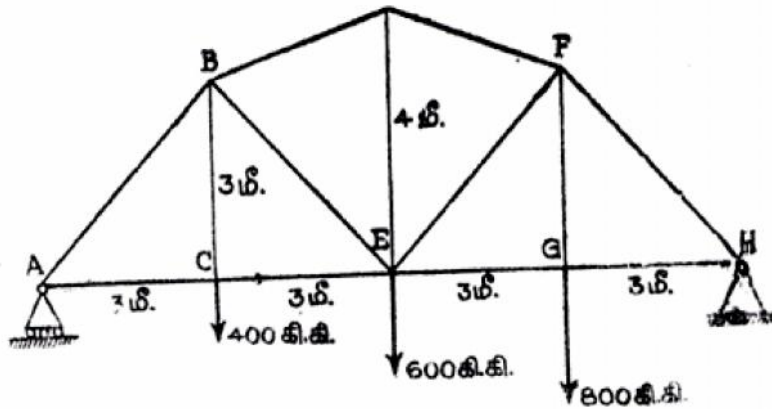


Figure 1-104

$$S_{EC} = 800 \text{ kN (Tension)}$$

$$S_{ED} = 600 \text{ kN (Tension)}$$

$$S_{EF} = 100\sqrt{2} \text{ kN (Compression)}$$

1.124. Determine the force in the members of the truss shown in Figure 1.124.

1. Determine the force in the members of the truss shown in Figure 1.124?

2. $\int_{\partial \Omega} \mathbf{u} \cdot \mathbf{n} \, dS = \int_{\Omega} \operatorname{div} \mathbf{u} \, dV$, $\int_{\partial \Omega} \mathbf{u} \cdot \mathbf{n} \, dS = \int_{\Omega} \operatorname{div} \mathbf{u} \, dV$?
3. $\int_{\partial \Omega} \mathbf{u} \cdot \mathbf{n} \, dS = \int_{\Omega} \operatorname{div} \mathbf{u} \, dV$ « $\int_{\partial \Omega} \mathbf{u} \cdot \mathbf{n} \, dS = \int_{\Omega} \operatorname{div} \mathbf{u} \, dV$?
4. $\int_{\partial \Omega} \mathbf{u} \cdot \mathbf{n} \, dS = \int_{\Omega} \operatorname{div} \mathbf{u} \, dV$ $\int_{\partial \Omega} \mathbf{u} \cdot \mathbf{n} \, dS = \int_{\Omega} \operatorname{div} \mathbf{u} \, dV$ (supports) $\int_{\partial \Omega} \mathbf{u} \cdot \mathbf{n} \, dS = \int_{\Omega} \operatorname{div} \mathbf{u} \, dV$
5. $\int_{\partial \Omega} \mathbf{u} \cdot \mathbf{n} \, dS = \int_{\Omega} \operatorname{div} \mathbf{u} \, dV$ $\int_{\partial \Omega} \mathbf{u} \cdot \mathbf{n} \, dS = \int_{\Omega} \operatorname{div} \mathbf{u} \, dV$ (connections) $\int_{\partial \Omega} \mathbf{u} \cdot \mathbf{n} \, dS = \int_{\Omega} \operatorname{div} \mathbf{u} \, dV$
6. $\int_{\partial \Omega} \mathbf{u} \cdot \mathbf{n} \, dS = \int_{\Omega} \operatorname{div} \mathbf{u} \, dV$ $\int_{\partial \Omega} \mathbf{u} \cdot \mathbf{n} \, dS = \int_{\Omega} \operatorname{div} \mathbf{u} \, dV$?

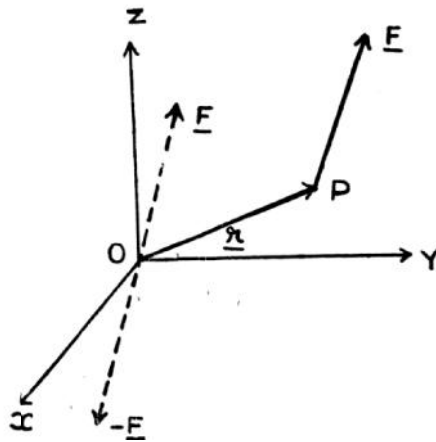
« ÄĬ - 2

„ðĒŪĭ „ôĭ Äĭ ÖŪ „ÇŸ °ÄĬĬ Ä

2.1 ÄĬĬ °ðĭ ¼ĭĭ ¼ĬĬ « Ĭ ÄôÄŸ ĬĬ ĭ „ö

Ĭ Ö „ðĒŪĭ „ôĭ Äĭ ÖÇŸ Ĭ ÈöÄĬð¼ ðŪÇŸ ĬŸÈŸ Ĭ °ÄøÄĬ ö ĬŪĬ È ÄĬĬ ° ÄĬÖôÄöÄĒ Äĭ §¼Ū Ĭ Äĭ Ö ðŪÇŸÄŸ Ĭ °ÄŪÄĬ „ŸÈ Ĭ Ö ÄĬĬ °, « ðð¼Ÿ Ĭ ÖÄĬ „ « Ĭ ÄÖö Ĭ Ö Ĭ ÄĬĬ ½ - „ ÄÄŪÈĭø ®Ĭ Ĭ °öð °ÄöÄĬ ð¼ø

„ðĒŪĭ „ôĭ Äĭ ÖŪ ĬŸÈŸ P ±ŸŪö ðŪÇŸÄŸ F ±ŸŪö ÄĬĬ ° Ĭ °ÄŪÄĬ Ä¼ĭĭ Ĭ Ĭ ĭ Ū.

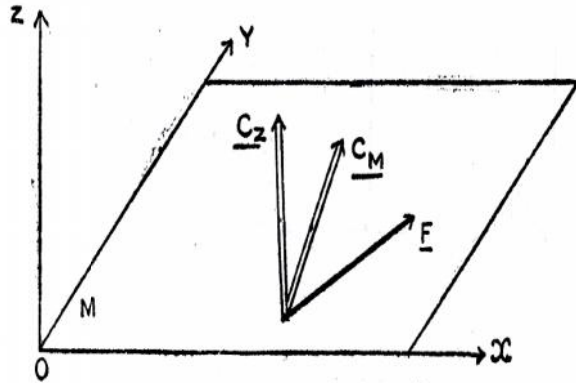


Ä¼ö 2-1

O ±ŸÄð ÄĬÖôÄöÄĒ ±Ĭ ððĭ Ĭ Ĭ ŪŪö Ĭ Ö ðŪÇŸÄĬ Ĭ „ F ±ŸŪö ÄĬĬ °Ĭ Ä O ±ŸŪö ðŪÇŸÄĬ Ĭ ¼öĭ ÄÄ÷ð¼ø Ĭ °öÄ¼ŪĬ Ĭ ÄĬ « Ĭ Äöð ÄŸ ÄÖÄĭŪ ÄĬ ÄÄŪĭ „öÄĬ ö.

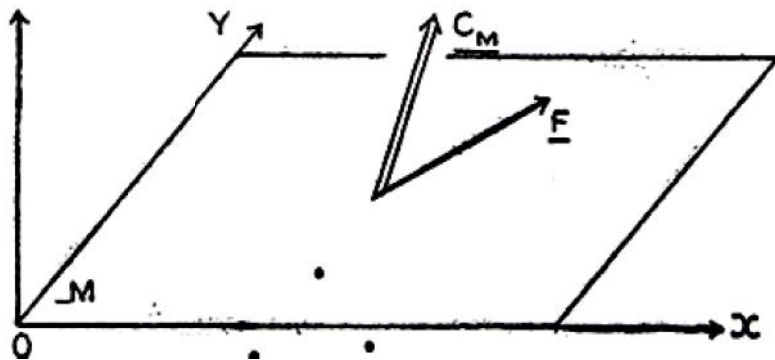
O Ĭ Äð ðÄĬ „ðŪÇŸÄĬ Ĭ Ĭ Ĭ ĬĬ P ÄŸŸ ĬĬ Äð¼ĬĬ °Ĭ Ä Ĭ ±ĒĬĬ ÈŸ „xö. O ÄŸ ÄĒŸÄ F Ĭ °ÄŪÄĬ ö §ĭ ðĒŪĭ Ĭ Ĭ ½Äĭ „ ÄĬ ÄÖö §ĭ ðĒŸ Ä¼ö 2.1 ø „ ðĒĒÄĭŪ F, -F ±ŸŪö ÄĬĬ ° „ Çö ðĬ ð¼xö. Ĭ Ĭ ÄŪ Ĭ ŠÄ §Ĭ÷ĭ §ĭ ðĒŸ °ÄŪ Ĭ Ä¼ĬÖÄĭ ĬĬ Ĭ °ÄŪÄĬ Ä¼ĭø Ĭ ÄŪÈŸŸ Ĭ¼ĭĭ ÄÄŸ Ĭ ÄĬĬ ö. - „ ŠÄ Ĭ Ĭ Ä « öĭ Äĭ ÖÇŸŸ °ÄĬĬ ÄĬ Äö Äĭ¼Ĭ Ĭ Ĭð.

$\underline{C} \pm y \Delta D$ í $\underline{E} \underline{A} \underline{C} \dots \frac{1}{2} \delta \delta \delta \delta \frac{3}{4} \underline{E} y \frac{3}{4} \underline{C} \dots \circ \dots \underline{A} \underline{A} \dots \underline{A} \underline{A} \underline{U} \underline{i} \dots \delta \underline{I} \delta \dots$ « $\underline{D} \underline{L} \pm y \underline{U} \delta$
 $\frac{3}{4} \underline{C} \delta \delta \frac{3}{4} \underline{U} \underline{i} \underline{i} \dots \underline{i} \dots \underline{i} \dots \delta \frac{3}{4} \underline{i} \dots \underline{E} \frac{3}{4} \underline{C} \dots \circ \underline{A} \underline{C} \delta \frac{3}{4} \dots \frac{1}{4} \underline{A} \underline{U} \underline{E} \frac{3}{4} \underline{C} \dots \circ \underline{A} \underline{C} \underline{i} \dots \underline{i} \dots \underline{i} \dots \underline{A} \underline{U} \underline{A} \underline{I} \delta \dots$ $\underline{C} \underline{A} \underline{y}$
 $\underline{A} \dots \underline{x} \dots \underline{C} \underline{M} \frac{3}{4} \underline{C} \delta \delta \frac{3}{4} \underline{U} \underline{i} \underline{i} \dots \underline{i} \dots \underline{i} \dots \delta \frac{3}{4} \underline{i} \dots \underline{E} \frac{3}{4} \underline{C} \dots \circ \underline{A} \underline{C} \delta \delta \underline{M} \frac{3}{4} \underline{C} \delta \delta \frac{3}{4} \underline{O} \delta \underline{A} \dots \underline{A} \underline{A} \underline{U} \delta \underline{D}$
 « $\underline{A} \underline{U} \dots \underline{E} \frac{\underline{C}_z, \underline{C}_M}{\dots} \pm \underline{E} \underline{i} \underline{i} \dots \underline{E} \underline{C} \dots \underline{x} \delta \dots$ ($\underline{A} \frac{1}{4} \delta 2.4^3 \underline{A} \underline{i} \dots$)



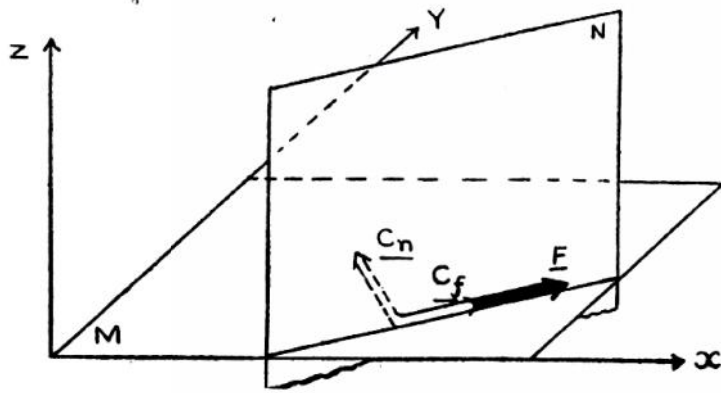
Á¼õ 2-4

$\underline{E}, \underline{C}_z \pm y \underline{A} \dots \underline{A} \dots y \underline{U} \underline{i} \dots \underline{i} \dots y \underline{U} \dots \underline{i} \dots \delta \frac{3}{4} \underline{i} \dots$ « $\dots \underline{A} \underline{A} \frac{3}{4} \delta$ « $\dots \underline{A} \dots \underline{U} \underline{i} \underline{i} \dots \underline{i} \dots \underline{i} \dots \underline{A} \underline{i} \underline{E}$
 $\dots \underline{E} \underline{A} \dots \circ \dots \underline{A} \underline{M} \frac{3}{4} \underline{C} \delta \delta \frac{3}{4} \underline{C} \delta \underline{P} \pm y \underline{U} \delta \delta \underline{U} \underline{C} \underline{C} \underline{A} \delta \dots \underline{A} \underline{U} \underline{A} \underline{I} \delta \dots$ $\underline{F} \pm y \underline{U} \delta$
 $\underline{A} \dots \circ \dots \underline{A} \underline{Q} \pm y \underline{U} \delta \underline{A} \underline{C} \delta \delta \underline{A} \underline{A} \delta \underline{U} \underline{C} \underline{C} \underline{A} \underline{E} \underline{C} \underline{i} \dots \underline{p} \dots \frac{1}{2} \underline{A} \dots \underline{p} \frac{1}{4} \delta \dots \underline{A} \underline{A} \delta \delta \underline{D}$
 $\underline{i} \underline{A} \underline{E} \underline{A} \underline{i} \delta \dots$ « $\frac{3}{4} \underline{U} \underline{i} \dots \underline{z} \underline{U} \underline{E} \frac{3}{4} \underline{E} \dots$ « $\dots \underline{A} \delta \delta \underline{A} \frac{1}{4} \delta 2.5 \delta \dots \underline{i} \dots \delta \frac{1}{4} \delta \underline{A} \underline{I} \underline{U} \underline{C} \underline{D}$.



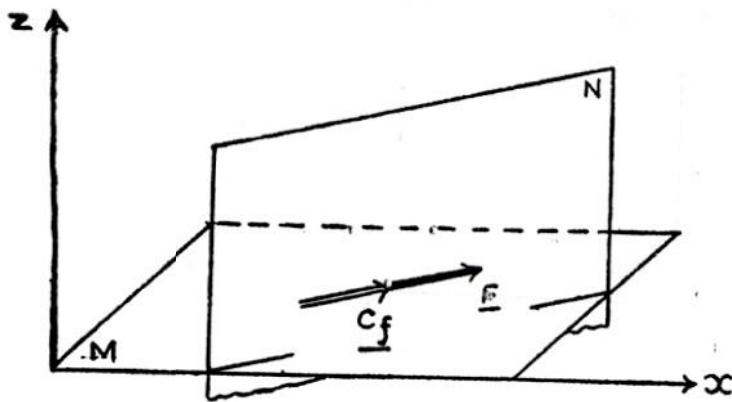
Á¼õ 2-5

$\underline{C}_M \pm y \underline{U} \delta \frac{3}{4} \underline{C} \dots \circ \underline{A} \underline{C} \underline{M} \frac{3}{4} \underline{C} \delta \delta \frac{3}{4} \underline{A} \dots \underline{A} \underline{A} \frac{3}{4} \delta$ « $\frac{3}{4} \underline{y} \underline{A} \dots \underline{x} \dots \underline{C} \underline{F} \dots \underline{A} \underline{U} \underline{A} \underline{I} \delta$
 $\frac{3}{4} \underline{C} \dots \circ \underline{A} \underline{C} \delta \delta \underline{F} \underline{i} \underline{i} \dots \underline{i} \dots \underline{i} \dots \delta \frac{3}{4} \underline{i} \dots \underline{E} \frac{3}{4} \underline{C} \dots \circ \underline{A} \underline{C} \delta \delta \underline{A} \dots \underline{A} \underline{A} \underline{U} \delta \underline{D}$ « $\underline{A} \underline{U} \dots \underline{E} \underline{O} \dots \underline{E} \underline{S} \underline{A} \frac{\underline{C}_f, \underline{C}_n}{\dots}$
 $\pm \underline{E} \underline{i} \underline{i} \dots \underline{E} \underline{C} \dots \underline{x} \delta \dots$ ($\underline{A} \frac{1}{4} \delta 2.6 \delta \dots \underline{i} \dots \delta \frac{1}{4} \delta \underline{A} \underline{I} \underline{U} \underline{C} \underline{D}$) $\underline{F}, \underline{C}_n \pm y \underline{A} \dots \underline{A} \underline{M} \frac{3}{4} \underline{C} \delta \delta \frac{3}{4} \underline{C} \delta$
 $\dots y \underline{U} \underline{i} \dots \underline{i} \dots y \underline{U} \dots \underline{i} \dots \delta \frac{3}{4} \underline{i} \dots \underline{p} \delta \delta \frac{3}{4} \delta$



À¼õ 2-6

« " Á, Û ì Ì ° ì Ç Ç, Á ì É " ü " È Á " ° " Á M ¼ Ç ò ¼ Ç ù Ì î | ° í Ì ò ¼ ì É N ± ý Û ò
 ¼ Ç ò ¼ Ç ò \underline{F} ± ý Û ò Á " ° " Á p " ½ Á ì, p ¼ ò | Á Á ÷ ò ð ò | Á È Á ì ò. ± É § Á
 ($\underline{F}, \underline{C}$) " , Ç " Á p Û ¼ Ç Á ì, " Ì ì , ò Á ð Ì ($\underline{F}, \underline{C}_f$) ± ý Û ò " § Á § Á ì, Á ì É
 « " Á ò " Á ò
 À¼õ 2.7 ø , ì ð È Á Á ì Û | Á Û ò.



À¼õ 2-7

($\underline{F}, \underline{C}_f$) " , Ç " Á Á ü È Ç ý § ò : ì " , § Á Ó Û ì , ø (wrench) ± É ò Á Ì ò. ± ò Á ì
 Á " ° í , ½ í , " Ç ì Ì " È × Á Ì ò ð ò Ç " Á , Ç ò Ó Û ì , ø Ç " Á § Á « Á ü È Ç ù Ì î
 ° ì Ç Ç, Á ì É ± Ç Ç Á « " Á ò " Á ò | Á ü Û ü Ç ð. ($\underline{F}, \underline{C}_f$) ± ý Á " Á " § Á ¼ Ç " ° Á Ç
 « " Á ò | Á ý È ì ø, Ó Û ì , ø Á " , Á ì É ¼ ì , × ò (positive) « " Á , Û

$$\underline{r}_i = x_i \underline{i} + y_i \underline{j} + z_i \underline{k}$$

$$\underline{F}_i = F_{ix} \underline{i} + F_{iy} \underline{j} + F_{iz} \underline{k}$$

$$\underline{R} = R_x \underline{i} + R_y \underline{j} + R_z \underline{k}$$

$$\underline{M}_o^R = M_{ox}^R \underline{i} + M_{oy}^R \underline{j} + M_{oz}^R \underline{k} \quad \pm \dot{y} \hat{\Delta} \bar{\Delta}$$

$$\underline{R} = \sum_{i=1}^n \underline{F}_i \quad \pm \dot{y} \hat{\Delta} \bar{\Delta}$$

$$\begin{aligned} R_x \underline{i} + R_y \underline{j} + R_z \underline{k} &= \sum_{i=1}^n (F_{ix} \underline{i} + F_{iy} \underline{j} + F_{iz} \underline{k}) \\ &= \left(\sum_{i=1}^n F_{ix} \right) \underline{i} + \left(\sum_{i=1}^n F_{iy} \right) \underline{j} + \left(\sum_{i=1}^n F_{iz} \right) \underline{k} \quad \mp \dot{y} \bar{\Delta} \end{aligned}$$

« $\frac{3}{4} \dot{y} \hat{\Delta} \bar{\Delta}$

$$R_x = \sum_{i=1}^n F_{ix}$$

$$R_y = \sum_{i=1}^n F_{iy}$$

$$R_z = \sum_{i=1}^n F_{iz}$$

« $\dot{y} \hat{\Delta} \bar{\Delta}$

$$\underline{M}_o^R = \sum_{i=1}^n \underline{r}_i \wedge \underline{F}_i \quad \pm \dot{y} \hat{\Delta} \bar{\Delta}$$

$$\begin{aligned} \underline{M}_o^R x_i + \underline{M}_o^R y_j + \underline{M}_o^R z_k &= \sum_{i=1}^n \begin{vmatrix} \underline{i} & \underline{j} & \underline{k} \\ x_i & y_i & z_i \\ F_{ix} & F_{iy} & F_{iz} \end{vmatrix} \\ &= \sum_{i=1}^n \left\{ (y_i F_{iz} - z_i F_{iy}) \underline{i} + (z_i F_{ix} - x_i F_{iz}) \underline{j} + (x_i F_{iy} - y_i F_{ix}) \underline{k} \right\} \\ &= \left\{ \sum_{i=1}^n (y_i F_{iz} - z_i F_{iy}) \right\} \underline{i} + \left\{ \sum_{i=1}^n (z_i F_{ix} - x_i F_{iz}) \right\} \underline{j} + \left\{ \sum_{i=1}^n (x_i F_{iy} - y_i F_{ix}) \right\} \underline{k} \quad \mp \dot{y} \bar{\Delta} \end{aligned}$$

« ¼_i ÅÐ

$$M_{ox}^R = \sum_{i=1}^n (y_i F_{iz} - z_i F_{iy})$$

$$M_{oy}^R = \sum_{i=1}^n (z_i F_{ix} - x_i F_{iz})$$

$$M_{oz}^R = \sum_{i=1}^n (x_i F_{iy} - y_i F_{ix})$$

– , ŞÅ « ù ÅĈ´ ° , ÇŸ , ½Á_iÉÐ

$$OX \text{ ÅÆ}(\hat{S}\hat{A} \sum_{i=1}^n F_{ix} = R_x \pm y \hat{E} \text{ ÅĈ´ °} \hat{i} \hat{l} \hat{o},$$

$$OY \text{ ÅÆ}(\hat{S}\hat{A} \sum_{i=1}^n F_{iy} = R_y \pm y \hat{E} \text{ ÅĈ´ °} \hat{i} \hat{l} \hat{o},$$

$$OZ \text{ ÅÆ}(\hat{S}\hat{A} \sum_{i=1}^n F_{iz} = R_z \pm y \hat{E} \text{ ÅĈ´ °} \hat{i} \hat{l} \hat{o},$$

$$OX \text{ ÅüÈĈ} (y_i F_{iz} - z_i F_{iy}) = \underline{M}_{ox}^R \pm y \hat{E} \text{ ¼ĈÖôðð¼ĈÈÛîî ò},$$

$$OY \text{ ÅüÈĈ} (z_i F_{ix} - x_i F_{iz}) = \underline{M}_{oy}^R \pm y \hat{E} \text{ ¼ĈÖôðð¼ĈÈÛîî ò},$$

$$OZ \text{ ÅüÈĈ} (x_i F_{iy} - y_i F_{ix}) = \underline{M}_{oz}^R \pm y \hat{E} \text{ ¼ĈÖôðð¼ĈÈÛîî ò},$$

ŞÅÖô O ÅÆĈĀ_i , î | °Öô R ± y Ūô | ¼_iĭ ÅĀý ÅĈ´ °ĀŸ ± ñ Á¼Ĉðð

$$R = \sqrt{R_x^2 + R_y^2 + R_z^2} \pm y \hat{E} \hat{i} \hat{l} \hat{o}.$$

ðò | ¼_iĭ ÅĀý ÅĈ´ ° x, y, z – Āí , Ū ¼ý „ x , „ y , „ z ± y Ūô Ş_i ½í , „ Ç

– ñ ¼_iĭ , ĈÉ_iø R | °ĀüĀĭ ô Ş_i ðĒý ¼Ĉ´ °î , ÇĀĭ „ „ Ç

$$\frac{\cos \alpha_x}{R_x} = \frac{\cos \alpha_y}{R_y} = \frac{\cos \alpha_z}{R_z} = \frac{1}{R} \pm y \hat{E} \hat{i} \hat{l} \hat{o} \text{ ÅýĀĭĭ , ÇĈÖóÐ | ÅĒĀ_iô.}$$

« ùĀ_iŞÈ O ÅüÈĈ « .. ĀÔô M_o^R ± y Ūô ÅĈ´ ° Ç × ÍÆĈ´ ° ½ððð¼ĈÈÉŸ ± ñ

$$\text{Å¼Ĉðð} M_o^R = \sqrt{(M_{ox}^R)^2 + (M_{oy}^R)^2 + (M_{oz}^R)^2} \pm y \hat{E} \hat{i} \hat{l} \hat{o}.$$

ŞAÖö püÄc' Çx ÍÆÄc' ½öððð¾Æý x, y, z - Âí , Û ¼ý w_x, w_y, w_z ±ý Ûö

Ş_s ½í , Ç - ñ ¼jì , Æjø M_o^R | °ÄüŞ_s ðÆý ¾c' °ì , Çjì ' , Ç

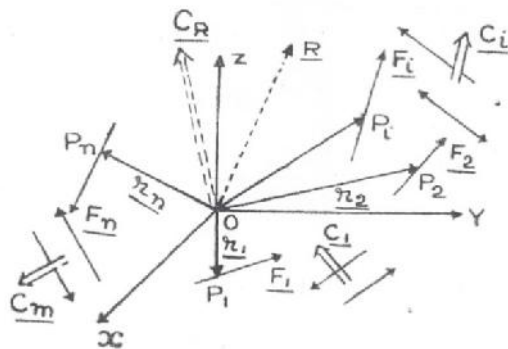
$$\frac{\cos W_x}{M_{o_x}^R} = \frac{\cos W_y}{M_{o_y}^R} = \frac{\cos W_z}{M_{o_z}^R} = \frac{1}{M_o^R} \pm ý Ûö °ÁýÄjî , ù Ä' ÄÄÜì ì ö.$$

R, "x, "y, "z ±ý ÄÉ ÄüÆý Á¾öð , ù, OÄý ç' Ä' Âî °j÷ö¾É Äj , pø' Ä ±ý ÄÐ |¾Çx:

z | ÉÉø « ÄüÆý Á¾öð P₁, P₂, ..., P_i, ..., P_n ±ý ÄÉ ÄüÆý - Äð |¾j' Ä , ù p¼ö | ÄÉÄø' Ä. - Éjø M_o^R Äý Á¾öð OÄý ç' Ä' Âî °j÷ö¾¾jö pöì ì | ÁýÄÐ |¾Çx.

2.4(2) ' Ö , ðÆÜì , ö | Äj ÖÇø | °ÄüÄî , ý È Äj Ş¾Ü | Äj Ö Äc' ° , Çý , ½ö , « ö | Äj ÖÇø ¾jì ì , ý È ÍÆÄc' ½ , Çý , ½ö - , ÇÄüÆüì î °jçç, Äj Äc' ° - ÍÆÄc' ½ « ' Äö' Ä ÄöðÄÄ Äj Ş¾Ü | Äj Ö ðüÇÄø Ä' ÄÄÜð¾ø:

' Ö , ðÆÜì , ö | Äj ÖÇø P₁, P₂, ..., P_i, ..., P_n ±ý Ûö ðüÇç, Çø Ó' ÈŞÄ F₁, F₂, ..., F_i, ..., F_n ±ý Ûö "ÍÆÄc' ½ , Ç - ÖÄjì , ÓÉÄj¾ Äc' ° , ù" (non-couple forces) | °ÄüÄî Ä¾jì | , jü , C₁, C₂, ..., C_n ±ý Ä' Ä ÍÆÄc' ½ , Ç - ÖÄjì ì ö Äc' ° , Çý ¾öððð¾Æý , Ç « ÈÄöÄ¾jì | , jü , Ä¼ö 2.9 ø O ±ý ÄÐ Ä¾ç , ðÆý ÈÄ ÄöðÄÄÄjü ±î ì ö ðüÇç' Äì ì Èç , ðì ö. O' Ä ÐÄì , öðüÇÄjì | , jñ ¼ , ð¾' ÄöÄø, P₁, P₂, ..., P_i, ..., P_n ±ý Ûö ðüÇç, Çý ç' Äð¾c' °Äç, Ç L₁, L₂, ..., L_i, ..., L_n ±Éì ì Èç , × ö.



Ä¼ö 2-9

$$R_x = \sum_{i=1}^n F_{iX}; R_y = \sum_{i=1}^n F_{iY}; R_z = \sum_{i=1}^n F_{iZ}$$

$$C_{Rx} = \sum_{i=1}^n (y_i F_{iZ} - z_i F_{iY}) + \sum_{i=1}^m C_{iX}$$

$$C_{Ry} = \sum_{i=1}^n (z_i F_{iX} - x_i F_{iZ}) + \sum_{i=1}^m C_{iY}$$

$$C_{Rz} = \sum_{i=1}^n (x_i F_{iY} - y_i F_{iX}) + \sum_{i=1}^m C_{iZ}$$

Áċċ' °ò ò | ¾ĵĭ ĭ ¾ĵĵ « ċċ ÁôÀĵŷ 'Ĥ ĭ ĵ, õ
 §ÁÖõ

$$R^2 = R_x^2 + R_y^2 + R_z^2$$

$$C_R^2 = C_{Rx}^2 + C_{Ry}^2 + C_{Rz}^2 \pm \text{ý Èĭ ĭ õ.}$$

2.5 ¾ÉĊċ' °ÈôÀĵĭ É Áċċ' ° « ċċ Áôò, Çŷŷ 'Ĥ ĭ ĵ, õ (Reduction of Special Force Systems):

'õ ĵ, õ ðÈÛĭ ĵ, õ | Àĵĭ õ Çŷŷ ÁĐ ĵ, õ ÁüĀĤ ĵ, õ È Áĵĭ §¾Û | Áĵĭ õ
 Áċċ' °ò ò | ¾ĵĭ ĭ ¾ĵĵ Áċċ' °ò ÁôÀĤ ±Ĥ ĭ ĭ õ O ±ŷ Ûõ ðÛÇĊÁĵ ĵ, õ ÁüĀĤ õ | ¾ĵĭ ĭ ÁĤŷ

Áċċ' °ò \underline{R} - ¾ŷŷ §°:óĐ 'õ ĭ ĤĊċċ' ½ $\frac{M_o^R}{\dots}$ ĭ ĭ 'Ĥ ĭ ĵ, õ ÓÈôĵĭ ÁÉ ÓŷÉŠĀ
 ÛÈôÀð¾Đ.

2.5.1 Áċċ' ĵ, 1:

| ¾ĵĭ ĭ ÁĤŷ Áċċ' °ò \underline{R} ±ŷŷ ÁĐ ĭ ĤĊĊĵĭ | ÁŷÈĭø $\frac{M_o^R}{\dots}$ ±ŷŷ Ûõ °Èôò ð¾Éċċ' Éô
 | ÁüÈ 'õ ĭ ĤĊċċ' ½ Áĵĭ, 'Ĥ ĭ ĵ, õ ÁĤĤ õ.

2.5.2 Áċċ' ĵ, 2:

$\frac{M_o^R}{\dots}$ ±ŷŷ ÁĐ O ÁüÈĊ ±Ĥ ĭ ĭ õ Áċċ' °ò | ¾ĵĭ ĭ ¾ĵĵ Áċċ' °ò Çŷŷ
 ¾ĵĵ ðò ð¾Éŷŷ Çŷŷ ĭ ÈĊĊĊĵ ÛĐĤ ð | ¾ĵĭ ĵ, õ ÁĤ ĭ ÈĊĊĵ. p¾ŷŷ Á¾Ċòò

ĭ ĤĊĊĵĭ | ÁÉĵ ±Ĥ ð¾ Áċċ' °ò | ¾ĵĭ ĭ ¾ĵĵ O Áĵĵ « ċċ Áôõ | ¾ĵĭ ĭ ÁĤŷ Áċċ' °ò \underline{R}
 ĵ, 'Ĥ ĭ ĵ, õ ÁĤĤ õ.

2.5.3 $\hat{A}^{\circ}, 3:$

" $\hat{A}^{\circ} \circ \hat{I} \hat{E} \hat{A}^{\circ} 1/2$ " « $\hat{A} \hat{o} \hat{A} \hat{o} \hat{A}^{\circ} \hat{o} \hat{o} \hat{I} \hat{E} \hat{A}^{\circ} 1/2 \hat{o} \hat{o}$ $\hat{y} \hat{U} \hat{i} \hat{,} \hat{y} \hat{U}$
 $\hat{I} \hat{o} \hat{I} \hat{o} \hat{,} \hat{I} \hat{,} \hat{I} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{,} \hat{A} \hat{E} \hat{o}$ « $\hat{A} \hat{u} \hat{E} \hat{u} \hat{i} \hat{I} \hat{,} \hat{o} \hat{i} \hat{C} \hat{,} \hat{A} \hat{i} \hat{,} \hat{O} \hat{o} \hat{A} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{i} \hat{I}$
 $\hat{p} \hat{,} 1/2 \hat{A} \hat{i} \hat{E} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{A} \hat{S} \hat{A} \hat{,} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{,} \hat{y} \hat{E} \hat{,} \hat{O} \hat{,} \hat{u} \hat{,} \hat{E} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{,} \hat{A} \hat{,} \hat{A} \hat{,} \hat{A} \hat{u} \hat{i} \hat{,} \hat{O} \hat{E} \hat{o} \hat{o}$
 $\pm \hat{E} \hat{,} \hat{O} \hat{y} \hat{S} \hat{A} \hat{,} \hat{U} \hat{E} \hat{o} \hat{A} \hat{o} \hat{,} \hat{D}.$

$\hat{p} \hat{u} \hat{A} \hat{C} \hat{,} \hat{A} \hat{C} \hat{,} \hat{A} \hat{,} \hat{A} \hat{,} \hat{u} \hat{i} \hat{,} \hat{i} \hat{,} \hat{o}$ « $\hat{A} \hat{o} \hat{D} \hat{,} \hat{C} \hat{o} \hat{,} \hat{A} \hat{I} \hat{,} \hat{o}$

- (i) $\hat{O} \hat{D} \hat{u} \hat{C} \hat{,} \hat{A} \hat{E} \hat{C} \hat{S} \hat{A} \hat{,} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{,} \hat{o} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{D} \hat{,} \hat{I} \hat{,} \hat{I} \hat{,} \hat{A} \hat{C}$
- (ii) $\hat{O} \hat{,} \hat{C} \hat{o} \hat{,} \hat{A} \hat{S} \hat{A} \hat{,} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{,} \hat{y} \hat{E} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{D} \hat{,} \hat{I} \hat{,} \hat{I} \hat{,} \hat{A} \hat{C}$
- (iii) $\hat{O} \hat{I} \hat{E} \hat{o} \hat{A} \hat{o} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{i} \hat{I} \hat{,} \hat{p} \hat{,} 1/2 \hat{A} \hat{i} \hat{,} \hat{I} \hat{,} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{,} \hat{o} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{D} \hat{,} \hat{I} \hat{,} \hat{I} \hat{,} \hat{A} \hat{C}.$

2.5.3.1 $\hat{O} \hat{D} \hat{u} \hat{C} \hat{,} \hat{A} \hat{o} \hat{,} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{,} \hat{y} \hat{E} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{,} \hat{u}:$

$\hat{A} \hat{C} \hat{,} \hat{o} \hat{,} \hat{C} \hat{,} \hat{E} \hat{o} \hat{D} \hat{o} \hat{,} \hat{O} \hat{D} \hat{u} \hat{C} \hat{,} \hat{A} \hat{E} \hat{C} \hat{S} \hat{A} \hat{,} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{,} \hat{A} \hat{,} \hat{p} \hat{,} 1/2 \hat{,} \hat{A} \hat{,} \hat{A} \hat{o} \hat{A} \hat{E}$
« $\hat{A} \hat{u} \hat{E} \hat{y} \hat{,} \hat{I} \hat{,} \hat{A} \hat{A} \hat{y} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{o} \hat{o}$ « $\hat{o} \hat{D} \hat{u} \hat{C} \hat{,} \hat{A} \hat{E} \hat{C} \hat{S} \hat{A} \hat{,} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{,} \hat{o}.$ $\pm \hat{E} \hat{S} \hat{A} \hat{,} \hat{I} \hat{,} \hat{o} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{D} \hat{,} \hat{I} \hat{,} \hat{I} \hat{,} \hat{o} \hat{,} \hat{I} \hat{,} \hat{o} \hat{,} \hat{I} \hat{,} \hat{A} \hat{A} \hat{y} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{,} \hat{A}$
 $\hat{A} \hat{,} \hat{A} \hat{u} \hat{i} \hat{,} \hat{O} \hat{E} \hat{,} \hat{D}.$

2.5.3.2 $\hat{O} \hat{,} \hat{C} \hat{o} \hat{,} \hat{A} \hat{S} \hat{A} \hat{,} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{,} \hat{y} \hat{E} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{D} \hat{,} \hat{I} \hat{,} \hat{I} \hat{,} \hat{A} \hat{C}.$

$\hat{O} \hat{,} \hat{o} \hat{E} \hat{U} \hat{i} \hat{,} \hat{o} \hat{,} \hat{I} \hat{,} \hat{O} \hat{C} \hat{y} \hat{,} \hat{A} \hat{D} \hat{,} \hat{O} \hat{,} \hat{C} \hat{o} \hat{,} \hat{A} \hat{S} \hat{A} \hat{,} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{,} \hat{y} \hat{E}$
 $\hat{A} \hat{i} \hat{S} \hat{U} \hat{,} \hat{A} \hat{i} \hat{O} \hat{,} \hat{D} \hat{u} \hat{C} \hat{,} \hat{A} \hat{S} \hat{A} \hat{,} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{,} \hat{y} \hat{E} \hat{,} \hat{O} \hat{,} \hat{A} \hat{E} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{S} \hat{A} \hat{i} \hat{I} \hat{,} \hat{S} \hat{o} \hat{,} \hat{o} \hat{A} \hat{,} \hat{O}$
 $\hat{I} \hat{E} \hat{A} \hat{C} \hat{,} \hat{I} \hat{,} \hat{I} \hat{,} \hat{o} \hat{A} \hat{A} \hat{i} \hat{I} \hat{,} \hat{o} \pm \hat{E} \hat{,} \hat{C} \hat{U} \hat{A} \hat{,} \hat{O} \hat{E} \hat{o} \hat{o}.$ $\underline{F}_1, \underline{F}_2, \dots, \underline{F}_i, \dots, \underline{F}_n$ $\pm \hat{y} \hat{E} \hat{,} \hat{O} \hat{,} \hat{C} \hat{o} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{,} \hat{u}$
 $\underline{P}_1, \underline{P}_2, \dots, \underline{P}_i, \dots, \underline{P}_n$ $\pm \hat{y} \hat{E} \hat{,} \hat{D} \hat{u} \hat{C} \hat{,} \hat{C} \hat{o} \hat{,} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{,} \hat{o}.$

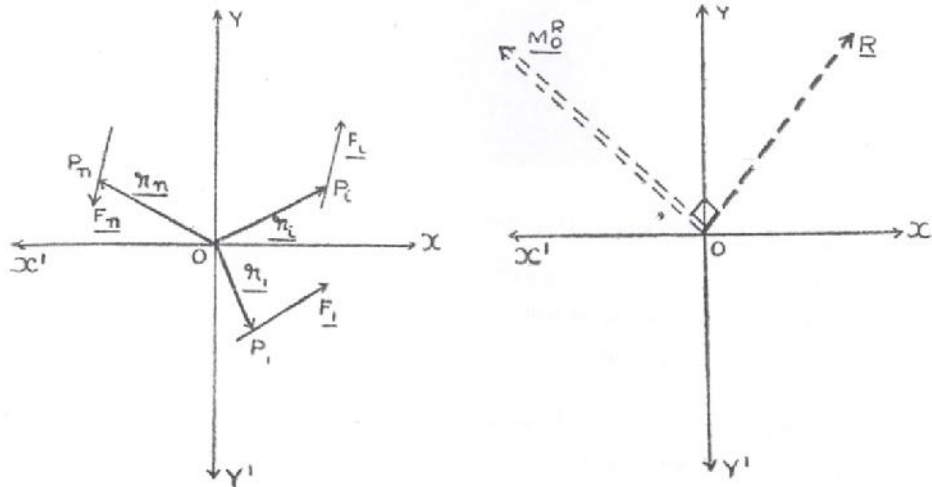
$\hat{O} \pm \hat{y} \hat{A} \hat{D}$ « $\hat{u} \hat{A} \hat{C} \hat{,} \hat{o} \hat{,} \hat{C} \hat{y} \hat{,} \hat{C} \hat{o} \hat{,} \hat{O} \hat{u} \hat{C} \hat{,} \hat{A} \hat{i} \hat{S} \hat{U} \hat{,} \hat{A} \hat{i} \hat{O} \hat{,} \hat{D} \hat{u} \hat{C} \hat{,} \hat{A} \hat{i} \hat{,} \hat{o} \hat{I} \hat{,} \hat{o}.$

$\hat{A} \hat{,} \hat{o} \hat{,} 2.10 \hat{o} \hat{,} \hat{o} \hat{,} \hat{o} \hat{E} \hat{A} \hat{A} \hat{i} \hat{U} \hat{,} \hat{O} \hat{,} \hat{A} \hat{o} \hat{,} \hat{D} \hat{A} \hat{i} \hat{,} \hat{o} \hat{D} \hat{u} \hat{C} \hat{,} \hat{A} \hat{i} \hat{,} \times \hat{o}, \hat{O} \hat{,} \hat{A} \hat{E} \hat{C} \hat{S} \hat{A}$
 $\hat{x}' \hat{o} \hat{x}, \hat{y}' \hat{o} \hat{y} \hat{,} \hat{y} \hat{U} \hat{o} \hat{,} \hat{I} \hat{,} \hat{I} \hat{,} \hat{o} \hat{D} \hat{i} \hat{S} \hat{,} \hat{I} \hat{,} \hat{,} \hat{C} \hat{i} \hat{,} \hat{C} \hat{,} \hat{I} \hat{,} \hat{A} \hat{C} \hat{,} \hat{I} \hat{,} \hat{I} \hat{,} \hat{C} \hat{i} \hat{,} \times \hat{o} \hat{,} \hat{I} \hat{,} \hat{u} \hat{,}.$

$\underline{P}_1, \underline{P}_2, \dots, \underline{P}_i, \dots, \underline{P}_n$ $\pm \hat{y} \hat{A} \hat{E} \hat{A} \hat{u} \hat{E} \hat{y} \hat{,} \hat{C} \hat{,} \hat{A} \hat{o} \hat{,} \hat{A} \hat{C} \hat{,} \hat{,} \hat{C} \hat{,} \underline{r}_1, \underline{r}_2, \dots, \underline{r}_i, \dots, \underline{r}_n$
 $\pm \hat{E} \hat{i} \hat{,} \hat{I} \hat{,} \hat{u} \hat{,}.$

$\hat{O} \hat{,} \hat{A} \hat{y} \hat{,} \hat{A} \hat{E} \hat{C} \hat{S} \hat{A} \hat{,} \underline{F}_i \hat{,} \hat{A} \hat{C} \hat{E} \hat{D} \hat{,} \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{,} \hat{o} \hat{,} \hat{S} \hat{,} \hat{o} \hat{E} \hat{u} \hat{i} \hat{,} \hat{p} \hat{,} 1/2 \hat{A} \hat{i} \hat{,} \hat{A} \hat{,} \hat{A} \hat{o} \hat{o}$

$\hat{S} \hat{,} \hat{o} \hat{E} \hat{o} \hat{A} \hat{,} \hat{o} \hat{,} 2.10 \hat{o} \hat{,} \hat{o} \hat{,} \hat{o} \hat{E} \hat{A} \hat{A} \hat{i} \hat{U} \hat{,} \underline{F}_i, -\underline{F}_i \hat{,} \hat{y} \hat{U} \hat{o} \hat{,} \hat{o} \hat{A} \hat{U} \hat{o} \hat{,} \pm \hat{C} \hat{o} \hat{O} \hat{A} \hat{i} \hat{E} \hat{,} \hat{A} \hat{C} \hat{,} \hat{o} \hat{,} \hat{,} \hat{C}$
 $\hat{z} \hat{u} \hat{A} \hat{i} \hat{,} \hat{o} \hat{D} \hat{,} \hat{p} \hat{,} \hat{A} \hat{,} \hat{u} \hat{,} \hat{S} \hat{A} \hat{S} \hat{z} \hat{,} \hat{i} \hat{,} \hat{S} \hat{,} \hat{o} \hat{E} \hat{o} \hat{,} \hat{o} \hat{A} \hat{U} \hat{o} \hat{,} \pm \hat{C} \hat{o} \hat{O} \hat{A} \hat{i} \hat{,} \hat{p} \hat{o} \hat{o} \hat{A} \hat{i} \hat{,} \hat{p} \hat{A} \hat{u} \hat{E} \hat{y}$
 $\hat{I} \hat{,} \hat{I} \hat{,} \hat{A} \hat{A} \hat{y} \hat{,} \hat{I} \hat{E} \hat{C} \hat{,} \hat{I} \hat{,} \hat{o}.$ $\hat{,} \hat{S} \hat{A} \hat{p} \hat{,} \hat{A} \hat{C} \hat{,} \hat{A} \hat{C} \hat{,} \hat{A} \hat{,} \hat{o} \hat{,} \hat{A} \hat{i} \hat{O} \hat{C} \hat{y} \hat{,} \hat{o} \hat{A} \hat{C} \hat{,} \hat{A} \hat{,} \hat{A} \hat{o} \hat{A} \hat{i} \hat{o} \hat{A} \hat{C} \hat{o} \hat{,} \hat{A}.$



À¼õ 2-10

±ÉŞÅ P_i Å¸ | °ÄüÄÎ õ $\frac{F_i}{r_i}$ ±ý Û õ Å¸ °ÄüÄÎ õ $\frac{F_i}{r_i}$ ±ý Û õ
 Å¸ °ÄüÄÎ õ « òÐ¼ý 'ÖÄ¸, « °ÄüÄÎ õ $\frac{r_i \wedge F_i}{r_i^3}$ « ÇÅ¸ ¼Öòòò¼È° È õ | ÄÜÈ
 $\frac{F_i}{r_i}, -\frac{F_i}{r_i}$ ±ý Û õ 'ÖÄ¸ ½ìì õ °ÄüÄÎ õ.

þíì $\frac{F_i}{r_i}$ ±ý ÄÐ Å¸ °ò | ¼ìì ¼ÄÖÜç ¼¼¼Ä | ¼¼¼Ö Å¸ °ÄüÄÎ õ
 Ì ÈòÄ¼¼¼, þùÄ¼¼¼ | °ÄüÄÎ õ ¼¼¼ÄÖÜç 'ù | Ä¼¼¼ Å¸ °ÄüÄÎ õ | Ä¼¼¼ÖÐð.
 ±ÉŞÅ Å¸ °ò | ¼ìì ¼ÄÖÜç 'ù | Ä¼¼¼ Å¸ °ÄüÄÎ õ, ÖÄý ÅÆÇÅ | °ÄüÄÎ õ
 °ÄüÄÎ õ Å¸ °ÄüÄÎ õ, « òÐ¼ý ÜÈÄÍÆÄ¸ ½Ä¼¼, ×õ « °ÄüÄÎ õ, Ä¼¼¼.

$$\pmÉŞÅ \quad \left\{ P_1 \text{ Å¸ | °ÄüÄÎ õ Å¸ °ÄüÄÎ õ } \frac{F_1}{r_1}, \right.$$

$$P_2 \text{ Å¸ | °ÄüÄÎ õ Å¸ °ÄüÄÎ õ } \frac{F_2}{r_2},$$

$$P_i \text{ Å¸ | °ÄüÄÎ õ Å¸ °ÄüÄÎ õ } \frac{F_i}{r_i},$$

$$\left. P_n \text{ Å¸ | °ÄüÄÎ õ Å¸ °ÄüÄÎ õ } \frac{F_n}{r_n} \right\} \rightarrow \text{ÅÄÜÈ¼¼ Å¸ °ÄüÄÎ õ, } \text{ÅÄÜÈ¼¼ Å¸ °ÄüÄÎ õ}$$

Å¸ °ò | ¼ìì ¼ÄÖÜç, Å¸ °ÄüÄÎ õ

$$\text{ÅÆÇÅ | °ÄüÄÎ õ } \frac{F_1 + F_2 + \dots + F_i + \dots + F_n}{r} = \underline{R} \quad \pmý È \quad | ¼ìì \text{ ÄÄý}$$

Å¸ °ÄüÄÎ õ,

« òð¼ý §Áüì ÈòÀçð¼ ÍÆÄç ½òðð ¾Èý Çý ÌÈÄÄø

ÜðÏ ò¼j'' Æð ¾Ïððð¾ÈÉ j × ¼Ä $\underline{M}_o^R = \sum_{i=1}^n \underline{r}_i \wedge \underline{F}_i$ ±ý Ûð ÷Ï
¼j Ì ÄÄý ÍÆÄç ½ì Ì ò (resultant couple) °ÁÄj Ì ò.

þí Ì \underline{R} ±ý Àð xoy ¾Çð¾Ïð \underline{M}_o^R ±ý Àð xoy ¾Çð¾Ï Ì
|óì ð¼jÉ ¾ç °ÄÏð | °ÄüÄ Ä¾jø « '' Ä'' Ç Ä'' ÄÄÜì Ì ò ¾ç °Ä Ç ü
ýÜì | jýÜ |óì ð¼jÉ ¾ç ° Çø | °ÄüÄ ò.

±É §Ä {F_i} = 1, 2, n ±ý Ûð ÷Ï ¾ÇÄç òð¼j Ì ¾ç « ð¾Çð¾§Ä

Äj §¾Û | Äj Ò Ò ±ý Ûð $\underline{M}_o^R = \sum_{i=1}^n \underline{r}_i \wedge \underline{F}_i$ òüÇÄø | °ÄüÄ ò ÷Ï ¾ÉÄç ° \underline{R}

¼ × ò, « òð¼ý §ð÷ó¼ ¾Ïððð¾Èý ¼ × ¼Ä ÷Ï ÍÆÄç ½Äj × ò
÷ì Ì ò. §ÄÏð « ò¼j Ì ¾ç ÷Ï ¾ÉÄç °Äj §Äj « øÄð ÷Ï
¾ÉÄç ÍÆÄç ½Äj §Äj ÷ì Ì òÄ¼ì ÜÏ ò ±ý Ûð jð¼Äj ò.

±ÉýÈjø ¾ÉÄç ° $\underline{R} = 0$ ±ýÈj ò §Äjð ±Ï ð¾Ç Äç òð¼j Ì ¾ç

\underline{M}_o^R ±ý Ûð ÷Ï ÍÆÄç ½Äj ÷ì Ì ò. $\underline{M}_o^R = 0$ ±ýÈj ò ±Ï ð¾Ç

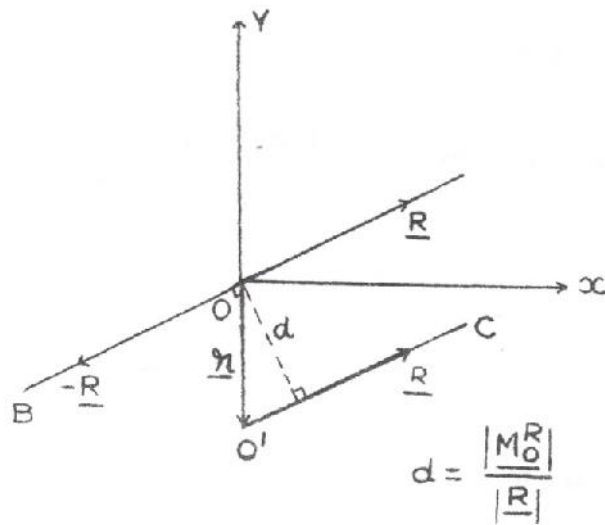
¾ÇÄç òð¼j Ì ¾ç ÷Ï ¾ÉÄç Äç ° \underline{R} ¼ ÷ì Ì ò. $\underline{R} \neq 0, \underline{M}_o^R \neq 0$ ±Éø
« ò¼j Ì ¾ç ÷Ï ¾ÉÄç òì ÷ì Ì | ÁÉì jð¼Äj ò.

÷Ï ðÈÜì òÄj ÒÇý Áð §¾Çð¾§Ä | °ÄüÄ ÇýÈ ÷Ï ¾ÉÄç ðð
÷Ï ÍÆÄç ½ðð §ð÷óð °Äç Ä'' Ä'' ñ Ì Äñ ½jð. ¼Éjø « Ä'' È
Óó¾Ä¾ç òì þ'' ½ÄjÉ ¾ç °Ä§Ä | °ÄüÄ ÇýÈ ÷Ï ¾ÉÄç òì Ì °ÁÄj
ÄjüÈÓÈð.

þ'' ¾ çÜÄ \underline{M}_o^R ±ýÈ ÍÆÄç ½'' Ä, ÷üÄjýÜð R « Ç × üÇ þÏ

°ÄÛ | Ä¾ÏÄjÉ ($\underline{R}_i, -\underline{R}$) ±ý Ûð Äç ° Çì | jñ Ì, ýÜ \underline{R}_y ¾ç òì

§ç | Ä¾Äj Ä¼ð 2.11 ø



À¼õ 2-11

s; ðÉÁÁ; Ú OB ÁÆÁ; xõ, o'c Áü|È; ýÚ ÁÆÁ; xõ |°ÁøÁÎ õ
 ÍÆÁ; ½Á; ø Á; üÈË |°õ. píl oc ±ýÚõ s; jÎ, $\frac{M_o^R}{|R|}$ Áý ÎÈ s; ùÁ
 OB Î ÁÁ; sÁ; « øÄÐ p¼Á; sÁ; « ÁóÐ OB, O'C p¼Á; Áóõ
 |°Í ÎðÐ ð¼; Áx = $\frac{|M_o^R|}{|R|}$ - s; çÚÁøÁÎ õ. O Áø |°ÁüÁÎ õ Á; õ; ù
 ý È; Á; ýÚ °ÁøÁÎ ð¼; |; ùÁ¼; ø, O' pø O'C ÁÆÁ; |°ÁüÁÎ õ $\frac{R}{|R|}$
 ±ýÚõ ¾ÉÁ; °SÁ ±í °Öüç¼; Î õ. $\frac{R, M_o^R}{|R|}$ - ÁüÈý Á; çx; ç; ð
 ; Î ¾ø:

$$\underline{F}_i = F_{ix} \underline{i} + F_{iy} \underline{j}$$

$$\underline{r}_i = x_i \underline{i} + y_i \underline{j}$$

$$\therefore \underline{R} = \sum_{i=1}^n \underline{F}_i$$

« ¾; ÁÐ

$$R_x \underline{i} + R_y \underline{j} = \sum_{i=1}^n (F_{ix} \underline{i} + F_{iy} \underline{j})$$

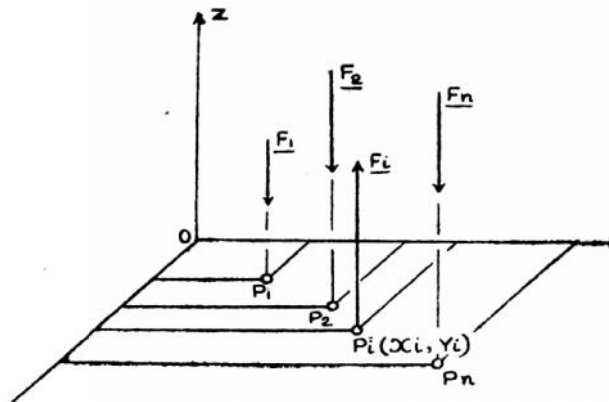
$$= \left(\sum_{i=1}^n F_{ix} \right) \underline{i} + \left(\sum_{i=1}^n F_{iy} \right) \underline{j}$$

$\vec{r}_i = \vec{r}_i \cdot \vec{e}_i$

$\vec{M}_O = \sum_{i=1}^n \vec{r}_i \wedge \vec{F}_i$

$\vec{M}_O = \sum_{i=1}^n (\vec{r}_i \wedge \vec{F}_i)$

$\vec{M}_O = \sum_{i=1}^n (\vec{r}_i \wedge \vec{F}_i)$



À¼õ 2-12

$\vec{R} = \vec{F}_1 + \vec{F}_2 + \dots + \vec{F}_i + \dots + \vec{F}_n$

$\vec{M}_O = \sum_{i=1}^n \vec{r}_i \wedge \vec{F}_i$

$\vec{M}_O = \sum_{i=1}^n \vec{r}_i \wedge \vec{F}_i$

$$\text{pí l } \underline{R} = \sum_{i=1}^n F_i = \sum_{i=1}^n F_i \underline{k} = \left(\sum_{i=1}^n F_i \right) \underline{k} \quad \text{— l } \circ.$$

$$\begin{aligned} \underline{M}_0^R &= \sum_{i=1}^n \underline{r}_i \wedge \underline{F}_i = \sum_{i=1}^n (x_i \underline{i} + y_i \underline{j}) \wedge (F_i \underline{k}) \\ &= \sum_{i=1}^n (-x_i F_i) \underline{j} + \sum_{i=1}^n (y_i F_i) \underline{i} \\ &= \sum_{i=1}^n (y_i F_i) \underline{i} + \sum_{i=1}^n (x_i F_i) \underline{j} \quad \text{— l } \circ. \end{aligned}$$

±ÉŞÅ \underline{R} ±ýÀÐ \underline{k} ±ýÛõ µÄÄl ¼c° ÆÄÖõ, \underline{M}_0^R ±ýÀÐ XOY ¼Çð¼Öõ
 |°ÄüÄl Å¼jø « ° Ä, ü ýÚl |, jýÚ |°í l ð¼jÉ ¼c° °, Çø
 |°ÄüÄl Å¼j l õ.

— ¼Äjø p° ½ Äc° ð¼j l ¼c° ý° È, ÄjŞ¼Ûõ °Ï O ±ýÛõ
 ðüÇÄø °Äjð¼ÄÄj, î |°ÄüÄl õ °Ï ¼ÉcÄc° ° \underline{R} —, ×õ, « ðÐ¼ý °ÖÄj,
 p° ½ Äc° °, Ûl l î |°í l ð¼j, « ° ÄÖõ ¼Çð¼Öõ |°ÄüÄl õ °Ï
 ÍÆÄc° ½Äj, ×õ °Í l, ÓÉÖõ.

¼ÉcÄc° ° $\underline{R}=0$ ±Éø, p° ½ Äc° ð¼j l ¼c° \underline{M}_0^R ±ýÛõ °Ï
 ÍÆÄc° ½Äj l õ.

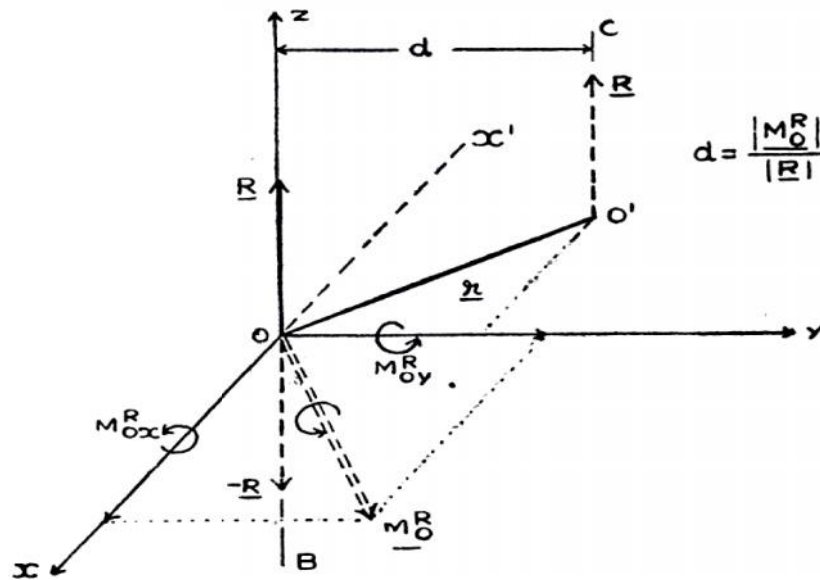
$\underline{M}_0^R=0$ ±Éø p° ½ Äc° ð¼j l ¼c° °Ï ¼ÉcÄc° ° R —, °Í l l õ.

$\underline{R} \neq 0, \underline{M}_0^R \neq 0$ ±Éø, « ùÄc° ½ð¼j l ¼c° °Ï ¼ÉcÄc° °í l °Í l l õ ±Él
 , jð¼Äjõ.

p° ¼ ÇÜÄ, Ó¼Äø \underline{R} ±ýÀÐ, z « °ý ÄÆŞÄ |°ÄüÄl Å¼j, ×õ,

\underline{M}_0^R ±ýÛõ ÍÆÄc° ½ XOY ¼Çð¼Öõ ÄÄ¼j, ×õ |, jüÇ×õ.

\underline{M}_0^R ±ýÛõ ÍÆÄc° ½ °Ä, °üÄjýÚõ \underline{R} « Ç×üÇ pÕ °ÄÛ |Ä¼ÖÄjÉ
 ($\underline{R}, -\underline{R}$) ±ýÛõ Äc° °, °Çl |, jñ Î, ýÚ \underline{R} ý ¼c° °í l Ş¼Ä¼Äj, Ä¼õ
 2.13ø , jðÉÄÄjÜ OB ÄÆÄj, ×õ ÄüÈjýÚ O'C ÄÆÄj, ×õ |°ÄüÄl õ
 ÍÆÄc° ½Äjø ÄjüÈÍ |°õ.



À¼õ 2-13

pıı 0'C ±y Üõ ş,ıı $\frac{M_o^R}{R}$ Äy İÈŞ,üÀ z «ıııı pıı ½Äı, Äı, ð¼ıı °ÄŞÄı «øÄĐ İı Èxð¼ıı °ÄŞÄı «ıı ÁóĐõ, OB 0'C, Üıı pıı ¼ÄÄı ÄÖõ |ıı İðĐı¼ıı Äx = $\frac{|M_o^R|}{|R|}$ ı, pÖıı ÄıÜõ çÜÄöÄı õ. Ö Äø |°ÄüÄı õ Äı, üı yı ÈıÄıyÜ °ÄöÄı ð¼ıı |ıı üÄ¼ıø 0' Äø, 0'C ÄÈÄı,ıı |°ÄüÄı õ R ±y Üõ ¼ÉÄıı °ŞÄıı °ÖüÇ¼ıı õ.

$R, \frac{M_o^R}{R}$ ı, ÄÄüÈy Äı,ıı Çı,ıı ¼ø:

$$\underline{F}_i = F_i \underline{k}$$

$$\therefore R_i = \sum_{i=1}^n F_i = \sum_{i=1}^n F_i \underline{k}$$

«¼ıı ÄĐ $R \underline{k} = \left(\sum_{i=1}^n F_i \right) \underline{k}$

$$\therefore R = \sum_{i=1}^n F_i \quad \text{ıı õ.}$$

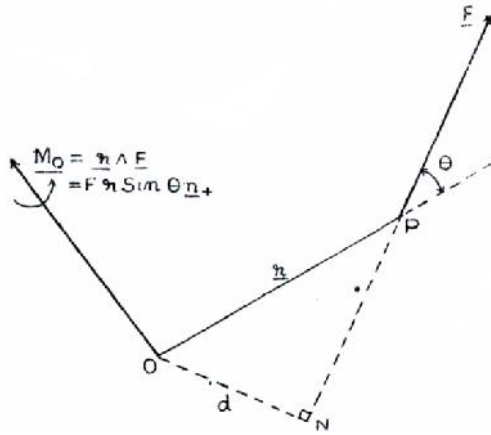
$\vec{r} = x\vec{i} + y\vec{j} + z\vec{k}$
 $\vec{F} = F_x\vec{i} + F_y\vec{j} + F_z\vec{k}$
 $\vec{M}_O = \vec{r} \times \vec{F} = (yF_z - zF_y)\vec{i} + (zF_x - xF_z)\vec{j} + (xF_y - yF_x)\vec{k}$

2.7 Moment of a force about a point

$\vec{M}_O = \vec{r} \times \vec{F}$
 $M = rF \sin \theta$

$\vec{M}_O = \vec{r} \times \vec{F}$
 $M = rF \sin \theta$

$M = Fd$



À¼õ 2-32

\underline{n} ±ýÀÐ (O,F) ¼Çò¼üì ŞÁøŞçìì ,ÇÁ |°í ì ò¼j É ¼ç° °° Â « ÈÇÁü ì õ µÄÄì ¼ç° °Äç ±ýÈjø

$$M_o = F \cdot d \underline{n} \text{ -- } \text{ì } \text{õ}.$$

2.7.1 ¼ç° °Äç, Çüý ì Üì ì õ | ÀÕì , ÇÁjø ¼Öò¼É°° É Á° ÄÄÜò¼ø

\underline{F} ±ýÈ Áç° ° |°ÄüÄî õ Şç÷Şçj ðÈø À¼õ 2.16ø ,j ðÈÄjÁÜ P ±ýÈ ²¼jÁ |¼j Õ òüÇç° Ä ±î ì , ×õ. P ý çç° Äò¼ç° °Äç° Ä $\underline{OP} = \underline{r} \pm \text{ýÈ} \text{ì } \text{,j} \text{üÇ} \times \text{õ}$ ($\underline{OP}, \underline{F}$) -- , ÇÄüÈüì p° ¼ÄÇÄ°° ÁÕõ ì Üí Şçj ½ò°° ¼ , ±Éì ì Èü , ×õ.

ÕÄÇÖóÐ \underline{F} ì ì ON ±ýÈ |°í ì ðÐì Şçj ð°° ¼ Ä° ÄÄ ×õ $ON = d = r \sin \theta$, -- ì õ.

$$\therefore \underline{M}_o = Fr \sin \theta \underline{n} \pm \text{ýÈ} \text{ì } \text{õ}.$$

$\underline{F}, \underline{r}$ -- , ÇÄüÈüý ì Üì ì õ | ÀÕì , çç° Ä ±î ð¼ç¼ $\underline{r} \wedge \underline{F} = Fr \sin \theta \underline{n} \pm \text{ýÈ} \text{ì } \text{õ}$, ¼Öò¼É°° ý ¼ç° °Äç° Ä (Vector Moment) $\underline{r}, \underline{F}$ -- , ÇÄüÈüý ì Üì ì õ | ÀÕì , çç° « ÈÇÁü , ÈÐ -- ì õ.

¼Öò¼É°° ý |°ÄüÄî õ Şçj ð°° ¼ « î°jì |çjñ î |ÄjÕü (O,F) ¼Çò¼üì ÍÆÖ, ÈÐ. « üÄ¼ ÍÆüç p¼òðÈ « øÄÐ ÄÄòðÈî ÍÆüç°° Äò |ÄüÈÇöÄÐ ($\underline{r}, \underline{f}, \underline{n}+$) ±ýÄ°° Ä °õ p¼î ÍÆç « øÄÐ ($\underline{F}, \underline{M}, \underline{n}-$) ±ýÄ°° Ä °õ ÄÄî ÍÆç « °° Äò° Ä ŞÄü |çjüÄ°° ¼ °j÷óÐüÇÐ. pí ì $\underline{n}-$ ±ýÀÐ (O,F) ¼Çò¼üì ì , üŞçìì , ÇÁ |°í ì ðÐò ¼ç° °° Ä « ÈÇÁü ì õ µÄÄì ¼ç° °Äçjì õ. ŞÁÕõ \underline{F} |°ÄüÄî õ Şçj ðÈø P' ±ýÈ Äü |Èj Õ

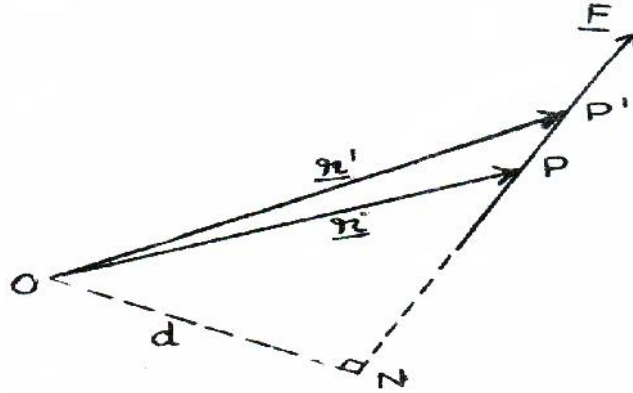


Fig. 2-16

Let $\mathbf{r}' = \mathbf{r} + \mathbf{PP}'$ and $\mathbf{r}' \wedge \mathbf{F} = (\mathbf{r} + \mathbf{PP}') \wedge \mathbf{F}$. Then

$$\mathbf{r}' = \mathbf{r} + \mathbf{PP}'$$

$$\mathbf{r}' \wedge \mathbf{F} = (\mathbf{r} + \mathbf{PP}') \wedge \mathbf{F}$$

$$= \mathbf{r} \wedge \mathbf{F} + \mathbf{PP}' \wedge \mathbf{F}$$

$$= \mathbf{r} \wedge \mathbf{F}$$

$$= \mathbf{M}_O$$

$$\mathbf{PP}' \wedge \mathbf{F} = 0$$

$$\mathbf{r}' \wedge \mathbf{F} = \mathbf{r} \wedge \mathbf{F}$$

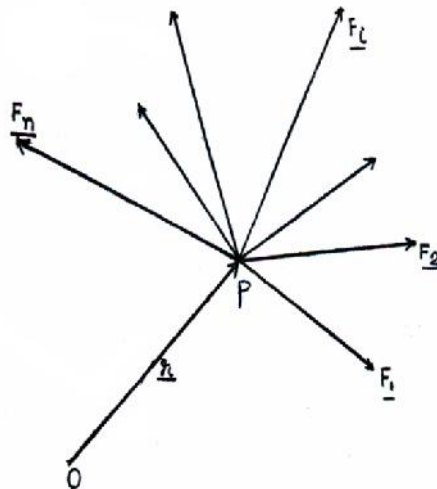
The vector \mathbf{PP}' is perpendicular to the line of action of \mathbf{F} . Therefore, $\mathbf{PP}' \wedge \mathbf{F} = 0$. This result is independent of the choice of the reference point O . The vector \mathbf{r}' is called the sliding vector.

Let $\mathbf{r}' = \mathbf{r} + \mathbf{PP}'$ and $\mathbf{r}' \wedge \mathbf{F} = (\mathbf{r} + \mathbf{PP}') \wedge \mathbf{F}$. Then $\mathbf{r}' \wedge \mathbf{F} = \mathbf{r} \wedge \mathbf{F} + \mathbf{PP}' \wedge \mathbf{F}$. Since \mathbf{PP}' is perpendicular to the line of action of \mathbf{F} , $\mathbf{PP}' \wedge \mathbf{F} = 0$. Therefore, $\mathbf{r}' \wedge \mathbf{F} = \mathbf{r} \wedge \mathbf{F}$. The vector \mathbf{r}' is called the sliding vector. The dimensions of $\mathbf{r}' \wedge \mathbf{F}$ are $[FL]$. The vector \mathbf{r}' is perpendicular to the line of action of \mathbf{F} . Therefore, $\mathbf{r}' \wedge \mathbf{F} = r' F \sin 90^\circ = r' F$.

2.8 Áííí ÉÉý §¼ÛË (Varignon's Theorem)

ÁÁó¼; ÁÇÁÏ Ò ÒÛÇÁÏ | °ÄÜÁÏ ò ,½Á' °, Çý (Set of Concurrent Forces) ¼ÛËË¼ËÉý ¼ÛËË¼ËÉý Ò ÒÛÇÁÏ | °ÄÜÁÏ | ÒÛÇÁÏ ±Í ò ,òÄ¼íø « ¼ý |¼í ÁÁý Á' °Áý ¼ÛËË¼ËÉÛÏÏ î°ÁÁí ò

$\underline{F}_1, \underline{F}_2, \dots, \underline{F}_i, \dots, \underline{F}_n$ ±ýÄ' Á Á¼Ë 2.17 , ðÉÁÉ P ±ýË ÒÛÇÁÏ | °ÄÜÁÏ Á¼í, ò |¼Û×Ë.



Á¼Ë 2-17

ò ±ýË , ð¼' Áòò ÒÛÇÁÏ ,½Á' °, Çý ¼ÛËË¼ËÉý §¼' ÁòÁ Á¼í, ò |¼Û×Ë.

$\underline{F}_1, \underline{F}_2, \dots, \underline{F}_i, \dots, \underline{F}_n$ ±ýË Á' °, Û P Áý ÁÉ§Á | °ÄÜÁÏ Á¼íø « ' Á, Çý |¼í ÁÁý Á' °Ë, þ' ½, Á Á¼ËËÉ « òòÛÇÁý ÁÉ§Á | °ÄÜÁÏ ò. \underline{R} ±ýÄ ò,½Á' °, Çý |¼í ÁÁý Á' °' Áí Ì ÈÏÏ | ÁýËø,

$$R = \underline{F}_1 + \underline{F}_2 + \dots + \underline{F}_i + \dots + \underline{F}_n \quad \text{Ì ò.}$$

±É §Á P ±ýË ÒÛÇÁÏ ,½Á' °, Çý ¼ÛËË¼ËÉý , ÛÏÏ - íÄ ÜÏ ¼ø

$$= \underline{r} \wedge (\underline{F}_1 + \underline{F}_2 + \dots + \underline{F}_i + \dots + \underline{F}_n)$$

$$= \underline{r} \wedge (\underline{F}_1 + \underline{F}_2 + \dots + \underline{F}_i + \dots + \underline{F}_n),$$

(Ì ÜÏ , ò | ÁÏÏ , ÇÁí , ðÏ Á¼í Ì þ' °òòÛÇ¼íø)

$$= \underline{r} \wedge \underline{R}$$

= òø |¼í ÁÁý Á' °Áý ¼ÛËË¼ËÉÉí ò.

$\vec{r} = x\vec{i} + y\vec{j} + z\vec{k}$

2.8.1 $\vec{r} = x\vec{i} + y\vec{j} + z\vec{k}$ (Rectangular Components of Moment)

$\vec{M}_O = \vec{r} \times \vec{F}$

$\vec{M}_O = M_x\vec{i} + M_y\vec{j} + M_z\vec{k}$

$\vec{r} = x\vec{i} + y\vec{j} + z\vec{k}$

$$\vec{r} = x\vec{i} + y\vec{j} + z\vec{k}$$

$$\vec{F} = F_x\vec{i} + F_y\vec{j} + F_z\vec{k}$$

$$\vec{M}_O = \vec{r} \times \vec{F}$$

$\vec{M}_O = M_x\vec{i} + M_y\vec{j} + M_z\vec{k}$

$$\vec{M}_O = \vec{r} \wedge \vec{F}$$

$$= \begin{pmatrix} \vec{i} & \vec{j} & \vec{k} \\ x & y & z \\ F_x & F_y & F_z \end{pmatrix}$$

$$= (yF_z - zF_y)\vec{i} - (xF_z - zF_x)\vec{j} + (xF_y - yF_x)\vec{k}$$

$$= (yF_z - zF_y)\vec{i} - (zF_x - xF_z)\vec{j} + (xF_y - yF_x)\vec{k}$$

$$\vec{M}_O = M_x\vec{i} + M_y\vec{j} + M_z\vec{k}$$

$$M_x = yF_z - zF_y$$

$$M_y = zF_x - xF_z$$

$$M_z = xF_y - yF_x$$

$\vec{M}_O = M_x\vec{i} + M_y\vec{j} + M_z\vec{k}$

$\vec{F} = F_x\vec{i} + F_y\vec{j} + F_z\vec{k}$

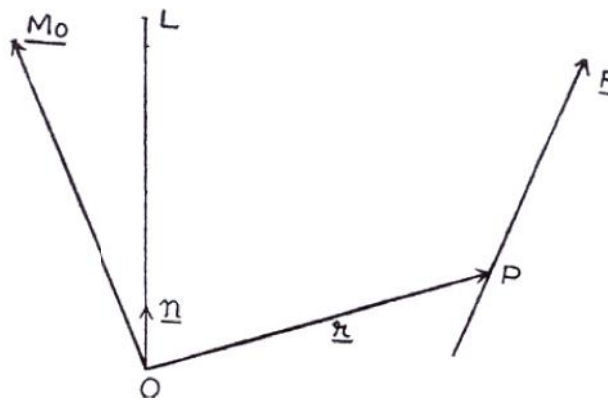
$$\vec{M}_O = (xF_y - yF_x)\vec{k}$$

$\mu = \frac{M_{OL}}{M_0} = \frac{\mathbf{n} \cdot (\mathbf{r} \wedge \mathbf{F})}{|\mathbf{r} \wedge \mathbf{F}|}$

2.9 $\mu = \frac{M_{OL}}{M_0} = \frac{\mathbf{n} \cdot (\mathbf{r} \wedge \mathbf{F})}{|\mathbf{r} \wedge \mathbf{F}|}$

$\mu = \frac{M_{OL}}{M_0} = \frac{\mathbf{n} \cdot (\mathbf{r} \wedge \mathbf{F})}{|\mathbf{r} \wedge \mathbf{F}|}$

$M_{OL} = \mathbf{n} \cdot (\mathbf{r} \wedge \mathbf{F}) = n_x(yF_z - zF_y) + n_y(zF_x - xF_z) + n_z(xF_y - yF_x)$



À¼õ 2-18

$M_{OL} = \mathbf{n} \cdot (\mathbf{r} \wedge \mathbf{F}) = n_x(yF_z - zF_y) + n_y(zF_x - xF_z) + n_z(xF_y - yF_x)$

$$\therefore M_{OL} = \mathbf{n} \cdot (\mathbf{r} \wedge \mathbf{F})$$

$$= \mathbf{n} \cdot (\mathbf{r} \wedge \mathbf{F})$$

$$= \begin{pmatrix} n_x & n_y & n_z \\ x & y & z \\ F_x & F_y & F_z \end{pmatrix}$$

$$= n_x(yF_z - zF_y) + n_y(zF_x - xF_z) + n_z(xF_y - yF_x) \quad \text{ñ ò.$$

2.10.1 ĐÁi ̣òòúÇṭĀø ÍÆÄċ̣ 1/2òò3/4Ẹ̀ Ēì ̣jĭ 3/4ø

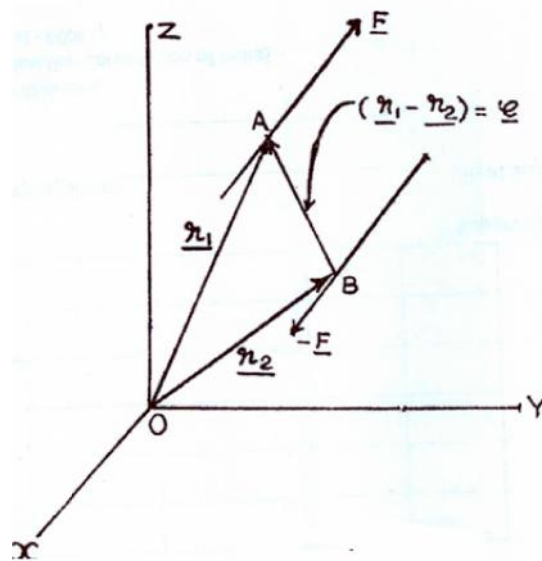
O ±ýÈ òòúÇṭĀ ð ĐÁi ̣òòúÇṭĀj̣i ĩ ̣j̣iñ 1/4 ̣j̣iđ 1/4 ĀòĀṭø
 ÍÆÄċ̣ 1/2ì ĩ ĩĀ pŌĀċ̣ ò ̣ú {F, -F} ĩ °ĀüĀĭ ò Ṣjĭĭ ̣Çṭø Ó ĒÈŞĀ A, B
 ±ýÈ 2Ş3/4Ū ò òòúÇṭj̣ Ċ Ā1/4ø 2.20 ̣j̣iđĒĀĭŪ r₁, r₂ ±Éì ĩ ̣j̣iŪÇxõ.

$$\underline{BA} = \underline{OA} - \underline{OB}$$

$$= \underline{r}_1 - \underline{r}_2$$

$$= \underline{\Phi} \pm \text{Éì ĩ ̣j̣iŪÇxõ.}$$

ĐÁi ̣òòúÇṭø Āċ̣ ò ò3/4Ō ò ò 3/4Ẹ̀ý ̣Çṭý Ūĭ 3/4ø.



Ā1/4ø 2-20

$$\underline{M} = \underline{r}_1 \wedge \underline{F} + \underline{r}_2 \wedge (-\underline{F})$$

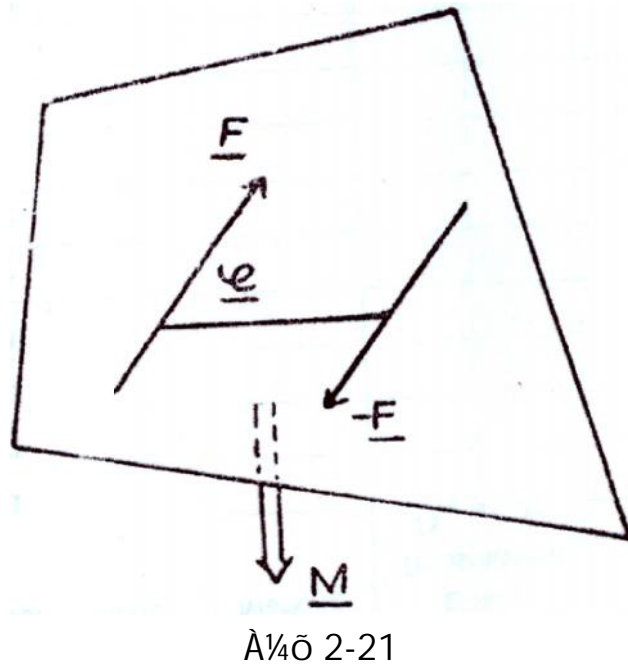
$$= \underline{r}_1 \wedge \underline{F} - \underline{r}_2 \wedge \underline{F}$$

$$= (\underline{r}_1 - \underline{r}_2) \wedge \underline{F}$$

$$= \underline{\Phi} \wedge \underline{F} \quad \text{Ē ĩ ò.}$$

ĭ Ūĭ ĩ ò ĩĀŌĭ ̣Çṭ Ċ Ā3/4øĀĒ Ē Ē ±ýĀĐ (̄, F) Ē ̣Āċ̣ Ā Āċ̣ ĀĀŪĭ ĩ ò
 3/4Çò3/4Ūĭ ĩ ĩ ĩ ĩ ò3/4ĭÉ ṢÇĭ ĩ ṢjĭđĒø ĩ °ĀüĀĭ ò. « ĐŞĀ
 ÍÆÄċ̣ 1/2òòð3/4Ẹ̀ Ē Āċ̣ ĀĀŪĭ ĩ ̣ÈĐ.

p[er]pendicular to the axis of rotation. The force F is applied at a distance r from the axis. The moment M is the product of the force and the perpendicular distance from the axis to the line of action of the force. The diagram shows a force F acting on a lever arm of length r at an angle θ to the lever arm. The perpendicular distance from the axis to the line of action of the force is $r \sin \theta$. The moment M is then $M = F r \sin \theta$.



The force F is applied at a distance r from the axis. The moment M is the product of the force and the perpendicular distance from the axis to the line of action of the force. The diagram shows a force F acting on a lever arm of length r at an angle θ to the lever arm. The perpendicular distance from the axis to the line of action of the force is $r \sin \theta$. The moment M is then $M = F r \sin \theta$.

$$|M| = |F| |r| \sin 90^\circ$$

$A_j \cdot \vec{u}_E \ll \dots \vec{A} \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{n} \cdot \vec{A}_j \cdot \vec{u}_E, \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$ (sense) $\rightarrow \vec{A} \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{A} \cdot \vec{A}_j \cdot \vec{u}_E$
 $A_j \times \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$ (equivalent) $\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$

$A_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$
 $\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$

2.11 $\vec{A} \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$ (Equivalence of Couples):

$\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{A} \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$
 $\vec{A} \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$
 $\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$
 $\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$

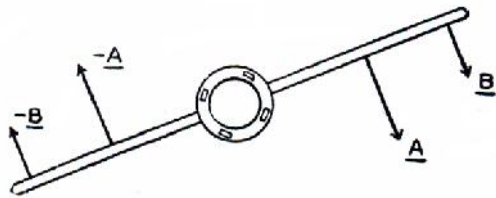
(1) $\vec{A} \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$
 $\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$
 $\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$

(2) $\vec{A} \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$
 $\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$

(3) $\vec{A} \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$
 $\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$
 $\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$

$\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$
 $\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$

$\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$
 $\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$
 $\vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \ll \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E \pm \vec{u}_E \cdot \vec{A}_j \cdot \vec{u}_E$



À¼õ 2-24

$\pm \epsilon \{rA, -rA\} \pm y \in \{ \dots \} \dots 2.25 \epsilon$

$\dots \frac{y}{2} \dots$

$$\frac{1-r}{1} = \frac{\frac{y-d}{2}}{\frac{y}{2}} = \frac{y-d}{y} = 1 - \frac{d}{y}$$

$$\therefore r = \frac{d}{y} \dots y = \frac{d}{r} \dots$$

$\{A, -A\} \pm y \in \{ \dots \} \dots |C| = |A|d \dots$

$\dots \{rA, -rA\} \pm y \in \{ \dots \} \dots$

$$\begin{aligned} r|A|y &= r|A|\frac{d}{r} \\ &= |A|d \\ &= |C| \dots \end{aligned}$$

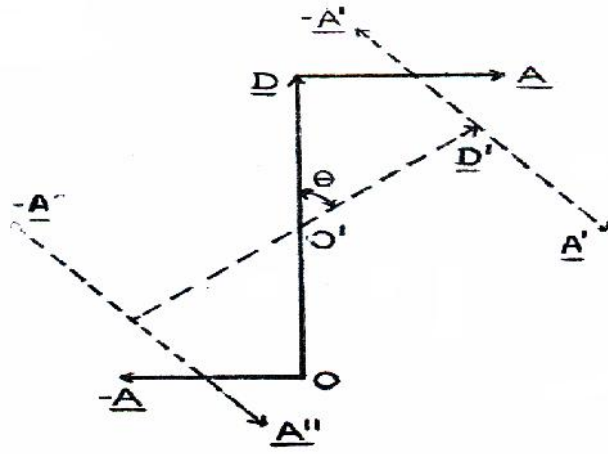
$\dots d \dots \{A, -A\} \pm y \in \dots y = \frac{r}{d} \dots$

$\dots |A|d \dots \dots \dots$

$\{rA, -rA\} \pm y \in \dots$

$\dots \dots \dots \dots \dots \dots \dots \dots \dots \dots \dots$

$\{A, -A\} \pm y \in \dots \dots \dots 2.26 \dots$



À¼õ 2-26

d |¼j¨ ÄÄø « ¨ ÁÔÁjÚ ±Î ì ,xõ. \underline{A} Äý ±ñ Á¼õ¨ ¨ Ä a ±Éì |¼jûÇxõ.
 $(-\underline{A})$ ±ýÈ Ä¨ ¨ |°ÄüÄî õ§,jðÈø, O ±ýÈ òùÇ¨ ¨ Ä ±Î òÐ \underline{A} ±ýÈ
 Ä¨ ¨ òì |°í ò¼j, OD ±ýÈ §,jð¨ ¨ ¼ Ä¨ ¨ Äxõ. \underline{P} Äý ç¨ ¨ Äð¼¨ ¨ ¨ Ä¨ ¨ Ä
 $\underline{OP}=\underline{D}$ ±Éì |¼jûÇxõ. O' ±ýÄÐ OP Äý \underline{P} ¨ ¨ ÄðòùÇ¨ ¨ Äì òÈü, òí õ.
 ±ýÈ ÍÄ¨ ¨ ½ « ¨ ÁÔõ ¼Çð¼ø OP º, O' ±ýÈ òùÇÄø, ¨ « Çxì ò Ì
 ÍÈüÈxõ. « õ§ÄjÐ \underline{D}' ±ýÈ ¼¨ ¨ ¨ Ä, \underline{D} Äý ç,ø§ÄjýÚ « ¨ ÁÔõ. \underline{D} Äý
 Ó¨ ¨ ÈòùÇ, Çø Ó¨ ¨ È§Ä $(\underline{A}',-\underline{A}'),(\underline{A}'',-\underline{A}'')$ ±ýÈ¼¨ ¨ ¨ Ä, ¨ Ç \underline{D}' ±ýÈ ¼¨ ¨ ¨ Ä
 |°ÄüÄî õ §,jðÈü ò ò¼j,xõ, « ¨ Ä, Çý ±ñ Á¼õð,ü a òì ò
 ¨ Äj, þõì ò ÄjÚõ À¼õ 2.26ø ,jðÈÄÄjÚ ±Î ì ,xõ.

$$[(\underline{A}',-\underline{A}'),(\underline{A}'',-\underline{A}'')] \rightarrow \text{ÄüÈý |¼jì ÄÄý ÍÄÄj¼jø,}$$

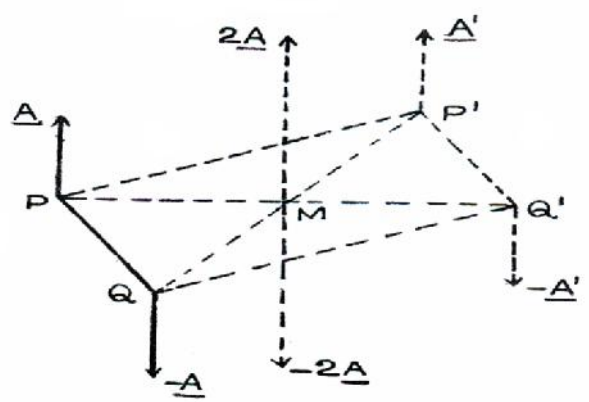
$$= \{(\underline{A},-\underline{A})\} \equiv \{(\underline{A},-\underline{A});(\underline{A}',-\underline{A}');(\underline{A}'',-\underline{A}'')\} \rightarrow \text{ì õ. } \rightarrow \text{Éjø } (\underline{A},-\underline{A});(\underline{A}'',-\underline{A}'')$$

$$\rightarrow \text{ÄüÈý |¼jì ÄÄý Ä¨ ¨ ¨ ü ýÚì |¼jýÚ ±¼±¼Äj, ÍÄ$$

$$§ç:ì §,jðÈø |°ÄüÄî Ä¼jø, [(\underline{A},-\underline{A}');(-\underline{A},\underline{A}'')] \equiv 0 \rightarrow \text{ì õ.}$$

±É§Ä Á¼ÓùÇ Ä¨ ¨ ¨ ü $\{(\underline{A},-\underline{A})\} \equiv \{(\underline{A}'',-\underline{A}'')\} \rightarrow \text{ì õ. } \rightarrow \text{¼Äjø ÍÄÄ¨ ¨ ½Äø}$
 « ¨ ÁÔõ Ä¨ ¨ ¨ Ç → ÄüÈý ¼Çð¼§Ä§Ä ÍÈüÈÄ¼jø
 ÍÄÄ¨ ¨ ½òðð¼Èý Äj¼ç, òÄÄ¼ø¨ ¨ Ä ±ýÈj,ÈÐ. þ¼Äj, $\{(\underline{A},-\underline{A}),(\underline{A}',-\underline{A}')\}$

$\pm y \in p \circ \text{ÍÆÄ} \cdot \frac{1}{2} \cdot \hat{u} \text{ 'ŞÄ ŞÄ}_i \cdot \hat{A}_i \cdot \times \hat{o} \quad |A| = |A'| = a \quad \pm y \hat{u} \hat{o}, \quad \hat{u} \hat{A}_i \hat{O}$
 $\text{ÍÆÄ} \cdot \frac{1}{2} \hat{A} \hat{y} \hat{A} \hat{c} \cdot \hat{o} \cdot \hat{U} \hat{i} \hat{i} \quad p \cdot \frac{1}{4} \hat{A} \hat{c} \hat{A} \cdot \hat{A} \hat{O} \hat{o} \quad | \hat{o} \hat{i} \hat{i} \hat{o} \hat{D} \hat{o} \quad | \frac{3}{4} \hat{i} \cdot \hat{A} \times d \ll \zeta \times$
 $p \hat{O} \hat{o} \hat{A} \frac{3}{4} \hat{i} \cdot \times \hat{o} p \frac{1}{4} \hat{c} \cdot \hat{A} \hat{o} \hat{A} \hat{c} \hat{o} \quad \hat{A} \hat{O} \hat{i} \hat{o} \quad \text{ŞÄÜÄ}_i \hat{i} \cdot \frac{1}{4} \hat{A} \frac{3}{4} \hat{i} \cdot \times \hat{o} \quad \hat{A} \frac{1}{4} \hat{o} \quad 2.27 \hat{o}$
 $\cdot \hat{o} \hat{E} \hat{A} \hat{A} \hat{E} \ll \cdot \hat{A} \hat{A} \hat{O} \hat{i} \hat{o}. \quad \hat{A} \frac{1}{4} \hat{o} \frac{3}{4} \hat{c} \hat{o} \quad P, Q, P', Q' \quad \pm y \hat{A} \cdot \hat{A} \quad \underline{A}, -\underline{A}, \underline{A}' - \underline{A}' \quad M \rightarrow \cdot \hat{A}$
 $\hat{A} \hat{c} \cdot \hat{o} \cdot \hat{u} \quad | \hat{o} \hat{A} \hat{u} \hat{A} \hat{i} \hat{o} \quad \hat{o} \hat{u} \hat{c} \hat{c} \cdot \hat{c} \hat{i} \hat{i} \hat{E} \hat{c} \cdot \hat{y} \hat{E} \hat{E}. \quad p \hat{i} \hat{i} \quad \underline{D} = \underline{D}' \quad \pm y \hat{E}_i \hat{A} \frac{3}{4} \hat{i} \hat{o},$
 $PQ Q' P' \quad \pm y \hat{A} \hat{D} \mu \div p \cdot \frac{1}{2} \cdot \hat{A} \hat{A}_i \hat{i} \hat{o}.$



Ä¼õ 2-27

$\hat{a} \cdot \hat{A} \hat{A} \hat{c} \hat{o} \frac{1}{4} \hat{i} \cdot \hat{u} \quad | \hat{A} \hat{O} \hat{i} \hat{o} \hat{o} \hat{u} \hat{c} \hat{c} \cdot \hat{A} \hat{M} \pm \hat{E} \hat{i} \hat{i} \hat{E} \hat{c} \cdot \times \hat{o}.$

$\therefore PM = MQ'; QM = MP' \quad \hat{i} \hat{o}. \quad M \pm y \hat{E} \hat{o} \hat{u} \hat{c} \hat{c} \hat{o}, \quad 2\underline{A}, -2\underline{A} \quad \pm y \hat{E} \hat{A} \hat{c} \cdot \hat{o} \cdot \hat{c} \quad \underline{A} -$

$\hat{i} \hat{i} \quad p \cdot \frac{1}{2} \hat{A}_i \cdot \ll \cdot \hat{A} \hat{O} \hat{A}_i \hat{U} \pm \hat{i} \hat{i} \cdot \times \hat{o}.$

$\ll \hat{o} \hat{A}_i \hat{O} \hat{D},$

$$(\underline{A}, \hat{A} \hat{c} \cdot \hat{o} \underline{P}) + (-2\underline{A} \hat{A} \hat{c} \cdot \hat{o} M) \equiv (-\underline{A}' \hat{A} \hat{c} \cdot \hat{o} Q') \quad \pm y \hat{U} \hat{o},$$

$$(\underline{A}, \hat{A} \hat{c} \cdot \hat{o} \underline{P}) + (-2\underline{A} \hat{A} \hat{c} \cdot \hat{o} M) \equiv (-\underline{A}' \hat{A} \hat{c} \cdot \hat{o} P') \quad \pm y \hat{U} \hat{o} \quad \hat{A} \frac{3}{4} \hat{i} \hat{o},$$

$$\{\underline{A}, -\underline{A}\} \equiv \{(\underline{A}, -\underline{A})(2\underline{A}, -2\underline{A})\}$$

$$\equiv \{(\underline{A}, -2\underline{A})(-\underline{A}, -2\underline{A})\}$$

$$\equiv \{-\underline{A}', \underline{A}\} \quad \hat{i} \hat{o}.$$

$\hat{A} \frac{3}{4} \hat{i} \hat{o}, \quad \text{ÍÆÄ} \cdot \frac{1}{2} \cdot \hat{u} \quad p \frac{1}{4} \hat{o} \quad | \hat{A} \hat{A} \hat{c} \hat{o} \hat{A} \frac{3}{4} \hat{i} \hat{o} \quad \hat{A}_i \frac{3}{4} \hat{c} \hat{i} \cdot \hat{o} \hat{A} \hat{i} \hat{A} \frac{3}{4} \hat{o} \cdot \hat{A} \pm y \hat{E}_i \cdot \hat{c} \hat{E} \hat{D}.$

$\pm \hat{E} \text{ŞÄ} \quad \text{ÍÆÄ} \cdot \frac{1}{2} \cdot \hat{A} \quad \hat{A} \cdot \hat{A} \hat{A} \hat{U} \hat{i} \hat{i} \hat{o} \quad \hat{A} \hat{c} \cdot \hat{o} \cdot \hat{u} \quad \ll \hat{A} \hat{u} \hat{E} \hat{u} \hat{i} \quad p \cdot \frac{1}{4} \hat{A} \hat{c} \hat{A} \cdot \hat{A} \hat{O} \hat{o}$

$| \frac{3}{4} \hat{i} \cdot \hat{A} \times \quad \hat{A} \hat{A} \hat{u} \cdot \hat{E} \quad \hat{A} \hat{c} \hat{i} \frac{3}{4} \hat{o} \hat{O} \hat{A} \hat{i} \hat{o} \hat{D} \hat{A} \hat{D} \ll \hat{o} \hat{A} \hat{D} \hat{i} \cdot \hat{E} \hat{o} \hat{A} \hat{D}, \quad \text{ÍÆÄ} \cdot \frac{1}{2} \cdot \hat{A} \hat{i}$

$\text{ÍÆüÜÄ} \hat{D} \quad p \frac{1}{4} \hat{o} \quad | \hat{A} \hat{A} \hat{c} \hat{o} \frac{3}{4} \hat{o} \quad \hat{A} \hat{c} \cdot \hat{o} \hat{A} \hat{o} \cdot \hat{c} \hat{o} \quad \hat{A} \hat{A} \hat{y} \hat{A} \hat{i} \hat{o} \frac{3}{4} \hat{o} \quad \frac{3}{4} \hat{c} \hat{o} \hat{O} \hat{o} \frac{3}{4} \hat{c} \hat{E} \hat{y} \cdot \hat{u}$
 $\hat{o} \hat{A} \hat{i} \hat{o} \hat{u} \hat{c} \quad p \hat{O} \quad \text{ÍÆÄ} \cdot \frac{1}{2} \cdot \hat{u} \quad \hat{o} \hat{i} \hat{c} \hat{c} \cdot \hat{A} \hat{i} \hat{E} \cdot \hat{A} \pm \hat{E} \quad \hat{c} \hat{O} \hat{A} \hat{c} \cdot \hat{A} \hat{i} \hat{o}.$

$$= Fd(\underline{n}_+ \wedge \underline{D}) \pm \dot{E} \text{ Ş} \dot{A}$$

$= Fd(1.d)\underline{a}$ (a $\pm \dot{y} \wedge \dot{D} \quad \underline{A} \quad \pm \dot{y} \dot{E} \quad \dot{A} \dots \circ \quad | \circ \hat{A} \hat{U} \hat{A} \hat{I} \quad \circ \quad \text{Ş} \text{,} \text{i} \text{ð} \text{É} \text{ø} \ll \dots \hat{A} \hat{O} \hat{o}$
 $\mu \hat{A} \hat{A} \hat{I} \quad \text{¾} \hat{c} \dots \hat{A} \hat{A} \hat{I} \quad \hat{o}$).

$$= F\underline{a}(d^2)$$

$$= F\underline{a}(\underline{D}.\underline{D})$$

$$= F(\underline{D}.\underline{D})$$

$$\therefore \underline{F} = \frac{(\underline{C}_2 \wedge \underline{D})}{(\underline{D}.\underline{D})}$$

$\pm \dot{E} \text{ Ş} \dot{A} \quad \{(P, -P); p\} \pm \dot{y} \dot{E} \quad \{ \dot{E} \dot{A} \dots \text{½} \hat{i} \hat{l} \hat{i} \quad \circ \text{,} \text{i} \text{ç} \text{ç} \text{,} \hat{A} \hat{i} \dot{E} \quad \{(F, -F); d\} \pm \dot{y} \dot{E}$
 $\{ \dot{E} \dot{A} \dots \text{½} \hat{A} \hat{y} \quad \hat{A} \dots \circ \dots \hat{A} \hat{A} \dots \hat{A} \hat{A} \hat{U} \hat{i} \text{,} \text{Ó} \hat{E} \text{,} \text{Ç} \hat{E} \hat{D}$.

$$\therefore \underline{C}_1 + \underline{C}_2 - (\underline{A}, -\underline{A}) + (\underline{P}, -\underline{P})$$

$$= (\underline{A}, -\underline{A}) + Pp\underline{n}_+$$

$$= (\underline{A}, -\underline{A}) + Fd\underline{n}_+$$

$$= (\underline{A}, -\underline{A}) + (\underline{F}, -\underline{F})$$

$$\{ \underline{A} + \underline{F} \}, -(\underline{A} + \underline{F})$$

$\neg \text{,} \text{Ş} \dot{A} \quad \text{´} \hat{O} \quad \text{¾} \text{Ç} \text{ð} \text{¾} \text{Ç} \text{ø} \ll \dots \hat{A} \hat{O} \hat{o} \quad (\underline{A}, -\underline{A}), (\underline{P}, -\underline{P}) \pm \dot{y} \dot{E} \quad p \hat{O} \quad \{ \dot{E} \dot{A} \dots \text{½} \text{,} \hat{U} \hat{o},$
 $\hat{A} \dots \text{,} \hat{u} \quad \text{´} \hat{u} \quad | \quad \hat{A} \hat{i} \hat{y} \hat{U} \hat{o} \quad \{ \dot{E} \dot{A} \dots \text{½} \hat{i} \hat{l} \hat{i} \quad \hat{i} \quad \circ \hat{A} \hat{E} \text{,} \text{i} \hat{o} \quad d \ll \text{Ç} \times \dots \text{¾} \hat{A} \quad | \circ \hat{i} \quad \hat{l} \quad \hat{o} \hat{D} \hat{o}$
 $| \text{¾} \hat{i} \dots \hat{A} \hat{A} \text{Ş} \hat{A} \quad | \circ \hat{A} \hat{U} \hat{A} \hat{I} \text{,} \text{y} \hat{E} \quad \text{´} \hat{O} \quad \{ \dot{E} \dot{A} \dots \text{½} \hat{i} \hat{l} \hat{i} \quad \hat{i} \quad \circ \hat{A} \hat{A} \hat{i} \quad \hat{o} \text{.} \quad p \hat{i} \quad \{ \dot{E} \dot{A} \dots \text{½} \hat{A} \hat{y}$
 $\text{¾} \hat{O} \hat{o} \hat{D} \text{¾} \hat{E} \hat{y}$

$$(A + \frac{Pp}{d}) d\underline{n}_+$$

$$A d\underline{n}_+ + P p\underline{n}_+$$

$$= \underline{C}_1 + \underline{C}_2 \quad \neg \hat{l} \hat{o}.$$

$\text{Ş} \dot{A} \hat{O} \hat{o} \quad \text{´} \hat{O} \quad p \hat{U} \hat{i} \text{,} \text{ø} \quad | \quad \hat{A} \hat{i} \quad \hat{O} \text{Ç} \text{ø} \quad | \circ \hat{A} \hat{U} \hat{A} \hat{I} \text{,} \text{y} \hat{E} \quad \text{´} \hat{O} \quad \text{¾} \text{Ç} \text{ð} \hat{D} \quad \{ \dot{E} \dot{A} \dots \text{½} \text{,} \hat{u}$
 $\pm \hat{o} \quad | \text{¾} \hat{i} \dots \hat{A} \text{¾} \hat{i} \hat{A} \hat{U} \hat{o} \ll \hat{i} \quad \{ \dot{E} \dot{A} \dots \text{½} \text{,} \text{ç} \text{ø} \hat{A} \hat{i} \hat{o} \ll \hat{A} \hat{U} \hat{E} \hat{y} \quad \text{¾} \hat{O} \hat{o} \hat{D} \text{¾} \hat{E} \hat{y} \text{,} \text{Ç} \hat{y}$
 $p \hat{A} \hat{U} \text{,} \text{½} \text{¾} \hat{i} \quad \hat{U} \hat{D} \hat{i} \quad \hat{o} \quad | \text{¾} \hat{i} \quad \hat{l} \quad \hat{i} \quad \hat{i} \quad \hat{i} \quad \circ \hat{A} \hat{A} \hat{i} \dot{E} \quad \text{¾} \hat{O} \hat{o} \hat{D} \text{¾} \hat{E} \dots \hat{E} \hat{o} \quad | \quad \hat{A} \hat{U} \hat{E} \quad \text{´} \text{Ş} \hat{A} \hat{i} \hat{A} \hat{i} \hat{O}$

$\{ \dot{E} \dot{A} \dots \text{½} \hat{i} \hat{l} \hat{i} \quad \hat{i} \quad \circ \hat{A} \hat{A} \hat{i} \quad \hat{o} \text{.} \quad \{(P_1, -P_1); p_1\}, \{(P_2, -P_2); p_2\} \dots \dots \dots \{(P_n, -P_n); p_n\} \pm \dot{y} \dot{E} \quad n$

ÍÆÄÇ´ ½, ù ´ŞÄ ¾Çð¾Ä´ ÄÄ¾, ì |, ì ù, « ÄüÈý |¾, ì ÄÄ´ Éì, ì ½

{(P₁, -P₁); P₁} ±ýÈ ÍÆÄÇ´ ½, Ä « ÈðÄ´ ¼Ä, ì |, ì ñ Î ÄüÈ

ÍÆÄÇ´ ½, ù ì ì ´, ó¾ °, ì Ç, Ä, É ÍÆÄÇ´ ½, Ç {(P₁, -P₁); P₁} ±ýÈ

ÍÆÄÇ´ ½ |°ÄüÄÎ õ §, ì Î, Çø Ä´ ÄÄÜðÐ « ´ Ä, ´ Ç Ó´ ÈŞÄ

{(F₂, -F₂)P₁}.....{(F_n, -F_n)P₁} ±Éì ì ÈÇ, ×õ.

¬, ŞÄ ±øÄ, ì ÍÆÄÇ´ ½, Çý |¾, ì ÄÄý ÍÆÄÇ´ ½, ðð¾Èý

$$C_R = C_1 + C_2 + \dots + C_n$$

$$= \{(P_1, -P_1); P_1\} + \{(P_2, -P_2); P_2\} + \dots + \{(P_n, -P_n); P_n\}$$

$$= \{(P_1, -P_1); P_1\} + \{(F_2, -F_2); P_1\} + \dots + \{(F_n, -f_n); P_1\}$$

$$= \{(P_1, -F_2 + \dots + F_n), -(P_1 + F_2 + \dots + F_n); P_1\}$$

¬ ì õ.

þ ì $F_i = \frac{C_i \wedge D_i}{(D_i \cdot D_i)}, i = 2, 3, \dots, n$ ¬ ì õ.

¬¾Ä, ì |, ì ð¾ ÍÆÄÇ´ ½, |ÇøÄ, ì ¾õ ÍÆø¾Èý, Çý þÄü, ½Ç, ì ÜðÎ ð, ì¾, ì ì ì °ÄÄ, É ¾Öðð¾Èý |, ì ñ ¼ ´ŞÄ ´Ö ÍÆÄÇ´ ½, ì ì °ÄÄ, ì õ.

ÍÆÄÇ´ ½, |ÇøÄ, ÄüÈü ì ´ŞÄ ì Èç (same sign) þ´ ÄÄ, Äý ´ù, Ä, Ö ÍÆÄÇ´ ½, ðð¾ÈÜ ì ì Ä ì Èç´ Ä þðÎ ŞÄŞÄ |, ì Î ì, ðÄð¾ ÇÖÄ, ½ð´ ¾ð ÄÄýÄÎ ð¾Ä, ì õ.

2.12.2. þ´ ½ÄüÈ ¾Öðð¾Èý ¾ç´ °Ä, ´ Ç Ä´ ÄÄÜ ì ì õ þÖ ÍÆÄÇ´ ½, Çý |¾, ì ÄÄ´ Éì, ì ì ¾ø,

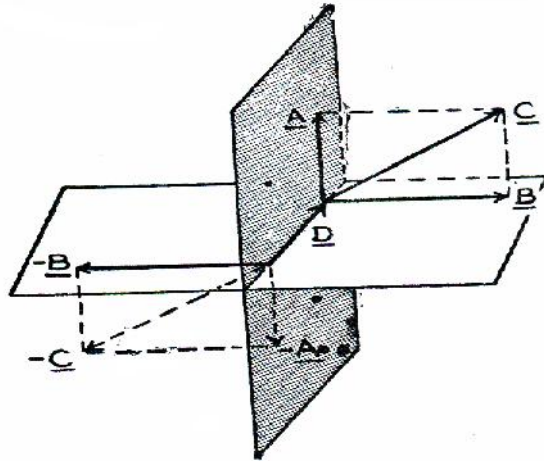
þ ì ÍÆÄÇ´ ½, ù ´ù, Ä, ý´ ÈÖõ Ä´ ÄÄÜ ì ì õ Ä´ °, ù |ÄüŞÄÈ, É ¾Ç, ì Çø |°ÄüÄÎ, ýÈÉ. ¾Ç, ì ù |ÄðÈ ì, ì ù ù õ §, ì ì §, ì ðÈø Ä¼õ

2.29ø, ì ðÈÄÄ, ì Ü D ±ýÈ |¾, ¼÷ðÄÎ ðÐõ ç´ Äð¾ç´ °Ä´ Ä « ´ Äì, ×õ.

ŞÄü, ì ñ ¼ ÍÆÄÇ´ ½, ù ´ù, Ä, ýÈü ì õ D ±ýÈ ¾ç´ °Ä´ Ä ð |¾, ¼÷ðÄÎ ðÐõ ç´ Äð¾ç´ °Ä´ Ä, ì ì ñ ¼ ÍÆÄÇ´ ½, Ä ´ù, Ä, Ö

¾Çð¾Öõ Ä´ ÄÄÜðÐ « ´ Ä, ´ Ç {A, -A}; {B, -B} ±Éì |, ì ù, A, B ±ýÄ´ Ä

$\vec{O} \vec{O} \vec{C} \vec{A} \vec{O} \quad | \circ \vec{A} \vec{O} \vec{A} \vec{I} \vec{A} \frac{3}{4} \vec{i} \vec{o} \ll \vec{A} \vec{u} \vec{E} \vec{y} \quad | \frac{3}{4} \vec{i} \vec{l} \vec{A} \vec{A} \vec{y} \quad \vec{A} \vec{c} \vec{c} \circ \vec{C} \quad \exists \quad \rho \vec{c} \frac{1}{2} \vec{A}$
 $\vec{A} \frac{3}{4} \vec{O} \vec{O} \vec{A} \vec{E} \ll \vec{o} \vec{O} \vec{u} \vec{C} \vec{A} \vec{y} \quad \vec{A} \vec{E} \vec{C} \vec{A} \vec{i} \vec{s} \vec{t} \quad | \circ \vec{O} \vec{O} \vec{o} \ll \vec{u} \vec{A} \vec{c} \vec{c} \frac{1}{2} \vec{A} \vec{O} \frac{3}{4} \vec{y} \quad \vec{a} \vec{c} \vec{c} \vec{A} \vec{A} \vec{O} \frac{1}{4} \vec{o}$
 $\pm \vec{n} \vec{A} \frac{3}{4} \vec{O} \vec{O} \vec{A} \vec{O} \vec{o} \quad \frac{3}{4} \vec{c} \vec{c} \circ \vec{A} \vec{O} \vec{o} \quad \vec{A} \vec{c} \vec{c} \vec{A} \vec{A} \vec{U} \vec{i} \vec{s} \vec{O} \vec{E} \vec{D} \ll \vec{u} \vec{A} \vec{i} \vec{s} \vec{E} \quad (-\vec{A}, -\vec{B}) \rightarrow \vec{C} \vec{A} \vec{A} \vec{u} \vec{E} \vec{y}$
 $| \frac{3}{4} \vec{i} \vec{l} \vec{A} \vec{A} \vec{y} \quad \vec{A} \vec{c} \vec{c} \circ (-\vec{C}) \quad \vec{O} \vec{o} \quad \vec{A} \vec{c} \vec{c} \vec{A} \vec{A} \vec{U} \vec{i} \vec{s} \vec{O} \vec{A} \vec{I} \vec{o} \quad \rightarrow \frac{3}{4} \vec{A} \vec{i} \vec{o} \quad \{\vec{C}, -\vec{C}\} \pm \vec{y} \vec{E} \quad \vec{I} \vec{E} \vec{A} \vec{c} \vec{c} \frac{1}{2}$
 $\vec{s} \vec{A} \vec{u} \vec{i} \vec{s} \vec{n} \frac{1}{4} \quad \rho \vec{O} \quad \vec{I} \vec{E} \vec{A} \vec{c} \vec{c} \frac{1}{2} \vec{s} \vec{y} \quad \circ \vec{i} \vec{c} \vec{c} \vec{A} \vec{i} \vec{E} \quad | \frac{3}{4} \vec{i} \vec{l} \vec{A} \vec{A} \vec{E} \vec{i} \vec{l} \vec{o} \quad \vec{s} \vec{A} \vec{O} \vec{o} \quad \vec{C} \pm \vec{y} \vec{E}$
 $\vec{A} \vec{c} \vec{c} \circ \vec{i} \vec{l} \vec{o} \quad \vec{D} \pm \vec{y} \vec{E} \quad \frac{3}{4} \vec{c} \vec{c} \circ \vec{s} \vec{A} \quad | \frac{3}{4} \vec{i} \vec{l} \frac{1}{4} \vec{O} \vec{c} \vec{c} \frac{1}{4} \vec{A} \text{ (relative)} \quad \vec{c} \vec{c} \vec{A} \vec{O} \frac{3}{4} \vec{c} \vec{c} \circ \vec{A} \vec{C} \vec{A} \vec{i} \vec{s} \vec{O} \vec{E} \vec{D} \dots$



À¼õ 2-29

$$\therefore \{(\underline{A}, -\underline{A}); (\underline{B}, -\underline{B})\} \equiv \{\underline{C}, -\underline{C}\}$$

ÍÆÄċċ ½, ũ ũ ĩ ÄĳËÛĳ ĩ ĩ ĩÄ ¾ÖÖĳËË Óċ ÈŞÄ

$$\underline{C}_A = \underline{D} \wedge \underline{A}; \underline{C}_B = \underline{D} \wedge \underline{B}; \underline{C}_R = \underline{D} \wedge \underline{C} \quad \pm \vec{y} \vec{E} \vec{i} \vec{l} \vec{o}.$$

ĳ Èĳĳ

$$\underline{A} + \underline{B} = \underline{C}$$

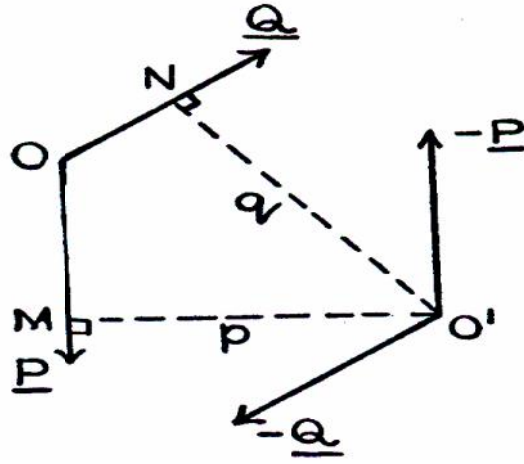
$$\therefore \underline{C}_R = \underline{D} \wedge \underline{C}$$

$$= \underline{D} \wedge (\underline{A} + \underline{B})$$

$$= \underline{D} \wedge \underline{A} + \underline{D} \wedge \underline{B}$$

$$= \underline{C}_A + \underline{C}_B$$

$\pm \vec{E} \vec{s} \vec{A} \quad \rho \vec{O} \quad \vec{I} \vec{E} \vec{A} \vec{c} \vec{c} \frac{1}{2} \vec{U} \vec{i} \vec{l} \quad \vec{c} \vec{c} \vec{A} \frac{3}{4} \vec{O} \vec{O} \vec{O} \frac{3}{4} \vec{E} \vec{y} \quad \frac{3}{4} \vec{c} \vec{c} \circ \vec{A} \vec{c} \vec{c} \vec{s} \vec{y} \quad \vec{U} \vec{I} \frac{3}{4} \vec{o} \ll \vec{A} \vec{u} \vec{E} \vec{y}$
 $| \frac{3}{4} \vec{i} \vec{l} \vec{A} \vec{A} \vec{y} \quad \vec{I} \vec{E} \vec{A} \vec{c} \vec{c} \frac{1}{2} \vec{i} \vec{l} \quad \vec{c} \vec{c} \vec{A} \frac{3}{4} \vec{O} \vec{O} \vec{O} \frac{3}{4} \vec{E} \vec{y} \quad \frac{3}{4} \vec{c} \vec{c} \circ \vec{A} \vec{C} \vec{A} \vec{i} \vec{o} \quad \vec{A} \vec{c} \vec{c} \vec{A} \vec{A} \vec{U} \vec{i} \vec{s} \vec{O} \vec{A} \vec{I} \vec{s} \vec{O} \vec{E} \vec{D}.$



À¼õ 2-30

À¼õ 2.30 ø $O' \hat{A} \hat{U} \hat{E} \hat{C} \underline{P}, \underline{Q}$ - , $\hat{C} \hat{A} \hat{U} \hat{E} \hat{Y} \hat{C} \hat{O} \hat{O} \hat{C} \hat{E} \hat{Y} \hat{C} \hat{U} \hat{O} \hat{C} \hat{E} \hat{S} \hat{A}$

$\underline{O'M} \wedge \underline{P}, \underline{O'N} \wedge \underline{Q}$ - Ì õ.

$\underline{O'M} \wedge \underline{P}$ ±ýÀÐ p¼î ÍÆĀ_i × õ $\underline{O'N} \wedge \underline{Q}$ ±ýÀÐ ĀĀî ÍÆĀ_i × õ
 !°Āøðîĉ, ŸÈÉ. ±ÉŞĀ « ĀüËŸ pĀü, ½¼î ÛÎ ¼ø.

$\underline{O'M} \wedge \underline{P} + \underline{O'N} \wedge \underline{Q}$
 = $Pp_{n_{\pm}} - Qq_{n_{\pm}}$
 = 0

- Ì õ. - É_iø Ā_iĵ ÉÉŸ §¼_iüÈòĀĒ (Varignon's theorem) $O' \pmý \hat{U} \hat{o} \hat{U} \hat{C} \hat{C} \hat{A} \hat{U} \hat{E} \hat{C}$

$\underline{O'O} \wedge \underline{P} + \underline{O'O} \wedge \underline{Q} = \underline{O'O} \wedge \underline{R}$ - Ì õ.

« ¼_iĀÐ

$\underline{O'O} \wedge \underline{R} = (\underline{O'M} + \underline{MO}) \wedge \underline{P} + (\underline{O'N} + \underline{NO}) \wedge \underline{Q}$
 $(\underline{O'M} \wedge \underline{P}) + (\underline{O'N} \wedge \underline{Q}) + (\underline{MO} \wedge \underline{P}) + (\underline{NO} \wedge \underline{Q})$
 = $Pp_{n_{\pm}} - Qq_{n_{\pm}} + 0 + 0$
 = 0

±ýĀ¼_iø $O' \pmý \hat{A} \hat{D} \underline{R}$!°ĀøĀî õ §_iðÈöüç 'õ ðüçĀ_i Ì õ. « ¼_iĀÐ

$OO' \pmý \hat{A} \hat{D} !¼_i ĀĀý \underline{R} \hat{Y} !°ĀøĀî õ ¼_i °ĀĀ_i Ì õ. $O' \hat{A} \hat{C} \hat{o} \hat{C} \hat{U} \hat{C} \hat{P}, \hat{Q}$$

±ýĀÉĀüËŸ !¼_i ĀĀý Ā_i ° - \underline{R} - Ì õ. « Ð × õ $O'O \pmý \hat{U} \hat{o} \hat{C} \hat{C} \hat{A} \hat{U} \hat{E} \hat{C}$

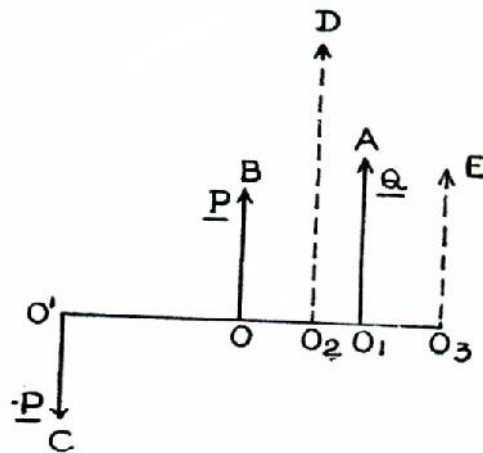
$O'A' \pm y \in S_{\pm} S_{\pm} i \delta'' \frac{1}{4} OA \text{ il } p'' \frac{1}{2} \hat{A}_i, \hat{A}'' \hat{A}_s. p \hat{o} | \hat{A}_i \hat{o} \hat{D} \underline{R} \pm y \in$
 $\hat{A}'' \hat{o}'' \hat{A}. OA \text{ il } p'' \frac{1}{2} \hat{A}_i \hat{E} O'A' \pm y \in S_{\pm} S_{\pm} i \delta \hat{E} \hat{o} | \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \underline{Q} \pm y \hat{U} \hat{o}$
 $\hat{A}'' \hat{o} \hat{A}_i, \times \hat{o}. O'C \text{ il } \pm \frac{3}{4} \hat{C}_i \hat{C} \hat{o} \frac{3}{4} \hat{C}'' \hat{o} \hat{A} \hat{C} \hat{o} | \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \underline{P} \pm y \hat{U} \hat{o} \hat{A}'' \hat{o} \hat{A}_i, \times \hat{o}$
 $\hat{A} \hat{C}_i \hat{C}_i, \hat{A}_i \hat{o}.$

$\underline{P} \pm y \hat{U} \hat{o} \hat{A} \hat{C}_y \hat{E} \frac{3}{4} \hat{A}_i, \hat{C} \hat{A} \text{ (latter), } p \hat{u} \hat{A}'' \hat{o}, O'C \frac{3}{4} \hat{C}'' \hat{o} \hat{A} \hat{C} \hat{o} | \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \hat{C}_y \hat{E}$
 $\hat{I} \hat{E} \hat{A} \hat{C}'' \frac{1}{2} \hat{A} \hat{C}_y p \hat{A} \hat{n} \frac{1}{4} \hat{o} \hat{A} \hat{C}'' \hat{o} (-\underline{P}) \hat{A} \hat{C} \hat{E}_i \hat{S} \hat{A} \hat{o} \hat{A} \hat{A}_i \hat{i}, \hat{o} \hat{A} \hat{I} \hat{o} \hat{C}_y \hat{E} \hat{D}.$

$\pm \hat{E} \hat{S} \hat{A} p \hat{U} \frac{3}{4} \hat{A}_i, OA \hat{A} \hat{u} \hat{i} p'' \frac{1}{2} \hat{A}_i \hat{o} \hat{u} \hat{C} O'A' \pm y \hat{U} \hat{o} \frac{3}{4} \hat{C}'' \hat{o} \hat{A} \hat{C} \hat{S} \hat{A}$
 $| \hat{o} \hat{A} \hat{u} \hat{A} \hat{I} \hat{o} \hat{C}_y \hat{E} \underline{Q} \pm y \hat{U} \hat{o} \hat{A} \hat{C}'' \hat{o} \hat{S} \hat{A} \ll \hat{o} | \frac{3}{4} \hat{i} | \frac{3}{4} \hat{A} \hat{C}_y \hat{A} \hat{C}'' \hat{C} \hat{A}_i, \ll '' \hat{A}_s \hat{C} \hat{E} \hat{D}.$

$\hat{A}'' \hat{o} 2:$

$\hat{A} \hat{C}'' \hat{o} \underline{Q} - \hat{E} \hat{D} \ll \hat{i} \hat{I} \hat{E} \hat{C} \hat{A} \hat{C}'' \frac{1}{2} \hat{A} \hat{C}_y \hat{A} \hat{C}'' \hat{o}, \hat{U} \hat{i} \hat{i} p'' \frac{1}{2} \hat{A}_i, \ll '' \hat{A} \hat{A} \hat{o} \hat{I} \hat{o}.$



$\hat{A} \hat{I} \hat{o} 2-33$

$O'O \pm y \hat{A} \hat{D} \underline{Q} \pm y \hat{U} \hat{o} \hat{A} \hat{C}'' \hat{o}'' \hat{A} o_1 p \hat{o} \hat{o} \hat{o} \frac{3}{4} \hat{C}_i, \hat{o} \hat{I} \hat{o}. O \hat{A} \hat{C} \hat{o} \hat{u} \hat{C} p o_1 \hat{o} \hat{u} \hat{C} \underline{Q}$
 $\pm y \hat{U} \hat{o} \hat{o} \frac{3}{4} p'' \frac{1}{2} \hat{A} \hat{C}'' \hat{o}, \hat{C} \hat{C}_y | \frac{3}{4} \hat{i} | \hat{A} \hat{A} \hat{y} (\underline{P} + \underline{Q}) \pm y \hat{E} \hat{o} \hat{A} \hat{C}'' \hat{o} \hat{i} \hat{i} \hat{o} \hat{A} \hat{y}.$

$p \hat{D} \pm y \hat{E} S_{\pm} i \delta \hat{E} \hat{u} \hat{i} p'' \frac{1}{4} \hat{S} \hat{A}, \frac{O_2}{O_2 O_1} = \frac{Q}{P} \pm y \hat{E} \hat{A} \hat{C}_s \hat{C} \hat{o} \frac{3}{4} \hat{o} \frac{3}{4} \hat{i} \hat{o} \hat{A}'' \hat{A} \hat{A} \hat{U} \hat{i}, \hat{o} \hat{A} \hat{I} \hat{o} o_2$
 $\pm y \hat{E} \hat{o} \hat{u} \hat{C} \hat{A} \hat{C} \hat{o} OB \pm y \hat{U} \hat{o} \frac{3}{4} \hat{C}'' \hat{o} \hat{i} \hat{i} p'' \frac{1}{2} \hat{A}_i, \hat{i} | \hat{o} \hat{A} \hat{o} \hat{A} \hat{I} \hat{o}.$

$\Delta \approx 2.34 \delta_{ij} \delta_{\epsilon} \hat{A}_i \hat{A}_j \hat{U} \hat{B} \hat{A} \hat{C} \hat{O} \hat{\delta} \hat{D} \hat{A} \hat{C} \hat{i} \hat{l} \hat{B} \hat{N} \pm \hat{y} \hat{E} \hat{i} \hat{o} \hat{r} \hat{i} \hat{l} \hat{o} \hat{D} \hat{i} \hat{S}_{ij} \hat{\delta} \hat{r} \hat{1} \hat{4}$
 $\hat{A} \hat{r} \hat{A}_j \hat{p} \hat{u} \hat{A} \hat{r} \hat{o} \hat{u} \hat{Q} \hat{B} \hat{N} \pm \hat{y} \hat{A} \hat{r} \hat{3} \hat{4} \hat{o} \hat{3} \hat{4} \hat{E} \hat{D} \hat{3} \hat{4} \hat{O} \hat{o} \hat{D} \hat{o} \hat{3} \hat{4} \hat{E} \hat{E} \hat{i} \hat{x} \hat{u} \hat{C} \hat{r} \hat{O}$
 $\hat{I} \hat{E} \hat{A} \hat{r} \hat{1} \hat{2} \hat{r} \hat{A} \hat{r} \hat{n} \hat{1} \hat{4} \hat{i} \hat{l} \hat{o}.$

$\hat{S} \hat{A} \hat{O} \hat{o} \hat{Q} \hat{B} \hat{N} = \hat{A} \hat{C} \hat{B} \hat{N}$

$$= 2 \times \frac{1}{2} \hat{A} \hat{C} \hat{B} \hat{N}$$

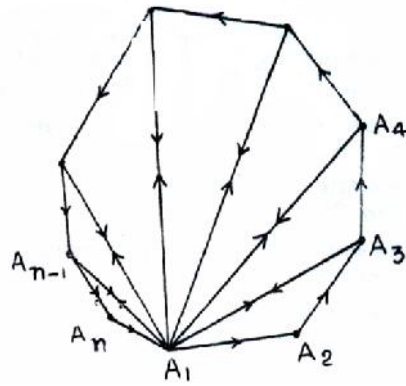
$= \hat{O} \hat{i} \hat{S}_{ij} \hat{1} \hat{2} \hat{o} \hat{A} \hat{B} \hat{C} \hat{A} \hat{r} \hat{A} \hat{o} \hat{A} \hat{r} \hat{p} \hat{O} \hat{A} \hat{1} \hat{4} \hat{i} \hat{l}.$

$\hat{p} \hat{u} \hat{A} \hat{r} \hat{O} \hat{E} \hat{x} \pm \hat{o} \hat{3} \hat{4} \hat{i} \hat{r} \hat{A} \hat{r} \hat{o} \hat{u} \hat{i} \hat{l} \hat{o} \hat{2} \hat{u} \hat{E} \hat{3} \hat{4} \hat{i} \hat{o}.$

2.12.6 $\hat{r} \hat{O} \hat{S} \hat{D} \hat{E} \hat{U} \hat{i} \hat{o} \hat{A} \hat{i} \hat{O} \hat{C} \hat{r} \hat{A} \hat{D} \hat{i} \hat{o} \hat{A} \hat{u} \hat{A} \hat{i} \hat{r} \hat{y} \hat{E} \hat{r} \hat{O} \hat{3} \hat{4} \hat{C} \hat{o} \hat{D} \hat{A} \hat{r} \hat{o} \hat{i}$
 $\hat{1} \hat{2} \hat{A} \hat{i} \hat{y} \hat{U} \pm \hat{n} \hat{A} \hat{3} \hat{4} \hat{o} \hat{D} \hat{3} \hat{4} \hat{r} \hat{o} \hat{i} \hat{o} \hat{A} \hat{u} \hat{A} \hat{i} \hat{o} \hat{S}_{ij} \hat{1} \hat{r} \hat{A} \hat{r} \hat{A} \hat{r} \hat{A} \hat{r} \hat{A} \hat{i} \hat{O} \hat{r} \hat{S} \hat{A} \hat{r} \hat{1} \hat{o} \hat{3} \hat{4}$
 $\hat{r} \hat{O} \hat{A} \hat{o} \hat{S}_{ij} \hat{1} \hat{2} \hat{o} \hat{3} \hat{4} \hat{r} \hat{A} \hat{i} \hat{r} \hat{1} \hat{C} \hat{i} \hat{o} \hat{1} \hat{E} \hat{i} \hat{o} \hat{A} \hat{o} \hat{D} \hat{1} \hat{4} \hat{i} \hat{o} \hat{r} \hat{A} \hat{i} \hat{o} \hat{A} \hat{i} \hat{o} \hat{S}_{ij} \hat{1} \hat{2} \hat{o} \hat{A} \hat{o} \hat{A} \hat{r} \hat{y}$
 $\hat{p} \hat{O} \hat{A} \hat{1} \hat{4} \hat{i} \hat{r} \hat{1} \hat{E} \hat{i} \hat{o} \hat{A} \hat{i} \hat{o} \hat{3} \hat{4} \hat{O} \hat{o} \hat{D} \hat{3} \hat{4} \hat{E} \hat{r} \hat{E} \hat{o} \hat{A} \hat{u} \hat{E} \hat{r} \hat{O} \hat{I} \hat{E} \hat{A} \hat{r} \hat{1} \hat{2} \hat{i} \hat{l} \hat{o} \hat{A} \hat{A} \hat{i} \hat{l} \hat{o}.$

$\Delta \approx 2.35 \delta_{ij} \delta_{\epsilon} \hat{O} \hat{u} \hat{C} \hat{A}_1 \hat{A}_2 \dots \hat{A}_n \pm \hat{y} \hat{U} \hat{o} \hat{A} \hat{o} \hat{S}_{ij} \hat{1} \hat{2} \hat{o} \hat{3} \hat{4} \hat{r} \hat{A} \hat{i} \hat{r} \hat{1} \hat{C} \hat{i} \hat{o} \hat{1} \hat{E} \hat{i} \hat{o}$
 $\hat{A}_1 \hat{A}_2 \hat{A}_2 \hat{A}_3 \dots \hat{A}_{n-1} \hat{A}_n \pm \hat{y} \hat{A} \hat{r} \hat{A} \hat{3} \hat{4} \hat{C} \hat{A} \hat{r} \hat{o} \hat{i} \hat{1} \hat{2} \hat{o} \hat{3} \hat{4} \hat{A} \hat{1} \hat{4} \hat{i} \hat{r} \hat{A} \hat{r} \hat{F}_1 \hat{F}_2 \dots \hat{F}_n \pm \hat{y} \hat{U} \hat{o}$
 $\hat{A} \hat{r} \hat{o} \hat{r} \hat{C} \hat{r} \pm \hat{n} \hat{A} \hat{3} \hat{4} \hat{o} \hat{D} \hat{3} \hat{4} \hat{r} \hat{o} \hat{i} \hat{o} \hat{A} \hat{u} \hat{A} \hat{i} \hat{o} \hat{S}_{ij} \hat{1} \hat{r} \hat{A} \hat{r} \hat{A} \hat{u} \hat{E} \hat{o} \hat{1} \hat{E} \hat{i} \hat{o} \hat{D} \hat{i} \hat{o}$
 $\hat{A}_1 \hat{A}_3 \hat{A}_1 \hat{A}_4 \dots \hat{A}_1 \hat{A}_{n-1} \pm \hat{y} \hat{A} \hat{E} \hat{A} \hat{u} \hat{E} \hat{o} \hat{1} \hat{4} \hat{i} \hat{o} \hat{A} \hat{u} \hat{E} \hat{i} \hat{o} \hat{O} \hat{u} \hat{E} \hat{O} \hat{o} \hat{1} \hat{E} \hat{i} \hat{o} \hat{A} \hat{o} \hat{D} \hat{1} \hat{o} \hat{A} \hat{U} \hat{o}$
 $\pm \hat{3} \hat{4} \hat{O} \hat{A} \hat{i} \hat{E} \hat{A} \hat{r} \hat{o} \hat{r} \hat{C} \hat{r} \hat{u} \hat{C} \hat{i} \hat{l} \hat{o}.$

$\ll \hat{o} \hat{A} \hat{i} \hat{o} \hat{D} \hat{A}_1 \hat{A}_2 \hat{A}_3 \pm \hat{y} \hat{E} \hat{O} \hat{i} \hat{S}_{ij} \hat{1} \hat{2} \hat{o} \hat{3} \hat{4} \hat{r} \hat{A} \hat{i} \hat{r} \hat{1} \hat{C} \hat{i} \hat{o} \hat{1} \hat{E} \hat{i} \hat{o} \hat{A}_1 \hat{A}_2 \hat{A}_2 \hat{A}_3 \hat{A}_3 \hat{A}_1$
 $\pm \hat{y} \hat{A} \hat{E} \hat{A} \hat{u} \hat{E} \hat{i} \hat{o} \hat{1} \hat{E} \hat{i} \hat{o} \hat{A} \hat{o} \hat{D} \hat{i} \hat{o} \ll \hat{o} \hat{A} \hat{i} \hat{r} \hat{1} \hat{C} \hat{i} \hat{o} \hat{A} \hat{r} \hat{A} \hat{u} \hat{A} \hat{i} \hat{o} \hat{S}_{ij} \hat{1} \hat{r} \hat{C} \hat{i} \hat{o} \hat{x} \hat{o}$
 $\hat{1} \hat{2} \hat{r} \hat{n} \hat{1} \hat{4} \hat{A} \hat{r} \hat{o} \hat{u} \hat{2} \hat{\Delta} \hat{A}_1 \hat{A}_2 \hat{A}_3 \pm \hat{y} \hat{E} \hat{A} \hat{o} \hat{A} \hat{C} \hat{r} \hat{A} \hat{r} \pm \hat{n} \hat{A} \hat{3} \hat{4} \hat{o} \hat{A} \hat{i} \hat{r} \hat{1} \hat{2} \hat{r} \hat{n} \hat{1} \hat{4}$
 $\hat{3} \hat{4} \hat{O} \hat{o} \hat{D} \hat{3} \hat{4} \hat{E} \hat{r} \hat{E} \hat{r} \hat{1} \hat{4} \hat{A} \hat{r} \hat{O} \hat{I} \hat{E} \hat{A} \hat{r} \hat{1} \hat{2} \hat{i} \hat{l} \hat{o} \hat{A} \hat{A} \hat{i} \hat{l} \hat{o}.$

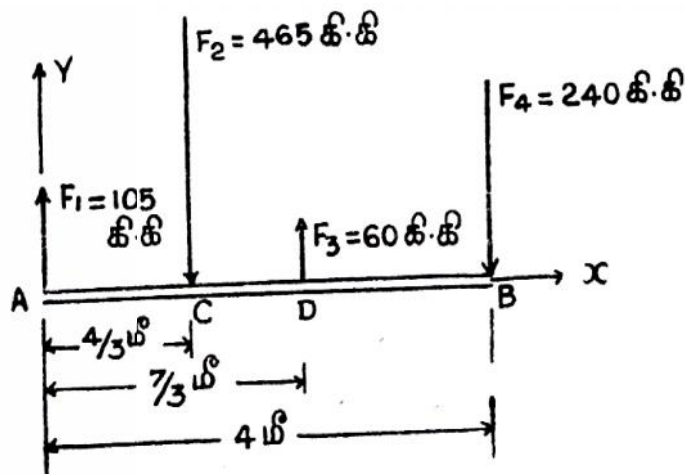


À¼õ 2-35

« ùÅ_jŠÈ ΔA₁A₃A₂, ΔA₁A₄A₅, ..., ΔA₁A_{n-1}A_n ±ýÈ Óì Š_{s,j} ½í_s Ç_sŸ Àì_s í_s Ç_s∅ ±ñ Á¼õòò, ¼ç[°], |°ÃüÃî õ Š_{s,j}î ¬_sÇÃü[°] È ÄüÈÇ Ì ÈÇ_s ôÃî õ Åç[°] ù Ó[°] ÈŠÃ 2ΔA₁A₃A₄, 2ΔA₁A₄A₅, ..., 2ΔA₁A_{n-1}A_n ±ýÚ Ì ÈÇ_s ôÃî õ ¼õòò ¼çÈý_s Ç[°] ¼Ã ÍÆÄç[°] ½_s ùìì î °ÁÁ_j ¬ ùÇ^¾_j ×õ_s Õ¼Ä_jõ. « ò¼ÉÇ ÍÆÄç[°] ½òòò ¼çÈý « ó¼ ÍÆÄç[°] ½òòò ¼çÈý_s Ç_sŸ þÃü_s ½ç^¾î Ùî ¼Öì Ì î °ÁÁ_jî õ.

¬_s ŠÅ « ò¼ÉÇ ÍÆÄç[°] ½òòò ¼çÈý, ŠÃü_s ñ ¼ ÅøŠ_{s,j} ½õ A₁A₂, ..., A_n þý ÄõÄý þõÁ¼í_s ùì î °Áõ.

Áj 340; 2.3 4 ÁD ¼ ÷ j ÇÓúÇ - ò¾Áõ (beam) ´ýÈø À¼õ 2.36ø j ðÉÁÁj Ú
 Áç´ ° ù | °ÁøÁÍ ´ýÈÉ. « ´ Á Ù ì ì î ° j Çç, Áj É "Áç´ ° ÍÆÁç´ ½"
 « ´ Áõ´ À (a) A ±ýÛõ òúÇç (b) B ±ýÛõ òúÇçÁÖõ Á´ ÁÁÚì, (c)
 « ùÁç´ òð |¾j ì¾ç ì î °ÁÁj, ´ Í ì ò ´ Ö¾ÉçÁç´ °´ Áì j ñ j.



Á¼õ 2-36

A ð ÐÁì, òòúÇçÁj, xõ, AB ±ýÛõ - ò¾Áõ´¾ x « î°j, xõ | j ù j. A
 Áø Á´ ÁÁøÁÍ õ | ° í ì ò Ð ì §, j ð´ ¼ y « î°j, xõ | j ù j.

« ô | Áj Ø Ð, $\underline{F}_1 = 105 \underline{j}$ ±ýÛõ Áç´ ° A (0, 0) ±ýÛõ òúÇçÁç´ | °ÁøÁÍ, çÈÐ.

$\underline{F}_2 = -465 \underline{j}$ ±ýÛõ Áç´ ° C $(\frac{4}{3}, 0)$ ±ýÛõ òúÇçÁç´ | °ÁøÁÍ, çÈÐ. $\underline{F}_3 = 60 \underline{j}$

±ýÛõ Áç´ ° D $(\frac{7}{3}, 0)$ ±ýÛõ òúÇçÁç´ | °ÁøÁÍ, çÈÐ.

$\underline{F}_4 = -240 \underline{j}$ ±ýÛõ Áç´ ° B(4,0) ±ýÛõ òúÇçÁç´ | °ÁøÁÍ, çÈÐ.

(a) A ±ýÛõ òúÇçÁç´ "Áç´ ° ÍÆÁç´ ½" « ´ Áõ´ À ò | ÀÚ¾ø:

| j ì ì, òÁø¾ Áç´ òð |¾j ì¾ç ì î °ÁÁj, A ±ýÛõ òúÇçÁç´

« ´ Áõõ ´ Ö¾ÉçÁç´ °, ´ Ö¾Éç ÍÆÁç´ ½ - j ÇÁÁü´ È $\underline{R}, \underline{M}_A^R$ ±Éì | j ù j.

« ô | Áj Ø Ð $\underline{R} = \sum_{i=1}^n \underline{F}_i = 105 \underline{j} - 465 \underline{j} + 60 \underline{j} - 240 \underline{j} = -540 \underline{j}$

$$\underline{M}_A^R = \sum_{i=1}^n \underline{r}_i \wedge \underline{F}_i$$

$$= \frac{100}{\sqrt{a^2 - 400}} \{ \underline{a}\underline{i} + 12\underline{j} - 16\underline{k} \}$$

$$\begin{aligned} \underline{DA} &= \underline{OA} - \underline{OD} \\ &= 12\underline{j} - (\underline{a}\underline{i} + 16\underline{k}) \\ &= -\underline{a}\underline{i} + 12\underline{j} - 16\underline{k} \end{aligned}$$

$$= \sqrt{a^2 - 400} \left\{ -\frac{a}{\sqrt{a^2 - 400}} \underline{i} + \frac{12}{\sqrt{a^2 - 400}} \underline{j} - \frac{16}{\sqrt{a^2 - 400}} \underline{k} \right\}$$

$$\therefore \underline{M} = 1000 \left\{ -\frac{a}{\sqrt{a^2 - 400}} \underline{i} + \frac{12}{\sqrt{a^2 - 400}} \underline{j} - \frac{16}{\sqrt{a^2 - 400}} \underline{k} \right\}$$

$$= \frac{1000}{\sqrt{a^2 - 400}} \{ -\underline{a}\underline{i} + 12\underline{j} - 16\underline{k} \}$$

$(\underline{F}, \underline{M}) \pm \dot{\gamma} \dot{\lambda} \dots \dot{\lambda} \dot{\gamma} \dot{U} \dot{i} \dots \dot{i} \dot{\gamma} \dot{U} \dot{i} \dot{o} \dot{i} \dot{l} \dot{o} \dot{3}_4 \dot{i} \dots \ll \dots \dot{\lambda} \dot{\lambda} \dot{3}_4 \dot{i} \dot{o},$

$$\underline{F} \cdot \underline{M} = 0$$

$$\ll \dot{3}_4 \dot{i} \dot{\lambda} \dot{D} (\underline{a}\underline{i} + 12\underline{j} - 16\underline{k}) \cdot (-\underline{a}\underline{i} + 12\underline{j} - 16\underline{k}) = 0$$

$$-a^2 + 144 + 256 = 0$$

$$a^2 = 400.$$

$$\ll \dot{3}_4 \dot{i} \dot{\lambda} \dot{D} a = 20 [10^{-2}] \dot{\lambda} \dot{f}$$

$$\therefore \underline{F} = \frac{100}{\sqrt{800}} \{ 20\underline{i} + 12\underline{j} - 16\underline{k} \}$$

$$= \frac{100}{20\sqrt{2}} \{ 20\underline{i} + 12\underline{j} - 16\underline{k} \}$$

$$= \frac{5\sqrt{2}}{2} (20\underline{i} + 12\underline{j} - 16\underline{k})$$

$$= \frac{5\sqrt{2}}{2} (10\underline{i} + 6\underline{j} - 8\underline{k})$$

$$\underline{M} = \frac{1000}{\sqrt{800}} \{ -20\underline{i} + 12\underline{j} - 16\underline{k} \}$$

$$= \frac{1000}{20\sqrt{2}} \{ -20\underline{i} + 12\underline{j} - 16\underline{k} \}$$

$$\begin{aligned}
&= \frac{50\sqrt{2}}{2}(20\mathbf{i} + 12\mathbf{j} - 16\mathbf{k}) \\
&= 50\sqrt{2}(10\mathbf{i} + 6\mathbf{j} - 8\mathbf{k}) \\
&= -500\sqrt{2}\mathbf{i} + 300\sqrt{2}\mathbf{j} - 400\sqrt{2}\mathbf{k} \quad [10^{-2}] \text{ Af } \dots
\end{aligned}$$

G(O, y, z) ± ŷ Ū Á¼ð¾¼ø °ÁŪ | Á¾ŌÁ; É F ± ŷ Ū ò Áº ° ŷ Ç ²üÁÎ ò¾¼ × ò.

« ô | À; ØÐ, G Áø - F ± ŷ Ū ò Áº ° Òò, P Áø F ± ŷ Ū ò Áº ° Òò GP ^ F
 ± ŷ Ū ò ¾Ōòð¾¼È È ò §¾üÚÁòÐ M | ³ Í ÁòÐÁŌ ò.

± ŷ Ū ò Áº ° Òò G Áø M = GP ^ F ± ŷ Ū ò ´ü È Áº ° Á¾Á; pŌì ì ò.
 « ô | À; ØÐ,

$$\begin{aligned}
(-500\sqrt{2}\mathbf{i} + 300\sqrt{2}\mathbf{j} - 400\sqrt{2}\mathbf{k}) &= \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ 10 & 6 - \bar{y} & 8 - \bar{z} \\ 10 & 6 & -8 \end{vmatrix} \\
&= 5\sqrt{2} \{ (8\bar{y} + 6\bar{z} - 96)\mathbf{i} - \mathbf{j}(-160 + 10z) + \mathbf{k}(10y) \} \\
5\sqrt{2}(10y) &= 400\sqrt{2} \text{ (iii)}
\end{aligned}$$

pŌèÈí , ÇŌò i, j, k - , ÅüÈý | , Øì , Çî ° ÁòÁÎ ò¾¼

$$\begin{aligned}
&= 5\sqrt{2} (5\bar{y} + 6\bar{z} - 96)\mathbf{i} - \mathbf{j} = -500\sqrt{2} \dots\dots\dots(i) \\
&= 5\sqrt{2} (-160 + 10z) = 300\sqrt{2} \dots\dots\dots(ii) \\
&= 5\sqrt{2} (10y) = 400\sqrt{2} \dots\dots\dots(iii)
\end{aligned}$$

(ii) ÁÐ ° Áý À; ðÈÄŌóÐ z = 10 [10⁻²] Af ± É × ò

(iii) ÁÐ ° Áý À; ðÈÄŌóÐ y = -8 [10⁻²] Af ± É × ò , Çî ¼ì ì ò

Ì Èòð : y, z - , ÅüÈý Á¾òð , ù (i) ÁÐ ° Áý À; ð´¼ Ç ÈŞüÚÁ´¾Ōò
 , ½Ä; ò. Áº ò |¾ì ¾¼ « ´ ÁòÁý ´ Î ì , ò

Á;¾¼; 2-5 O ´ ÁŌ Í ð¾´ ÁòÁ; ì | , ñ ¼ - Áò |¾´ Á (coordinate system)

F = (10 \mathbf{i} + 6 \mathbf{j} - 6 \mathbf{k}) , Ç , Ç - ù Ç Áº ° ´ý Ū (10, 3, 4) Af ± ŷ Ū Á¼ð¾¼Ä´ ÁŌò

0úççÅÆçšÅ ãÅøÀÏ çÈÐ. O ÀüÈç F ±ýÛõ Åç' °Äý ¼Öòðð¼È' Éì çìñ ç.

$\underline{F} = (10\underline{i} + 6\underline{j} - 6\underline{k})$ (10,3,4) ±ýÀÐ P ±ýÛõ 0úçç' Åì Ì Èò¼ìø
 $\underline{r} = \underline{OP} = 10\underline{i} + 3\underline{j} + 4\underline{k}$ ãì õ.

$\therefore \underline{M}_0 = \underline{r} \wedge \underline{F} = \begin{pmatrix} \underline{i} & \underline{j} & \underline{k} \\ 10 & 3 & 4 \\ 10 & 6 & -6 \end{pmatrix} = (-42\underline{i} + 100\underline{j} + 30\underline{k}) \text{ Åæ ç ç ç}$

Áì¼çç 2-6 Óó¼çÅ Áì¼ççì ç½ì çø («¼;ÅÐ Áì¼çç 2.5ø) ±Î ð¼ F ±ýÛõ
 Åç' °Äý ¼Öòðð¼È' É Q(6,-4,-3)Åæ±ýÛõ 0úççÀüÈç çìñ ç.

$\underline{QP} = \underline{OP} - \underline{OQ}$
 $= \underline{r}_1 - \underline{r}_2$
 $= (10\underline{i} + 3\underline{j} + 4\underline{k}) - (6\underline{i} - 4\underline{j} - 3\underline{k})$

$= 4\underline{i} + 7\underline{j} + 7\underline{k}$
 $\therefore \underline{M}_Q = \underline{QP} \wedge \underline{F}$

$= \begin{pmatrix} \underline{i} & \underline{j} & \underline{k} \\ 4 & 7 & 7 \\ 10 & 6 & -6 \end{pmatrix} = (-84\underline{i} + 94\underline{j} - 46\underline{k}) \text{ Åæ ç ç ç}$

Áì¼çç 2-7 F = (200i + 100j + 500k) ç ç ç ±ýÛõ Åç' ° Äý Û P(8,9,4)Åæ±ýÛõ

0úççÅÆçšÅ ãÅøÀÏ çÈÐ. $(\frac{6}{19}, -\frac{6}{19}, -\frac{17}{19})$ ±ýÀÉ Åü' Èò çç' °ì ç¼ì ç ç ç ç ç xõ, Q(-5,3,2)Åæ±ýÛõ 0úçç ÅÆçšÅ ãøÖõ §ç÷§çì ÅüÈç F
 ý ¼Öòðð¼È' Éì çìñ ç.

\underline{r} ±ýÀÐ Q(-5,3,2)Åæ ±ýÛõ 0úçç' Å P (8,9,4)Åæ ±ýÛõ 0úçç¼ý
 þ' ½ì Ì õ çç' °Äç' Åì Ì Èç Ì ; ÅÉø,

$\underline{r} = \underline{QP} = \underline{OP} - \underline{OQ}$

Đặt $\vec{u}, \vec{v}, \vec{w}$ là các vectơ đơn vị theo trục Ox, Oy, Oz , $\vec{a} = 2\vec{u} + 2\vec{v} + 3\vec{w}$, $\vec{b} = 0\vec{u} - 3\vec{v} + \vec{w}$, $\vec{c} = \vec{u} - \vec{v} + \vec{w}$.

\vec{F}_1, \vec{F}_2 là các vectơ lực có độ lớn lần lượt là $20\sqrt{2}$ và 40 đơn vị, hướng lần lượt là \vec{a} và \vec{b} .

$$\vec{r}_1 = \frac{1}{\sqrt{2}}\vec{i} - \frac{1}{2}\vec{j} + \frac{1}{2}\vec{k}$$

$$\vec{r}_2 = \frac{3}{5}\vec{i} + \frac{4}{5}\vec{j} + 0\vec{k}$$

$$\vec{F}_1 = F_1 \vec{r}_1$$

$$= 20 \left(\frac{1}{\sqrt{2}}\vec{i} - \frac{1}{2}\vec{j} + \frac{1}{2}\vec{k} \right)$$

$$= 10\sqrt{2}\vec{i} - 10\vec{j} + 10\vec{k}$$

$$\vec{F}_2 = F_2 \vec{r}_2$$

$$= 40 \left(\frac{3}{5}\vec{i} + \frac{4}{5}\vec{j} + 0\vec{k} \right)$$

$$= (24\vec{i} + 32\vec{j})$$

Đặt $P(2, 2, 3), Q(0, -3, 1)$ là hai điểm thuộc trục Ox, Oy, Oz lần lượt.

$$\vec{r}_1 = \vec{OP} = 2\vec{i} + 2\vec{j} + 3\vec{k}$$

$$\vec{r}_2 = 0\vec{i} - 3\vec{j} + \vec{k}$$

Đặt \vec{F}_1, \vec{F}_2 là các vectơ lực có độ lớn lần lượt là $20\sqrt{2}$ và 40 đơn vị, hướng lần lượt là \vec{a} và \vec{b} .

$$= \vec{r}_1 \wedge \vec{F}_1 + \vec{r}_2 \wedge \vec{F}_2$$

$$= \begin{pmatrix} \vec{i} & \vec{j} & \vec{k} \\ 2 & 2 & 3 \\ 10\sqrt{2} & -10 & 10 \end{pmatrix} + \begin{pmatrix} \vec{i} & \vec{j} & \vec{k} \\ 0 & -3 & 1 \\ 24 & 32 & 0 \end{pmatrix}$$

$$= \{50\vec{i} - (20 - 30\sqrt{2})\vec{j} + (20 + 20\sqrt{2})\vec{k}\} + \{-32\vec{i} + 24\vec{j} + 72\vec{k}\}$$

$$= (18\mathbf{i} + 46.42\mathbf{j} + 23.72\mathbf{k}) \text{ Af } \dots$$

Áj 3/4; 2-10 $\underline{F} = 6\mathbf{i} + 3\mathbf{j} + 10\mathbf{k}$ ±y Û õ Å ¸ ¸, A(0,2,3) ±y Û õ ò ù Ç Å ¸ ¸
 | ° Å Ø Å Î ¸ Ç È. B(2,-3,0) ±y Û õ ò ù Ç Å ¸ ¸ ° Å Û õ ± 3/4 Ç Å Î É - \underline{F} ±y Û õ Å ¸ ¸ ¸
 | ° Å Ø Å Î ¸ Ç È. « ù Å ¸ ¸ ¸ Ç Ç Ý Í Æ Å ¸ ¸ 1/2 ò ò ò 3/4 Ç È Ý Å Î Ð? « Ð | ° Å Û Å Î ò
 § ¸ j ð È Ý 3/4 ¸ ¸ ¸ ò ù Ç Å ¸ ¸ ¸ Ç Ò õ ¸ j ñ ¸.

A(0,2,3) B(2,-3,0) ±y Û õ ò ù Ç Ç Ç Ý Ç ¸ ¸ Å ò 3/4 ¸ ¸ ° Å ¸ ¸ ¸ Ç $\underline{r}_1, \underline{r}_2$ ±É ì | ¸ j ù ¸
 « ô | Å j Ø Ð.

$$\underline{w} = \underline{BA} = \underline{OA} - \underline{OB}$$

$$= (0\mathbf{i} + 2\mathbf{j} + 3\mathbf{k}) - (2\mathbf{i} - 3\mathbf{j} + 0\mathbf{k})$$

$$= -2\mathbf{i} + 5\mathbf{j} + 3\mathbf{k}$$

$$\pm \text{É } \underline{S} \text{ Å } \underline{C} = \underline{BA} - \underline{F}$$

$$= \underline{w} \wedge \underline{F}$$

$$= \begin{pmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ -2 & 5 & 3 \\ 6 & 3 & 10 \end{pmatrix}$$

$$= 41\mathbf{i} + 38\mathbf{j} - 36\mathbf{k}$$

Áj 3/4; 2-11. Ó ó 3/4 Å ¸ 1/2 ì ¸ Ç (« 3/4 Å Ð Áj 3/4; 2-10 Ø,

(i) x « î Í Å ù È Ç Í Æ Å ¸ ¸ 1/2 Å ¸ ¸ 3/4 Ç Å Ò ò 3/4 Ç È Ý Å Î Ð?

(ii) Å ¸ ¸ ¸ Û ì ì p ¸ ¸ 1/4 Å ¸ Ç Å Ò ù Ç | ¸ ò ò ò ò ò 3/4 j ¸ ¸ Å × Å Î Ð?

(iii) « ò | 3/4 j ¸ ¸ Å ¸ ¸ Å 10 « Å ì ¸ ù Å ì 3/4 Å ¸ ¸ p Ò ì ì Á j Ù ± Î ò 3/4 j Ø « § 3/4
 Í Æ Å ¸ ¸ 1/2 ò ò ò 3/4 Ç È ¸ ¸ É ò | Å Ù Å 3/4 ù ì | Å Å ¸ ¸ ¸ ù | Å j ý È Ý ± ñ Å 3/4 Ç Å Ò Å Î Ð?

$$(i) C_{OX} = \underline{C} \cdot \underline{i} = (41\mathbf{i} + 38\mathbf{j} - 36\mathbf{k}) \cdot \mathbf{i} = 41$$

(ii) $(\underline{F}, -\underline{F})$ ±y Û õ Í Æ Å ¸ ¸ 1/2 ì ì p ¸ ¸ 1/4 Å ¸ Å ¸ Å Ò õ | ¸ ò ò ò ò ò 3/4 j ¸ ¸ Å × d ±É ì
 | ¸ j ù ¸ « ô | Å j Ø Ð.

$$|\underline{C}| = |\underline{F}|d \text{ - ì õ.}$$

$$\{(41)^2 + (38)^2 + (-36)^2\}^{\frac{1}{2}} = \{(6)^2 (3)^2 (10)^2\}^{\frac{1}{2}} d$$

$$d = 5.54 \text{ m}$$

$$(iii) \text{ } \vec{r} = 5.54 + 10 = 15.54 \text{ m}$$

$$|F_1| \times 15.54 = |C|$$

$$F_1 = \frac{66.49}{15.54} = 4.28$$

2-12. A cube of side length a is shown in the figure. A force F is applied at the corner P in the direction of the diagonal PO . Find the magnitude of the component of the force F acting along the diagonal OR .

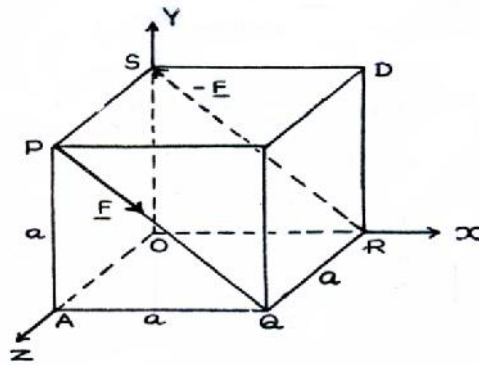


Figure 2-38

2-38. A cube of side length a is shown in the figure. A force F is applied at the corner P in the direction of the diagonal PO . Find the magnitude of the component of the force F acting along the diagonal OR .

Solution: The cube is shown in the figure. The origin O is at the bottom-left-back corner. The x , y , and z axes are shown. The corners A, P, Q, S, D are labeled. The force F is applied at P in the direction of PO . The diagonal OR is also shown.

$$\vec{PQ} = \vec{OQ} - \vec{OP} = (a\mathbf{i} + a\mathbf{k}) - (a\mathbf{j} + a\mathbf{k}) = a\mathbf{i} - a\mathbf{j}$$

$$= a\sqrt{2} \left(\frac{1}{\sqrt{2}}\mathbf{i} - \frac{1}{\sqrt{2}}\mathbf{j} \right)$$

$$= a\sqrt{2} \left\{ \frac{1}{\sqrt{2}}\mathbf{i} - \frac{1}{\sqrt{2}}\mathbf{j} \right\}$$

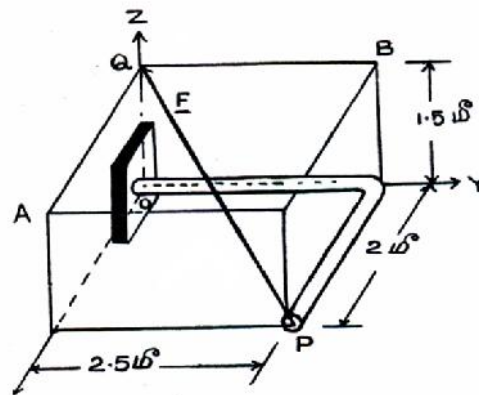
The magnitude of the component of the force F acting along the diagonal OR is

$$= 15\sqrt{2}(\underline{i} + \underline{j}) \cdot \left(\frac{1}{\sqrt{3}}\underline{i} + \frac{1}{\sqrt{3}}\underline{j} - \frac{1}{\sqrt{3}}\underline{k} \right)$$

$$= 10\sqrt{6}$$

$$= 24.5 [10^{-2}] \text{ m}^3 \cdot \text{s}^{-1}$$

Ái 3/4; 2-13. ' Ō Å" Ç× Ĩ Æiö ÑÉç ' ýÈç À¼õ 2-39ø ,i ðËÄÅi Ú 50√2
 ,çç Äç" °ÅjÉÐ | °ÅøÄÎ çÈÐ.



À¼õ 2-39

(a) x, y, z

(b) A ±ý Ūõ ðùçç

(c) B ±ý Ūõ ðùçç

→ çÄ" Å ÄüÈç, Åç" °Åý ¾çŌõð¾çÈ" Éi ,iñ ,.

O ±ý Ūõ ðùçç Ĩ - jÄ Ĩ ð¼" ÅøÄç P, Q, A, B → çÄ ðùçç, ççý → Åð
 |¾j" Ä, ù Ó" ÈŞÅ P (2, 2.5, 0) Q (0, 0, 1.5) A (2, 0, 1.5) B (0, 2.5, 1.5) → Ĩ õ.

PQ ±ý È Şç÷Ş, iðËÄ" ÅŌõ µÄÄĨ ¾ç" °Åç" Å } ±Éi Ĩ Èç ,õ.

$$\underline{PQ} = \underline{OQ} - \underline{OP} = -2\underline{i} - 2.5\underline{j} + 1.5\underline{k}$$

$$= \frac{5}{\sqrt{2}} \left[-\frac{2\sqrt{2}}{5}\underline{i} - \frac{5}{2} \times \frac{\sqrt{2}}{5}\underline{j} + \frac{3}{2} \times \frac{\sqrt{2}}{5}\underline{k} \right]$$

$$= \frac{5}{\sqrt{2}} \underline{\lambda}$$

$$\therefore \underline{\lambda} = \frac{1}{5\sqrt{2}} [-4\underline{i} - 5\underline{j} + 3\underline{k}]$$

F ±ý È Äç" °PQÄç | °ÅüÄĨ Å¾jø

$$\begin{aligned}\underline{F} &= F \underline{j} \\ &= 50\sqrt{2} \times \frac{1}{5\sqrt{2}} [-4\underline{i} - 5\underline{j} + 3\underline{k}] \\ &= -40\underline{i} - 50\underline{j} + 30\underline{k}\end{aligned}$$

(a) $\underline{F} \perp \underline{y} \Rightarrow \underline{A} \cdot \underline{OQ} \perp \underline{y} \Rightarrow \underline{A} \cdot \underline{OQ} \cdot \underline{y} = 0$. $\underline{O} \perp \underline{y} \Rightarrow \underline{O} \cdot \underline{y} = 0 \Rightarrow \underline{O} \cdot \underline{y} = 0$.

$$\begin{aligned}\underline{M}_O &= \underline{OQ} \wedge \underline{F} \\ &= \frac{3}{2} \underline{k} \wedge (-40\underline{i} - 50\underline{j} + 30\underline{k}) \\ &= -60\underline{j} - 75\underline{i}\end{aligned}$$

$$= (75\underline{i} - 60\underline{j} + 0\underline{k}) \cdot \underline{A} \cdot \underline{OQ} \cdot \underline{y} = 0.$$

$$\therefore M_x = 75 \cdot \underline{A} \cdot \underline{OQ} \cdot \underline{y} = -60 \cdot \underline{A} \cdot \underline{OQ} \cdot \underline{y} \quad M_z = 0 \cdot \underline{A} \cdot \underline{OQ} \cdot \underline{y}$$

$$(b) \underline{M}_A = \underline{AQ} \wedge \underline{F}$$

$$\begin{aligned}&= -2\underline{i} \wedge (-40\underline{i} - 50\underline{j} + 30\underline{k}) \\ &= 100\underline{k} + 60\underline{j} \\ &= (60\underline{j} + 100\underline{k}) \cdot \underline{A} \cdot \underline{AQ} \cdot \underline{y}\end{aligned}$$

$$(c) \underline{M}_B = \underline{BQ} \wedge \underline{F}$$

$$\begin{aligned}&= (-2.5\underline{j}) \wedge (-40\underline{i} - 50\underline{j} + 30\underline{k}) \\ &= -100\underline{k} - 75\underline{i} \\ &= -25(3\underline{i} + 4\underline{k})\end{aligned}$$

$\underline{A} \cdot \underline{y} = 2-14$. XOY $\perp \underline{y} \Rightarrow \underline{A} \cdot \underline{y} = 0 \Rightarrow \underline{A} \cdot \underline{y} = 0$. $\underline{O} \perp \underline{y} \Rightarrow \underline{O} \cdot \underline{y} = 0 \Rightarrow \underline{O} \cdot \underline{y} = 0$. $\underline{O} \perp \underline{y} \Rightarrow \underline{O} \cdot \underline{y} = 0 \Rightarrow \underline{O} \cdot \underline{y} = 0$.

$\underline{P} \perp \underline{y} \Rightarrow \underline{P} \cdot \underline{y} = 0 \Rightarrow \underline{P} \cdot \underline{y} = 0$.

$$\underline{r} = \underline{OP} = 2\underline{i} + \underline{j} \Rightarrow \underline{r} \cdot \underline{y} = 0.$$

$$\underline{F} = 5\underline{i} + 5\underline{j}$$

$$\therefore \underline{M}_0 = \underline{r} \wedge \underline{F}$$

$$= \begin{pmatrix} \underline{i} & \underline{j} & \underline{k} \\ 2 & 1 & 0 \\ 5 & 5 & 0 \end{pmatrix}$$

$$= 5\underline{k} - 1\underline{o}$$

Þá ñ ¼; ÁÐ ÁÆ:

ÁÆ °F | °ÄüÄÎ õ ¾Æ °ÄÆ } ±ý ÁÐ μÄÄÎ ¾Æ °ÄÆ Äî Ì ÈÆ , ðÎ õ.

$$\therefore \underline{F} = 5\underline{i} + 5\underline{j} = 5\sqrt{2} \left(\frac{1}{\sqrt{2}}\underline{i} + \frac{1}{\sqrt{2}}\underline{j} \right)$$

$$= 5\sqrt{2} \underline{\hat{u}}$$

Æ | °ÄüÄÎ õ S, î x « î °¼ý „ ±ý Û õ S, î ½ð °¼ « °° ÁðÄ¾; }Æ

$$\cos_{„} = \frac{1}{\sqrt{2}}, \sin_{„} = \frac{1}{\sqrt{2}}$$

$$\therefore \tan_{„} = 1 = \tan \frac{f}{4}$$

$$\ll \text{ðÄÐ } „ = \frac{f}{4}$$

±É SÄÆ | °ÄüÄÎ õ S, î ðÈø °iÆ × 1 - Ì õ. « Ì S, î ðÈý °Áý Äî Î

$$y-1 = 1(x-2)$$

$$\ll \text{¾; ÁÐ } x-y-1=0.$$

P ±ý ÁÐ O ÁÄÖóÐ x-y-1=0 ±ý Û õ S, ÷ S, î ðÈü Ì Á° ÄÄóÄÎ õ | °í Ì ðÐ Ì S, î ðÈý |¾; °° Ä° Äî Ì ÈÆ Ì Á; É; }Æ.

$$p = -\left(\frac{-1}{\sqrt{1+1}} \right) = \frac{1}{\sqrt{2}}$$

Óì , Äð ¾Æ °ÄÆ , ½ÄÍ , ù

$$\therefore |\underline{M}_0| = |\underline{F}| p$$

$$= 5\sqrt{2} \times \frac{1}{\sqrt{2}}$$

$$= 5 \text{ N}\cdot\text{m}$$

Right handed system) $\underline{M}_O = 5\hat{j} \text{ N}\cdot\text{m}$

Varignon's theorem

Varignon's theorem

(varignon's theorem) $\underline{M}_O = \underline{r} \times \underline{F}$

$\underline{M}_O = (2\hat{i} + \hat{j}) \times (5\hat{j}) = 10\hat{k} \text{ N}\cdot\text{m}$

$\underline{M}_O = 10\hat{k} \text{ N}\cdot\text{m}$

$$|\underline{M}_O| = (-)1 \times 5 + (+)2 \times 5$$

$$= 5 \text{ N}\cdot\text{m}$$

Direction of \underline{M}_O is given by the right hand rule

$\underline{M}_O = 10\hat{k} \text{ N}\cdot\text{m}$

Direction of \underline{M}_O

$$\underline{M}_O = 5\hat{k} \text{ N}\cdot\text{m}$$

Direction of \underline{M}_O

Direction of \underline{M}_O is given by the right hand rule

$\underline{M}_O = 10\hat{k} \text{ N}\cdot\text{m}$

$\underline{M}_O = 10\hat{k} \text{ N}\cdot\text{m}$

$\underline{M}_O = 10\hat{k} \text{ N}\cdot\text{m}$

Problem 2-15

$(12\hat{i} + 4\hat{j} + 3\hat{k}) \times (3\hat{i} + 4\hat{j} + 0\hat{k}) = 12(4\hat{k}) - 3(16\hat{i}) = 48\hat{k} - 48\hat{i} \text{ N}\cdot\text{m}$

(a) $\underline{M}_O = 48\hat{k} - 48\hat{i} \text{ N}\cdot\text{m}$

(b) $\underline{M}_O = 48\hat{k} - 48\hat{i} \text{ N}\cdot\text{m}$

(c) $\underline{M}_O = 48\hat{k} - 48\hat{i} \text{ N}\cdot\text{m}$

(d) $\underline{M}_O = 48\hat{k} - 48\hat{i} \text{ N}\cdot\text{m}$

$\underline{r} = \underline{OP} = 3\hat{i} + 4\hat{j} + 0\hat{k}$

$$= 5\mathbf{i} - 5\mathbf{k}$$

$$= 5\sqrt{2} \left(\frac{\mathbf{i}}{\sqrt{2}} - \frac{\mathbf{j}}{\sqrt{2}} \right)$$

$$= 5\sqrt{2} \underline{w_2}, \underline{w_2} \pm \dot{y} \Delta \theta \underline{BC} \hat{A} \ll \dots \hat{A} \hat{O} \hat{o} \mu \hat{A} \hat{A} \hat{I} \hat{o} \frac{3}{4} \hat{C} \dots \hat{A} \hat{A} \hat{j} \hat{l} \hat{o}.$$

$$\therefore M_{BC} = \underline{M_B} \cdot \underline{w_2}$$

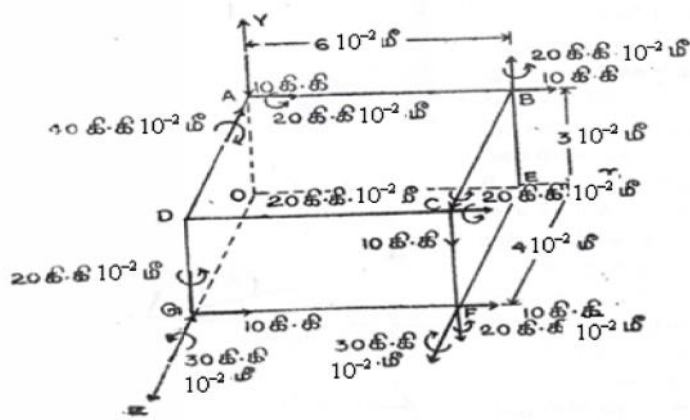
$$= \underline{BP} \wedge \underline{F} \cdot \underline{w_2}$$

$$= \begin{pmatrix} 3 & 4 & -5 \\ 12 & 4 & 3 \\ \frac{1}{\sqrt{2}} & 0 & \frac{-1}{\sqrt{2}} \end{pmatrix}$$

$$= 34\sqrt{2} \hat{A} \hat{e}_x \hat{e}_y \hat{e}_z$$

(ÀÇ· ¼ (a) B, G ±ý Ûõ òùÇÇ, ÇÇø « ·· ÁÔõ ÁÇ· ° ÍÆÄÇ· ½ò |¾|Ì ¾Ç, Û
 ° ìÇÇ, ÄìÉ ·· Ä.

(a) C ±ý Ûõ òùÇÇÄÇø « ·· ÁÔõ ÁÇ· ° ÍÆÄÇ· ½)



À¼õ 2-47

2.9 À¼õ 2.48ø A ±ý Ûõ òùÇÇÄÇø ÁÇ· ° ÍÆÄÇ· ½ |¾|Ì ¾ÄÇø ÁÇ· °,
 ÍÆÄÇ· ½òòò ¾ÇÉý ¬, ÄÄüÉý ±ñ Á¾òò, Û Ó· ÈŠÄ |E|12.5 Ç, Ç ,

$$M_A = 250 \text{ Ç, Ç, Ç } 10^{-2} \text{ Af} \pm \text{ÉÇø} \ll \text{¾ù} \hat{i} \text{ ° } \text{ìÇÇ, ÄìÉ} \text{ ÁÇ· ° ÍÆÄÇ· ½ò |¾|Ì ¾Ç· Ä}$$

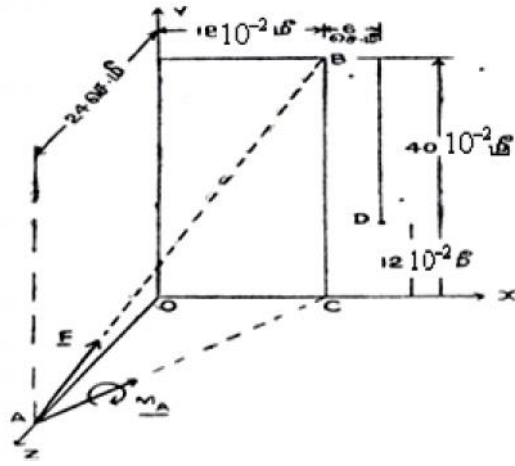
- (i) D ±ý Ûõ òùÇÇ
- (ii) E ±ý Ûõ òùÇÇ
- ¬, ÇÄüÉÇø , ìñ ,

(ÀÇ· ¼ (i) $\underline{F} = (4.5\underline{i} + 10\underline{j} - 6\underline{k}) \text{ Ç, Ç, Ç}$

$$\underline{M}_D = (-18\underline{i} - 36\underline{j} - 386\underline{k}) \text{ Ç, Ç, Ç } 10^{-2} \text{ Ä}$$

(ii) $\underline{F} = (4.5\underline{i} + 10\underline{j} - 6\underline{k}) \text{ Ç, Ç, Ç}$

$$\underline{M}_E = (150\underline{i} + 108\underline{j} - 20\underline{k}) \text{ Ç, Ç, Ç } 10^{-2} \text{ Ä}$$

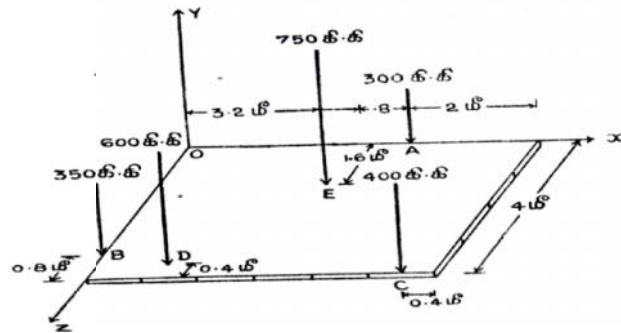


À¼õ 2-48

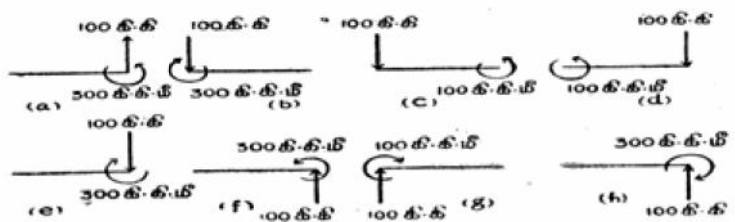
2.10 4ÁÊ X6ÁÊ « Ç×ûÇ ,iý ,ñõ ¼Çõ ´ýÚ (concrete slab) À¼õ 2-49ø (« Í ò¼ Àì õ ,iñ ,) ,iðÊÁÁ;Ú 5 àñ ,Çø |°ÅøÁÍ õ Áç° , Çò ¼jíl Ì ,ÈÐ. Þ´ Á,Úìì î °içç,Áj, « ´ Á0õ ´ü´ È Áç° Åý |°ÅøÁÍ õ òúÇ±ñ Á¼õð - ,ÁÁü´ Èì ,iñ ,.

(Áç° ¼ R = 2400 ,çç,ç±ý Úõ |¼jì ÁÁý Áç° ° (2.732, 0,2.532) Áç±ý Úõ òúÇ±ñ |°ÅøÁÍ ,ÈÐ.

2.11 4Áð¼÷ ççÓúç - ò¼õ (beam) ´ýÈø À¼õ 2.50ø ,iðÊÁÁ;Ú |Áù\$ÁÈ;É Áçç,Çø Áç° ´ýÚõ ¼0õðòð ¼0Èý ´ýÚõ |°ÅøÁÍ ,ýÈÈ. « ÁüÈø ±ùÁõ « ´ Áòð ,ü °içç,Áj,É´ Á±Éì ,iñ ,.



À¼õ 2-49



À¼õ 2-50

2.15. $XY = \frac{3}{4}i + \frac{3}{4}j + \frac{1}{4}k$ $\vec{a} = y\vec{u} + z\vec{v} + w\vec{w}$ $\vec{A} = x\vec{i} + y\vec{j} + z\vec{k}$ $\vec{A} \cdot \vec{a} = 10 \angle 30^\circ$, $(1,0)$
 $\pm y\vec{u} + z\vec{v} + w\vec{w} = 10 \angle -60^\circ, (0, -2)$ $\pm y\vec{u} + z\vec{v} + w\vec{w} = 10 \angle 120^\circ, (0, -4)$
 $\pm y\vec{u} + z\vec{v} + w\vec{w}$. (příl. 1. $\vec{A} = y\vec{u} + z\vec{v} + w\vec{w}$ $\vec{A} \cdot \vec{a} = 10 \angle 30^\circ$ $\vec{A} \cdot \vec{b} = 10 \angle 60^\circ$ $\vec{A} \cdot \vec{c} = 10 \angle 120^\circ$)

- (i) $\vec{A} = y\vec{u} + z\vec{v} + w\vec{w}$ $\vec{A} \cdot \vec{a} = 10 \angle 30^\circ$ $\vec{A} \cdot \vec{b} = 10 \angle 60^\circ$ $\vec{A} \cdot \vec{c} = 10 \angle 120^\circ$
- (ii) $(3,0)$ $\vec{A} = y\vec{u} + z\vec{v} + w\vec{w}$ $\vec{A} \cdot \vec{a} = 10 \angle 30^\circ$ $\vec{A} \cdot \vec{b} = 10 \angle 60^\circ$ $\vec{A} \cdot \vec{c} = 10 \angle 120^\circ$

$\vec{A} \cdot \vec{a} = 10 \cos 30^\circ = 5\sqrt{3}$ (i) $-5k = y\vec{u} + z\vec{v} + w\vec{w}$

(ii) $-20k = y\vec{u} + z\vec{v} + w\vec{w}$

2.16. $30\vec{i} + 40\vec{j} + 50\vec{k}$ $\vec{A} = x\vec{i} + y\vec{j} + z\vec{k}$ $(4,4,-2,5)$ $\vec{A} \cdot \vec{a} = 10 \angle 30^\circ$ $\vec{A} \cdot \vec{b} = 10 \angle 60^\circ$ $\vec{A} \cdot \vec{c} = 10 \angle 120^\circ$
 $\vec{A} \cdot \vec{a} = 10 \cos 30^\circ = 5\sqrt{3}$ $\vec{A} \cdot \vec{b} = 10 \cos 60^\circ = 5$ $\vec{A} \cdot \vec{c} = 10 \cos 120^\circ = -5$
 $\pm y\vec{u} + z\vec{v} + w\vec{w} = 10 \angle 30^\circ$ $\vec{A} \cdot \vec{a} = 10 \angle 30^\circ$ $\vec{A} \cdot \vec{b} = 10 \angle 60^\circ$ $\vec{A} \cdot \vec{c} = 10 \angle 120^\circ$
 $\vec{A} \cdot \vec{a} = 10 \cos 30^\circ = 5\sqrt{3}$ $\vec{A} \cdot \vec{b} = 10 \cos 60^\circ = 5$ $\vec{A} \cdot \vec{c} = 10 \cos 120^\circ = -5$
 $\vec{A} = x\vec{i} + y\vec{j} + z\vec{k}$ $\vec{A} \cdot \vec{a} = 10 \angle 30^\circ$ $\vec{A} \cdot \vec{b} = 10 \angle 60^\circ$ $\vec{A} \cdot \vec{c} = 10 \angle 120^\circ$

($\vec{A} \cdot \vec{a} = 10 \cos 30^\circ = 5\sqrt{3}$)

2.17. $\vec{F} = (12\vec{i} - 7\vec{j} + 8\vec{k})$ $\pm y\vec{u} + z\vec{v} + w\vec{w} = \vec{A} = x\vec{i} + y\vec{j} + z\vec{k}$ $(7,2,2)$ $\pm y\vec{u} + z\vec{v} + w\vec{w} = \vec{A} \cdot \vec{a} = 10 \angle 30^\circ$
 $\vec{A} \cdot \vec{a} = 10 \cos 30^\circ = 5\sqrt{3}$ $\vec{A} \cdot \vec{b} = 10 \cos 60^\circ = 5$ $\vec{A} \cdot \vec{c} = 10 \cos 120^\circ = -5$

($\vec{A} \cdot \vec{a} = 10 \cos 30^\circ = 5\sqrt{3}$)

2.18. (2.17) $\vec{F} = (12\vec{i} - 7\vec{j} + 8\vec{k})$ $\pm y\vec{u} + z\vec{v} + w\vec{w} = \vec{A} = x\vec{i} + y\vec{j} + z\vec{k}$ $(4,-3,6)$ $\pm y\vec{u} + z\vec{v} + w\vec{w} = \vec{A} \cdot \vec{a} = 10 \angle 30^\circ$
 $\vec{A} \cdot \vec{a} = 10 \cos 30^\circ = 5\sqrt{3}$ $\vec{A} \cdot \vec{b} = 10 \cos 60^\circ = 5$ $\vec{A} \cdot \vec{c} = 10 \cos 120^\circ = -5$

($\vec{A} \cdot \vec{a} = 10 \cos 30^\circ = 5\sqrt{3}$)

2.19. (2.17) $\vec{F} = (12\vec{i} - 7\vec{j} + 8\vec{k})$ $\pm y\vec{u} + z\vec{v} + w\vec{w} = \vec{A} = x\vec{i} + y\vec{j} + z\vec{k}$ $(4,-3,6)$ $\pm y\vec{u} + z\vec{v} + w\vec{w} = \vec{A} \cdot \vec{a} = 10 \angle 30^\circ$

(i) $\vec{A} = x\vec{i} + y\vec{j} + z\vec{k}$ $\vec{A} \cdot \vec{a} = 10 \angle 30^\circ$

(ii) $\vec{A} = x\vec{i} + y\vec{j} + z\vec{k}$ $\vec{A} \cdot \vec{a} = 10 \angle 30^\circ$ $\vec{A} \cdot \vec{b} = 10 \angle 60^\circ$ $\vec{A} \cdot \vec{c} = 10 \angle 120^\circ$ $(0.5, 0.5, -0.707)$ $\pm y\vec{u} + z\vec{v} + w\vec{w} = \vec{A} \cdot \vec{a} = 10 \angle 30^\circ$
 $\vec{A} \cdot \vec{a} = 10 \cos 30^\circ = 5\sqrt{3}$ $\vec{A} \cdot \vec{b} = 10 \cos 60^\circ = 5$ $\vec{A} \cdot \vec{c} = 10 \cos 120^\circ = -5$

($\vec{A} \cdot \vec{a} = 10 \cos 30^\circ = 5\sqrt{3}$) (i) $M_x = 30; M_y = -32; M_z = -73$

(ii) 50.611

(iii) -36.239

2.34. $\underline{F} = 6\underline{i} + 3\underline{j} + 10\underline{k}$ ±ý Û õ Ä ¸ ¸ ° A(0,2,3) ±ý Û õ ð ù Ç Ä Å ø
 | ° Ä ü Ä Î ¸ È Ð. B(2,-3,0) ±ý Û õ - \underline{F} ð ù Ç Ä Å ø

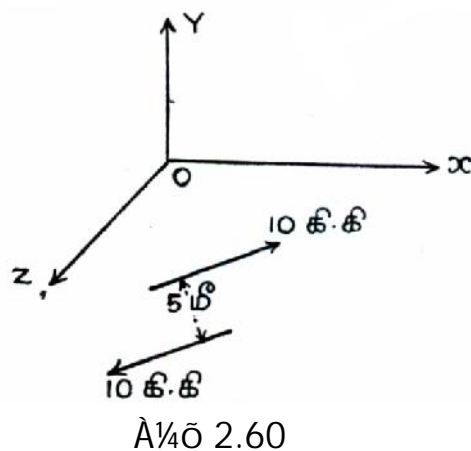
- (i) Í Ä Ä ¸ ¸ ½ ð ð ð ¾ Ä È ý ¾ Ä ¸ ¸ ° Ä ¸
- (ii) Í Ä Ä ¸ ¸ ½ | ° Ä ü Ä Î õ ¾ Ç ð ¾ Ä ü Î î | ° Í Î ð ¾ Í ¸ « ¸ ¸ Ä Ö õ § ¸ ¸ ð È È ý ¾ Ä ¸ ¸ ° ï
 ¸ Ç Ä ï ¸ ¸ ¸ ù.
- (iii) z « î Í Ä ü È Ç Í Ä Ä ¸ ¸ ½ Ä ¸ ý ¾ Ä Ö ð ð ð ¾ Ä È ý
- (iv) Í Ä Ä ¸ ¸ ½ î Î þ ¸ ¸ ¼ Ä Ö ü Ç | ° Í Î ð ð ð | ¾ Í ¸ Ä × ñ ¸ Ä Ä ü ¸ ¸ È ï ¸ ¸ ï ¸ ¸.

- (Ä ¸ ¸ ¼ (i) $\underline{C} = 41\underline{i} + 38\underline{j} - 36\underline{k}$
- (ii) $l = 0.616, m = 0.572, n = -0.541$
- (iii) $M_z = -36$
- (iv) $5.522 \ll \text{Ä Î ¸ ¸ ù}$

2.35. z x ¾ Ç ð ¾ Ä ø | ° Ä ü Ä Î õ Í Ä Ä ¸ ¸ ½ Ä ¼ õ 2.60 ø ¸ ¸ ð È Ä Ä Í Ú ¸ ¸ ù Ç Ð.

- (i) Ð Ä ï ¸ ¸ ð ð ù Ç Ç Ö Ä ü È Ç Í Ä Ä ¸ ¸ ½ ð ð ð ¾ Ä È ¸ ¸ È Ä ¸ ¸ Ä Ä Ü ï ¸ ¸.
- (ii) A(3,4,6) Ä È ±ý Û õ ð ù Ç Ç Ä ü È Ö õ ¾ Ä Ö ð ð ð ¾ Ä È ¸ ¸ È ¸ ¸ ï ¸ ¸.
- (iii) (1=0.8, m=-0.6, n=0) ±ý Ä È Ä ü ¸ ¸ È ð ¾ Ä ¸ ¸ ° ï ¸ ¸ Ç Ä ï ¸ ¸ ¸ Ç Í ¸ × õ Ð Ä ï ¸ ¸ ð
 ð ù Ç Ç Ä ý Ä È Ä Í ¸ × õ | ° ø Ö õ § ¸ ¸ ð § ¸ ¸ Î Ä ü È Ö õ Í Ä Ä ¸ ¸ ½ Ä ¸ ý ¾ Ä Ö ð ð ¾ Ä È ¸ ¸ È ï
 ¸ ¸ ï ¸ ¸.
- (iv) Ä Î ¾ Ä (iii) ø Ä ¸ ¸ Ä Ä Ü ð ¾ § ¸ ¸ ð ¸ ¸ ¼ þ ¸ ¸ ½ Ä Í ¸ þ ¼ õ | Ä Ä ð ð Ð, A(3,4,6) Ä È
 ±ý Û õ ð ù Ç Ç Ä È Ç Ä | ° ø Ö õ § ¸ ¸ ð § ¸ ¸ Î Ä ü È Ö õ Í Ä Ä ¸ ¸ ½ Ä ¸ ý
 ¾ Ä Ö ð ð ð ¾ Ä È ¸ ¸ È ï ¸ ¸ ï ¸ ¸.

Ä ¸ ¸ ¼ (i) $-50\underline{j}$ Ä È ¸ ¸ Ç. Ç. (ii) Ä È ¸ ¸ Ç. Ç. (iii) 0. (iv) 0



§ 3.1.4

Í Eü°ÇÄý ÁjÄÄj, | ÄiÖ | ÇiýÈý ÄÖÄö, ÄÈöÄi ì ö ÄÄö ÄüÜö
 ÄÈöÄi ì ö ÄÄö ÄÄ½ö | öÖö | ¾j Äx - ÇÄÄüÈý | ÄÖi ì ö
 | ¾j | ì î °ÄÄj ö.

¾ÜÄø

$$dv = 2f y dA \therefore v = \int dv = \int 2f y dA = 2f y_c A = (2f y_c) A$$

§Äö ÄÖÄö¾üì | Ä ¾½Çx ÄÄö
 (Ä Ä Ä ÄÄý ÄÄ ÄÖÄö¾üý ¾½Çx ÄÄö)

$$r_c = \frac{1}{v} \int r dv, \text{ - ì ö.}$$

$$\pm \text{É §Ä } x_c = \frac{1}{v} \int x dv; y_c = \frac{1}{v} \int y dv; z_c = \frac{1}{v} \int z dv$$

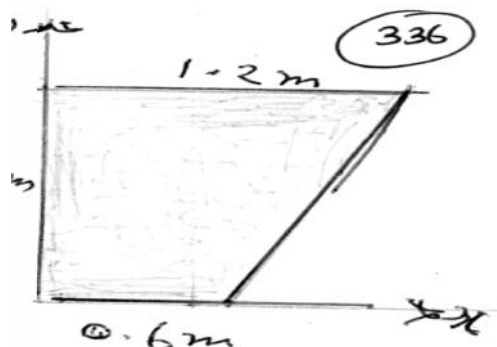
3.1.4 Í Eü°ÇÄý ÁjÄÄj ö | ÄÈöÄi ö ÄÖÄö¾üý ¾½Çx ÄÄí Üìì | Ä
 « ö¼Ä ½ (ÄöÖ ì ÄÈj Š §¾üÈí ü ä Äö)

ÄÇi ö	ÄÈÄö¾üì Ä « Ç Ä ü	x _c	ÄÖÄö
1. « Äi §j ö		$\frac{3}{8}R$	$\frac{2}{3}fR^3$
2. Äö¼ §jÜöð		$\frac{h}{4}$	$\frac{1}{3}fR^2h$
3. Í üÈø « ÄjÄÄj ÇxÖ (semiellipsoid of revolution)		$\frac{3}{8}h$	$\frac{2}{3}fR^2h$
4. Í üÈü ÄÄÄj ÇxÖ (Paraboloid of revolution)		$\frac{h}{3}$	$\frac{1}{3}fR^2h$
5. Äö¼ §jÜöð		$\frac{3}{4}h$	$\frac{1}{3}fR^2h$

3.1.4. ÄÄü°Ç

1. Ä¼ö¾üç jöÈöüç °jÄö ýÈý ÄÄöÄüì | Ä ¾ç Ä ÄÄö¾üç
 ¾ÄÄj Èj xö

$$(\text{Ä} \text{ } \frac{1}{4} : [\bar{x} = 0.433m, \bar{y} = 0.66m])$$



2. Óðø ðíðÁjÉ Àì ¼ÁÀø $y^2 = x, x^2 = y \pm yÉ$ ÞÖ ÁÁÁ Ç× Ùìì Þí ¼ÁÁ ÁÖö ÁÁðÀÇ ÁÁÿ ¼ñ Á ÁÁð ¼ì ðíñ

$$\text{Áç} \frac{1}{4} \left[\bar{x} = \frac{9}{20}, \bar{y} = \frac{9}{20} \right]$$

3. Óðø ðíðÁjÉ Àì ¼ÁÀø $x = y^2, y = \frac{b}{a}x \pm yÉ$ Á ÇÁ Á× Ùìì Þí ¼ÁÁ ÁÖö ÁÁðÀÇ ÁÁÿ ¼ñ Á ÁÁð ¼ì ðíñ

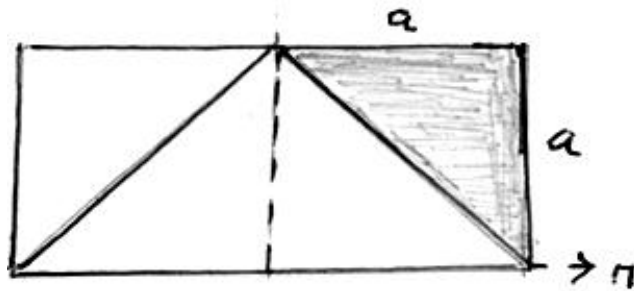
$$\text{Áç} \frac{1}{4} : \bar{x} = \frac{2}{5} \frac{\left(6a^{\frac{1}{2}} - b\right)a}{\left(4a^{\frac{1}{2}} - b\right)}, \bar{y} = \frac{1}{2} \frac{(3a - 2b^2)}{\left(4a^{\frac{1}{2}} - b\right)}$$

4. Óðø ðíðÁjÉ Àì ¼ÁÀø $y = \frac{x^3}{4}, x = \frac{y^2}{b} \pm yÉ$ Á ÇÁ Á× Ùìì Þí ¼ÁÁ ÁÖö ÁÁðÀÇ ÁÁÿ ¼ñ Á ÁÁððúÇ Áð ¼ÁÁjÉ ðíñ × ð.

Áç ¼

$$\bar{x} = \frac{24}{25}, \bar{y} = \frac{6}{7}$$

5. z-« ííì ì ÈðÐ Á ÁÁ¼ð¼ø ðíðÉÖúÇ ðÉø Óì § ðíð ÁÁðÀÇ× 360° « ÇÁùì ÍÉüç §Áü ðíð ð§ÁjÐ ÀÈðÀ ðð¼ ÁÖÁð¼ÿ ¼ñ Á ÁÁð¼ÿ z-« ííð¼ì Á Áì ðíñ



$$\text{Áç} \frac{1}{4} : \left[\bar{z} = \frac{5}{8}a \right]$$

6. Óðø ðíðÁjÉ ð Àì ¼ÁÀø $y = x, y = x^2 \pm yÉ$ Á ÇÁ Á× ù (0,0) (a,a) ±yÉ ðúÇçç ððÉì ðíðÿÉÉ. ÞùÁ ÇÁ Á× Ùìì Þí ¼ÁÁ ÁÖö ÁÁðÀÇ ÁÁÿ ¼ñ Á ÁÁð¼ÿ \bar{x} « ííð¼ì Á Áì ðíñ

Þí ç ÉÁÜÚ ÁÁðÀÇ× dA ðíð ðð « ííì Þí ½Áj ± ððð « ùÁ¼§Á dA ¼« ííì Þí ½Áj × ð ÞÖÖ ÈçÖ ðíñ ðíð¼ì ðíñ × ð.

$$\text{Áç} \frac{1}{4} : \left[\bar{x} = \frac{a}{2} \right]$$

7. Óðöðjörðunir $y = x$ og $y = \frac{1}{4}x^2$ á milli $x = 0$ og $x = 4$. Þetta myndar tvö flötur. Þú ert beðin um að reikna massa þessara flöturanna. (a) Reiknaðu massa flöturanna þegar $\rho = 1$. (b) Reiknaðu massa flöturanna þegar $\rho = 4x$.

3.1.5 Þyngri flötur

Massaflötur (mass) M er ákvarðaður með $M = \int \rho \, dV$ þar sem ρ er þyngdarmassi og dV er lítilnið. Þú ert beðin um að reikna massa flöturanna $y = x$ og $y = \frac{1}{4}x^2$ á milli $x = 0$ og $x = 4$ þegar $\rho = 4x$.

$$r_e = \frac{1}{m} \int r \, dm$$

$$x_c = \frac{1}{m} \int x \, dm; y_c = \frac{1}{m} \int y \, dm; z_c = \frac{1}{m} \int z \, dm$$

Þyngri flötur $y = x$ og $y = \frac{1}{4}x^2$ á milli $x = 0$ og $x = 4$. Þú ert beðin um að reikna massaflöturinn þegar $\rho = 4x$. Þú ert einnig beðin um að reikna þyngripunktið (x_c, y_c) fyrir þessa flötur.

Ástæða

1. Þyngripunkturinn (x_c, y_c) er á milli $x = 0$ og $x = 4$. Þú ert beðin um að reikna x_c og y_c fyrir þessa flötur.

$$dm = \rho \, dx = 4x \, dx$$

$$x_c = \frac{\int_0^4 x \cdot 4x \, dx}{\int_0^4 4x \, dx} = \frac{\int_0^4 x^2 \, dx}{\int_0^4 x \, dx} = \frac{\frac{1}{3}x^3 \Big|_0^4}{\frac{1}{2}x^2 \Big|_0^4} = \frac{\frac{64}{3}}{8} = \frac{8}{3}$$

2. Þyngripunkturinn (x_c, y_c) er á milli $x = 0$ og $x = 4$. Þú ert beðin um að reikna x_c og y_c fyrir þessa flötur.

$\ddot{A}\ddot{A}\ddot{o}\ddot{u}\ddot{c}\ddot{c}$, $\ddot{o}\ddot{A}\ddot{c}$ - $\ddot{O}\ddot{A}\ddot{j}\ddot{i}$ $\ddot{c}\ddot{A}$ $\ddot{O}\ddot{i}$ $\ddot{S}_{,i}$ $\ddot{1}/\ddot{2}\ddot{o}$ $\ddot{A}\ddot{A}\ddot{o}\ddot{A}\ddot{c}\ddot{A}\ddot{y}$ $\ddot{3}/\ddot{4}\ddot{c}\ddot{1}/\ddot{2}\ddot{c}\ddot{x}$
 $\ddot{A}\ddot{A}\ddot{o}\ddot{3}/\ddot{4}\ddot{c}\ddot{o}$ « $\ddot{A}\ddot{O}\ddot{j}\ddot{A}\ddot{E}\ddot{i}$ $\ddot{,i}$ $\ddot{O}\ddot{i}$ $\ddot{,s}$.

$\ddot{3}/\ddot{4}\ddot{c}\ddot{x}$ $\ddot{0}$ $\pm\ddot{y}\ddot{E}$ $\ddot{O}\ddot{u}\ddot{c}\ddot{c}$ $\ddot{,c}$ $\ddot{1}/\ddot{4}\ddot{A}\ddot{c}\ddot{A}$ $\ddot{A}\ddot{O}\ddot{o}$ $\ddot{2}l$, $\ddot{c}\ddot{O}\ddot{u}\ddot{c}$ $\ddot{o}\ddot{A}\ddot{c}\ddot{A}\ddot{y}$ $\ddot{A}\ddot{A}\ddot{o}\ddot{u}\ddot{c}\ddot{A}\ddot{j}$
 $\ddot{O}\ddot{3}/\ddot{4}\ddot{x}\ddot{o}$. $\ddot{o}\ddot{x},\ddot{o}\ddot{y}$ $\pm\ddot{y}\ddot{A}\ddot{E}$ $\ddot{,c}$ $\ddot{1}/\ddot{4}\ddot{c}$ \ddot{A} « $\ddot{i}\ddot{l}$ $\ddot{,c}\ddot{j}\ddot{i}$ \ddot{o} . $\ddot{O}\ddot{i}$ $\ddot{S}_{,i}$ $\ddot{1}/\ddot{2}\ddot{o}$

$\ddot{A}\ddot{A}\ddot{o}\ddot{A}\ddot{u}\ddot{i}$ $\ddot{j}\ddot{c}\ddot{A}$ $\ddot{3}/\ddot{4}\ddot{c}\ddot{1}/\ddot{2}\ddot{c}\ddot{x}$ $\ddot{A}\ddot{A}\ddot{o}$, $\ddot{x}_c = 0$, $\ddot{y}_c = \frac{h}{3}$, $h = \ddot{O}\ddot{i}$ $\ddot{S}_{,i}$ $\ddot{1}/\ddot{2}\ddot{o}\ddot{3}/\ddot{4}\ddot{c}\ddot{y}$
 $\ddot{j}\ddot{o}\ddot{i}$ \ddot{l} $\ddot{o}\ddot{D}$ - $\ddot{A}\ddot{A}\ddot{o}$ $\ddot{3}/\ddot{4}\ddot{c}\ddot{x}\ddot{i}$ \ddot{l} $\ddot{j}\ddot{c}\ddot{A}$ « $\ddot{o}\ddot{1}/\ddot{4}\ddot{A}$ $\ddot{,1}/\ddot{2}$

$\ddot{U}\ddot{U}$	$\ddot{j}\ddot{3}/\ddot{4}\ddot{j}$ $\ddot{A}\ddot{x}$	$\ddot{3}/\ddot{4}\ddot{c}\ddot{1}/\ddot{2}\ddot{c}\ddot{x}$	\ddot{y}_c	\ddot{y}_c $\ddot{3}/\ddot{4}\ddot{c}\ddot{1}/\ddot{2}\ddot{c}\ddot{x}$
« $\ddot{E}\ddot{O}\ddot{A}\ddot{i}$ $\ddot{,o}$	$2l$	$2 \dots l$	0	0
$\ddot{,u}\ddot{j}\ddot{A}\ddot{j}\ddot{O}$ $\ddot{o}\ddot{j}\ddot{O}\ddot{x}\ddot{A}\ddot{i}$ $\ddot{,o}$	$\sqrt{l^2 + h^2}$	$\dots\sqrt{l^2 + h^2}$	$\frac{h}{2}$	$\dots h\sqrt{l^2 + h^2}$
$\ddot{O}\ddot{i}$ $\ddot{S}_{,i}$ $\ddot{1}/\ddot{2}\ddot{o}$ $\ddot{3}/\ddot{4}\ddot{u}\ddot{i}$ $\ddot{j}\ddot{c}\ddot{A}$ $\ddot{j}\ddot{A}\ddot{j}\ddot{o}\ddot{3}/\ddot{4}\ddot{o}$	---	$2 \dots (l + \sqrt{l^2 + h^2})$	\ddot{y}_c	$\dots h\sqrt{l^2 + h^2}$

$$y_c = \frac{\dots h\sqrt{l^2 + h^2}}{2 \dots (l + \sqrt{l^2 + h^2})}$$

- $\ddot{E}\ddot{j}\ddot{o}$,

$$dm = \dots dv, m = \dots v, x_c = \frac{1}{n} \int x dv, y_c = \frac{1}{n} \int y dv, z_c = \frac{1}{n} \int z dv \quad y_c = \frac{h}{3} \pm \ddot{E}\ddot{S}\ddot{A}$$

$$\frac{h}{3} = y_c = \frac{\dots h\sqrt{l^2 + h^2}}{2 \dots (l + \sqrt{l^2 + h^2})}$$

$$h\sqrt{l^2 + h^2} = 2hl$$

$$l^2 + h^2 = 4l^2$$

$$h = \sqrt{3}l$$

$$\alpha = \tan^{-1} \frac{h}{l} = \tan^{-1}(\sqrt{3}) = 60^\circ$$

$$\pm \ddot{E}\ddot{S}\ddot{A} \quad \bar{y} = \frac{v_1 y_1 - v_2 y_2 - v_3 y_3}{v_1 - v_2 - v_3}$$

$$= \frac{19}{25} = 0.76m$$

$y = x, y = x^2$ $\pm\ddot{y}\ddot{E}$ \ddot{A} $\ddot{,c}\ddot{A}$ $\ddot{A}\ddot{x}$, $\ddot{U}\ddot{i}\ddot{l}$ \ddot{u} « $\ddot{1}/\ddot{4}\ddot{i}$ $\ddot{,O}\ddot{u}\ddot{c}$ $\ddot{A}\ddot{A}\ddot{o}\ddot{A}\ddot{c}$ $\ddot{A}\ddot{A}\ddot{y}$
 $\ddot{3}/\ddot{4}\ddot{c}\ddot{A}\ddot{o}\ddot{u}\ddot{c}\ddot{c}$ $\ddot{A}\ddot{o}$ $\ddot{3}/\ddot{4}\ddot{c}\ddot{A}\ddot{j}\ddot{E}\ddot{c}$ $\ddot{,s}$ $\ddot{x}\ddot{o}$.

3.1.1. $\bar{x} = \frac{\int_A x dA}{\int_A dA} = \frac{\int_0^1 x(y_2 - y_1) dx}{\int_0^1 (y_2 - y_1) dx} = \frac{\int_0^1 x(x - x^2) dx}{\int_0^1 (x - x^2) dx}$

$$\bar{x} = \frac{\int_0^1 x(x - x^2) dx}{\int_0^1 (x - x^2) dx} = \frac{\frac{1}{2}x^2 - \frac{1}{3}x^3}{\frac{1}{2}x^2 - \frac{1}{3}x^3} \Big|_0^1 = \frac{\frac{1}{2} - \frac{1}{3}}{\frac{1}{2} - \frac{1}{3}} = \frac{\frac{1}{6}}{\frac{1}{6}} = 0.5 \text{ m}$$

3.1.2. $\bar{x} = \frac{\int_A x dA}{\int_A dA} = \frac{\int_0^1 x(x_1 - x_2) dy}{\int_0^1 (x_1 - x_2) dy} = \frac{\int_0^1 \left[\frac{x_1 + x_2}{2} \right] (x_1 - x_2) dy}{\int_0^1 (x_1 - x_2) dy}$

3.2

3.2.1. $\bar{x} = \frac{\int_A x dA}{\int_A dA} = \frac{\int_0^1 \left[\frac{x_1 + x_2}{2} \right] (x_1 - x_2) dy}{\int_0^1 (x_1 - x_2) dy}$

$$\bar{x} = x_2 + \frac{x_1 - x_2}{2} = \frac{x_1 + x_2}{2}$$

$$\begin{aligned} \bar{x} &= \frac{\int_0^1 \left[\frac{x_1 + x_2}{2} \right] (x_1 - x_2) dy}{\int_0^1 (x_1 - x_2) dy} \\ &= \frac{\int_0^1 \left[\frac{\sqrt{y} + y}{2} \right] (\sqrt{y} - y) dy}{\int_0^1 (\sqrt{y} - y) dy} \\ &= \frac{\frac{1}{2} \int_0^1 [y - y^2] dy}{\int_0^1 (\sqrt{y} - y) dy} = \frac{1}{2} \text{ m} \end{aligned}$$

3.3

3.3.1. $\bar{x} = \frac{\int_A x dA}{\int_A dA} = \frac{\int_0^1 x(x_1 - x_2) dy}{\int_0^1 (x_1 - x_2) dy}$

3.3.2. $\bar{x} = \frac{\int_A x dA}{\int_A dA} = \frac{\int_0^1 \left[\frac{x_1 + x_2}{2} \right] (x_1 - x_2) dy}{\int_0^1 (x_1 - x_2) dy}$

$$\therefore \bar{x} = \frac{\int x dm}{M} = \frac{\int_0^a x(2fa^2 + x) dx}{\frac{1}{2}(fa^2 + a^3)}$$

$$= \frac{1}{a} \int_0^a x dx = \frac{1}{2} a$$

4. $\vec{r}_c = \frac{1}{M} \int \vec{r} dm$ $\vec{r}_c = \frac{1}{M} \int_0^a x \hat{i} (2fa^2 + x) dx = \frac{1}{M} \left(2fa^2 x + \frac{x^2}{2} \right) \Big|_0^a = \frac{1}{M} \left(2fa^3 + \frac{a^3}{2} \right) = \frac{a}{2}$

$$\vec{r}_c = \frac{ax}{h}$$

$\vec{r}_c = \frac{ax}{h}$ $\vec{r}_c = \frac{ax}{h}$ $\vec{r}_c = \frac{ax}{h}$

$$2f \frac{ax}{h} \Delta s = \frac{2f ax}{h} \frac{l}{h} \Delta x,$$

$$\left(\therefore \frac{\Delta s}{l} = \frac{\Delta x}{h} \right)$$

$\vec{r}_c = \frac{ax}{h}$

$$dm = \left(\frac{2fa}{h^2} \right) x \Delta x$$

$$\bar{x} = \frac{2fal}{h^2} \int_0^h x^2 dx = \frac{2}{3} h$$

3.3 $\vec{r}_c = \frac{1}{M} \int \vec{r} dm$

$\vec{r}_c = \frac{1}{M} \int \vec{r} dm$ $\vec{r}_c = \frac{1}{M} \int \vec{r} dm$ $\vec{r}_c = \frac{1}{M} \int \vec{r} dm$

$$\underline{F} = \int d\underline{F} = - \int g dm \underline{k} = -g \int dm \underline{k} = -mg \underline{k}$$

$\vec{r}_c = \frac{1}{M} \int \vec{r} dm$ $\vec{r}_c = \frac{1}{M} \int \vec{r} dm$ $\vec{r}_c = \frac{1}{M} \int \vec{r} dm$

$$\underline{r}_c \wedge \underline{F} = \underline{r} \wedge (-g dm \underline{k})$$

$$\ll \oint \underline{r}_c \wedge (-mg \underline{k}) = \int \underline{r} \wedge (-g dm \underline{k})$$

$$\ll \oint \underline{r}_c \wedge m \underline{k} = \int \underline{r} \wedge dm \underline{k}$$

$\pm \underline{E} \underline{S} \underline{A}$

$$x_c = \frac{1}{m} \int x dm = \frac{1}{m} \int x \dots dv$$

$$y_c = \frac{1}{m} \int y dm = \frac{1}{m} \int y \dots dv$$

$$\begin{aligned} \bar{x} &= \frac{\int x dA}{A} = \frac{\int_0^1 \left[\frac{x_1 + x_2}{2} \right] (x_1 - x_2) dy}{\int_0^1 (x_1 - x_2) dx} \\ &= \frac{\int_0^1 \left[\frac{\sqrt{y} + y_2}{2} \right] (\sqrt{y} - y) dx}{\int_0^1 (\sqrt{y} - y) dy} \\ &= \frac{1}{2} \frac{\int_0^1 (y - y^2) dy}{\int_0^1 (\sqrt{y} - y) dy} \end{aligned}$$

பொதுக்குறிப்பாக $\bar{x} = \frac{\int x dA}{A}$ மற்றும் $\bar{y} = \frac{\int y dA}{A}$.

மேலும், $\bar{x} = \frac{\int x dA}{A}$ மற்றும் $\bar{y} = \frac{\int y dA}{A}$ என்பனவே, \bar{x} மற்றும் \bar{y} ஆகியவை \bar{x} மற்றும் \bar{y} ஆகியவற்றின் மையநிலைகளைக் குறிக்கின்றன.

3.5 பொதுக்குறிப்பாக $\bar{x} = \frac{\int x dA}{A}$ மற்றும் $\bar{y} = \frac{\int y dA}{A}$ என்பனவே, \bar{x} மற்றும் \bar{y} ஆகியவை \bar{x} மற்றும் \bar{y} ஆகியவற்றின் மையநிலைகளைக் குறிக்கின்றன.

1. $\bar{x} = \frac{\int x dA}{A}$ மற்றும் $\bar{y} = \frac{\int y dA}{A}$
2. $\bar{x} = \frac{\int x dA}{A}$ மற்றும் $\bar{y} = \frac{\int y dA}{A}$
3. $\bar{x} = \frac{\int x dA}{A}$ மற்றும் $\bar{y} = \frac{\int y dA}{A}$

1. $\bar{x} = \frac{\int x dA}{A}$ மற்றும் $\bar{y} = \frac{\int y dA}{A}$ என்பனவே, \bar{x} மற்றும் \bar{y} ஆகியவை \bar{x} மற்றும் \bar{y} ஆகியவற்றின் மையநிலைகளைக் குறிக்கின்றன.

2. $\bar{x} = \frac{\int x dA}{A}$ மற்றும் $\bar{y} = \frac{\int y dA}{A}$ என்பனவே, \bar{x} மற்றும் \bar{y} ஆகியவை \bar{x} மற்றும் \bar{y} ஆகியவற்றின் மையநிலைகளைக் குறிக்கின்றன. m_1, m_2, m_3, \dots என்பனவே, \bar{x} மற்றும் \bar{y} ஆகியவற்றின் மையநிலைகளைக் குறிக்கின்றன. ox, oy என்பனவே, \bar{x} மற்றும் \bar{y} ஆகியவற்றின் மையநிலைகளைக் குறிக்கின்றன. $\bar{x} = \frac{\int x dA}{A}$ மற்றும் $\bar{y} = \frac{\int y dA}{A}$ என்பனவே, \bar{x} மற்றும் \bar{y} ஆகியவை \bar{x} மற்றும் \bar{y} ஆகியவற்றின் மையநிலைகளைக் குறிக்கின்றன. அமைவதாகக் குறிப்பிட்டு அமையும் திருப்புத்திறனைக் கொள்க, O புள்ளியில் அமையும்

$$\left\{ \bar{x} = \frac{\sum_{i=1}^n m_i x_i}{M}; \bar{y} = \frac{\sum_{i=1}^n m_i y_i}{M}; M = \sum_{i=1}^n m_i \right\}$$

« $\bar{x} = \frac{\int x dA}{A}$ மற்றும் $\bar{y} = \frac{\int y dA}{A}$ என்பனவே, \bar{x} மற்றும் \bar{y} ஆகியவை \bar{x} மற்றும் \bar{y} ஆகியவற்றின் மையநிலைகளைக் குறிக்கின்றன.

$$\left(\bar{x} = \frac{1}{M} \sum mx, \bar{y} = \frac{1}{M} \sum my, \bar{z} = \frac{1}{M} \sum mz \right) \text{ என்பனவே, } \bar{x} \text{ மற்றும் } \bar{y} \text{ ஆகியவை } \bar{x} \text{ மற்றும் } \bar{y} \text{ ஆகியவற்றின் மையநிலைகளைக் குறிக்கின்றன.}$$

" \vec{r}_c " - "Position Vector" $\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$

$\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$

$\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$

$\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$

$\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$

AEAO	AEAo	\vec{r}_c	x_c
<p>$\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$</p>		<p>$2Rr$</p> <p>$\frac{R}{2}$</p> <p>fR</p> <p>$2fR$</p>	<p>$\frac{R \sin r}{r}$</p> <p>$\frac{2\sqrt{2}R}{f}$</p> <p>$\frac{2R}{f}$</p> <p>$x_c = 0, y_c = 0$</p>

3.6 $\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$

1. $\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$
2. $\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$
3. $\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$
4. $\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$
5. $\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$
6. $\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$
7. $\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$
8. $\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$
9. $\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$
10. $\vec{r}_c = x_c \vec{i} + y_c \vec{j} + z_c \vec{k}$ $\pm \epsilon_i$ $\vec{r}_c = \int \vec{r} dl$ $r_c = \frac{1}{l} \int \vec{r} dl$

°ÁýÀ;Î ¸ ¸ Ç ±Ø¾×õ.

11. Í üÈÛý ŞÄüÄÄòð (Surface of revolution) ´ýÚ ±üÄ;Ú - ÕÄ;ì òÄÎ ÈÐ?
12. Í Äü°Äý Ä;ÄÄ; | Ä;Õü ´ýÚ - ÕÄ;ì òÄÎ Ä ¸ ¾ ÄÇì Ì ¸.
13. ÀòÕŠ - Í øÈÇ;ñ (GUI papusdinus) §¾üÈò ¸ì ÜÜ
14. Í Äü°Ä;ø Ç;øø ŞÄüÄÄ° Ä ¸ ÄÄÜòÄ¾ü;É §;ì Ä Äì |;ì ¸õ.
15. ±ò¾ ÇÄó¾ È Çý « ÈòÄ ¸ Äø (a) ¾ñ Ä ¸ ÄÄòüÇòò, ÒÄÄèò ¸ ÄÄóò (b) ÒÄÄèò ¸ ÄÄóò ¾½× ¸ ÄÄóò ´ŞÄ þ¾øø þ ¸ ½òò?
16. þØ¾ ¸ « Ç×Õ× ü (vectors) « Ç×ü ´ýÈü |;ýÚ | í Ì ò¾; ¸ « ¸ ÄÄ « ÄüÈý Ì Üì ò | ÄÖì ø äí°ÄÄ; ŞÄñ Í ò
17. ¾ ¸°ÄÄÄ Äò | Ä;Üòð, ¾ ¸ ¸ « Ç×ÕÄý Ä ¸ |;ø (DIFFERENTIATION) ¾ ¸ ¸ « Ç×Õ ¸ Õ Ä;ÈÄ¾ ¸ « Ç×ÕÄ;ø äí°ÄÄ;ì ò.
18. ¾ ¸°ÄÄÄ Äò | Ä;Üòð ¾ ¸ ¸ « Ç×ÕÄý |¾; ¸ (integral) |;ì Ì òÄò¾ ¾ ¸ ¸ « Ç×ÕÄý | ÄøÄÎ ò ¾ ¸ ¸ Äò ¾Äèòð, ÄüÈ¾ ¸ ¸ Ä ²üÜì |;üÇç ç ò.
19. ¾ ¸°ÄÄÄ Ä ò;÷¾ ò;÷ÄÄÉý ò;ç×, Õ ¾ ¸ ¸ « Ç×Õ, ¾ ¸°ÄÄÄ ò;÷¾ ò;÷ÄÄÉý | í Ì ò¾; É Ä;ÜÄ;ò Ì ¾ ¸ ¸°ÄÄÄ « ¸ ÄÄŞÄñ Í ò.
20. r - ¸ ÄòüÇ ¸ « ¸ ÄÄò¾ø¾Äø Äø ´ýÈý ¾½× ¸ ÄÄò¾ý þòòÄ¾ò ¸ ¸;ñ ¸.

$$\begin{aligned} \bar{A}_y &= 2 \int_0^{\frac{f}{2}} (R^2 dr) R \cos r = 2R^2 dr \int_0^{\frac{f}{2}} \cos r dr \\ &= 2R^2 [\sin r]_0^{\frac{f}{2}} = 2R^2 \\ A &= f R \\ \therefore \bar{y} &= \frac{2R^2}{f R} = \frac{2R}{f} \end{aligned}$$

$$\text{¾½× ¸ ÄÄò¾ý þòòÄ¾ò} = \left(0, \frac{2R}{f} \right)$$

21. ´ŞÄ°Ä;É ¾ÈòüÇ ¾;Î ´ýÚ °ÄÄÈò¾ð ¾;Î ´ýÈüì ¾½× ¸ ÄÄóò ÒÄÄèò ¸ ÄÄóò ´ýÜÄÎ ò.

Ä ¸ ¼:
 ÒÄÄèò ¸ ÄÄò (centre of gravity)
 ¾ ¸ ¸ §;ì ð §°;ì ¸ ±üÄ;É;ÄÜò | Ä;ÕÇý « ¸ Èòðò ÇÈò | ÄøÄÎ ò òüÇŞÄ ÒÄÄèò ¸ ÄÄò ±ýÚ Ä ¸ ÄÄÜì òÄÎ ò.

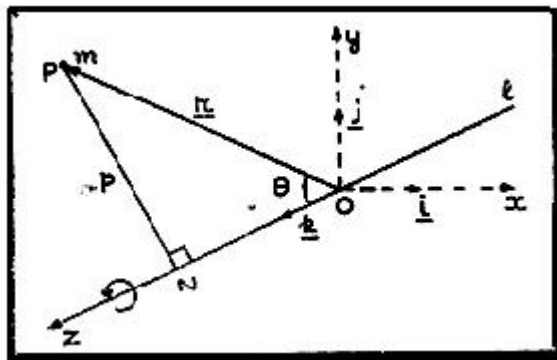
¾½× ¸ ÄÄòüÇç (centre of mass)
 | Ä;ÕÇý Óø ¸ ÄÄ;É ¾½×õ µ;¾ø¾ø ¾Äò¾òÄÎ Ä¾; ¾ü§;Ç ´ýÈ « ¸ Äòðì |;ñ ¼;ø, « òòüÇç ¸ ¾½× ¸ ÄÄòüÇç ±ýÚ

« $\frac{1}{2} \sum m_i r_i^2$
 (Moment of Inertia)

« $\frac{1}{2} \sum m_i r_i^2$ « $\frac{1}{2} \sum m_i r_i^2$ « $\frac{1}{2} \sum m_i r_i^2$

3.7 « $\frac{1}{2} \sum m_i r_i^2$.

« $\frac{1}{2} \sum m_i r_i^2$ « $\frac{1}{2} \sum m_i r_i^2$ « $\frac{1}{2} \sum m_i r_i^2$ « $\frac{1}{2} \sum m_i r_i^2$



(7.1)

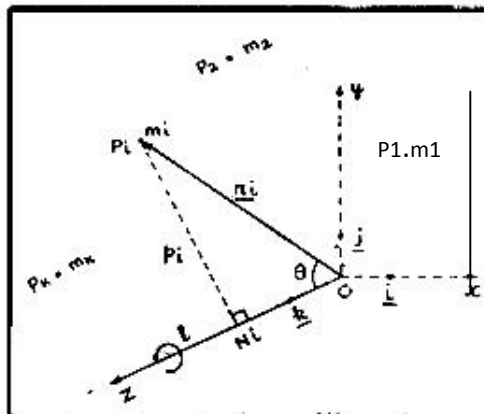
« $\frac{1}{2} \sum m_i r_i^2$

$$I = \sum m_i r_i^2 = \sum m_i (x_i^2 + y_i^2 + z_i^2)$$

« $\frac{1}{2} \sum m_i r_i^2$ « $\frac{1}{2} \sum m_i r_i^2$ « $\frac{1}{2} \sum m_i r_i^2$ « $\frac{1}{2} \sum m_i r_i^2$

$$I = m_1 p_1^2 + m_2 p_2^2 + \dots + m_i p_i^2 + \dots + m_n p_n^2$$

$$= \sum_{i=1}^n m_i p_i^2$$



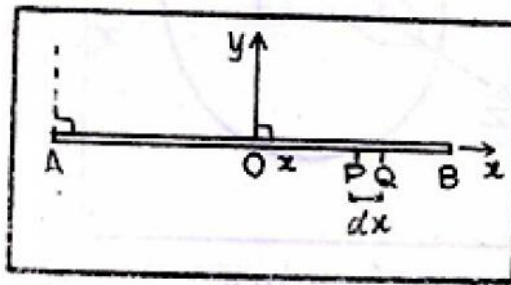
$$\begin{aligned}
 I_z &= \int_m (x^2 + y^2) dm \\
 &= \int_m x^2 dm + \int_m y^2 dm \\
 &= I_y + I_x \\
 &= I_x + I_y
 \end{aligned}$$

(İ Ğōō: pōš¼üĒō ¼Çō¼ĀĀ ĀŌō ¼đĪ šĀıyĒ ĨĀıŌüı ŨıĪ ĀđĪ šĀ ¼üĒ¼ıĪ ō, ¼đĒŪı ō ĨĀıŌüı ŨıĪ pĐ ĨĀıŌō¼ıĐ.)

3.10 ¼Ā ¼đĒŪı ō ĨĀıŌüı ÇŸ ĨĀĀđ ¼ŌŌđ¼ĒĒ

3.10.1 ¼Ō ¼ĀıĒ š¼ıø (Uniform rod)

Ā¼ō (7.6) AB ¼ŸĀĐ ¼ĀıĒ š¼ıı Āı ĨĒŸ đĪ ō. AB = 2a Ĩı. « ¼Ÿ ĨĀĀ ĒĪ ō. O ¼ŸĀĐ « ¼Ÿ ĀĀđ ¼ı ĨĒŸ đĪ ō. Oy ¼ŸĀĐ, š¼ıŌıĪ Ĩı Ĩı Ĩı « ĀŌō « Ĩı ĨĒŸ ĒĐ. š¼ıĀŸ « ¼÷¼Ē ... Ĩı.



Ā¼ō (7.6)

¼y pĪĪĀ, « Ĩ š¼ıĀŸ ĨĀĀđ ¼ŌŌđ¼ĒĒ

$$\begin{aligned}
 &\int_m \dots^2 dm \\
 &= \int_{-a}^{+a} x^2 (\dots dx) \\
 &= 2\rho \frac{a^2}{3} = (2a\dots) \frac{a^2}{3} = M \frac{a^2}{3} \text{ Ĩı.}
 \end{aligned}$$

Ā ¼Ÿ Ũō Ōı ĒĀĒšĀ Oy pĪĪĀ pı ¼ĀıĒ Ĩı Ĩı ŌŌō « Ĩı ¼ĀüĒĀ ĨĀĀđ ¼ŌŌđ¼ĒĒ, pĪĪĀĪ ō š¼üĒ¼ıĪ ĒĒ,

$$= M \frac{a^2}{3} + Ma^2 = \frac{4Ma^2}{3} \text{ Ĩı.}$$

3.10.2 ¼ĀıĒ Ĩı ŨĀđ ¼đĪ

$$I_z = \int_m \dots^2 dm$$

$$= \int_m \dots ds a^2 = a^2 \dots \int_0^{2af} ds = (2f a \dots) a^2 = Ma^2$$

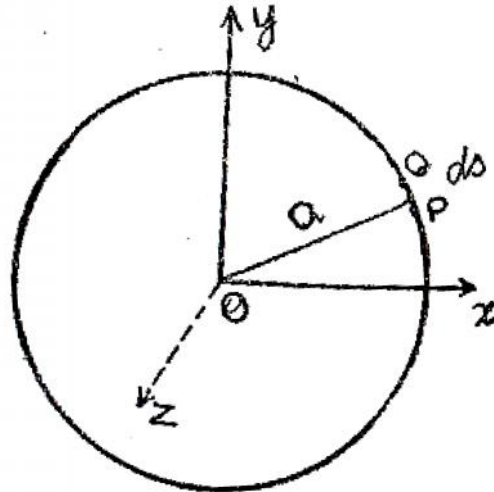


Figure 7.8

(ii) For a circular lamina of radius a and mass M , $I = I_x = I_y$ about the z -axis.

$$I_z = I_x + I_y = 2I_x = Ma^2$$

$$\therefore I = I_x = I_y = \frac{Ma^2}{2}$$

(iii) For a circular lamina of radius a and mass M , $I = I_x = I_y = \frac{Ma^2}{2}$ about the x -axis and y -axis.

$$I = \frac{Ma^2}{2} + Ma^2 = \frac{3Ma^2}{2}$$

(iv) For a circular lamina of radius a and mass M , $I = I_x = I_y = \frac{Ma^2}{2}$ about the x -axis and y -axis.

$$= Ma^2 + Ma^2 = 2Ma^2$$

3.10.4 Moment of Inertia of a Rod

Let a rod of length l and mass M be placed along the x -axis with one end at the origin O and the other end at $x = l$. The mass per unit length is $\frac{M}{l}$. The moment of inertia about the z -axis is to be found.

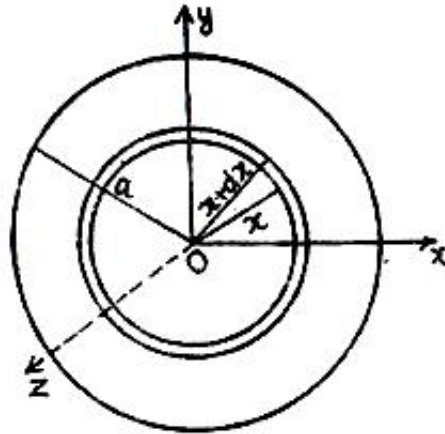


Figure 7.9

$$(1) I_z = \int_0^a x^2 dm = \int_0^a x^2 (2f x dx) = 2f \int_0^a x^3 dx = 2f \frac{a^4}{4} = (2f a^2) \frac{a^2}{2} = M \frac{a^2}{2}$$

(ii) The moment of inertia about the y-axis is given by

$$I_y = I_x = \frac{I_z}{2} = M \frac{a^2}{4}$$

(iii) The moment of inertia about the x-axis is given by

$$I_x = \frac{Ma^2}{2} + Ma^2 = \frac{3Ma^2}{2}$$

(iv) The moment of inertia about the z-axis is given by

$$I_z = \frac{Ma^2}{2} + Ma^2 = \frac{3Ma^2}{2}$$

3.10.5 The ellipse is given by

the ellipse is given by

$$\frac{x^2}{a^2} + \frac{y^2}{b^2} = 1$$

where $M = f ab$

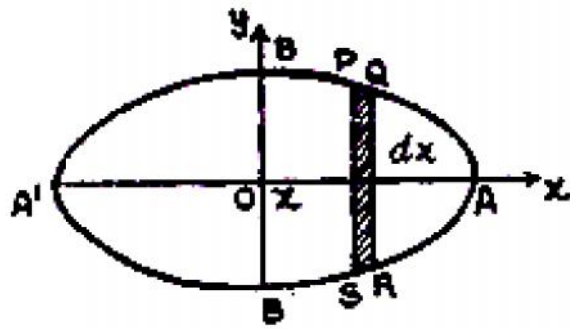


Figure 7.10

$$\begin{aligned}
 (i) \quad I_x &= \int_{-a}^{+a} (2y dx) \frac{y^2}{3} = \frac{4}{3} \int_0^a y^3 dy \\
 &= \frac{4}{3} \cdot \frac{b^3}{a^3} \int_0^a (a^2 - x^2)^{\frac{3}{2}} dx \\
 &= \frac{4}{3} \cdot \frac{b^3}{a^3} \int_0^{\frac{\pi}{2}} a^3 \cos^3 \theta a \cos \theta d\theta, (x = a \sin \theta) \\
 &= \frac{4}{3} \cdot \frac{b^3}{a^3} \int_0^{\frac{\pi}{2}} a^4 \cos^4 \theta d\theta \\
 &= \frac{4}{3} \cdot \frac{b^3}{a^3} \times \frac{3}{4} \times \frac{1}{2} \times \frac{\pi}{2} = \frac{4}{3} \cdot \frac{b^3}{a^3} \cdot \frac{3\pi}{8} = \frac{M}{4} \frac{b^2}{4}
 \end{aligned}$$

$$(ii) \quad I_y = M \frac{a^2}{4}$$

$$\begin{aligned}
 (iii) \quad I_z &= I_x + I_y = M \frac{a^2}{4} + M \frac{b^2}{4} = \frac{M}{4} (a^2 + b^2)
 \end{aligned}$$

3.10.6 Hollow circular cylinder

A hollow circular cylinder of radius a , height h , and mass m is shown in Figure 3.10.6. The cylinder is centered at the origin of the x - y axes. The z -axis is along the length of the cylinder.

$$\begin{aligned}
 (i) \quad I_x &= \int dm a^2 = a^2 \int dm = M a^2
 \end{aligned}$$

$$(ii) \quad I_y = M a^2$$

$$\begin{aligned}
&= 2f \dots \int_{-a}^{+a} y^3 \cdot \frac{a}{y} dx \\
&= 4af \dots \int_0^a y^2 dx \\
&= 4af \dots \int_0^a (a^2 - x^2) dx \\
&= 4af \dots \left[a^3 - \frac{a^3}{3} \right] \\
&= (4f a^2 \dots) \cdot \frac{2a^2}{3} \\
&= M \cdot \frac{2a^2}{3}
\end{aligned}$$

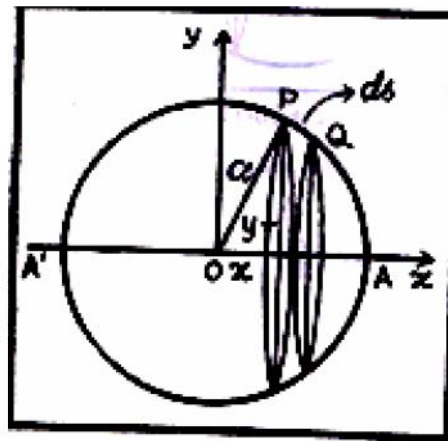


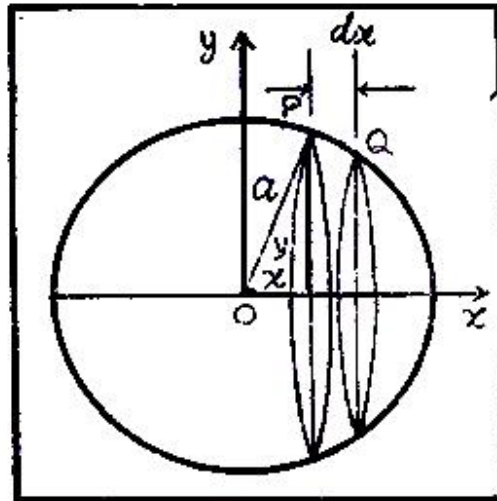
Figure 7.13

(ii) The moment of the lamina about the x-axis is given by

$$M \frac{2a^2}{3} + Ma^2 = \frac{5Ma^2}{3}$$

3.10.9. Uniform solid sphere

$$M = \frac{4}{3} f a^3 \dots, dm = f y^2 dx \dots$$



A 7.14

(i) $\frac{1}{2} \rho \int_{-a}^{+a} y^2 dx$ $\frac{1}{2} \rho \int_{-a}^{+a} y^2 dx$

$$= \int_{-a}^{+a} (f y^2 dx) \frac{y^2}{2}$$

$$V^2 = \frac{1}{h_o^2} (1 - 2e \sin \theta + e^2)$$

$$= f P a^5 \frac{4}{5} \times \frac{2}{3}$$

$$= \frac{4f a^3}{3} \times \frac{2a^2}{5}$$

$$= M \cdot \frac{2a^2}{5}$$

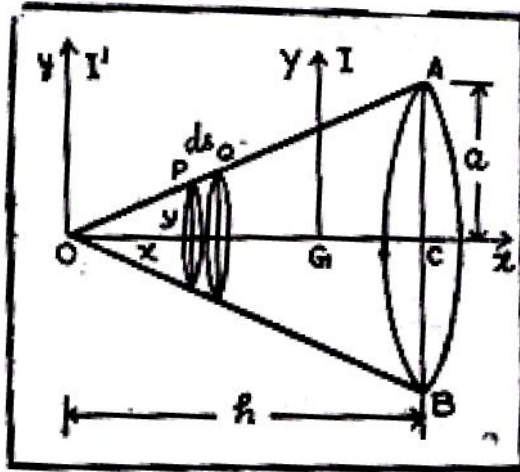
(ii) $\frac{2Ma^2}{5} + Ma^2 = \frac{7Ma^2}{5}$

$$= \frac{2Ma^2}{5} + Ma^2 = \frac{7Ma^2}{5}$$

3.10.10 $\rho \int_{-a}^{+a} y^2 dx$ (Hollow cylinder)

a, h, l, m $\frac{1}{2} \rho \int_{-a}^{+a} y^2 dx$ $\frac{1}{2} \rho \int_{-a}^{+a} y^2 dx$ $\ll \frac{1}{2} \rho \int_{-a}^{+a} y^2 dx$ $\frac{1}{2} \rho \int_{-a}^{+a} y^2 dx$

$$M = f a l p; dn = 2f y ds P, \frac{y}{a} = \frac{x}{h}$$



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(i) « ¾ý « îí ÀüËç çç' ÄÄð ¾ÄÖð¾ÄËÿ .

$$\begin{aligned}
 &= \int 2f y ds P \cdot y^2 \\
 &= 2f P \int_{x=0}^{x=h} y^3 \sqrt{1 + \left(\frac{dy}{dx}\right)^2} dx \\
 &= 2f P \int_0^h y^3 \cdot \frac{1}{h} dx \\
 &= \frac{2f P l a^3}{h^3} \int_0^h x^3 dx \\
 &= \frac{2f P l a^3}{h^4} \cdot \frac{h^4}{4} \\
 &= (f a l p) \cdot \frac{a^2}{2} \\
 &= M \cdot \frac{a^2}{2}
 \end{aligned}$$

(ii) « ¾ý - î°ÄËÄî çç' « ¾ý « îíîî î | °í î ð¾î çç' - üÇ S ç î ÄüËç - üÇËø ÜöÄÿ çç' ÄÄð ¾ÄÖð¾ÄËÿ

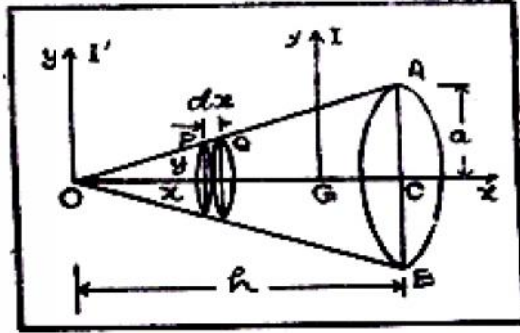


Figure 7.16

(i) To find the moment of inertia of the lamina about the y-axis.

$$\begin{aligned}
 &= \int dm \cdot \frac{y^2}{2} = \int_0^h f y^2 dx P \cdot \frac{y^2}{2} \\
 &= \frac{f p}{2} \int_0^h y^4 dx = \frac{f p}{2} \cdot \frac{a^4}{h^4} \int_0^h x^4 dx \\
 &= \frac{f p}{2} \cdot \frac{a^4}{h^4} \cdot \frac{h^5}{5} \\
 &= \frac{1}{3} f a^2 h p \cdot \frac{3a^2}{10} \\
 &= M \cdot \frac{3a^2}{10}
 \end{aligned}$$

(ii) To find the moment of inertia of the lamina about the x-axis.

$$\begin{aligned}
 &= \int (dm \frac{y^2}{4} + dm x^2) \\
 &= \int_0^h (\frac{y^2}{4} + x^2) f y^2 dx P \\
 &= f P \frac{a^2}{h^2} \cdot (\frac{a^2}{4h^2} + 1) \int_0^h x^4 dx \\
 &= \frac{f P a^2 (a^2 + 4h^2)}{4h^4} \times \frac{h^5}{5} \\
 &= (\frac{1}{3} f a^2 h p) \cdot \frac{3}{20} (a^2 + 4h^2) \\
 &= M \cdot \frac{3}{20} (a^2 + 4h^2) \\
 I' &= \frac{3M}{20} (a^2 + 4h^2)
 \end{aligned}$$

(iii) $\bar{U} \text{ o} \bar{A} \bar{C} \bar{E} \text{ o} \bar{D} \dots \bar{A} \bar{A} \bar{o} \text{ G} \bar{A} \bar{E} \bar{C} \bar{A} \bar{j} \dots \ll \bar{i} \bar{r} \bar{k} \bar{c} \bar{s} \bar{s} \bar{e} \bar{s} \bar{i} \bar{l} \bar{o} \bar{3} \bar{j} \bar{o} \bar{U} \bar{C} \bar{S} \bar{j} \bar{i} \bar{A} \bar{A} \bar{U} \bar{E} \bar{C} \bar{U} \bar{o} \bar{A} \bar{C} \bar{E} \bar{y} \bar{z} \bar{C} \bar{A} \bar{A} \bar{o} \bar{3} \bar{A} \bar{C} \bar{O} \bar{o} \bar{D} \bar{3} \bar{A} \bar{C} \bar{E} \bar{y} = I$

$$I + M \left(\frac{3h}{4} \right)^2 = I' = \frac{3M}{20} (a^2 + 4h^2)$$

$$\therefore I = \frac{3M}{20} (a^2 + 4h^2) - \frac{9Mh^2}{16}$$

$$= \frac{3M}{20} (4a^2 + 4h^2 - 15h^2) = \frac{3M}{8} (4a^2 + h^2)$$

(iv) $\ll \bar{3} \bar{4} \bar{y} \ll \bar{E} \bar{A} \bar{o} \bar{1} \bar{4} \bar{A} \bar{o} \bar{1} \bar{4} \bar{o} \bar{A} \bar{U} \bar{E} \bar{C} \bar{z} \bar{C} \bar{A} \bar{A} \bar{o} \bar{3} \bar{A} \bar{C} \bar{O} \bar{o} \bar{D} \bar{3} \bar{A} \bar{C} \bar{E} \bar{y}$

$$= I + M \left(\frac{h}{4} \right)^2$$

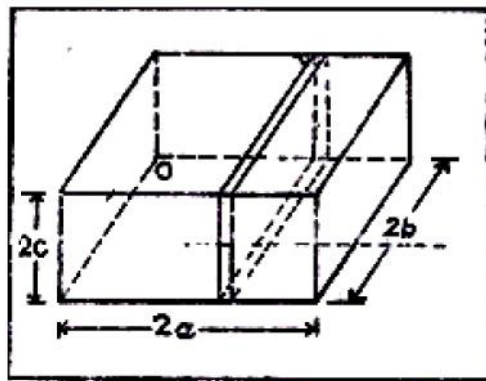
$$= \frac{3M}{80} (4a^2 + h^2) + \frac{Mh^2}{16}$$

$$= \frac{M}{80} (12a^2 + 3h^2 + 5h^2)$$

$$= \frac{M}{20} (3a^2 + 2h^2)$$

3.10.12 $\bar{E} \bar{i} \bar{o} \bar{u} \bar{A} \bar{o}$ (Rectangular parallelepiped).

$M \bar{z} \bar{C} \bar{E} \bar{O} \bar{u} \bar{C} \bar{E} \bar{i} \bar{o} \bar{u} \bar{A} \bar{o} \bar{3} \bar{4} \bar{y} \bar{A} \bar{i} \bar{r} \bar{i} \bar{u}, \bar{O} \bar{E} \bar{S} \bar{A} \bar{2} \bar{a}, \bar{2} \bar{b}, \bar{2} \bar{c} \bar{-} \bar{l} \dots$
 $\ll \bar{3} \bar{4} \bar{y} \bar{o} \bar{A} \bar{C} \bar{E} \bar{o} \bar{D} \dots \bar{A} \bar{A} \bar{o} \bar{a} \bar{-} \bar{l} \dots \bar{a} \bar{3} \bar{o} \bar{1} \bar{3} \bar{j} \bar{1} \bar{4} \bar{i} \bar{o} \bar{U} \bar{C} \bar{A} \bar{j} \bar{o}, \ll \bar{3} \bar{4} \bar{y} \bar{A} \bar{E} \bar{C} \bar{S} \bar{A} \bar{2} \bar{a}, \bar{2} \bar{b}, \bar{2} \bar{c} \bar{\pm} \bar{y} \bar{U} \bar{o} \bar{A} \bar{C} \bar{o} \bar{D} \bar{U} \bar{i} \bar{l} \bar{p} \bar{1} \bar{2} \bar{A} \bar{j} \bar{a} \bar{x}, \bar{a} \bar{y}, \bar{a} \bar{z} \bar{\pm} \bar{y} \bar{U} \bar{o} \bar{a} \bar{y} \bar{U} \bar{i} \bar{o} \bar{i} \bar{l} \bar{o} \bar{D} \bar{a} \bar{x} \bar{i} \bar{l} \bar{i} \bar{o} \bar{1} \bar{o} \bar{3} \bar{j} \bar{p} \bar{O} \bar{i} \bar{l} \bar{A} \bar{j} \bar{U}, \bar{E} \bar{i} \bar{o} \bar{u} \bar{A} \bar{o} \bar{3} \bar{4} \bar{i} \bar{o} \bar{E} \bar{C} \bar{A} \bar{U} \bar{U} \bar{C} \bar{j} \bar{o} \bar{A} \bar{C} \bar{i} \bar{o} \bar{u} \bar{i} \bar{A} \bar{j} \bar{O} \bar{D} \bar{n} \bar{i} \bar{o} \bar{2} \bar{b}, \bar{2} \bar{c} \bar{\pm} \bar{y} \bar{A} \bar{A} \bar{C} \bar{o} \bar{A} \bar{i} \bar{r} \bar{i} \bar{C} \bar{j} \bar{i} \bar{l} \bar{i} \bar{j} \bar{i} \bar{n} \bar{1} \bar{o} \bar{u} \bar{A} \bar{o} \bar{3} \bar{4} \bar{j} \bar{i} \bar{o}.$



$\bar{A} \bar{1} \bar{o} (7.17)$

$\bar{a} \bar{x} \bar{i} \bar{l} \bar{i} \bar{o} \bar{1} \bar{o} \bar{3} \bar{j} \bar{p} \bar{O} \bar{i} \bar{l} \bar{A} \bar{j} \bar{U}, \bar{E} \bar{i} \bar{o} \bar{u} \bar{A} \bar{o} \bar{3} \bar{4} \bar{i} \bar{o} \bar{E} \bar{C} \bar{A} \bar{U} \bar{U} \bar{C} \bar{j} \bar{o}$

$\int_{-a}^a \int_{-b}^b \int_{-c}^c \rho(x,y,z) dx dy dz$

$\cdot ax \text{ } \int_{-a}^a \int_{-b}^b \int_{-c}^c \rho(x,y,z) dx dy dz = \rho \int_{-a}^a x dx \int_{-b}^b dy \int_{-c}^c dz$
 $= \rho \left[\frac{x^2}{2} \right]_{-a}^a \cdot 2b \cdot 2c = \rho \cdot \frac{2a^2}{2} \cdot 4bc = 2\rho a^2 bc$

$\cdot oy, oz \text{ } \int_{-a}^a \int_{-b}^b \int_{-c}^c \rho(x,y,z) dx dy dz = 0$

$M \left(\frac{c^2 + a^2}{3} \right); M \left(\frac{a^2 + b^2}{3} \right) - \text{ஓ}$

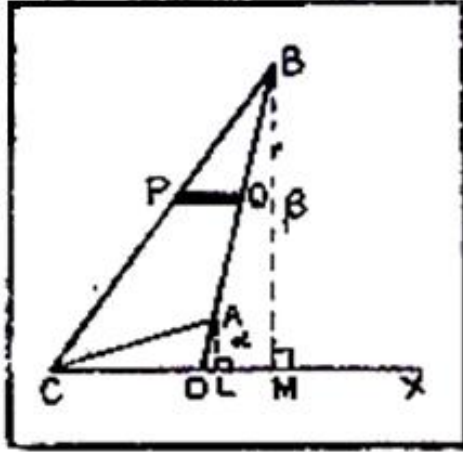
$\int \int \int \rho(x,y,z) dx dy dz = \rho \int_{-a}^a \int_{-b}^b \int_{-c}^c dx dy dz = \rho \cdot 2a \cdot 2b \cdot 2c = 8\rho abc$
 $\int \int \int \rho(x,y,z) x dx dy dz = \rho \int_{-a}^a x dx \int_{-b}^b dy \int_{-c}^c dz = \rho \cdot \frac{2a^2}{2} \cdot 4bc = 4\rho a^2 bc$

$(ii) \int \int \int \rho(x,y,z) y dy dx dz = \rho \int_{-a}^a dx \int_{-b}^b y dy \int_{-c}^c dz = \rho \cdot 2a \cdot \frac{2b^2}{2} \cdot 2c = 4\rho a b^2 c$
 $= \frac{2Ma^2}{3} + M \cdot (a^2 + ah^2) = \frac{8Ma^2}{3}$

3.11 Equimomental systems.

$\rho \int_{-a}^a \int_{-b}^b \int_{-c}^c x^2 dx dy dz = \rho \int_{-a}^a x^2 dx \int_{-b}^b dy \int_{-c}^c dz = \rho \cdot \frac{2a^3}{3} \cdot 4bc = \frac{8\rho abc a^2}{3}$

3.11.1 M $\int_{-a}^a \int_{-b}^b \int_{-c}^c x^2 dx dy dz = \rho \int_{-a}^a x^2 dx \int_{-b}^b dy \int_{-c}^c dz = \rho \cdot \frac{2a^3}{3} \cdot 4bc = \frac{8\rho abc a^2}{3}$
 $\int_{-a}^a \int_{-b}^b \int_{-c}^c y^2 dx dy dz = \rho \int_{-a}^a dx \int_{-b}^b y^2 dy \int_{-c}^c dz = \rho \cdot 2a \cdot \frac{2b^3}{3} \cdot 2c = \frac{8\rho abc b^2}{3}$
 $\int_{-a}^a \int_{-b}^b \int_{-c}^c z^2 dx dy dz = \rho \int_{-a}^a dx \int_{-b}^b dy \int_{-c}^c z^2 dz = \rho \cdot 2a \cdot 2b \cdot \frac{2c^3}{3} = \frac{8\rho abc c^2}{3}$



À¼õ (7.18)

A, B çÄÖó¼ CX ì Ì AL, BM ±ýÛõ òí Ì òDi §, î ç Ä" Å, AL=r, BM=s ñ Ì .

$$\begin{aligned}
 M &= \Delta ABC \text{ Äý ç" È} \\
 &= P \times \text{Óì §, j ½ò¼ý Ä" Åç} \times \\
 &= P[\Delta BCD - \Delta ACD] \\
 &= P\left[\frac{1}{2}CD.s - \frac{1}{2}CD.r\right] \\
 &= \frac{P}{2}.CD(\beta - \alpha)
 \end{aligned}$$

CD ì ç Ì ñ ñ Äì ç" Ä ± Ì Ì . « çý Ä" Ò, dA = PQ × dy

$$= \frac{CD}{s}(s - y)dy$$

$$\therefore dm = \text{Ññ Äì ç" È} = PdA = P \frac{CD}{s} (P - y)dy$$

$$CX \text{ Ä" Å ç" È} = PdA.y^2$$

$$\therefore CX \text{ Ä" Å, BCD} \pmýÛõ \text{ Óì §, j ½ò¼ý ç" Ä" Ò ç" Èý}$$

$$= \int_0^s P \cdot \frac{CD}{s} - (s - y)y^2 dy$$

$$= p \cdot \frac{CD}{s} \left[s \cdot \frac{s^3}{3} - \frac{s^4}{4} \right]$$

$$= \frac{P \cdot CD}{12} \cdot s^3$$

« ùÄjSÈ, CX Ä" Å w₁ - ACD ±ýÛõ Óì §, j ½ò¼ý ç" Ä" Ò

$$\text{ç" Èý} = \frac{P \cdot CD}{12} \cdot r^3 \text{ ñ Ì õ.}$$

$$\begin{aligned}
& \pm \text{É} \text{Ş} \text{Å}, \text{CX} \text{À} \text{ü} \text{È} \text{Ç}, \Delta ABC \text{ ý } \text{ç} \text{Ç} \text{''} \text{Ä} \text{Ä} \text{ò} \text{¾} \text{Ç} \text{Ö} \text{ò} \text{¾} \text{Ç} \text{È} \text{ý} \\
& = \frac{P \cdot CD}{12} \cdot (s^3 - r^3) \\
& = \frac{P \cdot CD}{12} \cdot (s - r) \frac{1}{6} (s^2 + rs + r^2) \\
& = \frac{M}{6} (s^2 + rs + r^2)
\end{aligned}$$

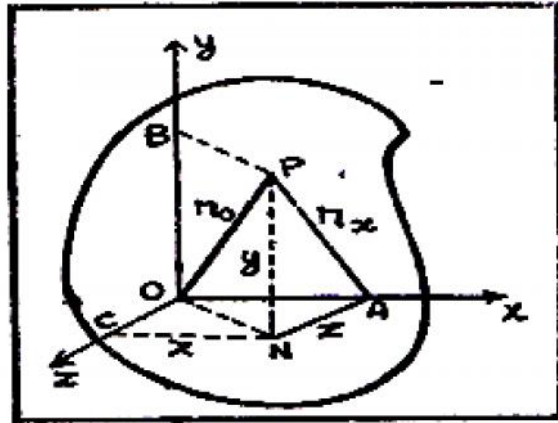
$A'B'C$ \pm ý $\hat{U} \text{õ}$ $\text{ò} \text{ü} \text{Ç} \text{Ç}, \text{ü} \text{ Ó} \text{''} \text{È} \text{Ş} \text{Å} \text{ BC, CA, AB} \pm$ ý $\hat{U} \text{õ}$ $\text{À} \text{ì} \text{,} \text{í} \text{,} \text{ç} \text{Ç} \text{ý}$
 $\text{ç} \text{Ì} \text{ò} \text{ò} \text{ü} \text{Ç} \text{Ç}, \text{Ç} \text{ç} \text{ì} \text{,} \text{ç} \text{,} \text{«} \text{ò} \text{ò} \text{ü} \text{Ç} \text{Ç}, \text{ü} \text{ 'ü} \text{!} \text{Ä} \text{ç} \text{ý} \text{È} \text{Ç} \text{ø} \text{«} \text{''} \text{Ä} \text{Ö} \text{õ} \frac{M}{3} \pm$ ý $\hat{U} \text{õ}$ $\text{ç} \text{Ç} \text{''} \text{È} \text{''} \text{Ä} \text{ò}$
 $\text{!} \text{Ä} \text{ü} \text{È} \text{ } \text{ã} \text{ý} \text{Ü} \text{ } \text{Đ} \text{,} \text{ü} \text{,} \text{ç} \text{Ç} \text{ý} \text{ } \text{¾} \text{Ç} \text{½} \text{Ç} \text{x} \text{''} \text{Ä} \text{Ä} \text{Ö} \text{õ}, \Delta ABC \text{ ý } \text{¾} \text{Ç} \text{½} \text{Ç} \text{x} \text{''} \text{Ä} \text{Ä} \text{Ö} \text{õ}$
 $\text{ý} \text{È} \text{ç} \text{ì} \text{õ.} \pm \text{É} \text{Ş} \text{Å}, \text{ÇX} \text{«} \text{î} \text{!} \text{Ä} \text{ü} \text{È} \text{Ç}, \text{«} \text{õ} \text{ã} \text{ý} \text{Ü} \text{ } \text{Đ} \text{,} \text{ü} \text{,} \text{ç} \text{Ç} \text{È} \text{ } \text{ç} \text{Ç} \text{''} \text{Ä} \text{Ä} \text{ò}$
 $\text{¾} \text{Ç} \text{Ö} \text{ò} \text{¾} \text{Ç} \text{È} \text{ý} \text{.}$

$$\begin{aligned}
& = \frac{M}{3} \left[\left(\frac{r}{2}\right)^2 + \left(\frac{s}{2}\right)^2 + \left(\frac{r+s}{2}\right)^2 \right] \\
& = \frac{M}{12} \times \frac{1}{4} [r^2 + s^2 + (r+s)^2] \\
& = \frac{M}{12} [2r^2 + 2s^2 + 2rs] \\
& = \frac{M}{6} (r^2 + rs + s^2)
\end{aligned}$$

$\text{CX} \text{À} \text{ü} \text{È} \text{Ç} \text{Ä} \text{Ó} \text{ì} \text{Ş} \text{,} \text{ç} \text{ç} \text{ì} \text{ } \text{½} \text{ò} \text{¾} \text{Ç} \text{ý} \text{ } \text{ç} \text{Ç} \text{''} \text{Ä} \text{Ä} \text{ò} \text{¾} \text{Ç} \text{Ö} \text{ò} \text{¾} \text{Ç} \text{È} \text{ü} \text{õ} \text{ } A'B'C \pm$ ý $\hat{U} \text{õ}$ $\text{ò} \text{ü} \text{Ç} \text{Ç}, \text{Ç} \text{Ç} \text{ø}$
 $\text{«} \text{''} \text{Ä} \text{Ö} \text{õ} \frac{M}{3} \pm$ ý $\hat{U} \text{õ}$ $\text{ç} \text{Ç} \text{''} \text{È} \text{,} \text{''} \text{Ç} \text{Ö} \text{''} \text{¼} \text{Ä} \text{ } \text{ã} \text{ý} \text{Ü} \text{°} \text{Ä} \text{Ä} \text{ç} \text{È} \text{ } \text{Đ} \text{,} \text{ü} \text{,} \text{ç} \text{Ç} \text{ý} \text{ } \text{ç} \text{Ç} \text{''} \text{Ä} \text{Ä} \text{ò}$
 $\text{¾} \text{Ç} \text{Ö} \text{ò} \text{¾} \text{Ç} \text{È} \text{ü} \text{õ} \text{ } \text{p} \text{í} \text{Ş} \text{,} \text{°} \text{Ä} \text{Ä} \text{ç} \text{È} \text{¾} \text{ç} \text{ø}, \text{«} \text{ü} \text{Ä} \text{Ö} \text{ } \text{!} \text{¾} \text{ç} \text{ì} \text{ } \text{¾} \text{Ç} \text{,} \text{Ü} \text{õ} \text{°} \text{Ä} \text{¾} \text{Ç} \text{Ö} \text{ò} \text{¾} \text{Ç} \text{È} \text{ý}$
 $\text{!} \text{¾} \text{ç} \text{ì} \text{ } \text{¾} \text{Ç} \text{,} \text{Ç} \text{ç} \text{ì} \text{,} \text{ç} \text{ç} \text{ý} \text{È} \text{È} \text{.}$

3.12 $\text{¾} \text{ò} \text{Đ} \text{Ä} \text{ò} \text{ } \text{!} \text{Ä} \text{Ö} \text{ì} \text{,} \text{õ}$ (Product of inertia)

$\text{O} \pm$ ý $\hat{U} \text{õ}$ $\text{ò} \text{ü} \text{Ç} \text{Ç} \text{Ä} \text{ø} \text{OX, OY, OZ} \pm$ ý $\text{Ä} \text{''} \text{Ä} \text{ } \text{ý} \text{È} \text{ì} \text{ } \text{!} \text{,} \text{ç} \text{ç} \text{ý} \text{Ü} \text{ } \text{!} \text{°} \text{í} \text{ } \text{ì} \text{ } \text{ò} \text{¾} \text{ç} \text{ç}$
 $\text{«} \text{''} \text{Ä} \text{Ö} \text{õ} \text{«} \text{î} \text{!} \text{''} \text{Ç} \text{ì} \text{ } \text{ì} \text{È} \text{ç} \text{ } \text{õ} \text{ì} \text{õ.} \text{P}(x, y, z) \pm$ ý $\text{Ä} \text{Đ} \text{ } \text{ø} \text{È} \text{Ü} \text{ì} \text{ } \text{ó} \text{ } \text{!} \text{Ä} \text{ç} \text{Ö} \text{ü}$
 $\text{ý} \text{È} \text{ø} \text{ } \text{2} \text{Ş} \text{¾} \text{Ü} \text{ } \text{!} \text{Ä} \text{ç} \text{Ö} \text{ü} \text{Ç} \text{Ç} \text{!} \text{ } \text{ç} \text{ç} \text{ì} \text{.} \text{«} \text{ò} \text{ò} \text{ü} \text{Ç} \text{Ç} \text{Ä} \text{ø} \text{«} \text{ò} \text{!} \text{Ä} \text{ç} \text{Ö} \text{ç} \text{ý} \text{ } \text{Ó} \text{°} \text{È} \text{Ç} \text{Ä} \text{ } \text{dm}$
 $\text{ç} \text{Ç} \text{''} \text{È} \text{Ö} \text{ü} \text{Ç} \text{Ä} \text{ì} \text{ } \text{¾} \text{Ç} \text{''} \text{Ä} \text{Ä} \text{¼} \text{õ} \text{(7.19)} \text{ø} \text{ } \text{ç} \text{ç} \text{È} \text{Ä} \text{ç} \text{Ü} \text{ } \pm \text{ì} \text{ } \text{ì} \text{ } \text{x} \text{õ.} \text{!} \text{Ä} \text{ç} \text{Ö} \text{ç} \text{ý} \text{ } \text{¾} \text{ò} \text{Đ} \text{Ä} \text{ò}$
 $\text{!} \text{Ä} \text{Ö} \text{ì} \text{ } \text{!} \text{,} \text{ç} \text{ç} \text{ü} \text{Ä} \text{ý} \text{Ä} \text{Ö} \text{õ} \text{Ä} \text{''} \text{Ä} \text{Ä} \text{Ü} \text{ò} \text{¾} \text{ } \text{!} \text{¾} \text{ç} \text{ì} \text{''} \text{ } \text{Ä} \text{ñ} \text{ } \text{ç} \text{ç} \text{ì} \text{ø} \text{Ä} \text{''} \text{Ä} \text{Ä} \text{Ü} \text{ì} \text{,} \text{ò} \text{Ä} \text{ì} \text{õ.}$



À¼õ (7.19)

$$I_{xy} = \int_m xy dm = I_{yx}$$

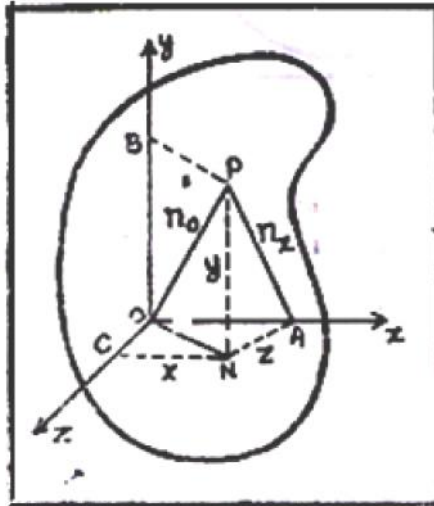
$$I_{yz} = \int_m yz dm = I_{zy}$$

$$I_{zx} = \int_m zx dm = I_{xz}$$

2§¼ÛŞÁ; « î° ò ÀüËÃ ç° ÄÀð ¼õðò¼õËý ±òŞÀ;Ðò Áç° Ì Èç° Äò
 |ÀüËÕì ò, - É;ø °¼ðÐÀò|ÀÕì ò, « î° Ç Ì ÈòÐ ç° ÈÃý
 ç° Àì Ì 2üËÁ;Û Áç° Ì Èõ° ¼Á¾; ×õ Ì ° È Ì Èõ° ¼Á¾; ×õ « øÄÐ
 âî°Ã Á¾õð° ¼Á¾; ×õ þÕì Ì ÛÌ ò. ŞÁÕò ðËÛì ò |Á;Õ|Ç;ýÛ
 2§¼ÛÁÕ - Áð|¾; Á |°í Ì ðÐò ¼Çí ° Çí °;÷¾ |°ù|Á;Øí Ì
 (symmetrical) « °° Äò° Äò |ÀüËÕì Ì |ÁËø, °¼ðÐÀò|ÀÕì Ì Ì ù
 âî°ÃÁ;ì ò.

3.12.1 ¼Çí ù, « î° ù, ðùÇç ù - ÇÁü° Èò ÀüËÃ ç° ÄÀð
 ¼õðò¼õËý, Ûì Ì þ° ¼ŞÁÕùÇ - È° Áì Ì Ì ¼ø.

- (i) 2§¼Û|Á;Õ « î° ò ÀüËÃ |Á;Õ|Ç;ýËý ç° ÄÀð
 ¼õðò¼õËý, « ùÁî°ý ÁËŞÁ Á° ÄÀðÁì ò þÕ |°í Ì ðÐ
 ¼Çí ù ÀüËÃ ç° ÄÀð ¼õðò¼õËý, Çý ÛÌ ¼Õì Ì °Á;ì ò.
 À¼õ (7-20) ø OX ±ý Ûò « î°, XOY, ZOY ±ý Ûò |°í Ì ðÐò
 ¼Çí ù |ÁðËì |ì ù Ûò S; ð¼;ø Á° ÄÁÛì Ì Ì ò.



À¼õ (7.20)

$I_{xx}, I_{(x,y)}, I_{(z,x)}$ ±ýÀ Á Ó ÈŞÀ |À;ÕÇý ox« îÍ ÀüÈÀ, (x, y) ¾ÇÕ (z,x) ÀüÈÀ ç ÁÀð ¾Õð¾Èý ç Ì Èà õ.

« ôŞÀ;Ð,

$$I(x, y) = \int_m z^2 dm$$

$$I(z, x) = \int_m y^2 dm$$

$$I_{xx} = \int_m rx^2 dm = \int_m (y^2 + z^2) dm$$

$$= \int_m y^2 dm + \int_m z^2 dm$$

$$= I(z, x) + I(x, y)$$

±ýÈ;Ì õ

$$\therefore I_{xx} = I(z, x) + I(x, y)$$

« ùÀ;ŞÈ

$$I_{yy} = I(x, z) + I(y, z)$$

$$I_{zz} = I(y, z) + I(z, x)$$

±ýÀ Á, Ù õ ç ¼ì Ì õ,

(ii) ¾Û |À;Õ ðüÇ Áò ÀüÈÀ, |À;Õ |Ç;ýÈý ç ÁÀð ¾Õð¾Èý ÁÈŞÀ ýÚ | ýÚ | í Ì ð¾; ÞÒÌ |À;Û Á ÁÀòÁÌ õ ã ýÚ ¾ÇÍ ù ÀüÈÀ ç ÁÀð ¾Õð¾Èý Çý Û Ì Ì ÁÀ;Ì õ.

(À¼õ 7.20)ø Ó±ýÛ ðüÇÀ;ÈÐ, ý È |À;ýÚ | í Ì ð¾; |ÀðÈì | ýÚ õ xoy, yoz, zox ±ýÛ ã ýÚ ¾ÇÍ Ç;ø Á ÁÀÛ ðÁÌ õ. Ó ðüÇ ÀüÈÀ |À;Õ |Ç;ýÈý ç ÁÀð ¾Õð¾Èý È I, ±Èì | ýÚ.

dm ±y Æ Ð | Àj Õ Çy Ä Ç Ññ ½ Ä À Ì ¾ Äy Ç È Æ Ì È Æ ð ï ö. « î ° È Ä Ç È (x, y, z) ±y Û Ä Õ ð ¾ Ç Ø p Þ Õ ð Ä ¾ j Ì | j Û j. o-ì Ì ö p-ì Ì ö Þ Ì ¼ Ä Õ Õ Ç | ¾ j Ì Ä × r_o Ì Ì j. ±É Š Ä

$$r_o^2 = x^2 + y^2 + z^2 \quad \text{Ì Ì ö.}$$

$$\begin{aligned} I_o &= \int \rho r_o^2 dm, \quad \text{O Ä Û È Ä Ç È Ä Ä ð ¾ Õ ð ¾ Ç È y} \\ &= \int_m r_o^2 dm \\ &= \int_m (x^2 + y^2 + z^2) dm \\ &= \int_m x^2 dm + \int_m y^2 dm + \int_m z^2 dm \\ &= I_{(y,z)} + I_{(z,x)} + I_{(x,y)} \\ \therefore I_o &= I_{(x,y)} + I_{(y,z)} + I_{(z,x)} \end{aligned}$$

Ì Ì ö.

(iii) ±y È | Äj y Û | ° í Ì ð ¾ j Ì | Ä ð È Ì | j Û Û ö ã y Û « î í Û Ä Û È Ä Ç È Ä Ä ð ¾ Õ ð ¾ Ç È y Ç y Û Ì ¾ Ø, « ù Ä î Ì Û « Ì Ä Õ ð ¾ Ç È ° Ì Ç î ° j Ä j Ä Ø, « Ì Ä Û | Ä ð È Ì | j Û Û ö ð ù Ç È Ä Ä ð Ì Š Ä ° j ð ¾ ¾ j Ì ö.

$I_{xx} + I_{yy} + I_{zz}$ ±y Ä Ä Ó È Š Ä, | Äj Õ | Ç j y È y OX, OY, OZ « î í Û Ä Û È Ä Ç È Ä Ä ð ¾ Õ ð ¾ Ç È y Ì Ç Ì È Ì | Ä È Ø,

$$\begin{aligned} I_{xx} + I_{yy} + I_{zz} &= \int_m (y^2 + z^2) dm + \int_m (z^2 + x^2) dm + \int_m (x^2 + y^2) dm \\ &= 2 \int_m (x^2 + y^2 + z^2) dm \\ &= 2I_o. \end{aligned}$$

Ì Ì ö.

O Ä Ä Õ ð ð dm ±y Û ö Ññ ½ Ä Ç È Ä y Ç È Ä Ä r_o ±y Û ö Ç È Ä ð ¾ Ç È ° Ä Ä Ä Ä Û Ì È ð. « ó Ç È Ä ð ¾ Ç È ° Ä Ç O Ä Ø « Ì Ä Õ « î í Ç y ¾ Ç È ° Ì Ç î ° j ð ¾ Ä j Ä Ø, O-Ì Ä Ä ð Ì Š Ä ° j ð ð Û Ç ð. ±É Š Ä I_o ±y Æ Ð Ä Õ Ä Ä Ä j Ì ö.

$$\text{Ì j Š Ä } I_{xx} + I_{yy} + I_{zz} = \text{Ì Ö Ä j È Ç.}$$

3.13 (¾ ð | ¼ j y È y) ¾ Ä Ä j Ä « î í Û Û ö, ¾ Ä Ä j Ä Ç È Ä Ä ð ¾ Õ ð ¾ Ç È y Û ö.

¾ ð | ¼ j y È y ¾ Ç ð ¾ Ç Ä ¼ ö (7.21) ð j ð È Ä Ä j Û, OX, OY ±y Ä Ä Ä Ç È Ä Ä Ä « î í Ì Ç Ì È Ì ð Ì ö. OZ ±y Æ Ð O Ø « ð ¾ Ç ð ¾ Ç Û Ì î ° í Ì ð ¾ j Ì « Ì Ä Õ « î ° j Ì Ä Ä ±y Æ Ð XOY ¾ Ç ð ¾ Ç O Ä È Š Ä | ° Ø Ö ö ² § ¾ Û | Äj Õ § j ð Ì ¼ Ì

È Ì Ò Ò. « Ð x « î Í ¼ y „ § „ i ½ ò ò ¾ « „ Á Ò Á ¾ i „ ì | „ i Û „ . p (x, y) ± y Û Á ¼ ò ¾ ò, dm ± y Û ò ¾ „ Ò È y Á „ î ò È Á „ ç „ È ò Ò Á ¾ i „ ì | „ i Û „ , ò „ § Á, Á „ Á Á „ È Ò Á È,

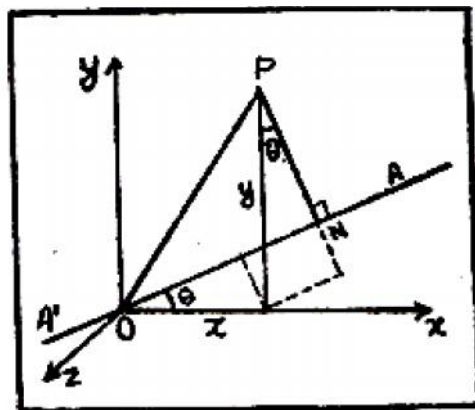
$$I_{xx} = \int_m y^2 dm$$

$$I_{yy} = \int_m x^2 dm$$

$$I_{xy} = \int_m xy dm$$

$$\begin{aligned} & \int_m (y^2 \cos^2 \alpha - 2xy \sin \alpha \cos \alpha + x^2 \sin^2 \alpha) dm \\ &= \cos^2 \alpha \int_m y^2 dm - 2 \sin \alpha \cos \alpha \int_m xy dm + \sin^2 \alpha \int_m x^2 dm \\ &= I_{xx} \cos^2 \alpha - I_{xy} \sin 2\alpha + I_{yy} \sin^2 \alpha \\ &= \left(\frac{1 + \cos 2\alpha}{2} \right) I_{xx} + \left(\frac{1 - \cos 2\alpha}{2} \right) I_{yy} - I_{xy} \sin 2\alpha \end{aligned}$$

ò Ì Ò.



Á ¼ Ò (7.21)

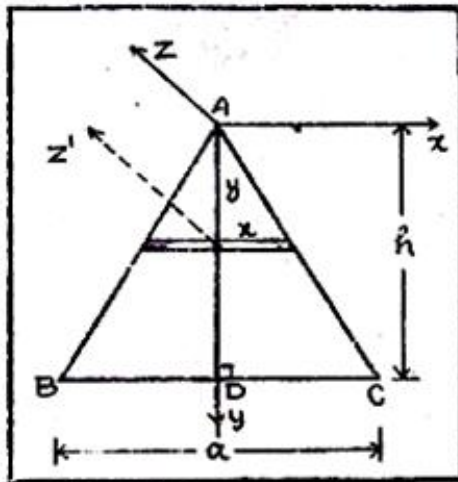
p-Á Á Ò ó Ð A' A ± y Û ò § „ i ò È ù ì , PN ± y Û ò

p í ì I - È Ð „ Á y ò ò Ì Á Á ¾ i ò, « Ð Ì Á Û ò | Á Ò Á, ò Ú Á Á ¾ ò ò Û ì ì z ù È Á Ì Û ò ò Ò « î Í „ ç „ Ò Á ò ¾ „ Ò È ù „ i È ¾ „ Á Á Ì Á « î Í „ ç „ i ò (Principal axes).

I y | Á Ò Á, ò Ú Á Á ¾ ò ò Û ì ¾ „ Á Á Ì ò ç „ Á Á ò ¾ ò Ò ò ¾ ò È y „ Û (Principal moments of inertia) ± È Ò Á Ì ò. « ò ¾ „ Á ¾ „ Á Á Ì Á « î Í „ Û „ x « î Í ¼ y ¾ „ i Ì ò § „ i ½ í „ Û Á „ Ì ñ „ ½ ò ¾ „ Ó „ È Ò Á È, Á y Á Ò Á Ì Û Á „ Á Á Û ì „ Ò Á Ì ò.

3.14.1 $\mu = \rho \bar{O} \bar{A} \bar{A} \bar{i}$ $\bar{O} \bar{i} \bar{S}_{,i} \frac{1}{2} \bar{d} \bar{3} \bar{4} \bar{y} \bar{ } \bar{i} \bar{o} \bar{d} \bar{0} \bar{u} \bar{C} \bar{C} \bar{A} \bar{A} \bar{E} \bar{C} \bar{S} \bar{A}$

- (i) $BC \pm y \bar{U} \bar{o} \pm \bar{3} \bar{4} \bar{C} \bar{A} \bar{i} \bar{ } \bar{d} \bar{3} \bar{4} \bar{u} \bar{l} \bar{ } \bar{A} \bar{ } \bar{A} \bar{A} \bar{o} \bar{A} \bar{I} \bar{ } \bar{o} \bar{ } \bar{i} \bar{o} \bar{l} \bar{ } \bar{d} \bar{D} \bar{i} \bar{S}_{,i} \bar{I} \bar{ } \bar{A} \bar{u} \bar{E} \bar{C} \bar{A}$
 $\bar{C} \bar{ } \bar{A} \bar{A} \bar{o} \bar{ } \bar{3} \bar{4} \bar{O} \bar{o} \bar{d} \bar{3} \bar{4} \bar{E} \bar{y}$
- (ii) $\bar{O} \bar{i} \bar{S}_{,i} \frac{1}{2} \bar{3} \bar{4} \bar{C} \bar{o} \bar{d} \bar{3} \bar{4} \bar{u} \bar{l} \bar{ } \bar{A} \bar{ } \bar{A} \bar{A} \bar{o} \bar{A} \bar{I} \bar{ } \bar{o} \bar{ } \bar{i} \bar{o} \bar{l} \bar{ } \bar{d} \bar{D} \bar{i} \bar{S}_{,i} \bar{I} \bar{ } \bar{A} \bar{u} \bar{E} \bar{C} \bar{A} \bar{C} \bar{ } \bar{A} \bar{A} \bar{o}$
 $\bar{3} \bar{4} \bar{O} \bar{o} \bar{d} \bar{3} \bar{4} \bar{E} \bar{y} \bar{ } \bar{C} \bar{i} \bar{ } \bar{S}_{,i} \bar{n}$



$\bar{A} \bar{3} \bar{o} (7.22)$

$ABC \pm y \bar{A} \bar{D} \mu = \rho \bar{O} \bar{A} \bar{A} \bar{i} \bar{ } \bar{O} \bar{i} \bar{S}_{,i} \frac{1}{2} \bar{A} \bar{i} \bar{l} \bar{ } \bar{o} \bar{ } \bar{O} \bar{i} \bar{S}_{,i} \frac{1}{2} \bar{3} \bar{4} \bar{C} \bar{o} \bar{d} \bar{3} \bar{4} \bar{u} \bar{l}$
 $AX, AY \pm y \bar{A} \bar{ } \bar{A} \bar{3} \bar{o} 7.22 \bar{ } \bar{i} \bar{o} \bar{E} \bar{A} \bar{A} \bar{i} \bar{U} \bar{A} \bar{A} \bar{E} \bar{C} \bar{S} \bar{A} \bar{ } \bar{i} \bar{o} \bar{O} \bar{o} \bar{ } \bar{C} \bar{ } \bar{3} \bar{4} \bar{C} \bar{ } \bar{A}$
 $\bar{S}_{,i} \bar{I} \bar{ } \bar{C} \bar{i} \bar{ } \bar{I} \bar{E} \bar{A} \bar{ } \bar{y} \bar{E} \bar{E} \bar{ } \bar{A} \bar{D} - \bar{B} \bar{C} \pm \bar{E} \bar{ } \bar{A} \bar{ } \bar{A} \bar{D} = h \bar{ } \bar{i} \bar{o} \bar{ } \bar{i} \bar{o}$
 $\bar{p} \bar{i} \bar{ } \bar{d} \bar{A} = 2x \bar{z} \bar{d} \bar{y}$

$$dm = (2x dy) \rho A y \bar{A} \bar{u} \bar{E} \bar{C}, dm = y \bar{C} \bar{ } \bar{A} \bar{A} \bar{o} \bar{ } \bar{3} \bar{4} \bar{O} \bar{o} \bar{d} \bar{3} \bar{4} \bar{E} \bar{y} = dm \frac{x^2}{3}$$

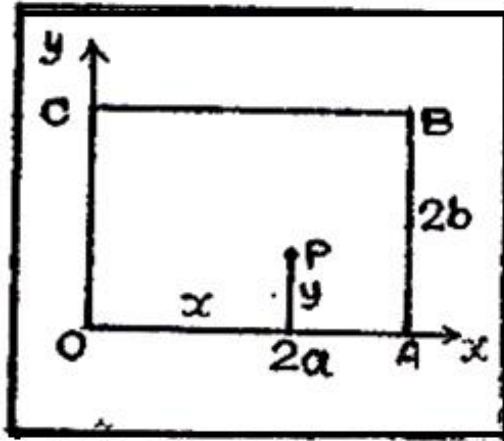
$\pm \bar{E} \bar{S} \bar{A} \bar{A} \bar{y} \bar{A} \bar{u} \bar{E} \bar{C} \bar{O} \bar{i} \bar{S}_{,i} \frac{1}{2} \bar{d} \bar{3} \bar{4} \bar{y} \bar{ } \bar{C} \bar{ } \bar{A} \bar{A} \bar{o} \bar{ } \bar{3} \bar{4} \bar{O} \bar{o} \bar{d} \bar{3} \bar{4} \bar{E} \bar{y}$
 $Az \pm y \bar{A} \bar{D} \bar{A} \bar{A} \bar{E} \bar{C} \bar{S} \bar{A} \bar{O} \bar{i} \bar{S}_{,i} \frac{1}{2} \bar{3} \bar{4} \bar{C} \bar{o} \bar{d} \bar{3} \bar{4} \bar{u} \bar{l} \bar{ } \bar{A} \bar{ } \bar{A} \bar{A} \bar{o} \bar{A} \bar{I} \bar{ } \bar{o} \bar{ } \bar{i} \bar{o} \bar{l} \bar{ } \bar{d} \bar{D} \bar{i} \bar{S}_{,i} \bar{I} \bar{ } \bar{d} \bar{ } \bar{3} \bar{4} \bar{i}$
 $\bar{I} \bar{E} \bar{A} \bar{ } \bar{d} \bar{I} \bar{ } \bar{o}$

$$= \int_0^h \frac{x^2}{3} (2x dy) \rho$$

$$= \frac{2\rho}{3} \frac{a^3}{8h^3} \int_0^h y^3 dy = \left(\frac{1}{2} a h \rho \right) \cdot \frac{a^2}{24} = M \frac{a^2}{24}$$

$$Az \bar{A} \bar{u} \bar{E} \bar{C} dm \bar{y} \bar{C} \bar{ } \bar{A} \bar{A} \bar{o} \bar{ } \bar{3} \bar{4} \bar{O} \bar{o} \bar{d} \bar{3} \bar{4} \bar{E} \bar{y} = dm \frac{x^2}{3} + dm y^2$$

$$Az \bar{A} \bar{u} \bar{E} \bar{C} \bar{O} \bar{i} \bar{S}_{,i} \frac{1}{2} \bar{d} \bar{3} \bar{4} \bar{y} \bar{ } \bar{C} \bar{ } \bar{A} \bar{A} \bar{o} \bar{ } \bar{3} \bar{4} \bar{O} \bar{o} \bar{d} \bar{3} \bar{4} \bar{E} \bar{y}$$



Á¼õ (7.26)

$$\begin{aligned}
 &= p \int_0^{2a} x dx \int_0^{2b} y dy \\
 &= 4a^2 b^2 p \\
 &= (4abp) \cdot ab \\
 &= M \cdot ab
 \end{aligned}$$

0Åõ « " ÁÕõ ¼" ÄÄ;Ä « îÍ,û 0A×¼ý " " + $\frac{f}{2}$ ±ý Ûõ §,;½ò" ¼
 « " Áì,õî õ, « ôŞÄ;Ð

$$\tan 2\alpha = \frac{2I_{xy}}{I_{yy} - I_{xx}} = \frac{2Mab}{\frac{4M}{3}(a^2 - b^2)} = \frac{3ab}{2(a^2 - b^2)}$$

–î õ.

$$\alpha_1 = \frac{1}{2} \tan^{-1} \left\{ \frac{3ab}{2(a^2 - b^2)} \right\}$$

$$\alpha_2 = \frac{f}{2} + \frac{1}{2} \tan^{-1} \left\{ \frac{3ab}{2(a^2 - b^2)} \right\}$$

3.15.6. "Õ°Ä;É |óí §,;½ Óì §,;½ò¼ý |óí §,;½ Ó" Éô òùÇÅõ
 « " ÁÕõ ¼" ÄÄ;Ä « îÍ,û « õÕ" É ÄÊŞÄ |øÕõ Äì,òÐ¼ý ¼;í ì õ
 §,;½í, Çì,;ñ,

$$I_{xx} = \frac{Mh^2}{6}; I_{yy} = \frac{Ma^2}{6}$$

$$I_{xy} = \int_0^a \int_0^b pxy dx dy$$

$$= p \int_0^a x \left\{ \int_0^{b/a(a-x)} y dy \right\} dx$$

$$= \frac{pb^2}{2a^2} \int_0^a x(a-x)^2 dx$$

$$= \frac{1}{2} pab \cdot \frac{ab}{12}$$

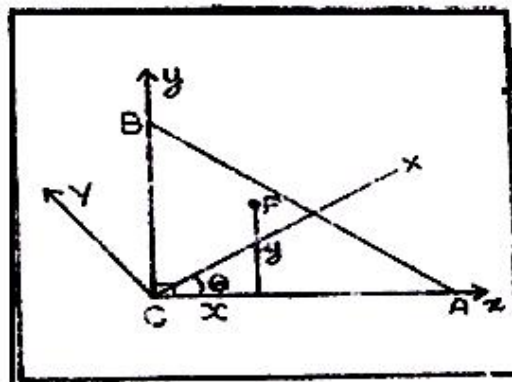
$$= M \frac{ab}{12}$$

CAO « .. AÔõ ¾» ÄÂjÂ « îÍ , û CA×¼ý „ „ + $\frac{f}{2}$ ±ýÛõ §, i ½ò .. ¾
¾j í Ì Á¾j , õ

$$\tan 2\alpha = \frac{2I_{xy}}{I_{yy} - I_{xx}} = \frac{2 \cdot \frac{Mab}{12}}{\left(\frac{Ma^2}{6} - \frac{Mb^2}{6} \right)} = \frac{ab}{a^2 - b^2}$$

$$\alpha_1 = \frac{1}{2} \tan^{-1} \left\{ \frac{ab}{a^2 - b^2} \right\}$$

$$\alpha_2 = \frac{f}{2} + \frac{1}{2} \tan^{-1} \left\{ \frac{ab}{a^2 - b^2} \right\}$$



À¼õ (7.27)

7-8-7. $\bar{O}^{\circ} \hat{A}_i \hat{E} \ll \bar{\bar{A}} \hat{\delta} \frac{1}{4} \hat{\delta} \frac{3}{4} \delta \hat{E} \hat{y} \hat{A} \hat{\delta} \frac{1}{4} \hat{O} \bar{\bar{E}} \hat{o} \hat{O} \hat{u} \hat{C} \hat{A} \hat{A} \bar{\bar{A}} \hat{O} \hat{o}$
 $\frac{3}{4} \bar{\bar{A}} \hat{A}_i \hat{A} \ll \hat{i} \hat{I} \hat{u} \hat{A} \hat{\delta} \frac{1}{4} \hat{\delta} \frac{1}{4} \hat{y} \hat{S} \hat{S}_i \frac{1}{2} \hat{i} \hat{o} \hat{C} \bar{\bar{A}} \hat{o} \hat{A} \hat{u} \hat{E} \hat{O} \hat{i} \hat{I} \hat{A} \hat{E} \hat{o}$
 $8 \cot \hat{S} = 3f \pm \hat{E} \hat{i} \hat{\delta} \hat{I} \hat{S}$

$\ll \bar{\bar{A}} \hat{\delta} \frac{1}{4} \hat{\delta} \frac{3}{4} \delta \hat{E} \hat{y} \hat{C} \hat{C} \hat{E} \hat{M} \hat{I} \hat{o}$
 $a \pm \hat{y} \hat{A} \hat{D} \hat{A} \hat{\delta} \frac{1}{4} \hat{\delta} \frac{3}{4} \hat{C} \hat{y} \hat{A} \hat{o} \hat{C} \hat{i} \hat{I} \hat{E} \hat{C} \hat{I} \hat{I} \hat{A} \hat{E} \hat{o} \hat{p} \hat{i} \hat{I}$

$$CG = \frac{49}{3f} \hat{I} \hat{o}$$

$$I_{xx} = OD \ll \bar{\bar{A}} \hat{\delta} \frac{1}{4} \hat{\delta} \frac{3}{4} \delta \hat{E} \hat{y} \hat{C} \hat{C} \bar{\bar{A}} \hat{o} \hat{C} \hat{O} \hat{o} \hat{\delta} \frac{3}{4} \hat{C} \hat{E} \hat{y}$$

$$= M \frac{a^2}{4}$$

$$I_{yy} = Oy \hat{A} \hat{u} \hat{E} \hat{C} \hat{A} \frac{3}{4} \delta \hat{E} \hat{y} \hat{C} \hat{C} \bar{\bar{A}} \hat{o} \hat{C} \hat{O} \hat{o} \hat{\delta} \frac{3}{4} \hat{C} \hat{E} \hat{y}$$

$$= GM \hat{A} \hat{u} \hat{E} \hat{C} \hat{A} \hat{C} \hat{C} \bar{\bar{A}} \hat{o} \hat{C} \hat{O} \hat{o} \hat{\delta} \frac{3}{4} \hat{C} \hat{E} \hat{y} + M \cdot a^2$$

$$= \frac{Ma^5}{4} + Ma^2 + \frac{5Ma^2}{4}$$

$$I_{xy} = ox, oy \hat{A} \hat{u} \hat{E} \hat{C} \hat{A} \frac{3}{4} \delta \hat{E} \hat{y} \hat{o} \hat{C} \hat{A} \hat{o} \hat{A} \hat{O} \hat{i} \hat{S} \hat{o}$$

$$= \left\{ \begin{array}{l} GL, GM \hat{A} \hat{u} \hat{E} \hat{C} \hat{A} \\ \frac{3}{4} \delta \hat{E} \hat{y} \\ \hat{o} \hat{C} \hat{A} \hat{o} \hat{A} \hat{O} \hat{i} \hat{S} \hat{o} \end{array} \right\} + \left\{ \begin{array}{l} ox, oy \hat{A} \hat{u} \hat{E} \hat{C} \hat{A} \\ M \hat{C} \hat{C} \hat{E} \bar{\bar{A}} \hat{o} \\ \hat{I} \hat{A} \hat{u} \hat{U} \hat{G} \hat{A} \hat{C} \hat{o} \ll \bar{\bar{A}} \hat{O} \hat{o} \hat{D} \hat{S} \hat{C} \hat{y} \\ \hat{o} \hat{C} \hat{A} \hat{o} \hat{A} \hat{O} \hat{i} \hat{S} \hat{o} \end{array} \right\}$$

$$= 0 + M \cdot OC \cdot CG$$

$$= M \cdot a \cdot \frac{4a}{3f} = \frac{4Ma^2}{3f}$$

$0 \hat{A} \hat{C} \hat{o} \ll \bar{\bar{A}} \hat{O} \hat{o} \frac{3}{4} \bar{\bar{A}} \hat{A}_i \hat{A} \ll \hat{i} \hat{I} \hat{S} \hat{C} \hat{o} \hat{S} \hat{S} \frac{3}{4} \hat{U} \hat{o} \hat{y} \hat{U} \hat{A} \hat{\delta} \frac{1}{4} \hat{\delta} \frac{1}{4} \hat{y} \hat{S} \hat{S}_i \frac{1}{2} \hat{i}$
 $\hat{o} \hat{C} \bar{\bar{A}} \hat{o} \hat{A} \hat{u} \hat{U} \hat{C} \frac{3}{4} \hat{C} \hat{o}$

$$\tan 2\hat{S} = \frac{2I_{xy}}{I_{yy} - I_{xx}} = \frac{2 \cdot \frac{4Ma^2}{3f}}{\left(\frac{5Ma^2}{4} - \frac{Ma^2}{4} \right)} = \frac{8}{3f}$$

$$\therefore 8 \cot 2\hat{S} = 3f$$

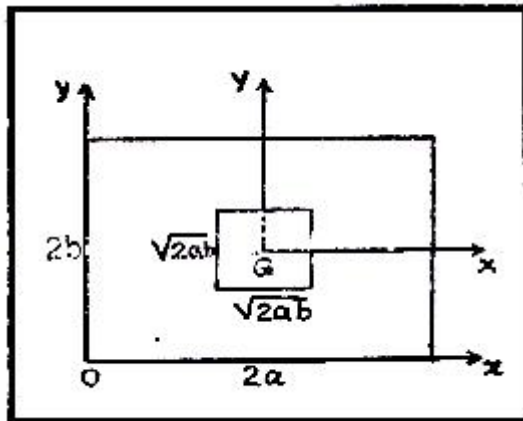
3.15.8 2a $\hat{C} \hat{o}$, 2b $\ll \hat{A} \hat{o} \hat{S} \hat{S} \frac{1}{4} \hat{A} \hat{C} \hat{o} \hat{A}_i \hat{E} \hat{I} \hat{o} \hat{u} \hat{A} \hat{o} \hat{C} \hat{A} \hat{A} \hat{C} \hat{o} \hat{S} \hat{S} \frac{1}{4} \delta \hat{E} \hat{y} \hat{C} \hat{C} \bar{\bar{A}} \hat{o} \hat{C} \hat{O} \hat{o} \hat{\delta} \frac{3}{4} \hat{C} \hat{E} \hat{y}$
 $\hat{p} \hat{O} \hat{o} \hat{D} \ll \frac{3}{4} \hat{y} \hat{C} \hat{C} \hat{E} \hat{A} \hat{C} \hat{o} \hat{A}_i \hat{C} \hat{C} \ll \hat{C} \bar{\bar{A}} \hat{o} \hat{A} \hat{u} \hat{U} \hat{C} \hat{D} \hat{o}, \hat{o} \hat{D} \hat{A} \hat{A} \hat{E} \hat{A} \hat{O} \hat{u} \hat{C} \hat{D} \hat{A}_i \hat{E}$
 $\hat{A} \hat{I} \frac{3}{4} \hat{C} \hat{A}_i \hat{y} \hat{U} \hat{A} \hat{\delta} \frac{1}{4} \hat{o} \hat{A} \hat{o} \hat{I} \hat{C} \hat{C} \hat{o} \hat{A} \hat{I} \hat{C} \hat{E} \hat{D}. \hat{A} \hat{B} \hat{O} \hat{u} \hat{C} \hat{I} \hat{o} \hat{u} \hat{A} \hat{o} \hat{A} \hat{I} \frac{3}{4} \hat{C} \hat{A}_i \hat{y} \hat{O}$
 $\hat{O} \hat{E} \hat{A} \hat{A} \hat{A} \hat{O} \hat{o} \frac{3}{4} \bar{\bar{A}} \hat{A}_i \hat{A} \ll \hat{i} \hat{I} \hat{S} \hat{u} \ll \hat{o} \hat{O} \hat{E} \hat{A} \hat{E} \hat{S} \hat{A} \hat{I} \hat{o} \hat{O} \hat{o} 2a \pm \hat{y} \hat{U} \hat{o}$
 $\hat{A} \hat{i} \hat{S} \hat{o} \hat{D} \frac{1}{4} \hat{y}$

$$= \frac{1}{2} \tan^{-1} \left\{ \frac{6ab}{5(a^2 - b^2)} \right\}$$

$$= \frac{f}{2} + \frac{1}{2} \tan^{-1} \left\{ \frac{6ab}{5(a^2 - b^2)} \right\}$$

±ý Ū ò §, i ½ í, ¨ Ç ò ¾ í í Ì | Á É ì, i ð Í, ¨

Á¼ Ó ù Ç | ° ù Á, ò ¾, ð Ê ý « ¨ Á ò ð (Á¼ ò 7.28) ø, i ð ¼ ò Á ð Í ù Ç ð.



(Á¼ ò 7.28)

| Á ð Ê ± Í ì, ò Á ð ¼ ° ð Á ò Á Ì ¾ Á Ç ý Á ì, ò ¾ Ç ý ¿ Ç ò

$$= \sqrt{\frac{4ab}{2}} = \sqrt{2ab}$$

$I_{xx} = GX \text{ À ù Ê Ç Á Á¼ Ó ù Ç } ¾, ð Ê ý ¿ ¨ \text{ Á Á ò } ¾ \text{ Ç ò ð } ¾ \text{ Ç Ê ý}$

$$= 4ab \dots \frac{b^2}{3} 2ab \dots \left(\frac{\sqrt{2ab}}{4 \times 3} \right)^2$$

$$= \frac{4ab \dots}{3} \left(b^2 - \frac{ab}{4} \right)$$

$$= \frac{ab \dots}{3} (4b^2 - ab)$$

$$I_{xx} = I_{xx} + (2ab \dots) \times b^2$$

$$= \frac{ab \dots}{3} (4b^2 - ab) + 2ab^2 \dots$$

$$= \frac{ab \dots}{3} (10b^2 - ab)$$

« ùĀĵŒĒ

$$I_{yy} = \frac{ab...}{3}(10b^2 - ab)$$

$$I_{xy} = I_{xy} + (2ab...) \cdot b \cdot a \cdot \\ = 0 + 2a^2b^2...$$

→ ĩ ō.

0Āĉ « ĩ ĀŌŃ ¼ĩ ĀĀĵĀ « ĩĀ ū OA ×¼ŷ „ „ + $\frac{f}{2}$ + 0±ŷ ŪŃ Œĵ ĨĀ

$$\tan 2\alpha = \frac{2I_{xy}}{I_{yy} - I_{xx}}$$

$$= \frac{2 \times 2ab^2...}{\frac{ab...}{3}(10a^2 - ab) - \frac{ab...}{3}(10b^2 - ab)} \\ = \frac{6ab}{5(a^2 - b^2)}$$

→ ĩ ō.

±ĒŒĀ

$$\alpha_1 = \frac{1}{2} \tan^{-1} \left\{ \frac{6ab}{5(a^2 - b^2)} \right\}$$

$$\alpha_2 = \frac{f}{2} + \frac{1}{2} \tan^{-1} \left\{ \frac{6ab}{5(a^2 - b^2)} \right\}$$

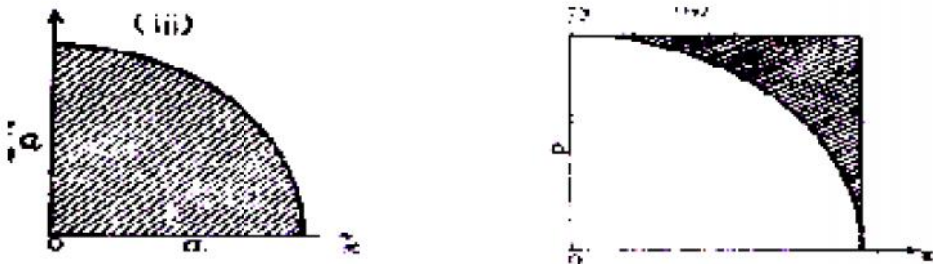
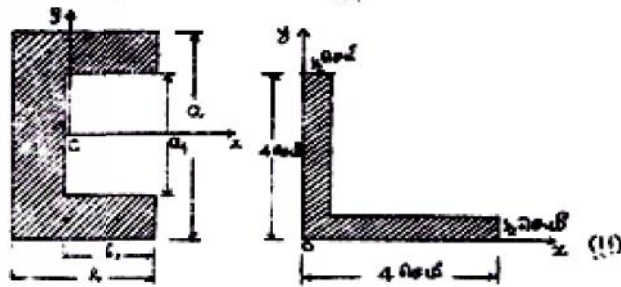
→ ĩ ō.

3.16.1

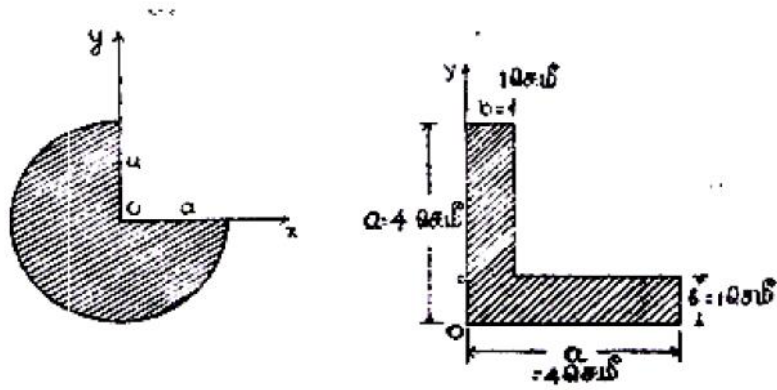
3.16.1 $\mu = \frac{b \bar{O} \bar{A} \bar{A} \bar{i}}{2} \dots$ (Áç' ¼ a ± y Æ ð ÷ ½ ð ¼ y | ¼ i' Ä x ± É ð ç' Ä ð ¼ Ö ð ¼ É y = $\frac{Ma^2}{24}$)

3.16.2 $\bar{O} \bar{D} \bar{A} \bar{D} \bar{A} \bar{y} \bar{a} \dots$ (Áç' ¼ : Ä ð ÷ ½ ð a - É ð ç' Ä ð ¼ Ö ð ¼ É y = $\frac{Ma^2}{12}$)
 $\bar{a} \dots$ (Áç' ¼ : Ä ð ÷ ½ ð l - É ð ç' Ä ð ¼ Ö ð ¼ É y = $\frac{Ml^2}{24}$)

3.16.3 $\bar{A} \bar{y} \bar{A} \bar{O} \bar{o} - \bar{O} \bar{A} \bar{o} \bar{A} \bar{y} \bar{i} \dots$ (Áç' ¼ : l_x = $\frac{P}{12} (ba^3 - b_1 a_1^5)$; l_x = 5.56 p | ° Ä É⁴)

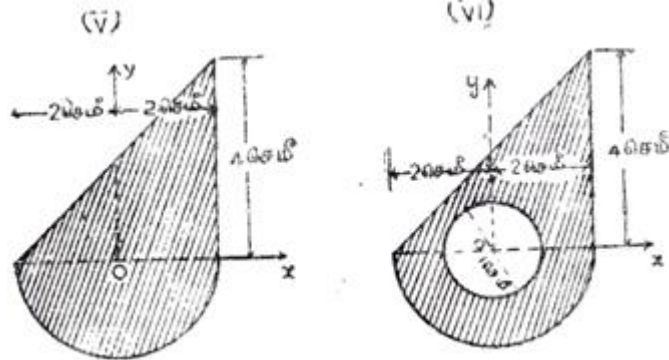


(Áç' ¼ : l_x = $\frac{f pa^4}{16}$; l_x = $\frac{a^4 \dots}{48} (16 - 3f)$)



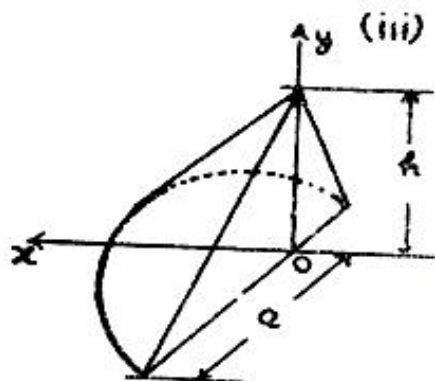
(Áĉĉ ¼ $I_x = 504.56p \mid \text{°} \cdot \text{ÁĒ}^4$, Áĉĉ ¼ $I_x = 26.83p \mid \text{°} \cdot \text{ÁĒ}^4$)

3.16.4 Áĉĉ Áĉĉ - ÖÁöÁ¼í Ÿ Û Ì Ì OX, OY « î Í Ÿ Û ÁÜÈĈÁ
 °¼öÐÁö | ÁÖì Ÿ ò'' ¾î Ÿ ñ Ÿ .



(Áĉĉ ¼: $I_{xy} = -\frac{a^4 p}{8}, I_{xy} = 7.75p \mid \text{°} \cdot \text{ÁĒ}$)

(iii) « '' Á¾ĉñ Áì Üöð



(Áĉĉ ¼ : $I_{xy} = \frac{2Mah}{f}$)

ρ (density) \times V (volume) = M (mass) \rightarrow $\rho \times \frac{4}{3}\pi R^3 = M$
 $\rho \times \frac{4}{3}\pi R^3 = M \rightarrow R = \sqrt[3]{\frac{3M}{4\rho\pi}}$

5. I_x, I_y (Radius of gyration) k_x, k_y

$I_x, I_y = \int y^2 dm, \int x^2 dm$
 $k_x = \sqrt{\frac{I_x}{M}}, k_y = \sqrt{\frac{I_y}{M}}$

$$k_x = \sqrt{\frac{I_x}{A}}, k_y = \sqrt{\frac{I_y}{A}}, k_o = \sqrt{\frac{J_o}{A}}$$

$\pm y \text{ è } \int y^2 dm \text{ (} \int y^2 \rho dx dy \text{)} \text{ } \hat{A} \text{ } \hat{A} \hat{U} \hat{i} \text{ } \hat{o}.$

6. I_{xy} (product of inertia) $I_{xy} = \int xy dm$

$dx, dy \ll \hat{i} \hat{l} \rightarrow \int xy dm = \int xy \rho dx dy$
 $I_{xy} = \int xy dm = \int xy \rho dx dy$

$$I_{xy} = \int xy dm = \int xy \rho dx dy$$

7. I_{xy} (product of inertia) $I_{xy} = \int xy dm$

$I_{xy} = \int xy dm = \int xy \rho dx dy$
 $I_{xy} = \int xy dm = \int xy \rho dx dy$

$$I_{xy} = \int (x^1 + d_x)(y^1 d_y) dA$$

$$= \int_A x^1 y^1 dA + d_x \int_A y^1 dA + d_y \int_A x^1 dA + d_x d_y \int_A dA$$

$$= \bar{I}_{x^1 y^1} + A d_x d_y$$

8. I (mass) $I = \int r^2 dm$

(i) $z \ll \hat{i} \hat{l} \rightarrow I = \int r^2 dm$

$$= \int r^2 \dots dv = \dots \int r^2 dv$$

(ii) $\rho \times V \ll \hat{i} \hat{l} \rightarrow I = \int r^2 dm$

$$I = \int r^2 dm = \int_m \left[(d + x^1)^2 + y^{1^2} \right] dm = I_G + md^2$$

$I_G = z' \ll \hat{i} \hat{l} \rightarrow I = \int r^2 dm$

$m = \rho \times V \ll \hat{i} \hat{l} \rightarrow I = \int r^2 dm$

$d = \rho \times V \ll \hat{i} \hat{l} \rightarrow I = \int r^2 dm$

$$A_2 \text{ (rectangle): } b = 4 \{ [10^{-2}] \text{ m} \};$$

$$h = 1.5 \{ [10^{-2}] \text{ m} \}$$

$$A_3 \text{ (triangle): } R = 1.5 \{ [10^{-2}] \text{ m} \}$$

11. Find the moment of inertia I_{xx} of the composite area shown in the figure.

$$I_{xx} = 0.055 (10^{-4}) 12^4 - \dots$$

$$I_{xx} = bd^3 / 12$$

$$\frac{bh^3}{36}$$

« ... »

$$I_{xx} = (\sum I_{xx})_i + \sum (A_i)(\bar{y}_i^2)$$

$$A_1 = (8)(6) = 48, \bar{y}_1 = \frac{6}{2} = 3$$

$$A_2 = \frac{1}{2}(4)(3) = 6$$

$$A_3 = \frac{fR^2}{4} = \frac{f}{4}(3^2) = 7.06858$$

A_i	Area (A)	\bar{y}_i	$(I_{xx})_i$	$A_i \bar{y}_i^2$
1	48	3	144	432
2	-6	10	-3	-6
3	-7.06858	$6 - \frac{4(3)}{3f}$	-44550	-157.930

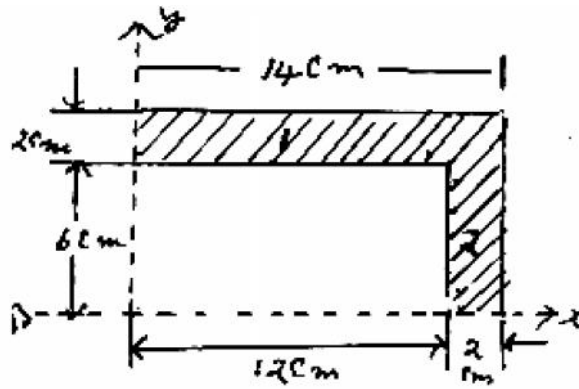
$$\sum A_i = 34.93142 \quad \sum I_{xx} = 0.47268$$

$$I_{xx} = 136.5450 + 268.0692742$$

$$= 404.6142742 \text{ cm}^4; \{ [10^{-2}] \text{ m} \}$$

$$x: \text{ centroid } \bar{x} = \sqrt{\frac{I_{xx}}{A}} = 3.40341 \text{ cm}; \{ [10^{-2}] \text{ m} \}$$

12. Find the moment of inertia I_{xx} of the composite area shown in the figure.



$I_{xy} = \sum (I_{xy})_i + \sum A_i (\bar{x}_i)(\bar{y}_i) = 1840$
 $= 1840 \text{ cm}^4 \{ [10^{-2}] \}$

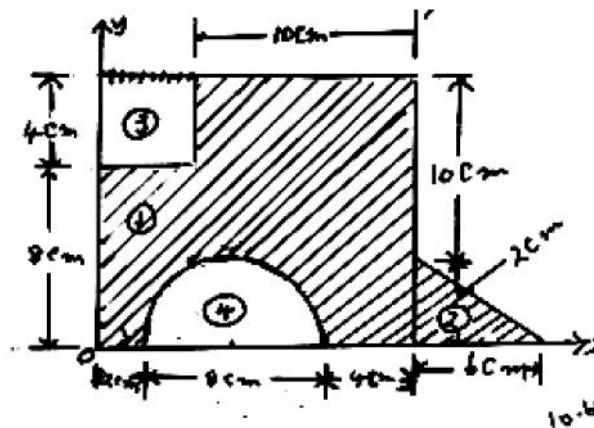
A_i	$A_i \bar{x}_i \bar{y}_i$	\bar{x}_i	\bar{y}_i	$A_i \bar{x}_i \bar{y}_i$
1	$(14)(2) = 28$	7.0	$6+1=7$	$(28)(7)(7) = 1372$
2	$(2)(6) = 12$	$12+1=13$	3	$(12)(13)(3) = 468$

$$I_{xy} = \sum (I_{xy})_i + \sum A_i (\bar{x}_i)(\bar{y}_i) = 1840$$

$$= 1840 \text{ cm}^4 \{ [10^{-2}] \}$$

13. $I_{xy} = \sum (I_{xy})_i + \sum A_i (\bar{x}_i)(\bar{y}_i)$
 $= 1840 \text{ cm}^4 \{ [10^{-2}] \}$

- (1) 14×12
- (2) 2×6
- (3) $-(4 \times 4) = -16$
- (4) $-\frac{f}{2} \times 16$
 $r = 4 \text{ cm} = -25.13$



\bar{A}_i	A	\bar{x}	\bar{y}	$A\bar{x}$	$A\bar{y}$
1	$14 \times 12 = 168$	7	6	1176	1008
2	$\frac{1}{2}(2)(6) = 6$	16	6.67	96	4.0
3	-16	2	10	-32	-160
4	-25.13	6	1.697	-150.780	-42.64561

$$\Sigma 132.87$$

$$\Sigma 1089.220 \quad \Sigma 809.357$$

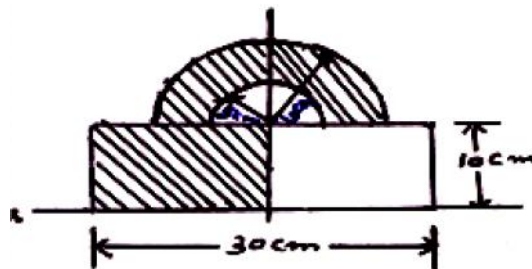
$$\bar{x} = \frac{1089.220}{132.87} = 8.197 \text{ cm}; \{[10^{-2}] \text{ m}\}$$

$$\underline{F}_k, \underline{f}_k = m_k \underline{t}_k; \{[10^{-2}] \text{ m}\}$$

$$\bar{x} = (8.197, 6.09 \text{ cm}) \{[10^{-2}] \text{ m}\}$$

14. $\bar{A} = \frac{1}{2} \pi r^2$ $\bar{x} = \frac{4r}{3\pi}$ $\bar{y} = \frac{4r}{3\pi}$ $\bar{A} = \frac{1}{2} \pi (10)^2 = 157.08 \text{ cm}^2$ $\bar{x} = \frac{4(10)}{3\pi} = 4.24 \text{ cm}$ $\bar{y} = \frac{4(10)}{3\pi} = 4.24 \text{ cm}$

- (1) $\bar{A} = \frac{1}{2} \pi r^2$
- (2) $\bar{x} = \frac{4r}{3\pi}$
- (3) $\bar{y} = \frac{4r}{3\pi}$



$$A = \frac{1}{2} \pi (10)^2 = 157.08 \text{ cm}^2$$

$$= 10000$$

$\bar{A} = \frac{1}{2} \pi r^2$ $\bar{x} = \frac{4r}{3\pi}$ $\bar{y} = \frac{4r}{3\pi}$

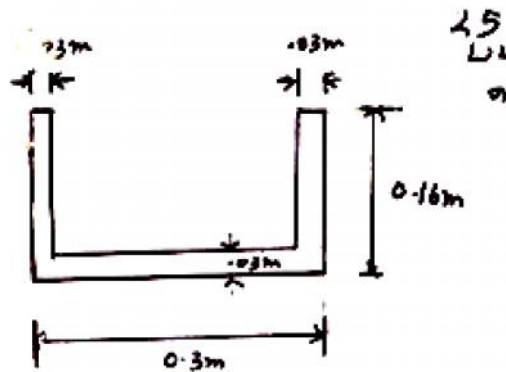
$$I = \frac{\pi r^4}{8} = \frac{\pi (10)^4}{8} = 15708$$

$$= 1100$$

$$A = f \frac{r^2}{2} = f \frac{(2.5)^2}{20} = 1.5757$$

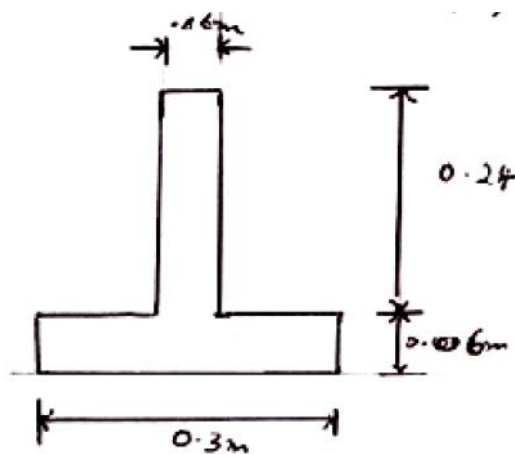
$$I = 1100 + 1.5707(14.244)^2 = 32968.1735$$

18. $I_{xx} = 2.40 \times 10^{-6} m^4$; $I_{yy} = 13.14 \times 10^{-6} m^4$; $I_p = 15.54 \times 10^{-6} m^4$



($I_{xx} = 2.40 \times 10^{-6} m^4$
 $I_{yy} = 13.14 \times 10^{-6} m^4$
 $I_p = 15.54 \times 10^{-6} m^4$)

19. $I_{xx} = 15.91 \times 10^{-6} m^4$; $I_{yy} = 8.71 \times 10^{-6} m^4$



($I_{xx} = 15.91 \times 10^{-6} m^4$; $I_{yy} = 8.71 \times 10^{-6} m^4$)

4.1 ÞÄì, ÄÄø (Ð, ù ÞÄí, ÄÄø)

4.1.1 ÞÄì, ÄÄÄý ã Ä í, ù (Elements of Kinematics)

Ä° ù, Äi Öü, ý, Èð ¼i Ì Ä¾j ø « Ä («) « ò Äi Ö° Ç µö ×
 Ä° ÄÄø Äi Äj ò « øÄÐ (-) « ò Äi ÖÇø ÞÄì ò ¾ð §¾j üÜÄÄi Äj ò
 « øÄÐ (p) « ò Äi ÖÇø Óýð ÞÖó¾ ÞÄì ò ¾ Äj üÄj ò.

Ä° Çj ø ¾j ò òÄöì ò Äi Öü, ù µö × Ä° ÄÄø Ì Äj Ü « ÄÖö
 « ù Ä° Çý ¾j ò ¾ð ÄüÉÄ ÄÄj òÐì ÜÜöá ø Ä° ÄÄø (Statics)
 ±ý Üö Ä° Çý ¾j ò ¾¾¾j ø Äi Öü, Çø ÞÄì ò ²üÄÄ Ä° ÄÄj òÐì
 ÜÜöá ø ÞÄì, Ä° ÄÄø (Dynamics) ±ý Üö Ä° ÇöÄÄ ò.

þöá üÄÄ ¾Äø, ÖÐ Çý (Particle) ÞÄì ò ¾ð ÄüÉÖö, ÄÉì Ö
 òÉÜì ò Äi ÖÇý (Rigid body) ÞÄì ò ¾ð ÄüÉÖö ÜÈöÄÄ ò,

Äi ÐÄj, ÞÄì Ä° ÄÄø, («) ÞÄì ÄÄø (Kinematics) (-) Ä° ÄÄø
 (Kinetics) ±É ÞÖÄÄ ¾Ç, Äj ò Äj ò ÄöÄÄ ÄÇì öÄÄ ò.

Ð, ù, òÉÜì ò Äi Öü, ù - ÄÄüÉø ÞÄì ò ±ì Äj ½Äj, Çj ø
 Ä° Çý ÈÐ ±ý Ü §¾j ò Äø, « Ä ÞÄì ò ÄøÄ° Äj Äj ¾Çý
 ÄÉÄ° Äö Ä (Geometry of motion) ÄÄj ò ÄÄ ¾§Ä ÞÄì ÄÄÄj ò.

ÞÄì ÄÄÄý ÖðÐ Ç ÄÉÄ ½¾¾¾ « ÄöÄø ýÄÄ « ÈÇÄj Äj Äý,
 ÞÄì ò ¾ Ä° ÇÄÄ ò ã Äi ÜÜ Üì Ì Þ¾¾ÄöüÇ Äj ¼=0, Çöø
 ÞÄì ò ¾ð ÄüÉÖö ±Ç¾j, ÄÇöÄÄ ò¾ ÞÄöö.

Äi Öü, Çý ÞÄì ò ¾üì ò Äj ½Äj Ä° ò, ÄüÜö ¾Éý, - üÈø
 - ÄÄüÈ ÄÄj ò ÄÄ ¾§Ä Ä° ÄÄÄj ò.

ÞÄì ò, « Ð Äj ¾¾¾üì Äj ½ö ò - ÄÄüÈ ÈöÄüÉÄ « ÈÇÄÄ ò
 « ÈÇøÐÈ Ä ÞÄì, Ä° ÄÄø (Dynamics) ±É öÄÄ ò.

4.1.2 ÞÄì, Ä° ÄÄÄý Äj Çx, ù

ÞÄì, Ä° ÄÄÄ Äi, Üì, j ò Äj Çx, Çj ø Äj ÇöÐ « È¾ø ÓÈÄj ò.

(«) ÖÐ, Üì Ì Äj ÞÄì, Ä° ÄÄø (Dynamics of a Particle)

Ð, ù ±ýÄÐ Äj Öñ Ä§Äj Ä ÜÉÄ üÄÈÄj ø ÖÄj ò, öÄö¾
 ÄÖÄÉüÈ öüÇÄj ò. ÞöÄj Çø Ð, Çý ÞÄì, ö ÄÄj ò, öÄÄ ò.

(-) Ð, ù, Çý Äj Ì Äj ÞÄì, Ä° ÄÄø (Dynamics of a System of
 Particles)

òÉÜì ò Äi Öü (Rigid body), Äj ò Äj Öü (Fluid) - ÄÄüÉý
 ÞÄì ò ¾üì ò ýÜ§ Äj « ÄÖö Äj ¼Ä° ¼, ÞÄì ò ¾ (Motion of
 continuous media) ÞöÄj Çx ÄÇì ò.

(p) òÉÜì ò Äi ÖÇý ÞÄì, Ä° ÄÄø (Dynamics of a Rigid body)

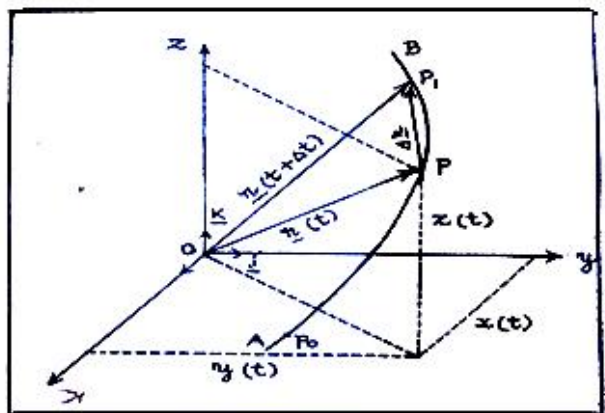
òÉÜì ò Äi Öü ±ýÄÐ, « ¾ý Ä ¾ü ýÜì Äj Äj Äj Äj
 Ä° ÄÄÄ° ÄöÐ, ÄÖÄÜ ¼ý Äj Öñ Ä° Äö ÄüÈ Äj Ö° Çì Ì ÈÄ ò.
 Ä° ÄÄÄÄ, ÄÄÄø (Mechanics) ÞöÄj Ç§Ä Ä, Ä° Äöð ÄüÈ¾j ò.

$\vec{r} = x\vec{i} + y\vec{j} + z\vec{k}$ « $\vec{r} = r\vec{e}_r$ « $\vec{v} = \dot{r}\vec{e}_r + r\dot{\theta}\vec{e}_\theta + r\sin\theta\dot{\phi}\vec{e}_\phi$
 $\vec{a} = \ddot{r}\vec{e}_r + 2\dot{r}\dot{\theta}\vec{e}_\theta - r\dot{\theta}^2\vec{e}_r + r\ddot{\theta}\vec{e}_\theta + 2\dot{r}\dot{\phi}\sin\theta\vec{e}_\phi - r\dot{\phi}^2\sin\theta\vec{e}_r + r\dot{\phi}^2\cos\theta\vec{e}_\theta + r\ddot{\phi}\sin\theta\vec{e}_\phi$
 $\vec{v} = \dot{r}\vec{e}_r + r\dot{\theta}\vec{e}_\theta + r\sin\theta\dot{\phi}\vec{e}_\phi$ « $\vec{v} = v_r\vec{e}_r + v_\theta\vec{e}_\theta + v_\phi\vec{e}_\phi$
 $\vec{a} = \ddot{r}\vec{e}_r + 2\dot{r}\dot{\theta}\vec{e}_\theta - r\dot{\theta}^2\vec{e}_r + r\ddot{\theta}\vec{e}_\theta + 2\dot{r}\dot{\phi}\sin\theta\vec{e}_\phi - r\dot{\phi}^2\sin\theta\vec{e}_r + r\dot{\phi}^2\cos\theta\vec{e}_\theta + r\ddot{\phi}\sin\theta\vec{e}_\phi$

$\vec{v} = \dot{r}\vec{e}_r + r\dot{\theta}\vec{e}_\theta + r\sin\theta\dot{\phi}\vec{e}_\phi$ « $\vec{v} = v_r\vec{e}_r + v_\theta\vec{e}_\theta + v_\phi\vec{e}_\phi$
 $\vec{a} = \ddot{r}\vec{e}_r + 2\dot{r}\dot{\theta}\vec{e}_\theta - r\dot{\theta}^2\vec{e}_r + r\ddot{\theta}\vec{e}_\theta + 2\dot{r}\dot{\phi}\sin\theta\vec{e}_\phi - r\dot{\phi}^2\sin\theta\vec{e}_r + r\dot{\phi}^2\cos\theta\vec{e}_\theta + r\ddot{\phi}\sin\theta\vec{e}_\phi$
 $\vec{v} = \dot{r}\vec{e}_r + r\dot{\theta}\vec{e}_\theta + r\sin\theta\dot{\phi}\vec{e}_\phi$ « $\vec{v} = v_r\vec{e}_r + v_\theta\vec{e}_\theta + v_\phi\vec{e}_\phi$
 $\vec{a} = \ddot{r}\vec{e}_r + 2\dot{r}\dot{\theta}\vec{e}_\theta - r\dot{\theta}^2\vec{e}_r + r\ddot{\theta}\vec{e}_\theta + 2\dot{r}\dot{\phi}\sin\theta\vec{e}_\phi - r\dot{\phi}^2\sin\theta\vec{e}_r + r\dot{\phi}^2\cos\theta\vec{e}_\theta + r\ddot{\phi}\sin\theta\vec{e}_\phi$

4.1.5 Đường đi của hạt (Equation of the path of a particle)

$\vec{r} = x\vec{i} + y\vec{j} + z\vec{k}$ « $\vec{r} = r\vec{e}_r$ « $\vec{v} = \dot{r}\vec{e}_r + r\dot{\theta}\vec{e}_\theta + r\sin\theta\dot{\phi}\vec{e}_\phi$
 $\vec{a} = \ddot{r}\vec{e}_r + 2\dot{r}\dot{\theta}\vec{e}_\theta - r\dot{\theta}^2\vec{e}_r + r\ddot{\theta}\vec{e}_\theta + 2\dot{r}\dot{\phi}\sin\theta\vec{e}_\phi - r\dot{\phi}^2\sin\theta\vec{e}_r + r\dot{\phi}^2\cos\theta\vec{e}_\theta + r\ddot{\phi}\sin\theta\vec{e}_\phi$



Hình 4-1-1

$\vec{r} = x\vec{i} + y\vec{j} + z\vec{k}$ « $\vec{r} = r\vec{e}_r$ « $\vec{v} = \dot{r}\vec{e}_r + r\dot{\theta}\vec{e}_\theta + r\sin\theta\dot{\phi}\vec{e}_\phi$
 $\vec{a} = \ddot{r}\vec{e}_r + 2\dot{r}\dot{\theta}\vec{e}_\theta - r\dot{\theta}^2\vec{e}_r + r\ddot{\theta}\vec{e}_\theta + 2\dot{r}\dot{\phi}\sin\theta\vec{e}_\phi - r\dot{\phi}^2\sin\theta\vec{e}_r + r\dot{\phi}^2\cos\theta\vec{e}_\theta + r\ddot{\phi}\sin\theta\vec{e}_\phi$

$\vec{A}_i \cdot \vec{D} \vec{A}_j = \delta_{ij}$ பற்றி $\vec{A}_i \cdot \vec{A}_j = \delta_{ij}$ எனக் கொள்ளும்.

4.1.5.1 \vec{r} இன் திசை (அல்லது \vec{e}_i)

$\vec{r} = x\vec{e}_1 + y\vec{e}_2 + z\vec{e}_3$ (4.1-1)-ல் \vec{e}_i ஐ \vec{r} இன் திசையாகக் கொள்ளும். \vec{r} இன் திசை \vec{e}_i ஐ $\vec{r} = r\vec{e}_i$ எனக் கொள்ளும். \vec{e}_i ஐ \vec{r} இன் திசையாகக் கொள்ளும்.

\vec{r} இன் திசை \vec{e}_i ஐ $\vec{r} = r\vec{e}_i$ எனக் கொள்ளும். \vec{r} இன் திசை \vec{e}_i ஐ $\vec{r} = r\vec{e}_i$ எனக் கொள்ளும். \vec{r} இன் திசை \vec{e}_i ஐ $\vec{r} = r\vec{e}_i$ எனக் கொள்ளும்.

$$\vec{PP}' = \vec{OP}' - \vec{OP}$$

$\vec{r}(t + \Delta t) - \vec{r}(t)$ ஆகும்.

$\Delta \vec{r} = \vec{r}(t + \Delta t) - \vec{r}(t)$ எனக் கொள்ளும்.

$\vec{r} = r\vec{e}_i$ எனக் கொள்ளும்.

$\vec{r} = x\vec{e}_1 + y\vec{e}_2 + z\vec{e}_3$ எனக் கொள்ளும்.

$\vec{r} = x\vec{e}_1 + y\vec{e}_2 + z\vec{e}_3$ எனக் கொள்ளும்.

$\vec{r}(t) = x(t)\vec{e}_1 + y(t)\vec{e}_2 + z(t)\vec{e}_3$ எனக் கொள்ளும்.

$\vec{r}(t) = x(t)\vec{e}_1 + y(t)\vec{e}_2 + z(t)\vec{e}_3$ எனக் கொள்ளும்.

$\vec{r}(t) = x(t)\vec{e}_1 + y(t)\vec{e}_2 + z(t)\vec{e}_3$ எனக் கொள்ளும்.

$\vec{r}(t) = x(t)\vec{e}_1 + y(t)\vec{e}_2 + z(t)\vec{e}_3$ எனக் கொள்ளும்.

$\vec{r}(t) = x(t)\vec{e}_1 + y(t)\vec{e}_2 + z(t)\vec{e}_3$ எனக் கொள்ளும்.

$\vec{r}(t) = x(t)\vec{e}_1 + y(t)\vec{e}_2 + z(t)\vec{e}_3$ எனக் கொள்ளும்.

$\pm \partial \ddot{A}_i \ddot{S}_i \ddot{A}_i \ddot{C} \ddot{O} \ddot{o} z(t) = 0 \pm \ddot{E} \ddot{O}, \ddot{D} \ddot{u} \ddot{p} \ddot{A} \ddot{i} \ddot{l} \ddot{o} \ddot{A}_i \ddot{r} \ddot{3/4} (x,y) \pm \ddot{y} \ddot{U} \ddot{o}$
 $\ddot{3/4} \ddot{C} \ddot{o} \ddot{3/4} \ddot{A} \ddot{i} \ddot{A} \ddot{o} \ddot{D} f(x,y) = 0 \pm \ddot{y} \ddot{U} \ddot{o} \ddot{O} \ddot{A} \ddot{y} \ddot{A}_i \ddot{O} \ddot{1/4} \ddot{O} \ddot{A} \ddot{i} \ddot{A} \ddot{A} \ddot{U} \ddot{i} \ddot{o} \ddot{A} \ddot{i} \ddot{o}.$

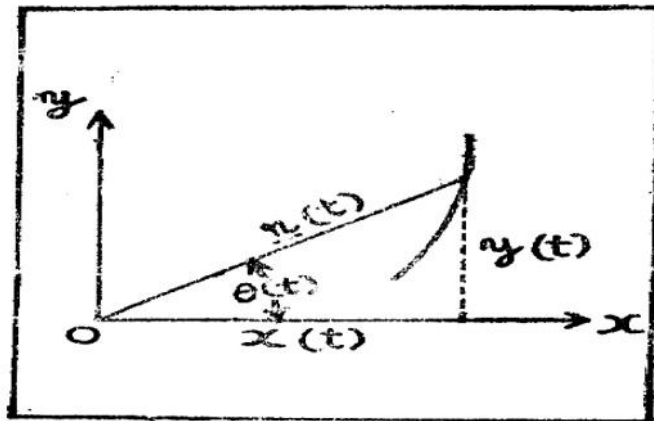
$\ddot{I} \ddot{E} \ddot{O} \ddot{A}_i \ddot{r}, \ddot{D} \ddot{u} \ddot{p} \ddot{A} \ddot{i} \ddot{l} \ddot{o} \ddot{A}_i \ddot{r} \ddot{3/4} \ddot{O} \ddot{S}_i \ddot{S}_i \ddot{1/4} \ddot{i} \ddot{l} \ddot{o} \pm \ddot{E} \ddot{O}, \ll \ddot{D} \ddot{O}$
 $\ddot{S}_i \ddot{S}_i \ddot{O} \ddot{E} \ddot{A} \ddot{i} \ddot{r} \ddot{O} \ddot{3/4} \ddot{o} \text{ (rectilinear motion) } \ddot{A} \ddot{u} \ddot{U} \ddot{U} \ddot{C} \ddot{1/4} \ddot{E} \ddot{o} \ddot{A} \ddot{i} \ddot{o}.$

$\ddot{O} \ddot{3/4} \ddot{C} \ddot{o} \ddot{3/4} \ddot{O} \ddot{D} \ddot{u} \ddot{p} \ddot{A} \ddot{i} \ddot{l} \ddot{A} \ddot{3/4} \ddot{i} \ddot{O} \ddot{S}_i \ddot{1/2} \ddot{i} \ddot{U} \ddot{U} \ddot{i} \ddot{C} \ddot{o} \text{ (Polar Coordinates)}$
 $\ddot{A} \ddot{A} \ddot{y} \ddot{A} \ddot{i} \ddot{O} \ddot{3/4} \ddot{O} \ddot{o} \ddot{O} \ddot{U} \ddot{C} \ddot{A} \ddot{y} \ddot{C} \ddot{A} \ddot{i} \ddot{A} \ddot{A} \ddot{A} \ddot{A} \ddot{A} \ddot{U} \ddot{i} \ddot{A} \ddot{j} \ddot{o}.$

$\ddot{A} \ddot{1/4} \ddot{o} \text{ (4.1-2)-} \ddot{O} \ddot{I} \ddot{E} \ddot{O} \ddot{A} \ddot{O} \ddot{I} \ddot{u} \ddot{C} \ddot{A}_i \ddot{U}, \ddot{P} \pm \ddot{y} \ddot{U} \ddot{o} \ddot{C} \ddot{S}_i \ddot{O} \ddot{o} \ddot{O} \ddot{U} \ddot{C} \ddot{A} \ddot{y} \ddot{S}_i \ddot{1/2} \ddot{i}$
 $\ddot{U} \ddot{U} \ddot{C} \ddot{1/4} \ddot{E} \ddot{r} \ddot{A} \ddot{O} \ddot{1/4} \ddot{i} \ddot{A} \times \ddot{r} = \ddot{r}(t), \ddot{r} \ddot{A} \ddot{i} \ddot{S}_i \ddot{1/2} \ddot{o} \theta = \theta(t) \pm \ddot{y} \ddot{A} \ddot{A} \ddot{D} \ddot{S}_i \ddot{C} \ddot{y}$

$\ddot{C} \ddot{A} \ddot{A} \ddot{A} \ddot{A} \ddot{A} \ddot{U} \ddot{i} \ddot{y} \ddot{E} \ddot{E}.$
 $\ddot{O} \ddot{i} \ddot{E} \ddot{o} \ddot{O} \ddot{U} \ddot{C} \ddot{O} \text{ (Pole) } \ddot{O} - \ddot{A} \ddot{A} \ddot{O} \ddot{O} \ddot{D} \ddot{C} \ddot{1/4} \ddot{A}_i \ddot{S} \ll \ddot{A} \ddot{O} \ddot{o} \ddot{S}_i \ddot{1/2} \ddot{o} \ddot{1/4} \ddot{O} \ddot{X}$

$\pm \ddot{y} \ddot{U} \ddot{o}, \ddot{I} \ddot{O} \ddot{I} \ddot{O} \ddot{3/4} \ddot{i} \ddot{S} \ll \ddot{A} \ddot{O} \ddot{o} \ddot{S}_i \ddot{1/2} \ddot{o} \ddot{1/4} \ddot{O} \ddot{Y} \pm \ddot{y} \ddot{U} \ddot{o} \ddot{1/4} \ddot{i} \ddot{u} \ddot{U} \ddot{o} \ddot{S} \ddot{A}_i \ddot{D}$



A_{1/4}o 4-1-2

$$x(t) = r(t) \cos \theta$$

$$y(t) = r(t) \sin \theta$$

$\pm \ddot{y} \ddot{U} \ddot{o} \ddot{O} \ddot{A} \ddot{y} \ddot{A}_i \ddot{I} \ddot{u} \ddot{C} \ddot{1/4} \ddot{i} \ddot{y} \ddot{E} \ddot{E}. \ddot{t} \pm \ddot{y} \ddot{U} \ddot{o} \ddot{D} \ddot{1/2} \ddot{A} \ddot{A} \ddot{i} \ddot{S}, \ddot{A} \ddot{A} \ddot{I} \ddot{A} \ddot{A} \ddot{i} \ddot{S}, \ddot{3/4} \ddot{C} \ddot{o} \ddot{3/4} \ddot{O}$
 $\ddot{O} \ddot{A} \ddot{C} \ddot{A} \ddot{A} \ddot{A} \ddot{A} \ddot{A} \ddot{I} \ddot{O} \ddot{A}_i \ddot{r} \ddot{3/4} \ddot{A}$

$$F(r, \theta) = 0$$

$\pm \ddot{y} \ddot{U} \ddot{o} \ddot{O} \ddot{A} \ddot{y} \ddot{A}_i \ddot{I} \ddot{A} \ddot{i} \ddot{A} \ddot{A} \ddot{U} \ddot{i} \ddot{l} \ddot{o}.$

4.1.5.2 p_{Añ} 1/4 i A_D O_i E

$\ddot{O} \ddot{A} \ddot{O} \ddot{A} \ddot{A} \ddot{i} \ddot{C} \ddot{O} \ddot{A} \ddot{O} \ddot{o} \ddot{A}_i \ddot{O} \ddot{u} \ddot{O} \ddot{1/4} \ddot{O} \ddot{A} \ddot{O} \ddot{3/4} \ddot{E} \ddot{C} \ddot{1/4} \ddot{O} \text{ (physical condition)}$
 $\ddot{D} \ddot{S}_i \ddot{C} \ddot{y} \ddot{p} \ddot{A} \ddot{i} \ddot{O} \ddot{O} \ddot{I} \ddot{o} \ddot{A} \ddot{i} \ddot{O} \ddot{3/4} \ddot{o} \ddot{A} \ddot{O} \ddot{I} \ll \ddot{3/4} \ddot{y} \ddot{A}_i \ddot{r} \ddot{3/4} \ddot{O} \ddot{y} \ddot{S} \ll \ddot{E} \ddot{C} \ddot{A} \ddot{i} \ddot{o} \ddot{A} \ddot{i} \ddot{o}.$

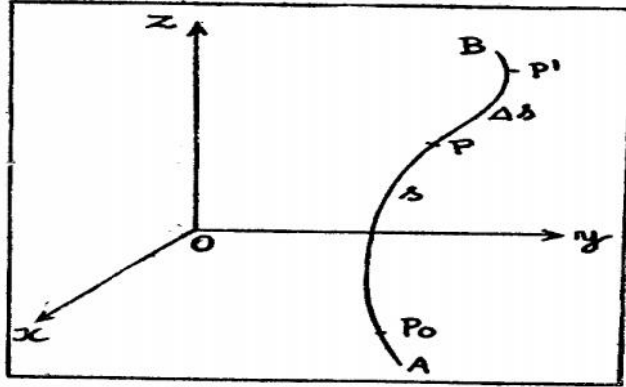
$\ddot{A} \ddot{1/4} \ddot{o} \text{ (4.1-3)-} \ddot{O} \ddot{S}_i \ddot{O} \ddot{E} \ddot{A} \ddot{A}_i \ddot{U} \ddot{D} \ddot{u} \ddot{p} \ddot{A} \ddot{i} \ddot{l} \ddot{o} \ddot{A} \ddot{B} \pm \ddot{y} \ddot{U} \ddot{o} \ddot{A}_i \ddot{r} \ddot{3/4} \ddot{A}$
 $f(x,y,z) = 0$

$\pm \ddot{y} \ddot{U} \ddot{o} \ddot{O} \ddot{A} \ddot{y} \ddot{A}_i \ddot{I} \ddot{A} \ddot{i} \ddot{A} \ddot{A} \ddot{U} \ddot{o} \ddot{A} \ddot{3/4} \ddot{i} \ddot{I} \ddot{1/4} \ddot{i} \ddot{u} \ddot{S}.$

$\ddot{P}_0 \pm \ddot{y} \ddot{U} \ddot{o} \ddot{O} \ddot{U} \ddot{C} \ddot{A} \ddot{i} \ddot{C} \ddot{A} \ddot{i} \ddot{A} \ddot{A} \ddot{O} \ddot{t} = 0 \pm \ddot{y} \ddot{U} \ddot{o} \ddot{S}_i \ddot{A} \ddot{O} \ddot{3/4} \ddot{O} \ddot{O} \ddot{C} \ddot{A} \ddot{i} \ddot{E}$

$\ddot{O} \ddot{U} \ddot{C} \ddot{A} \ddot{i} \ddot{l} \ddot{E} \ddot{O} \ddot{i} \ddot{O}. \ddot{A}_i \ddot{r} \ddot{3/4} \ddot{A} \ddot{O} \ddot{P} \pm \ddot{y} \ddot{U} \ddot{o} \ddot{O} \ddot{U} \ddot{C} \ddot{A} \ddot{i} \ddot{P}_0 \ddot{P} = s \pm \ddot{y} \ddot{U} \ddot{o} \ddot{A} \ddot{O} \ddot{t}$

$\ddot{S}_i \ddot{A} \ddot{O} \ddot{3/4} \ddot{O} \ddot{A} \ddot{i} \ddot{A} \ddot{A} \ddot{U} \ddot{i} \ddot{l} \ddot{o}. \ddot{P}_0 \cdot \ddot{P} - \ddot{d} \ddot{t} \pm \ddot{y} \ddot{U} \ddot{o} \ddot{O} \ddot{U} \ddot{C} \ddot{U} \ddot{i} \ddot{l} \ddot{p} \ddot{1/4} \ddot{A} \ddot{O} \ddot{U} \ddot{C} \ddot{A}_i \ddot{r} \ddot{3/4} \ddot{A} \ddot{y}$
 $\ddot{1/4} \ddot{i} \ddot{A} \times \ddot{S}_i \ddot{A} \ddot{O} \ddot{3/4} \ddot{O} \ddot{S}_i \ddot{u} \ddot{E} \ddot{A}_i \ddot{U} \ddot{A}_i \ddot{U} \ddot{A} \ddot{i} \ddot{A} \ddot{3/4} \ddot{O},$
 $s = F(t)$



Ảnh 4-1-3

Để tìm độ dài của đường cong C trong không gian, ta cần tính tích phân bội hai của độ dài vi phân ds dọc theo đường cong. Công thức tính độ dài đường cong trong không gian là:

$$L = \int_a^b \sqrt{\left(\frac{dx}{dt}\right)^2 + \left(\frac{dy}{dt}\right)^2 + \left(\frac{dz}{dt}\right)^2} dt$$

4.1.6 Ví dụ 1

4.1.6.1 Tìm độ dài của đường cong C trong không gian được xác định bởi phương trình vectơ:

$$\vec{r}(t) = (t^2 + 3)\vec{i} + (1 + t^2)\vec{j} + 0\vec{k} \quad \text{với } 0 \leq t \leq 3$$

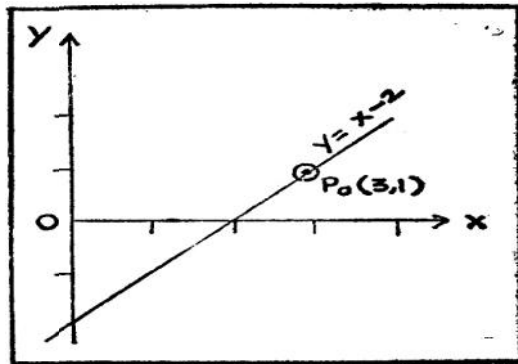
$$\begin{aligned} x(t) &= 3 + t^2 \\ y(t) &= 1 + t^2 \\ z(t) &= 0 \end{aligned}$$

Để tìm độ dài của đường cong, ta cần tính tích phân bội hai của độ dài vi phân ds dọc theo đường cong.

$$x - 3 = y - 1$$

$$\Leftrightarrow y = x - 2$$

Đường cong C nằm trong mặt phẳng $y = x - 2$ và đi qua điểm $P_0(3, 1)$.



Ảnh 4-1-4

Để tính độ dài của đường cong C trong mặt phẳng, ta cần tính tích phân bội hai của độ dài vi phân ds dọc theo đường cong. Công thức tính độ dài đường cong trong mặt phẳng là:

$$L = \int_a^b \sqrt{\left(\frac{dx}{dt}\right)^2 + \left(\frac{dy}{dt}\right)^2} dt$$

ŞzÃõ t=3 ÅÉjÊ ±ýÛõŞjÐ Ð, ù Àj ¼Å« « Åõ òùÇÀ ì jÃ
 - À ò ¼j Å, ù Ó ÈŞÃ x=3+9 = 120 Å.Å, y=1+9 = 100 Å.Å - ì õ.

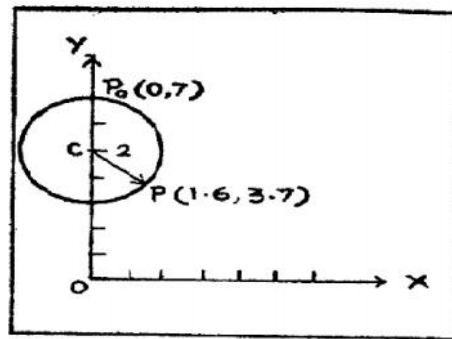
4.1.6.2. t ±ýÛõ ŞzÃõ Ð, ù pÃ ì õ Àj ¼Å Åõ òùÇÃý
 ç Åõ Å

$$\underline{r}(t) = 2 \sin 10t \underline{i} + (5 + 2 \cos 10t) \underline{j} \text{ Å.Å}$$

±ýËj, Ð, ù pÃ ì õ Å ÇÃ Åý Åj ð ¼õ ŞzÃõ t=4 ÅÉjÊ
 ±ýÛõŞjÐ Ð, ù pÕ ì Åõ ¼õ jñ.

$$\begin{aligned} \text{pÃ ì } x(t) &= 2 \sin 10t \\ y(t) &= 5 + 2 \cos 10t \end{aligned}$$

ì ì ¼ Å Çõ Şj ½õ - ÅÅÉ (Radians) ì È õÃ õ.



Åõ 4-1-5

t ±ýÛõ Ð ½ÅÅ Å Å Å X² + (y-5)² = 4(sin²10t + cos²10t) = 4 ±ýÛõ
 Åý Åj ì ¼ ÅÐ. pÃ Åý Åj ì (x,y) Çõ Çõ c(0,5) ±ýÛõ òùÇÃ Å
 ÅÅj xõ r=2 Å ±ýÛõ ç Çõ ¼ - ÅÅj xõ (radius) jñ ¼
 Åõ ¼õ ¼õ Åõ (4.1.5) - õ j ð ÅÅj Û Å ÅÅÛ ÅÐ.

ŞzÃõ t=0 ±ýÛõŞjÐ Ð, ù x=0, y=7 ±ýÛõ ¼j Åx Çõ ¼Å
 p₀ ±ýÛõ òùÇÃ « ì õõ.

ŞzÃõ t=4Å - ùÇŞjÐ Ð, ù x=2sin40, y=5+2cos40 ±ýÛõ
 òùÇÃ pÕ ì õ. ŞÅÛÛÈ Åý Åj ì Çõ ì ì ¼ Å Çõ ùÇ 40
 ±ýÅÐ, 40 - ÅÅý Ç ì È ì Åj ¼j ð - ÅÅý 57.3° ±ýË
 Å ÅÅÛõõÅÈ

$$\begin{aligned} x &= 2 \sin(40 \times 57.3^\circ) \\ &= 2 \sin 2292^\circ \\ &= 2 \sin 132^\circ \\ &= 2 \sin 48^\circ \\ &= 1.5862 \\ &= 16 \text{ Å.Å} \end{aligned}$$

$$y = 5 + 2 \cos(40 \times 57.3^\circ)$$

4.2.3.1 \vec{v} (Uniform velocity)

$\vec{v} = \frac{\Delta \vec{r}}{\Delta t}$ (Average velocity) $\vec{v} = \frac{\vec{r}(t) - \vec{r}(t_0)}{t - t_0}$

$\vec{v} = \frac{\Delta \vec{r}}{\Delta t}$ (Instantaneous velocity) $\vec{v} = \lim_{\Delta t \rightarrow 0} \frac{\Delta \vec{r}}{\Delta t} = \frac{d\vec{r}}{dt}$

$\vec{v} = \frac{d\vec{r}}{dt}$ (Average velocity) $\vec{v} = \frac{\vec{r}(t) - \vec{r}(t_0)}{t - t_0}$

$\vec{v} = \frac{d\vec{r}}{dt}$ (Instantaneous velocity) $\vec{v} = \lim_{\Delta t \rightarrow 0} \frac{\Delta \vec{r}}{\Delta t} = \frac{d\vec{r}}{dt}$

4.2.3.2 \vec{v} (Average velocity)

$\vec{v} = \frac{\Delta \vec{r}}{\Delta t}$ (Average velocity) $\vec{v} = \frac{\vec{r}(t) - \vec{r}(t_0)}{t - t_0}$

4.2.3.3 \vec{v} (Instantaneous velocity)

$\vec{v} = \frac{d\vec{r}}{dt}$ (Instantaneous velocity) $\vec{v} = \lim_{\Delta t \rightarrow 0} \frac{\Delta \vec{r}}{\Delta t} = \frac{d\vec{r}}{dt}$

$\vec{r}(t) = x(t)\vec{i} + y(t)\vec{j} + z(t)\vec{k}$

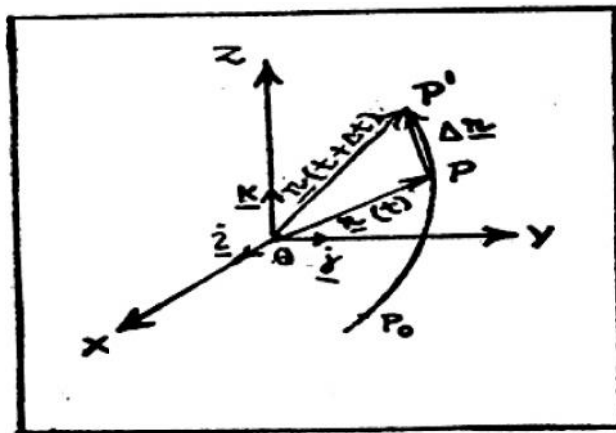


Figure 4-2-3

$\vec{v} = \frac{d\vec{r}}{dt}$ (Instantaneous velocity) $\vec{v} = \lim_{\Delta t \rightarrow 0} \frac{\Delta \vec{r}}{\Delta t} = \frac{d\vec{r}}{dt}$

$\vec{v} = \frac{d\vec{r}}{dt}$ (Instantaneous velocity) $\vec{v} = \lim_{\Delta t \rightarrow 0} \frac{\Delta \vec{r}}{\Delta t} = \frac{d\vec{r}}{dt}$

$$\begin{aligned}
PP' &= OP' - OP \\
&= \underline{r}(t+\Delta t) - \underline{r}(t) \\
&= x(t+\Delta t)\underline{i} + y(t+\Delta t)\underline{j} + z(t+\Delta t)\underline{k} - x(t)\underline{i} - y(t)\underline{j} - z(t)\underline{k} \\
&= \{x(t+\Delta t) - x(t)\}\underline{i} + \{y(t+\Delta t) - y(t)\}\underline{j} + \{z(t+\Delta t) - z(t)\}\underline{k} \\
&= \Delta x\underline{i} + \Delta y\underline{j} + \Delta z\underline{k}
\end{aligned}$$

→ \hat{t} o.

$PP' = \Delta r$ o \hat{t} o. « Δr o \hat{t} o. »

$\Delta \underline{r}(t) = \Delta r$ o \hat{t} o. « Δr o \hat{t} o. »

$$\frac{\Delta r}{\Delta t} = \frac{dr}{dt}$$

$$\frac{\Delta s}{\Delta t} = \frac{ds}{dt}$$

« Δr o \hat{t} o. » Δr o \hat{t} o. « Δr o \hat{t} o. »

« Δr o \hat{t} o. »

« Δr o \hat{t} o. » Δr o \hat{t} o. « Δr o \hat{t} o. »

« Δr o \hat{t} o. » Δr o \hat{t} o. « Δr o \hat{t} o. »

$$\frac{dr}{dt} = \frac{ds}{dt}$$

$\cos \alpha_x = \frac{v_x}{v} = \frac{v_x}{\sqrt{v_x^2 + v_y^2 + v_z^2}}$

$$\cos \alpha_x = \frac{v_x}{v} = \frac{v_x}{\sqrt{v_x^2 + v_y^2 + v_z^2}}$$

$$\cos \alpha_y = \frac{v_y}{v} = \frac{v_y}{\sqrt{v_x^2 + v_y^2 + v_z^2}}$$

$$\cos \alpha_z = \frac{v_z}{v} = \frac{v_z}{\sqrt{v_x^2 + v_y^2 + v_z^2}}$$

$\cos \alpha_x = \frac{v_x}{v} = \frac{v_x}{\sqrt{v_x^2 + v_y^2 + v_z^2}}$

$\cos \alpha_y = \frac{v_y}{v} = \frac{v_y}{\sqrt{v_x^2 + v_y^2 + v_z^2}}$

$\cos \alpha_z = \frac{v_z}{v} = \frac{v_z}{\sqrt{v_x^2 + v_y^2 + v_z^2}}$

$$\underline{t} = \frac{v_x}{v} \underline{i} + \frac{v_y}{v} \underline{j} + \frac{v_z}{v} \underline{k} = \cos \alpha_x \underline{i} + \cos \alpha_y \underline{j} + \cos \alpha_z \underline{k}$$

$\cos \alpha_x = \frac{v_x}{v} = \frac{v_x}{\sqrt{v_x^2 + v_y^2 + v_z^2}}$

$\cos \alpha_y = \frac{v_y}{v} = \frac{v_y}{\sqrt{v_x^2 + v_y^2 + v_z^2}}$

$$\frac{ds}{dt} = v$$

$$s = \int v dt + c$$

$\cos \alpha_z = \frac{v_z}{v} = \frac{v_z}{\sqrt{v_x^2 + v_y^2 + v_z^2}}$

$\cos \alpha_x = \frac{v_x}{v} = \frac{v_x}{\sqrt{v_x^2 + v_y^2 + v_z^2}}$

$$\underline{v} = v_x \underline{i} + v_y \underline{j} + v_z \underline{k} = v (\cos \alpha_x \underline{i} + \cos \alpha_y \underline{j} + \cos \alpha_z \underline{k})$$

$$\frac{dx}{dt} = v_x; \frac{dy}{dt} = v_y; \frac{dz}{dt} = v_z$$

$$\therefore x = \int v_x dt + c_1; y = \int v_y dt + c_2; z = \int v_z dt + c_3$$

$\cos \alpha_x = \frac{v_x}{v} = \frac{v_x}{\sqrt{v_x^2 + v_y^2 + v_z^2}}$

$\cos \alpha_y = \frac{v_y}{v} = \frac{v_y}{\sqrt{v_x^2 + v_y^2 + v_z^2}}$

4.2.6.2 $\bar{\omega}_z$ (Average angular velocity)

OP \perp \vec{r} \perp \vec{v} \perp $\vec{\omega}$.
 « $\hat{I} \cdot \Delta \vec{\omega} \Delta t$ \perp $\vec{r} \perp \Delta \theta \perp \hat{I} \cdot \bar{\omega} \Delta t$ « $\hat{C} \times (\hat{I} \cdot \Delta \vec{\omega})$
 $\bar{\omega}_z = \frac{\Delta \theta}{\Delta t}$

4.2.6.3 ω_z (Instantaneous angular velocity)

Δt \perp $\vec{r} \perp \Delta \theta$ \perp $\hat{I} \cdot \bar{\omega} \Delta t$ \perp $\vec{v} \perp \vec{\omega}$ \perp $\vec{r} \perp \Delta \theta$ \perp $\hat{I} \cdot \bar{\omega} \Delta t$
 $\hat{I} \cdot \Delta \vec{\omega} \Delta t \perp \vec{r} \perp \Delta \theta \perp \hat{I} \cdot \bar{\omega} \Delta t$
 $\bar{\omega}_z = \frac{d\theta}{dt}$

$\vec{v} = \vec{\omega} \times \vec{r}$
 $\frac{d\vec{r}}{dt} = \vec{\omega} \times \vec{r}$
 $\vec{v} = \vec{\omega} \times \vec{r}$

$$\vec{v} = \vec{\omega} \times \vec{r}$$

4.2.7. Relationship between angular velocity and linear velocity

$\vec{v} = \vec{\omega} \times \vec{r}$

4.2.7.1 $\vec{v} = \vec{\omega} \times \vec{r}$

$\vec{v} = \vec{\omega} \times \vec{r}$
 $\vec{v} = \vec{\omega} \times \vec{r}$
 $\vec{v} = \vec{\omega} \times \vec{r}$

$$\vec{v} = \vec{\omega} \times \vec{r}$$

$$\Delta s = r \Delta \theta$$

$$\therefore \frac{\Delta s}{\Delta t} = r \frac{\Delta \theta}{\Delta t}$$

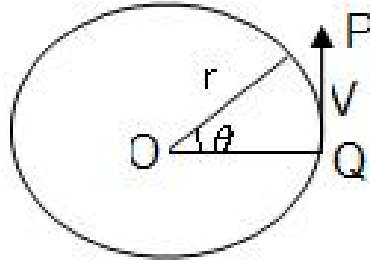
$$v = \lim_{\Delta t \rightarrow 0} \frac{\Delta s}{\Delta t} = \lim_{\Delta t \rightarrow 0} r \frac{\Delta \theta}{\Delta t}$$

$$v = \vec{\omega} \times \vec{r}$$

$$V = rS \rightarrow \vec{\omega}$$

$$\omega = \frac{v}{r} \quad r = \frac{v}{\omega}$$

$$\therefore \vec{S} = \frac{V}{r}$$



À¼õ 4-2-5

4.2.8 À·Ã·È ÓÎ ì õ (ŞÅ ĀÇ÷î°ò¼ x) (Acceleration)

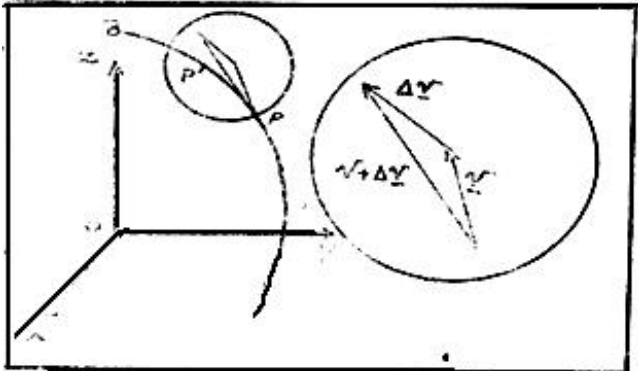
ÞÁÍ Ì ŸÉ Ò Ð ÇŸ ¼°ŞÅ ĀĪŪĀÏËŸ Ā¼õ « òÐ ÇŸ
 "ÓÎ ì õ" « ØĀÐ "ŞÅ ĀÇ÷î°ò¼ x" ±ĒôĀİ ò.
 ¼°ŞÅ ĀĪŪĒõ Ò ¼°ĀĀĪĀ¼Īø « ¼Ÿ Ā¼Óõ Ò ¼°ĀĀĪ ò.
 ŸŞÅ ÓÎ ì õ Ò ¼°ĀĀĪ ÇĒ.
 òŸÇÇ ÞÁÍ Ì õ ¼°Ÿİ ±¼ĀĪ ÓÎ ì õ ÞŌİ Ì ĀÉø « ¼
 "±¼Ÿ-ÓÎ ì õ" (Deceleration) ±Ēİ ŪŪĀÐ ĀĒİ õ.

4.2.8. 1. ĀĪÉÓÎ ì õ (Uniform acceleration)

ÞÁÍ Ì õ òŸÇÇ ŸĒŸ ¼°ŞÅ ò¼ø ±òÐ Ēİ ĒĀ¼ĪÉ
 °ĀŞĀĪ Çø, °ĀŞÅ ĀĪŪĒõ ŞÅ¼°Āø ²ŪĀĪ ĀĪĀŸ, « òòŸÇÇ ĀĪÉ
 ÓÎ ì õ ¼°ĀĪŪŪÇÐ ±ĒôĀİ ò.
 ÓÎ ì õ ĀĪÉ¼Ī ŸÇŞĀĪÐ, ÓÎ Ì ĀĪÉÐ µĀĀĪ ŞĀĀ¼ø
 òŸÇÇĀŸ ¼°ŞÅ ò¼ø ²ŪĀĪ õ ŞÅ ĀĪŪĒõ¼Īø « ÇĀ¼ôĀİ ò.

4.2.8.2. Ō Ì ĒôĀø¼ ½ò¼ø Ð ÇŸ ÓÎ ì õ (Instantaneous acceleration of a particle.)

Ò Ð ÇŸ ¼°ŞÅ õ °ĀĪĀ « Ç×Çø °ĀŞÅ ĀĪŪĒõ
 ²ŪĀ¼ĪĀĒŪõ « ØĀÐ ŞÅ ĀĪŪĒõ ŞÅ¼°Āø ĪĀĪĀĒŪõ, ÓÎ ì õ
 ĀĪŪĀĪĪŪĒĀÐ. ŸŞÅ ÓÎ ì õ ĀĪŪĀĪ õŞĀĪÐ, Ō Ì ĒôĀø¼ ŞĀĀ¼ø,
 « ¼Ÿ ÓÎ ì õ ¼ Ā ŸŃ Ÿ½ò¼ø ¼õ (Differential calculus) ĀĀŸĀĪ ò¼Ī
 ½ĀĪõ.



À¼õ 4-2-6

$$a_y = \frac{d^2y}{dt^2} = \ddot{y}$$

$$a_z = \frac{d^2z}{dt^2} = \ddot{z}$$

→ $\vec{a} = a_x \hat{i} + a_y \hat{j} + a_z \hat{k}$ $\vec{r} = x \hat{i} + y \hat{j} + z \hat{k}$ $\vec{v} = \dot{x} \hat{i} + \dot{y} \hat{j} + \dot{z} \hat{k}$

4.2.8.4. $\vec{a} = a_x \hat{i} + a_y \hat{j} + a_z \hat{k}$, $\vec{r} = x \hat{i} + y \hat{j} + z \hat{k}$, $\vec{v} = \dot{x} \hat{i} + \dot{y} \hat{j} + \dot{z} \hat{k}$

$$\vec{a} = a_x \hat{i} + a_y \hat{j} + a_z \hat{k}$$

$$a^2 = \vec{a} \cdot \vec{a} = a_x^2 + a_y^2 + a_z^2$$

$$a = \sqrt{a_x^2 + a_y^2 + a_z^2}$$

$\cos \theta_x = \frac{a_x}{a}$; $\cos \theta_y = \frac{a_y}{a}$; $\cos \theta_z = \frac{a_z}{a}$

$$\cos \theta_x = \frac{a_x}{a}; \cos \theta_y = \frac{a_y}{a}; \cos \theta_z = \frac{a_z}{a}$$

$\vec{v} = \dot{x} \hat{i} + \dot{y} \hat{j} + \dot{z} \hat{k}$

(1) $\vec{r} = x \hat{i} + y \hat{j} + z \hat{k}$, $\vec{v} = \dot{x} \hat{i} + \dot{y} \hat{j} + \dot{z} \hat{k}$, $\vec{a} = a_x \hat{i} + a_y \hat{j} + a_z \hat{k}$

(2) $\vec{r} = r \hat{e}_r$, $\vec{v} = \dot{r} \hat{e}_r + r \dot{\theta} \hat{e}_\theta$, $\vec{a} = (\ddot{r} - r \dot{\theta}^2) \hat{e}_r + (2\dot{r} \dot{\theta} + r \ddot{\theta}) \hat{e}_\theta$

$$\vec{r} = r \hat{e}_r$$

$$\vec{v} = \frac{dr}{dt} \hat{e}_r + r \frac{d\theta}{dt} \hat{e}_\theta$$

$$\vec{a} = \frac{d^2r}{dt^2} \hat{e}_r + \frac{d}{dt} \left\{ \frac{dr}{dt} \right\} \hat{e}_r + \frac{d^2r}{dt^2} \hat{e}_r$$

$\vec{r} = r \hat{e}_r$, $\vec{v} = \dot{r} \hat{e}_r + r \dot{\theta} \hat{e}_\theta$, $\vec{a} = (\ddot{r} - r \dot{\theta}^2) \hat{e}_r + (2\dot{r} \dot{\theta} + r \ddot{\theta}) \hat{e}_\theta$

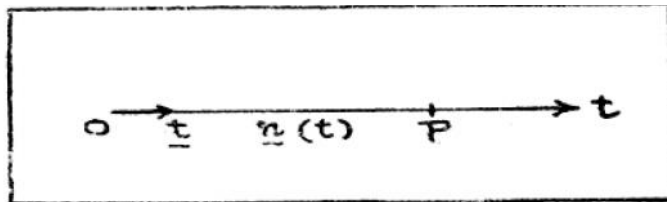


Figure 4-2-7

(3) $\frac{dv_x}{dt} = a_x$, $\frac{dv_y}{dt} = a_y$, $\frac{dv_z}{dt} = a_z$

$$\frac{dv_x}{dt} = a_x \quad \therefore v_x = \int a_x dt + c_1$$

$$\frac{dv_y}{dt} = a_y \quad \therefore v_y = \int a_y dt + c_2$$

$$\frac{dv_z}{dt} = a_z \quad \therefore v_z = \int a_z dt + c_3$$

c_1, c_2, c_3 என்பன $\int a_x dt, \int a_y dt, \int a_z dt$ (Constants of integration) ஆகும்.

எனவே,

$$\frac{dx}{dt} = v_x \quad \therefore x = \int v_x dt + c_4$$

$$\frac{dy}{dt} = v_y \quad y = \int v_y dt + c_5$$

$$\frac{dz}{dt} = v_z \quad z = \int v_z dt + c_6$$

$$\frac{ds}{dt} = v \quad s = \int v dt + c_7$$

(4) $\frac{dv_x}{dt} = a_x$ எனில், $\frac{dx}{dt} = v_x$ எனில், $x = \int v_x dt + c_2$

$\frac{dv_x}{dt} = a_x$ எனில், $\int \frac{dv_x}{dt} dt = \int a_x dt$ எனில், $v_x = \int a_x dt + c_1 = a_x t + c_1$

$$\frac{dv_x}{dt} = a_x \quad \therefore v_x = \int a_x dt + c_1 = a_x t + c_1$$

$$\begin{aligned} \frac{dx}{dt} &= v_x \\ \therefore x &= \int v_x dt + c_2 \\ &= \int (a_x t + c_1) dt + c_2 \\ &= a_x \frac{t^2}{2} + c_1 t + c_2 \end{aligned}$$

4.2.9 $\vec{r}(t) = 2\sin 5t \vec{j} + (5 + 2\cos 5t) \vec{i}$ எனில் $\vec{v}(t)$ மற்றும் $\vec{a}(t)$ காண்க.

4.2.9.1 $t = 3$ மற்றும் $t = 0$ க்கு $\vec{r}(t)$ மற்றும் $\vec{v}(t)$ காண்க.

$$\vec{r}(t) = 2\sin 5t \vec{j} + (5 + 2\cos 5t) \vec{i}$$

(i) $t = 3$ க்கு $\vec{r}(t)$ மற்றும் $\vec{v}(t)$ காண்க.

(ii) $t = 0$ க்கு $\vec{r}(t)$ மற்றும் $\vec{v}(t)$ காண்க.

$$\cos r = \frac{3}{\sqrt{19}}; \cos s = \frac{1}{\sqrt{19}}; \cos x = \frac{3}{\sqrt{19}} \quad \rightarrow \hat{i} \cdot \hat{o}.$$

$$\vec{v} = \frac{dr}{dt} = -\{(4-3t^2)\hat{i} - 2\hat{j} - 6\hat{k}\} \quad \text{Áf/Át.}$$

$$|v|_{t=1} = \hat{i} - 2\hat{j} - 6\hat{k} \quad \text{Áf/Át.}$$

$$\cos_{\text{ny}} = \frac{1}{\sqrt{41}}; \cos_{\text{y}} = \frac{-2}{\sqrt{41}}; \cos_{\text{z}} = \frac{-6}{\sqrt{41}} \quad \rightarrow \hat{i} \cdot \hat{o}.$$

4.2.9.3 $\vec{r}(t) = 4\cos t \hat{i} + 2\sin t \hat{j} + t^2 \hat{k}$
 $\vec{v} = \dot{\vec{r}} = -4\sin t \hat{i} + 2\cos t \hat{j} + 2t \hat{k}$
 $v = |\vec{v}| = \sqrt{16\sin^2 t + 4\cos^2 t + 4t^2}$
 $= \sqrt{16 + 4t^2}$
 $|\vec{v}|_{t=1} = \sqrt{16+4} = \sqrt{20} = \sqrt{0.20} \quad \text{Áf/Át.}$
 $\vec{a} = \ddot{\vec{r}} = -4\cos t \hat{i} - \sin t \hat{j} + 2\hat{k}$
 $|\vec{a}| = \sqrt{16\cos^2 t + 16\sin^2 t + 4}$
 $|\vec{a}|_{t=1} = \sqrt{16+4} = \sqrt{20} = \sqrt{0.20} \quad \text{Áf/Át.}$
 $\vec{r}(t) = (t - \sin t)\hat{i} + (1 - \cos t)\hat{j} + 4\sin \frac{t}{2} \hat{k}$

$$(i) \quad \vec{r}(t) = 4\cos t \hat{i} + 2\sin t \hat{j} + t^2 \hat{k}$$

$$\vec{v} = \dot{\vec{r}} = -4\sin t \hat{i} + 2\cos t \hat{j} + 2t \hat{k}$$

$$v = |\vec{v}| = \sqrt{16\sin^2 t + 4\cos^2 t + 4t^2}$$

$$= \sqrt{16 + 4t^2}$$

$$|\vec{v}|_{t=1} = \sqrt{16+4} = \sqrt{20} = \sqrt{0.20} \quad \text{Áf/Át.}$$

$$\vec{a} = \ddot{\vec{r}} = -4\cos t \hat{i} - \sin t \hat{j} + 2\hat{k}$$

$$|\vec{a}| = \sqrt{16\cos^2 t + 16\sin^2 t + 4}$$

$$|\vec{a}|_{t=1} = \sqrt{16+4} = \sqrt{20} = \sqrt{0.20} \quad \text{Áf/Át.}$$

$$\vec{r}(t) = (t - \sin t)\hat{i} + (1 - \cos t)\hat{j} + 4\sin \frac{t}{2} \hat{k}$$

$$(ii) \quad \vec{v} = \dot{\vec{r}} = (1 - \cos t)\hat{i} + \sin t \hat{j} + 4\cos \frac{t}{2} \cdot \frac{1}{2} \hat{k}$$

$$= (1 - \cos t)\hat{i} + \sin t \hat{j} + 2\cos \frac{t}{2} \hat{k}$$

$$|\vec{v}| = \sqrt{1 + \cos^2 t - 2\cos t + \sin^2 t + 4\cos^2 \frac{t}{2}}$$

$$= \sqrt{2(1 - \cos t) + 4\cos^2 \frac{t}{2}}$$

$$|\vec{v}|_{t=1} = 2 \quad 0.02 \quad \text{Áf/Át}$$

4.2.10 $\vec{r}(t)$

4.2.10.1 (x, y) - $\vec{r}(t) = x\vec{i} + y\vec{j}$ $\vec{r}(t) = 4t^2\vec{i} + 6t\vec{j}$ $\vec{v}(t) = 8t\vec{i} + 6\vec{j}$ $\vec{a}(t) = 8\vec{i}$ $\vec{v}(1) = 8\vec{i} + 6\vec{j}$ $|\vec{v}(1)| = 10$ $\alpha = 36.9^\circ$

4.2.10.2 $\vec{r}(t) = 1.36t^3\vec{i} + 3.62t^2\vec{j} + 2.37t\vec{k}$ $\vec{v}(t) = 4.08t^2\vec{i} + 7.24t\vec{j} + 2.37\vec{k}$ $\vec{a}(t) = 8.16t\vec{i} + 7.24\vec{j}$ $\vec{v}(0.5) = 1.02\vec{i} + 3.62\vec{j} + 2.37\vec{k}$ $|\vec{v}(0.5)| = 4.44$ $\alpha = 4.44$ $\vec{a}(0.5) = 4.08\vec{i} + 7.24\vec{j}$ $|\vec{a}(0.5)| = 8.16$ $\alpha = 4.44$

4.2.10.3 $\vec{r}(t) = 0.5t^2\vec{i} + 5t\vec{j}$ $\vec{v}(t) = t\vec{i} + 5\vec{j}$ $\vec{a}(t) = \vec{i}$ $\vec{v}(1) = \vec{i} + 5\vec{j}$ $|\vec{v}(1)| = 5.1$ $\alpha = 10.6^\circ$

4.2.10.4 $\vec{r}(t) = (2t^2 - 4t)\vec{i} + 2(t-1)^2\vec{j} + 4(t-1)\vec{k}$ $\vec{v}(t) = (4t-4)\vec{i} + 4(t-1)\vec{j} + 4\vec{k}$ $\vec{a}(t) = 4\vec{i} + 4\vec{j}$ $\vec{v}(1) = 4\vec{j} + 4\vec{k}$ $|\vec{v}(1)| = 5.66$ $\alpha = 45^\circ$

4.2.10.5 $\vec{r}(t) = 16(5-6t+2t^2)\vec{i}$ $\vec{v}(t) = 32(2-3t)\vec{i}$ $\vec{a}(t) = -32\vec{i}$ $\vec{v}(1) = -32\vec{i}$ $|\vec{v}(1)| = 32$ $\alpha = 180^\circ$

$\vec{r}(t) = 2\sqrt{2} \left(\frac{i}{\sqrt{2}} - \frac{j}{\sqrt{2}} \right)$ $\vec{v}(t) = 2\sqrt{2} \left(-\frac{i}{\sqrt{2}} - \frac{j}{\sqrt{2}} \right)$ $\vec{a}(t) = -2\sqrt{2} \left(\frac{i}{\sqrt{2}} - \frac{j}{\sqrt{2}} \right)$

4.2.10.6. $r = \pm y \hat{u}_o$ $S_{\hat{A}o}(\hat{A}E; \hat{E}A)$ $p\hat{A}i \hat{o} \hat{D}, \hat{C}y$ $\hat{c} \hat{A} \hat{A}$
 $r = \{(t+1)^2 \hat{i} + (t+1)^{-2} \hat{j}\} \hat{A} \hat{E} \pm y \hat{u}_o$ $\hat{c} \hat{A} \hat{A} \hat{o} \hat{A} \hat{A} \hat{U} \hat{o} \hat{A} \hat{i}, \ll \hat{y}$
 $p\hat{A}i \hat{A} \hat{A} \hat{O} \hat{i} \hat{o} \hat{u} \hat{A} \ll \hat{A} \hat{A} \hat{A} \hat{C} \times$ (Rectangular hyperbola) $\pm \hat{E} \hat{i}, \hat{j}, \hat{n}$
 $S_{\hat{A}o} t=0 \hat{A} \hat{E}; \hat{E} t = \frac{1}{2} \hat{A} \hat{E}; \hat{E} \pm y \hat{u} \hat{u} \hat{C} \hat{o} \hat{A} \hat{A} \hat{i}, \hat{C} \hat{o}, \hat{D}, \hat{C} \hat{o} \hat{A} \hat{A} \hat{o},$
 $\hat{O} \hat{I} \hat{i} \hat{o} \hat{n} \hat{A} \hat{A} \hat{u} \hat{E} \hat{O} \hat{o} \hat{i}, \hat{n}$
 $\hat{A} \hat{c} \hat{A}: xy=1, t=0 \hat{A} \hat{E}; \hat{E}$

$$\underline{v} = 2\sqrt{2} \left(\frac{\hat{i}}{\sqrt{2}} - \frac{\hat{j}}{\sqrt{2}} \right) \hat{A} \hat{E} / \hat{A} \hat{c}$$

$$\underline{a} = 2\sqrt{10} \left(\frac{\hat{i}}{\sqrt{10}} - \frac{3\hat{j}}{\sqrt{10}} \right) \hat{A} \hat{E} / \hat{A} \hat{c}^2$$

$$t = 0.5 \hat{A} \hat{c}$$

$$\underline{v} = 2\sqrt{2} \left(\frac{81\hat{i}}{82.50} - \frac{16\hat{j}}{82.50} \right) \hat{A} \hat{E} / \hat{A} \hat{c}$$

$$\underline{a} = 2.325(0.8602\hat{i} + 0.5097\hat{j}) \hat{A} \hat{E} / \hat{A} \hat{c}^2$$

4.2.10.7 $p\hat{A}i \hat{o} \hat{D}, \hat{u} \hat{y} \hat{E} \hat{y} \hat{A} \hat{i} \hat{A}, t \hat{A} \hat{E}; \hat{E} S_{\hat{A}o} x = 1000$
 $(1-e^{-t}) \hat{i}, \hat{A} \hat{E}; y = 1000t/(1+t) \hat{i}, \hat{A} \hat{E} \pm y \hat{u}_o \hat{o} \hat{A} \hat{y} \hat{A} \hat{i} \hat{u} \hat{A} \hat{A} \hat{U} \hat{i} \hat{A} \hat{E} \ll \hat{y}$
 $\hat{c} \hat{A}, \hat{A} \hat{A} \hat{o} \hat{A} \hat{A} \hat{o} \hat{E} t=0, t=1 \hat{A} \hat{E}; \hat{E} \hat{A} \hat{i} \hat{u} \hat{C} \hat{S} \hat{A} \hat{i} \hat{D}, \hat{i}, \hat{n}$
 $(\hat{A} \hat{c} \hat{A}: t=0 \pm y \hat{u}_o S_{\hat{A}o})$

$$\underline{r} = 0, \underline{v} = 10\sqrt{2} |315^\circ \hat{A} \hat{E} \hat{A} \hat{c}$$

$$\underline{a} = 10\sqrt{5} |153.8^\circ \hat{A} \hat{E} \hat{A} \hat{c}^2$$

$$\underline{r} = 6.321\hat{i} + 5\hat{j} \hat{A} \hat{E}$$

$$6321 \hat{i} + 5000 \hat{j} \hat{A} \hat{c} \hat{A} \hat{E}$$

$$\underline{v} = 4.45 |124.2^\circ \hat{A} \hat{E} \hat{A} \hat{c}$$

$$\underline{a} = 4.45 |304.2^\circ \hat{A} \hat{E} \hat{A} \hat{c}^2$$

4.2.11. $\hat{O} \hat{A} \hat{C} \hat{o} \hat{D} \hat{A} \hat{C} \hat{S}, \hat{i} \hat{o} \hat{E} \hat{A} \hat{A} \hat{i} \hat{o} \hat{D}, \hat{C} \hat{y} \hat{O} \hat{I} \hat{i} \hat{o} \hat{A} \hat{A} \hat{i} \hat{A} \hat{A}$
 $\hat{A} \hat{C} \hat{o} \hat{A} \hat{C} \hat{o} \hat{i} \hat{o} \hat{i} \hat{D} \hat{A} \hat{C} \hat{o} \hat{A} \hat{C} \hat{o} \hat{i} \hat{D} \hat{o}$

(To find expression for the acceleration of a particle moving in a plane curve along the tangential and normal directions)

$\hat{A} \hat{A} \hat{o} \hat{A} \hat{C} \hat{A} \hat{o} \hat{D}, \hat{C} \hat{y} p\hat{A}i \hat{o} \hat{A} \hat{C} \hat{S}, \hat{i} \hat{o} \hat{E} \hat{A} \hat{A} \hat{O} \hat{A} \hat{i} \hat{o} \hat{A} \hat{A} \hat{o},$
 $\hat{O} \hat{I} \hat{i} \hat{o} \hat{n} \hat{A} \hat{A} \hat{u} \hat{E} \hat{y} \hat{u} \hat{u} \hat{u}$ (components) $\hat{A} \hat{y} \hat{u} \hat{c} \hat{A} \hat{A} \hat{i} \hat{E} \hat{D} \hat{o}$
 $\hat{y} \hat{u} \hat{i} \hat{i}, \hat{j} \hat{y} \hat{u} \hat{i} \hat{o} \hat{i} \hat{o} \hat{A} \hat{o} (\hat{i}, \hat{j}, \hat{k}) \pm y \hat{u}_o \hat{A} \hat{E} \hat{o} \hat{A} \hat{o} \hat{E}.$
 $\hat{o} \hat{A} \hat{A} \hat{i} \hat{C} \hat{o} \hat{i} \hat{E} \hat{o} \hat{A} \hat{i} \hat{D}, \hat{C} \hat{y} \hat{A} \hat{i} \hat{A} \hat{A} \hat{o} \hat{A} \hat{o} \hat{S} \hat{A} \hat{i} \hat{D}, p\hat{A}i \hat{o}$

« Ð ŞÀĬŞĂ Ð, ũ P' ±ýÛÁ¼ð'' ¼ ±ðÐðŞÀĬÐ « ¼ý ¼Ĉ'' °ŞĂ, ð'' ¼ V+ΔV ±ÉĬĬ, ĩ ¼Ĭø, « Ð×ð P'-ø Ā'' ĀŌō Ĭ¼ĬĬ Ş, ĬðĒø Ĭ°ĀøĀĬ ò. ĩ ¼ĬĬø V+ΔV=(V+ΔV)t' V+ΔV=(V+ΔV)t' ĩ ò.

P, P' ±ýÛð ðÛÇĬ, Çø, ĀĬ'' ¼ĬĬ Ā'' ĀĀôĀĬ ò Ĭ¼ĬĬ Ş, ĬĬ, ũ x « ĬĬ¼ý Ē, Ē+ΔĒ ±ýÛð Ş, Ĭ¼ĬĬ, Ç « '' ĀôĀ¼ĬÉĬø, (t, t') ±ýÛð ¼Ĉ'' °ĀĬ, ũĬ, Ç'' ¼ĬĬĀ'' ĀŌō Ş, Ĭ¼Ĭð ΔĒ ĩ ò. ŞĀŌō n, n' ¼Ĉ'' °ĀĬ, Ç ĬĬĬ, « '' Ā, ũ C ±ýÛð p¼ð¼ø ĬĀðĒĬĬ, Ĭ, ĬÇĬĬ ò. C Āø n, n' ±ýĀ'' Ā, ũð ΔĒ ±ýÛð Ş, Ĭ¼Ĭð'' ¼ « '' ĀĬĬ ò. C ±ýÛð ðÛÇĬĬÉÐ Ā'' Ç×'' ĀĀō (Centre of curvature) ±ÉôĀĬ ò. C, P- ũĬĬ p'' ¼ĬĬĀ'' ĀŌō Ĭ¼ĬĬ Ā× Ā'' ÇĀĬĀō (Radius of curvature) ±ÉôĀĬ ò. « Ð ρ ±ýÛð ŞĀĬ, ±øð¼Ĭø ĬĒĬ, ôĀĬ ò. Ā¼ø 2.9 ĀŌŌóÐ Δs=... ΔĒ ±É « ĒĀĬĬø.

$$\therefore \frac{\Delta s}{\Delta t} = \dots \frac{\Delta \ell}{\Delta t}$$

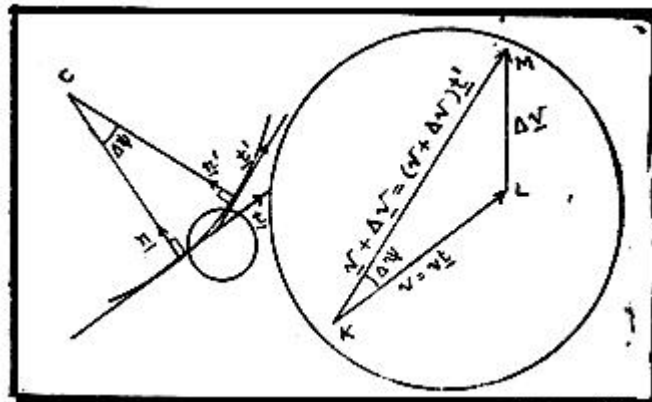
Ð, Çý ŞĂ, ĀĬÉÐ

$$v = \lim_{\Delta t \rightarrow 0} \frac{\Delta s}{\Delta t}$$

$$= \dots \lim_{\Delta t \rightarrow 0} \frac{\Delta \ell}{\Delta t}$$

$$= \dots \frac{d\ell}{dt}$$

$$\underline{v} = v\underline{t} = \dots \frac{d\ell}{dt} \underline{t}$$



Ā¼ø 4-2-9

Ā¼ø (4.2.9)ø Ĭ, ðĒĒÛÇĀĒ Δt ŞĬĀð¼ø ΔV ±ýÛð ¼Ĉ'' °ŞĂ, ð'' ¼ĬĬ ĀĬüĒø P ±ýÛð ðÛÇĬĬø Ĭ°ĀøĀĬ ò V ±ýÛð ¼Ĉ'' °ŞĂ, ð'' ¼ĬĬ "±Ĭ Ā¼øð" ĀĬ ¼ĬĬĬĬøĒ (Increase in the magnitude of the velocity at P) « ¼ý ¼Ĉ'' °ĀĬ ĀĬüĒø¼Ĭø ¼üĀðĬ pŌôĀ¼ø, « Ð Ō ¼Ĉ'' °ĀĬ ĩ ò. ±ÉŞĂ V+ΔV ±ýÛð ¼Ĉ'' °ŞĂ, ð, P' ±ýÛðĀ¼ð¼ø Ā'' ĀĀôĀĬ ò Ĭ¼ĬĬ Ş, ĬĬĬĬ ¼Ĉ'' °ĀĬ Ĭ°ĀøĀĬ ò. ±ÉŞĂ V+ΔV=(v+Δv)t' ĩ ò. pĬĬ ΔV ±ýĀÐ Ð, ũ

$\frac{d\mathbf{v}}{dt} = \mathbf{a} = \frac{d}{dt} \left(\frac{\mathbf{v}}{1 - \frac{v^2}{c^2}} \right)$

$\mathbf{a} = \frac{d\mathbf{v}}{dt} \frac{1 - \frac{v^2}{c^2}}{\left(1 - \frac{v^2}{c^2}\right)^2}$

$$\begin{aligned} \underline{a} &= \frac{d\underline{v}}{dt} \frac{1 - \frac{v^2}{c^2}}{\left(1 - \frac{v^2}{c^2}\right)^2} \\ &= \frac{d\underline{v}}{dt} \frac{(v + \Delta v)t' - vt}{\Delta t} \\ &= \frac{d\underline{v}}{dt} \frac{(v + \Delta v) \cos \Delta \xi t + (v + \Delta v) \sin \Delta \xi n - vt}{\Delta t} \\ &= \frac{d\underline{v}}{dt} \frac{(v + \Delta v)t + (v + \Delta v) \Delta \xi n - vt}{\Delta t} \\ &= \frac{d\underline{v}}{dt} \frac{\Delta v}{\Delta t} t + v \frac{\Delta \xi}{\Delta t} n \\ &= \frac{dv}{dt} t + v \frac{d\xi}{dt} n \\ &= \frac{dv}{dt} t + v \frac{v}{c^2} n \\ &= \frac{dv}{dt} t + \frac{v^2}{c^2} n \end{aligned}$$

\rightarrow $\mathbf{a} = \frac{dv}{dt} \mathbf{t} + \frac{v^2}{c^2} \mathbf{n}$

$\mathbf{a} = \frac{dv}{dt} \mathbf{t} + \frac{v^2}{c^2} \mathbf{n}$

$$\underline{a}_t = \frac{dv}{dt} \underline{t}$$

$$\underline{a}_n = \frac{v^2}{c^2} \underline{n}$$

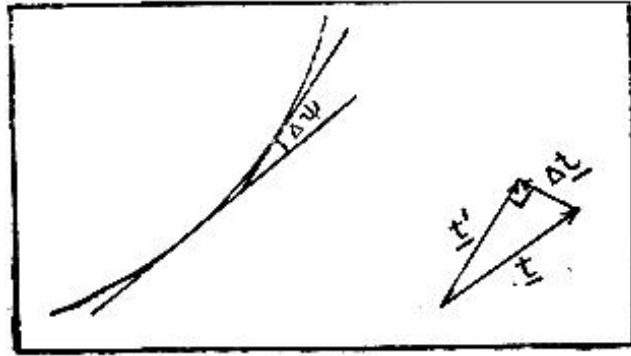
$\mathbf{a} = \frac{dv}{dt} \mathbf{t} + \frac{v^2}{c^2} \mathbf{n}$

$\mathbf{a} = \frac{dv}{dt} \mathbf{t} + \frac{v^2}{c^2} \mathbf{n}$

$$(2) \frac{dv}{dt} \mathbf{t} = \frac{d}{dt} \left(\frac{v}{1 - \frac{v^2}{c^2}} \right) \mathbf{t}$$

$$(3) \frac{v^2}{c^2} \mathbf{n} = \frac{v}{c^2} \frac{dv}{dt} \mathbf{n}$$

$\mathbf{a} = \frac{dv}{dt} \mathbf{t} + \frac{v}{c^2} \frac{dv}{dt} \mathbf{n}$



A¼ō 4-2-11

$$\begin{aligned} \frac{d\underline{t}}{dt} &= \frac{dt}{dE} \cdot \frac{dE}{dt} \\ &= \frac{dE}{dt} \underline{n} \\ &= \frac{v}{\dots} \underline{n} \end{aligned}$$

$$\begin{aligned} \underline{a} &= \left(\frac{dv}{dt} \right) \underline{t} + v \left(\frac{v}{\dots} \right) \underline{n} \\ &= \frac{dv}{dt} \underline{t} + \frac{v^2}{\dots} \underline{n} \end{aligned}$$

(4) \underline{b} ±ý Ūō μÄÄì þŌ· Áî | °í §, i ðî ¼ç· °ÄÄî ÉÐ (Unit binormal) $\underline{t}, \underline{n}$ ūî ì î | °í ì ð¼i, ×ō, « ¼ý §Äî ì $\underline{t}, \underline{n}, \underline{b}$ ±ý Ä· Ä´ Ō ÄÄō ðÈ ì ÈōÄō¼î Ì Ó· È· Ä´ züÄ¼i, ×ō ±î ì, ôÄî ò. « ô| Äî ØÐ $\underline{t}, \underline{n}, \underline{b}$ ±ý Ūō Äü| Èî Ō Ì ð¼· Äô Ō· ÈŌō ç· ¼î ì ò.

(5) $\underline{a}_t, \underline{a}_n$ ±ý ÄÄüÈý |¼î ÄÄý (Ä· Ç×) Óî ì, ò \underline{a} ñ ì ò. \underline{a} ñ ÉÐ, \underline{a}_n ñ ¼ý s ±ý Ūō §, i ½ð· ¼ð ¼î ì Ä¼i, ø \underline{a} ý "±ñ Ä¼ôð", " | °ÄøÄî ò ¼ç· °" ñ, ÄÄü· È.

$$\begin{aligned} a &= \sqrt{\left(\frac{dv}{dt} \right)^2 + \left(\frac{v}{\dots} \right)^2} \\ \tan s &= \frac{\frac{dv}{dt}}{\frac{v}{p}} \end{aligned}$$

±ý Ūō °ÄýÄîî, ù Ä· ÄÄüî, çýÈÈ.

(6) $\vec{v} = \vec{v}_t + \vec{v}_n$ $\vec{a} = \vec{a}_t + \vec{a}_n$ $dE = 0 \rightarrow \vec{v} \perp \vec{a}$

$$\frac{v}{\dots} = \frac{dE}{dt} = 0$$

$\ll \frac{v}{c} \rightarrow \infty \rightarrow \vec{v} \perp \vec{a}$

$$\therefore \underline{a_n} = \frac{v^2}{r} \neq 0 \rightarrow \vec{v} \perp \vec{a}$$

$$\vec{a} = \vec{a}_t + \vec{a}_n$$

$$= \vec{a}_t \rightarrow \vec{v} \perp \vec{a}$$

$\vec{v} \perp \vec{a}$ $\vec{v} = v \hat{e}_t$ $\vec{a} = a_t \hat{e}_t + a_n \hat{e}_n$ $\hat{e}_t \perp \hat{e}_n$ $\vec{v} \cdot \vec{a} = v a_t = 0 \rightarrow a_t = 0$

(6a) $\vec{v} = v \hat{e}_t$ $\vec{a} = a_t \hat{e}_t + a_n \hat{e}_n$ $\hat{e}_t \perp \hat{e}_n$ $\vec{v} \cdot \vec{a} = v a_t = 0 \rightarrow a_t = 0$

$a_x, a_y \pm \dot{y} \hat{e}_t$ $\hat{e}_t = \cos\epsilon \hat{e}_x + \sin\epsilon \hat{e}_y$ $\hat{e}_n = -\sin\epsilon \hat{e}_x + \cos\epsilon \hat{e}_y$ $\tan\epsilon = \frac{dy}{dx}$

$$a_x = a_t \cos\epsilon - a_n \sin\epsilon$$

$$a_y = a_t \sin\epsilon + a_n \cos\epsilon, \quad \tan\epsilon = \frac{dy}{dx}$$

$$a_t = a_x \cos\epsilon + a_y \sin\epsilon$$

$$a_n = a_y \cos\epsilon - a_x \sin\epsilon$$

$\rightarrow \vec{v} \perp \vec{a}$

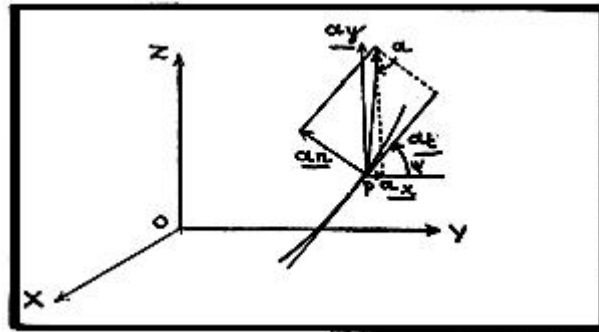


Figure 4-2-12

(7) $\vec{v} = v \hat{e}_t$ $\vec{a} = a_t \hat{e}_t + a_n \hat{e}_n$ $\hat{e}_t \perp \hat{e}_n$ $\vec{v} \cdot \vec{a} = v a_t = 0 \rightarrow a_t = 0$

$\hat{e}_t = \frac{ds}{r} \hat{e}_r$

$$\frac{ds}{dt} = r \frac{d\theta}{dt}$$

$$\underline{r} = 6t^2 \underline{i} - 4t \underline{j} + 3 \underline{k}$$

$$\underline{v} = \frac{d\underline{r}}{dt} = 12t \underline{i} - 4 \underline{j}$$

$$|\underline{v}|_{t=0.25} = 3 \underline{i} - 4 \underline{j}$$

$$|\underline{v}|_{t=0.25} = \sqrt{9+16} = 5 \text{ \AA f/\AA t}$$

$$\underline{t} = \frac{\underline{v}}{|\underline{v}|} = 0.6 \underline{i} - 0.8 \underline{j}$$

$$\underline{a} = \underline{\ddot{r}} = 12 \underline{i}$$

$$\underline{a}_t = \underline{a} \cdot \underline{t} = 12 \underline{i} \cdot (0.6 \underline{i} - 0.8 \underline{j}) = 7.2 \text{ \AA f/\AA t}^2$$

$$\underline{a}_t = 7.2 \underline{t} = 7.2(0.6 \underline{i} - 0.8 \underline{j}) = 4.32 \underline{i} - 5.76 \underline{j}$$

$$\underline{a}_n = \underline{a} - \underline{a}_t = 12 \underline{i} - (4.32 \underline{i} - 5.76 \underline{j}) = 7.68 \underline{i} + 5.76 \underline{j}$$

$$|\underline{a}_n| = \sqrt{(7.68)^2 + (5.76)^2} = 9.8 \text{ \AA f/\AA t}^2$$

$$\dots = \frac{v^2}{|\underline{a}_n|} = \frac{25}{9.8} = 2.6 \text{ \AA t} \cdot \text{\AA f}$$

4.2.12.2 $\underline{r} = 4 \cos 2t \underline{i} + 4 \sin 2t \underline{j} + 6t \underline{k}$ $\pm \underline{y} \text{ Ü ö ç} \text{ } \underline{v}, \underline{t}, \underline{a}_t, \underline{a}_n, \dots$ $\rightarrow \text{ } \underline{a} \text{ } \underline{t} \text{ } \underline{a}_n$

$$\underline{r} = 4 \cos 2t \underline{i} + 4 \sin 2t \underline{j} + 6t \underline{k} \text{ \AA f}$$

$$\underline{\dot{r}} = -8 \sin 2t \underline{i} + 8 \cos 2t \underline{j} + 6 \underline{k} \text{ \AA f/\AA t}$$

$$\underline{\ddot{r}} = -16 \cos 2t \underline{i} - 16 \sin 2t \underline{j} \text{ \AA f/\AA t}^2$$

$$|\underline{v}|_{t=1.57} = -(8 \sin 3.14) \underline{i} + (8 \cos 3.14) \underline{j} + 6 \underline{k} = 8 \underline{j} + 6 \underline{k}$$

$$|\underline{v}|_{t=1.57} = \sqrt{8^2 + 6^2} = 10 \text{ \AA f/\AA t}$$

$$\underline{t} = \frac{\underline{v}}{|\underline{v}|} = 0.8 \underline{j} + 0.6 \underline{k}$$

$$|\underline{a}|_{t=1.57} = |\underline{\ddot{r}}|_{t=1.57} = -16 \underline{i} \text{ \AA f/\AA t}^2$$

$$\underline{a}_t = \underline{a} \cdot \underline{t} = (-16 \underline{i}) \cdot (0.8 \underline{j} + 0.6 \underline{k}) = 0$$

$$\underline{a}_n = \underline{a} - \underline{a}_t = -16 \underline{i} - 0 = -16 \underline{i}$$

$$|\underline{a}_n| = 16 \text{ \AA f/\AA t}^2$$

$$\dots = \frac{v^2}{|\underline{a}_n|} = \frac{100}{16} = 6.25 \text{ \AA t} \cdot \text{\AA f}$$

4.2.12.3 \vec{O} \vec{D} \vec{u} $\mu \vec{A} \vec{A} \vec{O} \vec{o} \vec{D}$ $\vec{D} \vec{A} \vec{i}$ \vec{c} $10 \vec{i}$ $\vec{o} \cdot \vec{A} \vec{E}$ \vec{r} $\vec{A} \vec{O} \vec{u} \vec{C}$ $\vec{A} \vec{o} \vec{1} \vec{o} \vec{3} \vec{4} \vec{o}$
 $\vec{S} \vec{z} \vec{A} \vec{o} \vec{3} \vec{4} \vec{o} \vec{y}$ $\vec{S} \vec{z} \vec{A} \vec{c} \vec{3} \vec{4} \vec{o} \vec{3} \vec{4} \vec{o}$ $\vec{A} \vec{u} \vec{E}$ $\vec{S} \vec{A} \vec{o} \vec{3} \vec{4} \vec{o}$ $\vec{p} \vec{A} \vec{i}$ \vec{l} $\vec{E} \vec{D}$. « \vec{D} $\vec{A} \vec{o} \vec{1} \vec{o} \vec{3} \vec{4} \vec{o}$
 $\vec{O} \vec{O} \vec{E}$ \vec{I} $\vec{u} \vec{E}$ $2 \vec{A} \vec{c} \vec{E} \vec{i} \vec{E}$ \vec{u} $\pm \vec{l}$ $\vec{o} \vec{D} \vec{i}$ \vec{i} $\vec{u} \vec{A} \vec{3} \vec{4} \vec{i} \vec{E} \vec{i} \vec{o}$ $\vec{a} \vec{y} \vec{U} \vec{A} \vec{D}$ $\vec{A} \vec{c} \vec{E} \vec{i} \vec{E} \vec{i}$ \vec{o} $\vec{A} \vec{c} \vec{E} \vec{i}$
« $\vec{o} \vec{D}$ $\vec{C} \vec{O} \vec{y}$ $\vec{i} \vec{3} \vec{4} \vec{i} \vec{A} \vec{A}$ $\vec{O} \vec{i} \vec{i} \vec{o}$, $\vec{A} \vec{A} \vec{o}$ $\vec{S} \vec{z} \vec{i} \vec{A}$ $\vec{O} \vec{i} \vec{i} \vec{o}$, \vec{r} $\vec{A} \vec{A} \vec{u} \vec{E} \vec{y}$
 $\pm \vec{n}$ $\vec{A} \vec{3} \vec{4} \vec{o} \vec{o} \vec{i}$ $\vec{c} \vec{i}$ $\vec{j} \vec{n}$.

$$v = kt$$

$$\underline{v} = kt \underline{I}, \underline{I} \pm \underline{y} \vec{A} \vec{D} \vec{i} \vec{3} \vec{4} \vec{i} \vec{A} \vec{A} \vec{o} \vec{3} \vec{4} \vec{o} \vec{r} \vec{A} \vec{A} \vec{A} \vec{U} \vec{i} \vec{l} \vec{o} \mu \vec{A} \vec{A} \vec{l} \vec{o} \vec{3} \vec{4} \vec{o} \vec{r} \vec{A} \vec{A} \vec{i} \vec{l} \vec{o}.$$

$$a_t = \frac{dv}{dt} = k$$

$$s = \int ktdt = \frac{k}{2}t^2 + c, t=0 \pm \underline{y} \vec{U} \vec{u} \vec{C} \vec{S} \vec{A} \vec{i} \vec{D}, s=0. \therefore c=0 \pm \vec{E} \vec{S} \vec{A} s = \frac{k}{2}t^2$$

$$\vec{S} \vec{z} \vec{A} \vec{o} 2 \vec{A} \vec{c} \vec{E} \vec{i} \vec{E} \vec{A} \vec{i} \vec{s} \vec{r} \vec{u} \vec{C} \vec{S} \vec{A} \vec{i} \vec{D} s - 2f \times 10 = \frac{k}{2} \times 4$$

$$\therefore k = 10f$$

$$\therefore v = 10ft \vec{i} \vec{o} \cdot \vec{A} \vec{E} / \vec{A} \vec{c}$$

$$\therefore a_t = k = 10f = 31.4 \vec{i} \vec{o} \cdot \vec{A} \vec{E} / \vec{A} \vec{c}^2 = 0.314 \vec{A} \vec{E} / \vec{A} \vec{c}^2.$$

$$|a_n| = \frac{v^2}{r} = \frac{100f^2 \times 4}{10} = 40f^2 = 0.887 \vec{A} \vec{E} / \vec{A} \vec{c}^2.$$

4.2.12.4 \vec{O} $\vec{A} \vec{n} \vec{E}$ $\vec{r} \vec{y} \vec{U}$ $\vec{A} \vec{C} \times \vec{o} \vec{A} \vec{i} \vec{3} \vec{4} \vec{A} \vec{o}$ $\vec{A} \vec{C} \vec{A} \vec{A} \vec{A}$ $1000 \vec{A} \vec{E}$ $\vec{r} \vec{u} \vec{C}$
 $\vec{p} \vec{1} \vec{o} \vec{3} \vec{4} \vec{o} \vec{A} \vec{1} \vec{2} \vec{c} \vec{i} \vec{l}$ $144 \vec{c} \cdot \vec{A} \vec{E} \vec{S} \vec{A} \vec{o} \vec{3} \vec{4} \vec{o} \vec{i} \vec{o} \vec{y} \vec{U} \vec{i} \vec{j} \vec{n}$ $\vec{E} \vec{O} \vec{i} \vec{l} \vec{o}$ $\vec{S} \vec{z} \vec{A} \vec{o} \vec{3} \vec{4} \vec{o}$, $\vec{3} \vec{4} \vec{E} \vec{i} \vec{A} \vec{E}$
 $\vec{A} \vec{c} \vec{S} \vec{A} \vec{i} \vec{l}$ \vec{u} $\vec{S} \vec{A} \vec{i} \vec{1} \vec{o} \vec{A} \vec{o} \vec{l}$ \vec{O} $\vec{A} \vec{n} \vec{E} \vec{A} \vec{i} \vec{E} \vec{D}$ $\vec{A} \vec{i} \vec{E} \vec{A} \vec{3} \vec{4} \vec{o} \vec{3} \vec{4} \vec{o}$ $\vec{A} \vec{o} \vec{A}$ $\vec{p} \vec{A} \vec{i} \vec{l}$ $\vec{E} \vec{D}$. 6
 $\vec{A} \vec{c} \vec{E} \vec{i} \vec{E} \vec{U} \vec{i} \vec{l} \vec{o}$ $\vec{A} \vec{c} \vec{E} \vec{i}$ \vec{O} $\vec{A} \vec{n} \vec{E} \vec{A} \vec{y}$ $\vec{S} \vec{A} \vec{A} \vec{i} \vec{E} \vec{D}$, $\vec{A} \vec{1} \vec{2} \vec{c} \vec{i} \vec{l}$ $96 \vec{c} \cdot \vec{A} \vec{E}$ $\vec{r} \vec{i}$
 \vec{l} $\vec{E} \vec{o} \vec{3} \vec{4} \vec{i} \vec{o}$ $\vec{A} \vec{c} \vec{S} \vec{A} \vec{i} \vec{l}$ \vec{u} $\vec{S} \vec{A} \vec{i} \vec{1} \vec{o} \vec{A} \vec{o} \vec{l}$ $\vec{3} \vec{4} \vec{O} \vec{1} \vec{2} \vec{o} \vec{3} \vec{4} \vec{o}$ \vec{O} $\vec{A} \vec{n} \vec{E} \vec{A} \vec{y}$ $\vec{O} \vec{i} \vec{i} \vec{o}$ $\vec{3} \vec{4} \vec{i}$
 $\vec{j} \vec{n}$.

$\vec{S} \vec{A} \vec{o} \vec{A} \vec{1} \vec{2} \vec{c} \vec{i} \vec{l}$ $144 \vec{c} \cdot \vec{A} \vec{E} \pm \vec{E} \vec{o}$ $\vec{A} \vec{c} \vec{E} \vec{i} \vec{E} \vec{i} \vec{l}$ $\vec{S} \vec{A} \vec{o} 40 \vec{A} \vec{E} \vec{r} \vec{i} \vec{o}$. « $\vec{D} \vec{S} \vec{A} \vec{i} \vec{A} \vec{S} \vec{A}$
 $\vec{S} \vec{A} \vec{o} \vec{A} \vec{1} \vec{2} \vec{c} \vec{i} \vec{l}$ $96 \vec{c} \cdot \vec{A} \vec{E} \pm \vec{E} \vec{o}$ $\vec{A} \vec{c} \vec{E} \vec{i} \vec{E} \vec{i} \vec{l}$ $80/3 \vec{A} \vec{E} \vec{r} \vec{i} \vec{o}$. \vec{O} $\vec{A} \vec{n} \vec{E}$ $\vec{r} \vec{A} \vec{i} \vec{E}$
 $\vec{A} \vec{3} \vec{4} \vec{o} \vec{3} \vec{4} \vec{o}$ (constant rate) $\vec{A} \vec{o} \vec{A} \vec{i}$ $\vec{i} \vec{o} \vec{A} \vec{3} \vec{4} \vec{i} \vec{o}$

$$a_t = \vec{r} \vec{A} \vec{i} \vec{o} \vec{i} \vec{c} \vec{O} \vec{i} \vec{i} \vec{o} = \frac{\Delta v}{\Delta t} = \frac{\frac{80}{3} - 40}{6} = -2.2 \vec{A} \vec{E} / \vec{A} \vec{c}^2$$

$$a_n = \frac{v^2}{r} = \frac{40 \times 40}{1000} = 1.6 \vec{A} \vec{E} / \vec{A} \vec{c}^2$$

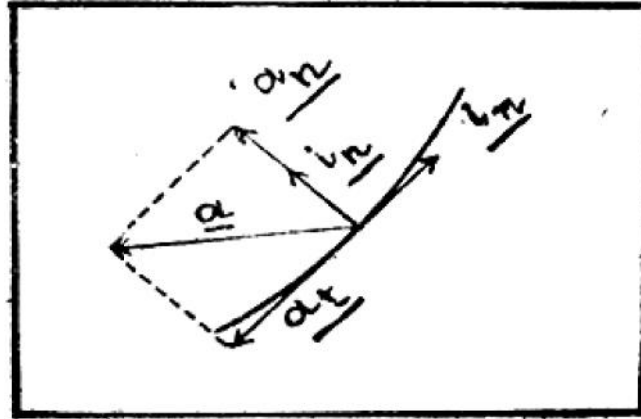


Fig. 4-2-13

Fig. 4.2.13 shows the decomposition of the acceleration vector a into normal and tangential components a_n and a_t . The angle between the acceleration vector and the normal component is s . The normal component is perpendicular to the path, and the tangential component is parallel to the path.

$$\tan s = \frac{a_t}{a_n} = \frac{2.2}{1.6} = 1.375$$

Therefore $s = 53^\circ 58'$.

$$a = \frac{a_n}{\cos s} = \frac{1.6}{\cos 53^\circ 58'} = \frac{1.6}{0.5901} = 2.71 \text{ m/s}^2$$

Therefore, the acceleration is 2.71 m/s^2 . The angle between the acceleration vector and the normal component is $53^\circ 58'$.

4.2.12.5 The car starts from rest and accelerates uniformly. The distance traveled is 108 m . The acceleration is 3 m/s^2 .

$$v^2 = \frac{2as}{1} = \frac{2 \times 3 \times 108}{1} = 648$$

4.2.12.6 The car starts from rest and accelerates uniformly. The distance traveled is 200 m . The acceleration is 2 m/s^2 .

$$v = \frac{2as}{1} = \frac{2 \times 2 \times 200}{1} = 80 \text{ m/s}$$

$$a_n = \frac{v^2}{r} = \frac{80^2}{200} = 32 \text{ m/s}^2$$

$$\frac{ds}{dt} = v; \frac{d^2s}{dt^2} = \frac{dv}{dt} = f \quad \text{--- } \text{! } \text{õ.}$$

þí ì $\frac{dv}{dt} = f \pm \text{ý } \hat{A} \cdot \frac{1}{4} | \frac{1}{4} \cdot \text{ü } \hat{A} \hat{C} \text{õ } \hat{S} \hat{A}_j \text{Ð}$

$$\int_{v_0}^v dv = \int_0^t f dt$$

$$v - v_0 = f \int_0^t dt = ft$$

« ðÄÐ $v = v_0 + ft \quad \text{--- } \text{! } \text{õ.}$

« ùÁ_j Æ $\frac{ds}{dt} = v = v_0 + ft \pm \text{ý } \hat{A} \cdot \frac{1}{4} | \frac{1}{4} \cdot \text{ü } \hat{A} \hat{C} \text{õ } \hat{S} \hat{A}_j \text{Ð}$

$$\int_0^s ds = \int_0^t (v_0 + ft) dt$$

$$s = v_0 t + \frac{1}{2} ft^2 \quad \text{--- } \text{! } \text{õ.}$$

ŠÄÖõ $\frac{v dv}{ds} = f \pm \text{ý } \hat{A} \cdot \frac{1}{4} \cdot \text{ü } \hat{A} \hat{C} \text{õ } \hat{S} \hat{A}_j \text{Ð}$

$$\int_{v_0}^v v dv = \int_0^s f ds$$

$$\frac{v^2}{2} = \frac{v_0^2}{2} = fs \pm \text{ý } \hat{U} \text{õ } \hat{A} \hat{C} \text{õ } \hat{S} \hat{A}_j \text{Ð,}$$

$$v^2 = v_0^2 + 2fs$$

þõã ý Úõ Æ_ç_÷ Æ_ç_÷ ðÉÄÄÄÍ ì ð Ð_ç_ý þÄì ÄÄø °Áý Ä_î_î_ç_ì_õ.
 þÄì ì ð Ð_ç_ù t=0 ±ý Ûõ Æ_ç_Äð¼ø ì õÄÄÖõð ðÈøÄð¼_ø þí °Áý Ä_î_î_ç_ì_õ
 Ó· ÈŠÄ $v = ft, s = \frac{1}{2} ft^2, v^2 = 2fs \pm \text{ý } \hat{E}_j \text{! } \text{õ.}$

4.2.13.2 $\frac{1}{4}$ É_j ŠÄ ðÄç_· Ä Æ_ç_ì_ì ç Äøõ | Ä_ì Ö_ù_ç_ý Óî ì_õ (Acceleration of freely falling bodies towards the earth)

Ó_ì | Ä_ì Ö_ç_í_É_ð | Ä_ù_È¼ð¼ø ðÄç_· Ä Æ_ç_ì_ì ç Äøõ Ä_î_î_ç_ì_õ « Ð
 ðÄç_ý ì¼ð¼ø ±ð Ä_ì Ö_ðõ_·_ŠÄ « Ç×ùÇ¼_É_·_Ö_Óî_ì_ð¼_ý
 þÄì_î_î_ç_ì_õ Ä_ì Ö_ç_·¼_É_ç_ý Ä_î_î_ç_ì_õ « ÈÄÖ_È_Ç_È. þ_ù_Ä¼_Óî_ì_õ
 « ò| Ä_ì Ö_·_Ç_ø_ðÄç_í_É_ð_¼_ý_·_Ä_ò_¼_Æ_ç_ì_ì_ç_ø_÷_ðÄ¼_ø_²_ü_Ä_î_î_ç_ì_õ, ±É_ŠÄ
 þ_ð_ðÄç_è_ð_Ä_ç_·_Ä_ì_ø_²_ü_Ä_î_î_ç_ì_õ Óî_ì_õ (Acceleration due to gravity)
 ±É_ì_Ü_È_Ä_î_î_ç_ì_õ. þ_ù_Ä¼_Óî_ì_õ "g" ±ý Ûõ ±ð¼_ø_ì_È_ù_ò_Ä_î_î_ç_ì_õ.

g Ä_ý Ä_ö_ö_Ó_î_È_ò_¼_þ¼ð¼ø ±ð Ä_ì Ö_ü_î_î_ç_ì_õ_·_ŠÄ « Ç×ùÇ¼_j_þ_Ö_ì_Ç_È.
 --- È_j_ø « $\frac{1}{4}$ ý Ä_ö_ö_ð_ðÄç_ý_ŠÄ_ü_Ä_ò_¼_þ¼ð¼ø_¼_ø_°_È_Ç_« ÇÄ_ø_Ä_ì_Ü_Ä_î_î_ç_ì_õ. ðÄç_ç_î_î_ç_ì_õ (Equator) ì_ì « Ö_ø « $\frac{1}{4}$ ý Ä_ö_ö_Ä_ç_ì_ì_·_È_Ä_ì_×_ø_ð_Ö_Ä_î_î_ç_ì_õ
 (poles) « Ö_Š_Ä_ç_ç_¼_Ä_ì_×_ø_þ_Ö_ì_Ç_È.

$\dot{v} = g$ $\dot{v} = 9.81 \text{ m/s}^2$ "C.G.S." $\dot{v} = 981 \text{ cm/s}^2$ $\pm y \dot{U} \dot{o}$
 "M.K.S." $\dot{v} = 9.81 \text{ m/s}^2$ $\pm y \dot{U} \dot{o}$ $\dot{v} = 32.2 \text{ ft/s}^2$ "F.P.S." $\dot{v} = 32.2 \text{ ft/s}^2$ / $\dot{v} = 32.2 \text{ ft/s}^2$ $\pm y \dot{U} \dot{o}$ $\dot{v} = 32.2 \text{ ft/s}^2$ $\pm y \dot{U} \dot{o}$

4.2.13.3 $\dot{v} = g$ (vertical motion under gravity)

$\dot{v} = v_0 - gt$
 $s = v_0 t - \frac{1}{2} gt^2$
 $v^2 = v_0^2 - 2gs$

$v = v_0 - gt$
 $s = v_0 t - \frac{1}{2} gt^2$
 $v^2 = v_0^2 - 2gs$

$\pm y \dot{E} \dot{i} \dot{l} \dot{o}$.

$\dot{v} = g$ $\dot{v} = 9.81 \text{ m/s}^2$ $\dot{v} = 981 \text{ cm/s}^2$ $\dot{v} = 32.2 \text{ ft/s}^2$ $\dot{v} = 32.2 \text{ ft/s}^2$ / $\dot{v} = 32.2 \text{ ft/s}^2$ $\pm y \dot{U} \dot{o}$

$v = gt$

$s = \frac{1}{2} gt^2$

$v^2 = 2gs$ $\pm y \dot{E} \dot{i} \dot{l} \dot{o}$.

4.2.13.4 $\dot{v} = -g$ (vertical motion against gravity)

$\dot{v} = v_0 - gt$
 $s = v_0 t - \frac{1}{2} gt^2$
 $v^2 = v_0^2 - 2gs$

$v = v_0 - gt$

$s = v_0 t - \frac{1}{2} gt^2$

$v^2 = v_0^2 - 2gs$

$\pm y \dot{U} \dot{o}$ $\dot{v} = g$ $\dot{v} = 9.81 \text{ m/s}^2$ $\dot{v} = 981 \text{ cm/s}^2$ $\dot{v} = 32.2 \text{ ft/s}^2$ $\dot{v} = 32.2 \text{ ft/s}^2$ / $\dot{v} = 32.2 \text{ ft/s}^2$ $\pm y \dot{U} \dot{o}$

$\dot{v} = g$ $\dot{v} = 9.81 \text{ m/s}^2$ $\dot{v} = 981 \text{ cm/s}^2$ $\dot{v} = 32.2 \text{ ft/s}^2$ $\dot{v} = 32.2 \text{ ft/s}^2$ / $\dot{v} = 32.2 \text{ ft/s}^2$ $\pm y \dot{U} \dot{o}$

$\dot{v} = g$ $\dot{v} = 9.81 \text{ m/s}^2$ $\dot{v} = 981 \text{ cm/s}^2$ $\dot{v} = 32.2 \text{ ft/s}^2$ $\dot{v} = 32.2 \text{ ft/s}^2$ / $\dot{v} = 32.2 \text{ ft/s}^2$ $\pm y \dot{U} \dot{o}$

$\dot{v} = g$ $\dot{v} = 9.81 \text{ m/s}^2$ $\dot{v} = 981 \text{ cm/s}^2$ $\dot{v} = 32.2 \text{ ft/s}^2$ $\dot{v} = 32.2 \text{ ft/s}^2$ / $\dot{v} = 32.2 \text{ ft/s}^2$ $\pm y \dot{U} \dot{o}$

Úsžjì ċ pĀí ĩ ōšĀjĐ « ù×ĀĀò'' ¼ « '' ¼Ā ±Ī òĐì ĩ ĩ ĩ ¼ šĵĀò'' ¼Ōō ¼Ōō ĩ ĩ ĩ ĩ.

šĀøšĵjì ċ ±Ēō¼ ĩ ĀjŌĶjĒĐ ĀĶ - Ā÷ó¼ òŪĶĶ'' Ā ±òĐōšĀjĐ ÓĒ× šĀō āĭ°ĀĀjĭ ō ±ýĀ¼jø « Đ ĩ°ýĒ ĀĶōĩĀĶ ĩ°ĭ ĩ òĐòĩ¼ĭ'' Ā× $\frac{v_0^2}{2g}$ ĩ ĩ.

4.2.14 Āj¼ĶĶ ĩ ½ĭ ĩ ĩ ū

4.2.14.1 Ō šĵ÷šĵjđĒĒĀĀĭ ĩ ō Đĵ ū ĩýŪ t ĀĒĶjĒĀø 0 ±ýŪō ĐĀĭ ōòŪĶĀĀŌóĐ $s = t^3 - 6t^2 + 15t + 40$ ±ýŪō ĩ¼ĭ'' Ā'' ĀōĩĀŪŪĶ¼ĭ Ķ (a) « ¼ýšĀō ±óšĵĀĭ Ķø āĭ°ĀĀjĭ ō, (b) 5 ĀĒĶjĒĀø Ķø ¼ó¼ ĩ¼ĭ'' Ā× (c) $t=5$ ĀĒĶjĒĀĭ - ŪĶšĀjĐ « ¼ý Ōĭ ĩ ō ĩ ĩĀŪ'' Ēĭ ĩ ĩ.

$$\text{pĭ ĩ } s = t^3 - 6t^2 + 15t + 40 \{ [10^{-2}] \text{ĀĶ} \}$$

$$s = \frac{ds}{dt} = 3t^2 - 12t + 15 \{ [10^{-2}] \text{ĀĶ} \}$$

$$a = \frac{d^2s}{dt^2} = 6t - 12 \{ [10^{-2}] \text{ĀĶ} \}$$

$$v=0 \pmýĒŌĭ ĩ$$

$$3t^2 - 12t + 15 = 0 \text{ ĩ ĩ ō}$$

$$t = -1 \ll \text{øĀĐ } t=5 \text{ ĀĶ } \pmýŪŪĶšĀjĐ \text{ šĀō } \text{āĭ}^\circ \text{ĀĀjĭ } \text{ō},$$

$$s_5 = |s|_{t=5} = 125 - 6 \times 25 + 15 \times 5 + 40 = -60 \{ [10^{-2}] \text{ĀĶ} \}$$

$$s_0 = |s|_{t=0} = 40 \{ [10^{-2}] \text{ĀĶ} \}$$

±ĒšĀ 5 ĀĒĶjĒĀø Ķø ĩ°ýĒ ĩ¼ĭ'' Ā×

$$s_5 = s_0 = -100 \text{ ĩ}^\circ \text{ĀĶ ĩ ĩ ō}$$

$$|a|_{t=5} = 6 \times 5 - 12 = 18 \{ [10^{-2}] \text{ĀĶ} / \text{ĀĶ} \}$$

4.2.14.2 Ō Đĵ ū x « ĭ°ø $v = \frac{x^2}{2}$ ±ýŪō šĀō¼ø pĀĭ ĩ ĩĒĐ. šĵĀō $t=0$ ĀĒĶjĒĀø ±ýŪŪĶšĀjĐ « Đ $x=1$ ĀĶ ±ýŪĀ¼ò¼ŌŪĶĐ. « Đ $x=2000$ ĀĶĀĶ ±ýŪĀ¼ò¼ø'' ¼ « '' ¼Ā ±Ī òĐì ĩ ĩ ūŪ ō šĵĀò'' ¼Ōō « ùĀ¼ò¼ø « ¼ý Ōĭ ĩ ō'' ¼Ōō ĩ ĩ.

$$\frac{dx}{dt} = v = \frac{x^2}{2}$$

$$\int_0^t dt \Rightarrow \int_t^2 \frac{2}{x^2} dx$$

$$t = 2 \left(\frac{-1}{x} \right) = 1 \text{ĀĶ}$$

$$\begin{aligned}
 a &= \frac{v dv}{dx} \\
 &= \frac{x^2}{2} \times x = \frac{x^3}{2} \\
 a|_{x=2} &= \frac{8}{2} = 4 \text{ Áf/Á}^2
 \end{aligned}$$

4.2.14.3 \hat{O} \hat{u} $x \ll \hat{c}$ $v = 0.6x + 0.9$ \hat{c} / \hat{c} $\pm \hat{y} \hat{u} \hat{o}$ $\hat{c} \hat{A} \hat{i} \hat{o} \hat{A} \hat{o} \hat{i}$
 $\hat{p} \hat{A} \hat{i} \hat{i}$ $\hat{c} \hat{e} \hat{D}$. « \hat{D} $\hat{i} \hat{A} \hat{i} \hat{A} \hat{i} \hat{o} \hat{D} \hat{u} \hat{c} \hat{A} \hat{y}$ $\hat{A} \hat{e} \hat{c} \hat{A} \hat{p} \hat{A} \hat{i} \hat{i} \hat{o} \hat{S} \hat{A} \hat{i} \hat{D}$ « $\hat{A} \hat{y}$ $\hat{O} \hat{i} \hat{i} \hat{o}$
 $\hat{A} \hat{i} \hat{D}$? $\hat{i} \hat{A} \hat{i} \hat{A} \hat{i} \hat{o} \hat{D} \hat{u} \hat{c} \hat{A} \hat{o} \hat{D}$ $x = 4.05$ \hat{c} . $\pm \hat{y} \hat{E}$ $\hat{i} \hat{A} \hat{i}$ $\hat{A} \hat{A} \hat{A}$ $\hat{A} \hat{o} \hat{o}$ $\hat{D} \hat{u} \hat{c} \hat{A} \hat{i} \hat{i}$
 $\hat{i} \hat{o} \hat{A}$, « $\hat{D} \hat{\pm} \hat{i} \hat{o} \hat{D} \hat{i} \hat{i} \hat{u} \hat{u} \hat{o}$ $\hat{S} \hat{z} \hat{A} \hat{o} \hat{A} \hat{i} \hat{D}$?
 $\hat{p} \hat{i} \hat{i}$

$$\begin{aligned}
 v &= 0.6x + 0.9 \text{ Áf/Á} \\
 a &= \frac{v dv}{dx} = (0.6x + 0.9)(0.6) \\
 &= 0.36x + 0.54 \\
 a|_{x=0} &= 0.54 \text{ Áf/Á}^2
 \end{aligned}$$

$\hat{c} \hat{i} \hat{o}$.

$\hat{S} \hat{A} \hat{o} \hat{o}$

$$\begin{aligned}
 \frac{dx}{dt} &= v = 0.6x + 0.9 \\
 \therefore \int_0^t dt &= \int_0^{4.05} \frac{dx}{0.6 + 0.9} \\
 t &= \frac{1}{0.6} [\log_e (0.6x + 0.9)]_0^{4.05} \\
 &= \frac{5}{3} \log_e \left(\frac{11}{3} \right) \hat{c} \hat{i}
 \end{aligned}$$

4.2.14.4 $\hat{A} \hat{c} \hat{A} \hat{n}$ $\hat{A} \hat{o} \hat{A} \hat{y}$ $\hat{A} \hat{e} \hat{c} \hat{A}$ $\hat{A} \hat{o} \hat{o}$ $\hat{D} \hat{u}$, $a = g(1 - k^2 v^2)$ $\pm \hat{y} \hat{u} \hat{o}$
 $\hat{O} \hat{i} \hat{i} \hat{o}$ $\hat{A} \hat{u} \hat{u} \hat{c} \hat{D}$. $t = 0$ $\pm \hat{y} \hat{u} \hat{o}$ $\hat{S} \hat{z} \hat{A} \hat{o} \hat{A} \hat{o} \hat{s} = 0$ $\pm \hat{y} \hat{u} \hat{c}$ $\hat{p} \hat{A} \hat{o} \hat{A} \hat{o}$,
 $\hat{D} \hat{u}$ $\hat{m} \hat{o} \hat{A} \hat{A} \hat{o} \hat{o} \hat{D}$ $\hat{p} \hat{A} \hat{i} \hat{i} \hat{A} \hat{i} \hat{c}$

(i) t $\hat{S} \hat{z} \hat{A} \hat{o} \hat{A} \hat{i} \hat{o} \hat{A} \hat{e} \hat{i}$ « $\hat{A} \hat{y}$ $\hat{S} \hat{A} \hat{o}$

$$v = \frac{1}{k} \tanh \left(\frac{gt}{k} \right) \pm \hat{y} \hat{u} \hat{o}$$

(ii) $\hat{D} \hat{u}$ \hat{s} $\hat{i} \hat{A} \hat{i}$ $\hat{A} \hat{A} \hat{o} \hat{u} \hat{c} \hat{S} \hat{A} \hat{i} \hat{D}$ $\hat{s} \hat{i} \hat{i} \hat{o}$, $\hat{v} \hat{i} \hat{i} \hat{o} \hat{c} \hat{E} \times$

$$v^2 = \frac{1}{k^2} (1 - e^{-2k^2 g s}) \pm \hat{y} \hat{u} \hat{o} \hat{c} \hat{u} \times$$

$$\frac{1}{k} \lim_{t \rightarrow 0} \ddot{A} \left\{ \frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right\}$$

$$= \frac{1}{k} \times 1$$

$$= \frac{1}{k}$$

4.2.14.5 $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$ $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$ $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$

$$a = -\frac{gR^2}{r^2}, \text{ } \ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$$

4.2.15. $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$ $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$ $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$

$$\frac{v dv}{dr} = a = -\frac{gR^2}{r^2}$$

$$\int_{v_0}^0 v dv = -gR^2 \int_R^\infty \frac{dr}{r^2}$$

$$\frac{-v_0^2}{2} = gR^2 \left[\frac{1}{r} \right]_R^\infty$$

$$v_0^2 = 2gR$$

$$v_0 = \sqrt{2gR}$$

4.2.15. $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$

4.2.15.1 $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$ $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$ $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$

$\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$ $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$ $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$

$$\left(\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right) \right)$$

4.2.15.2 $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$ $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$ $\ddot{A} = \frac{g}{k} \left(\frac{1 - e^{-2kgt}}{1 + e^{-2kgt}} \right)$

$$\ddot{A} = \frac{1}{2} \log_e \left(\frac{5}{2} \right) \ddot{A}$$

4.2.15.8 $x \ll \hat{i}^\circ \varnothing \quad | \frac{3}{4}; \frac{1}{4} \hat{i} \varnothing \circ \hat{o} \hat{u} \hat{c} \hat{A} \varnothing \quad \mu \hat{o} \hat{A} \hat{A} \hat{O} \hat{o} \hat{D} \quad \rho \hat{A} \hat{i} \hat{l} \hat{o} \quad \hat{D} \varnothing \hat{c} \hat{y}$
 $\hat{O} \hat{i} \hat{l} \varnothing \hat{A} \hat{i} \hat{E} \hat{D} \quad a = \left(10 - \frac{1}{3} x \right) \hat{A} \hat{V} \hat{A} \hat{c}^2 \pm \hat{y} \hat{U} \hat{o} \hat{o} \hat{A} \hat{y} \hat{A} \hat{i} \hat{o} \frac{1}{4} \hat{i} \varnothing \hat{A} \hat{A} \hat{U} \hat{i} \varnothing \hat{A} \hat{i} \varnothing \hat{E} \hat{D}.$

- (i) $\hat{S} \hat{A} \hat{o} \hat{A} \hat{c} \hat{E} \hat{i} \hat{E} \hat{i} \hat{l} \quad 15 \hat{A} \hat{f} \hat{m} \hat{s}^{-1} \hat{u} \hat{c} \hat{S} \hat{A} \hat{i} \hat{D} \hat{D} \quad \hat{u} \pm \hat{l} \hat{o} \hat{D} \hat{i} \quad | \quad \hat{i} \hat{n} \quad \frac{1}{4} \hat{S} \hat{A} \hat{o} \hat{A} \hat{i} \hat{D}?$
- (ii) $1 \hat{A} \hat{c} \hat{E} \hat{i} \hat{E} \hat{i} \hat{l} \quad \hat{o} \hat{A} \hat{c} \hat{E} \hat{i} \hat{D} \hat{u} \quad | \quad \frac{3}{4}; \frac{1}{4} \hat{i} \varnothing \circ \hat{o} \hat{u} \hat{c} \hat{A} \hat{A} \hat{O} \hat{o} \hat{D} \quad \pm \hat{o} \frac{3}{4} \hat{o} \quad | \quad \frac{3}{4} \hat{i} \varnothing \hat{A} \hat{A} \hat{A} \hat{O} \hat{i} \hat{l} \quad \hat{o}?$
 $(\hat{A} \hat{c} \hat{i} \varnothing \frac{1}{4} \quad (i) \quad 3 \log_e^2 \hat{A} \hat{c} \quad (ii) \quad 12.99 \hat{A} \hat{f})$

4.2.16. $\hat{A} \hat{A} \hat{u}^\circ \hat{c}$

4.2.16.1 $\hat{D} \varnothing \hat{c} \hat{y} \quad \hat{S} \hat{A} \hat{o} \quad (v = 20t^2 - 100t + 50) \quad (\hat{A} \hat{D} \frac{1}{4} \hat{i} \varnothing) \quad \pm \hat{y} \hat{E} \hat{i} \varnothing, \quad (t - \hat{A} \hat{c} \hat{E} \hat{i} \hat{E} \hat{A} \varnothing)$
 $\hat{O} \hat{i} \hat{l} \varnothing \hat{o} \hat{a} \hat{i}^\circ \hat{A} \hat{A} \hat{i} \hat{l} \varnothing \quad \frac{3}{4} \hat{O} \frac{1}{2} \hat{o} \frac{3}{4} \varnothing, \quad \hat{S} \hat{A} \hat{o} \hat{o} \quad \frac{3}{4} \hat{A} \frac{3}{4} \hat{o} \hat{A} \hat{c} \hat{i} \varnothing. \quad (\hat{A} \hat{c} \hat{i} \varnothing \frac{1}{4} \quad V = -75 \text{m/s})$

4.2.16.2 $s \ll \hat{i}^\circ \varnothing \quad \rho \hat{A} \hat{i} \hat{l} \hat{o} \quad \hat{D} \hat{u} \quad \hat{y} \hat{E} \hat{y} \quad \frac{3}{4} \hat{c} \varnothing \quad \hat{S} \hat{A} \hat{o} \quad v = 2 + 5t^{3/2} \quad (s \quad \hat{A} \hat{D} \frac{1}{4} \hat{i} \varnothing, \quad t \quad \hat{A} \hat{c} \hat{E} \hat{i} \hat{E} \hat{A} \varnothing)$
 $t = 4 \quad \hat{A} \hat{c} \hat{E} \hat{i} \hat{E} \hat{m} \hat{s}^{-1} \hat{u} \hat{c} \hat{S} \hat{A} \hat{i} \hat{D}, \quad \rho \frac{1}{4} \hat{o} \quad | \quad \hat{A} \hat{A} \hat{i} \hat{o} \hat{c}, \quad \frac{3}{4} \hat{c} \varnothing \quad \hat{S} \hat{A} \hat{o} \quad \hat{A} \hat{u} \hat{U} \hat{o}$
 $\hat{O} \hat{i} \hat{l} \varnothing \hat{o} \quad - \quad \hat{u} \hat{A} \hat{u} \hat{i} \hat{E} \hat{i} \hat{l} \varnothing \hat{i} \hat{n} \varnothing \quad (\hat{A} \hat{c} \hat{i} \varnothing \frac{1}{4}: s = 72 \text{m}; V = 42 \text{m/s}; G = 15 \text{m/s}^2)$

4.2.16.3 $80 \hat{c} \hat{A} \hat{V} \hat{A} \frac{1}{2} \hat{c} \hat{A} \hat{o} \hat{D} \quad | \quad \hat{i} \hat{n} \quad \hat{E} \hat{O} \hat{i} \hat{l} \varnothing \quad \hat{S} \hat{A} \hat{i} \hat{o} \frac{1}{4} \hat{i} \hat{o} \hat{A} \hat{n} \hat{E} \quad 30 \hat{A} \hat{f} \quad | \quad \frac{3}{4} \hat{i} \varnothing \hat{A} \hat{A} \varnothing$
 $\hat{c} \hat{y} \hat{U} \quad \hat{A} \hat{c} \hat{i} \varnothing \hat{E} \hat{D} \quad \ll \quad \hat{S} \frac{3}{4} \quad \hat{A} \hat{i} \hat{E} \hat{i} \frac{3}{4} \quad \hat{O} \hat{i} \hat{l} \varnothing \hat{o} \frac{3}{4} \varnothing \quad \hat{S} \hat{A} \hat{i} \hat{o} \frac{1}{4} \hat{o} \hat{A} \hat{n} \hat{E} \hat{A} \hat{y} \quad \hat{S} \hat{A} \hat{o}$
 $120 \hat{c} \hat{A} \hat{V} \hat{A} \frac{1}{2} \hat{c} \pm \hat{y} \hat{E} \hat{i} \varnothing, \quad \hat{S} \hat{A} \hat{i} \hat{o} \frac{1}{4} \hat{o} \hat{A} \hat{n} \hat{E} \quad \hat{c} \hat{u} \hat{A} \frac{3}{4} \hat{u} \hat{l} \quad \hat{O} \hat{y}, \quad | \quad \frac{3}{4} \hat{i} \varnothing \hat{A} \times \varnothing \frac{1}{4} \hat{o} \frac{3}{4} \hat{D} \pm \hat{y} \hat{E}$
 $\pm \hat{y} \hat{U} \quad \hat{i} \hat{n} \varnothing \quad (\hat{A} \hat{c} \hat{i} \varnothing \frac{1}{4} \quad s = 67.5 \hat{A} \hat{f})$

4.2.16.4 $\hat{D} \hat{u} \quad \hat{y} \hat{U} \quad \hat{A} \hat{c} \times \hat{o} \hat{A} \hat{i} \varnothing \quad \frac{3}{4} \hat{A} \varnothing \quad | \quad \hat{o} \hat{A} \hat{c} \quad \frac{3}{4} \quad V_x = (50 - 16t) \hat{A} \hat{V} \hat{A} \hat{c} \hat{E} \hat{i} \hat{E}$
 $y = (100t - 4t^2) \pm \hat{y} \hat{A} \hat{c} \hat{A} \hat{A} \hat{O} \hat{U} \hat{i} \varnothing \hat{y} \hat{E} \hat{E}. \quad t = 0 \quad \pm \hat{y} \hat{U} \hat{o} \hat{S} \hat{A} \hat{i} \hat{D} \quad x = 0 \quad - \quad \hat{E} \hat{D} \quad \pm \hat{E} \hat{i}$
 $| \quad \hat{i} \hat{l} \varnothing \hat{o} \hat{A} \hat{o} \hat{l} \hat{u} \hat{c} \hat{D} \quad y = 0 \quad \pm \hat{y} \hat{U} \hat{u} \hat{c} \hat{S} \hat{A} \hat{i} \hat{D}, \quad \ll \quad \hat{o} \hat{D} \varnothing \hat{c} \hat{y} \quad \frac{3}{4} \hat{c} \varnothing \quad \hat{S} \hat{A} \hat{o}, \quad \hat{A} \hat{u} \hat{U} \hat{o}$
 $\hat{O} \hat{i} \hat{l} \varnothing \hat{o} \quad - \quad \hat{u} \hat{A} \hat{u} \hat{i} \hat{E} \hat{i} \hat{l} \varnothing \hat{i} \hat{n} \varnothing. \quad (\hat{A} \hat{c} \hat{i} \varnothing \frac{1}{4} \quad V = 50 \hat{A} \hat{V} \hat{A} \hat{c} \hat{E} \hat{i} \hat{E}, \quad a = 17.89 \hat{A} \hat{V} \hat{A} \hat{c} \hat{E} \hat{i} \hat{E}^2)$

4.2.16.5 $0.4 \hat{A} \hat{f} \hat{m} \hat{s}^{-1} \hat{A} \hat{O} \hat{u} \hat{c} \hat{A} \hat{o} \frac{1}{4} \hat{o} \frac{3}{4} \varnothing \quad \hat{O} \hat{D} \hat{u} \quad \rho \hat{A} \hat{i} \hat{l} \varnothing \hat{E} \hat{D}. \quad \hat{D} \hat{u} \quad 0.6 \hat{A} \hat{V} \hat{A} \hat{c} \hat{E} \hat{i} \hat{E}$
 $\pm \hat{y} \hat{E} \quad \hat{A} \hat{i} \hat{E} \hat{i} \frac{3}{4} \quad \hat{S} \hat{A} \hat{o} \frac{3}{4} \varnothing \quad \rho \hat{A} \hat{i} \hat{l} \varnothing \hat{A} \frac{3}{4} \hat{i} \varnothing, \quad \ll \quad \hat{o} \hat{D} \varnothing \hat{c} \hat{y} \quad \hat{O} \hat{i} \hat{l} \varnothing \hat{o} \frac{3}{4} \hat{y} \quad \hat{A} \hat{O} \hat{A} \hat{i} \hat{E} \hat{i}$
 $\hat{i} \hat{n} \varnothing \quad (\hat{A} \hat{c} \hat{i} \varnothing \frac{1}{4} \quad \hat{O} \hat{i} \hat{l} \varnothing \hat{o} = 0.9 \hat{A} \hat{V} \hat{A} \hat{c} \hat{E} \hat{i} \hat{E}^2)$

4.2.16.6 $\hat{S} \hat{A} \hat{i} \hat{o} \frac{1}{4} \hat{i} \varnothing \quad \hat{y} \hat{U} \quad 240 \hat{A} \hat{f} \hat{m} \hat{s}^{-1} \hat{A} \hat{O} \hat{u} \hat{c} \hat{A} \hat{o} \frac{1}{4} \hat{o} \hat{A} \hat{i} \varnothing \quad \frac{3}{4} \hat{A} \varnothing \quad \rho \hat{A} \hat{i} \hat{l} \varnothing \hat{E} \hat{D}. \quad \hat{S} \hat{A} \hat{o}$
 $75 \hat{c} \hat{A} \hat{V} \hat{A} \frac{1}{2} \hat{c} \pm \hat{y} \hat{U} \hat{u} \hat{c} \hat{S} \hat{A} \hat{i} \hat{D} \quad \ll \quad \frac{3}{4} \hat{y} \quad | \quad \hat{A} \hat{i} \hat{o} \frac{3}{4} \quad \hat{O} \hat{i} \hat{l} \varnothing \hat{o} \frac{3}{4} \hat{y} \quad \hat{A} \hat{O} \hat{A} \hat{i} \hat{E} \hat{i} \quad 3 \hat{A} \hat{V} \hat{A} \hat{c} \hat{E} \hat{i} \hat{E}^2$
 $\pm \hat{y} \hat{E} \hat{i} \varnothing \quad \hat{S} \hat{A} \hat{i} \hat{o} \frac{1}{4} \hat{i} \varnothing \hat{y} \quad \hat{S} \hat{A} \hat{o} \quad \pm \hat{o} \frac{3}{4} \hat{A} \hat{c} \varnothing \quad \frac{3}{4} \hat{o} \frac{3}{4} \varnothing \quad \hat{A} \hat{i} \hat{U} \varnothing \hat{E} \hat{D} \quad \pm \hat{y} \hat{A} \hat{c} \quad \frac{3}{4} \quad \frac{3}{4} \hat{E} \hat{A} \hat{i} \hat{E} \hat{i} \varnothing \times \hat{o}.$
 $(\hat{A} \hat{c} \hat{i} \varnothing \frac{1}{4}: \quad a_t = \pm 2.39 \hat{A} \hat{V} \hat{A} \hat{c} \hat{E} \hat{i} \hat{E}^2)$

« ô | À; Õ ù Ò Æ ¨ À S ¸ j ì ÷ ç p Ø ì Ì ò Æ ¨ ° Æ ¸ y « Ç x - Ì ò. Ò Æ ¸ Æ ¸ ò Ò p Æ ì ÷ ò p ¼ ò ¾ ù ÷ ç ¸ ¼ S Æ Á; U Æ Æ Á ¾; j ø, | À; Ò Ç y ± ¸ ¼ Ò Ò Á; U Æ Æ ÷ ç È Ò.

4.3.2.2 ç ¸ È (Mass)

Ì ÷ j Æ ì ÷ ò Æ ¸ ¼ ¸ Ò | À; Ò Ç y ± ¸ ¼ w - x ò, Ò Æ ¸ Æ ¸ ò Ò Ó Æ ì ÷ ò g - Ò ò S ç ÷ Æ ¸ ¸ ò ¾ ò ¾ Ò Ò ÷ ç È. ± È S Æ « ô | À; Ò Ò ì Ì ÷ ç ± y Æ Ò ± ù Æ ¸ ò ¾ ò ¾ Ò Ò ¸ Ò Á; È Æ ¸ Æ ì ò. p ù Æ ¸ ¸ ¼ S Æ ± Æ ò ¾ | À; Ò Ç y ç ¸ È (Mass) ± È ò Æ ì ò. « Ò m ± y È ± Ø ò ¾; j ø Ì È ç ò Æ ì ò. | À; Ò Ç y ç ¸ È, « ¾ y Æ Ò Æ y, ¸ Ò Æ « ¸ Æ ò S Æ ÷ È Æ ù È ò j ÷ ò ¾ Ò Ò Æ ¸ Ò Ò, Æ Æ ò ¾ ¸ Æ ¸ « Ò « ¾ y p Ò ò Æ ¸ ò ¾ ç y ç ¸ Æ ¸ Æ ò | À; Ò ò ¾ ¾; j Æ ¸ Æ. - S Æ | À; Ò Ç y ± ¸ ¼ (w) p ¼ ò ¾ ù ÷ ç ¼ ò Á; U Æ ò ¼ S Æ ò ¾ Ò Ò, « ¾ y ç ¸ È (m) Á; È; ¾ Æ ¸ ò Æ ¸ Æ; p Ø ì Ì ò. | À; Ò ù ç y ç ¸ È ¸ Ç Æ ò j ¾; j Æ ½ ¾; j Æ Ì (Common balance) | ÷ j Æ Ì ò Æ ¸ ¼ È Æ Æ; j ò. ò j ¾; j Æ ½ ¾; j Æ ¸ ç Ò ì Ì ò S Æ Æ; j, p Ò | À; Ò ù ç y ± ¸ ¼ ¸ Ç Æ Ò Ì S Æ ¸ ò Æ ¸ ¼ S Æ ò ¾ Ò Ò, « ¸ Æ ù ¸ S Æ p ¼ ò ¾ ç p Ò ò Æ ¾; j ø, g - Æ y Æ ¸ ò Ò p Æ Æ È ù Ì ò ¸ y È; j (same) p Ø ì È Ò. - S Æ « Æ ù È y ç ¸ È ù ò j ¾; j Æ ½ ¾; j Æ ¸ ¸ ò Æ ¸ ò ¾ ò Æ ¸ ¾; j Æ ì ò Ò Æ ò Æ Ì ò. S Æ Ò ò ò j ¾; j Æ ½ ò ¾; j Æ ¸ ç Ò ù ò ¾; j ø, ¸ Ò | À; Ò Ç y ç ¸ È, Æ Æ ò ¾ ¸ Æ ¸ ± ù Æ ¸ ò ¾ ò ¾ Ò Ò ¸ y È; j S Æ (same) p Ø ì Ì ò.

4.3.3 ç Æ ò ¼ È y p Æ ì ÷ Æ ¸ ù

4.3.3.1 Ó ¾ ø Æ ¸ Æ ¸ (Ì Æ ò ¸ Æ 1)

¸ ù | À; Ò | À; Ò Ò ò Æ; j S ¾ U | À; Ò Ò È Æ ¸ ¸ ° Æ; j ø ¾; j ì ò Æ Ò Æ Ì Ó Æ ì ÷ ò Æ ¸ ¼; j Æ y È ç ¾ È Ò µ ò x ç ¸ Æ Æ S Æ S Æ; j « ø Æ Ò ¸ Ò S ç ÷ S ÷; j ò È Ò ù ç ¸ Æ; j È p Æ ì ÷ ç ¸ Æ Æ S Æ S Æ; j | ¾; j ¼ ÷ ò ¾ Ò Ì Ì ò.

Ó ¾ ø Æ ¸ Æ ¸ Æ ¸ Æ ¸ ò

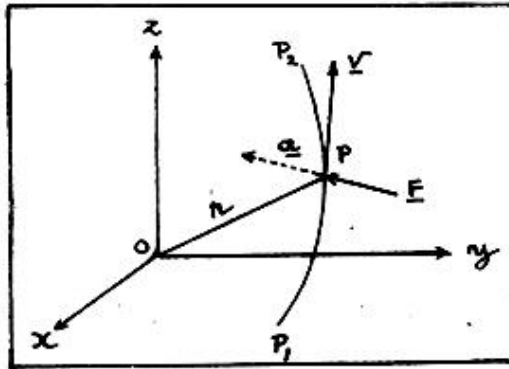
± ò ¾ ò | À; Ò Ò ò « Ò ¸ Æ ì ò Æ ¸ ¼ p ¼ ò ¾ ç S Æ S Æ µ ò x ç ¸ Æ Æ Æ ¸ Ò Ì Ì ò. 2 ¾; j Æ Ò ¸ Ò Æ ¸ ¸ « ¾ y S Æ ø | Æ ¸ Æ Æ Æ; j ø, « Ò ç Ò ò. ± È S Æ, | À; Ò Ç y µ ò x ç ¸ Æ ¸ Æ; j ù Æ Æ Æ « ¾ y S Æ ø | Æ ¸ Æ Æ ò Æ ¸ ¸ S Æ Æ; j ò. Ó ¾ ø Æ ¸ Æ ¸ Æ ¸ Æ ¸, ± ò | À; Ò Ò ò ¾ y ç ¸ Æ ¸ Æ ò ¾; j È; j S Æ Á; j ù È ç | ÷; j ù ç Ó È Æ; j | ¾ y Æ Ò « È Æ ò ¾; j ¾; j Ì ò. p ù Æ ¸ ò Æ Æ Æ; j È Ò | À; Ò Ç y "ç ¸ Æ Æ" « ø Æ Ò "¾ ò Æ Æ ò" (inertia) ± È ò Æ Ì ò.

4.3.3.2 p Æ Æ ¼; j Æ Ò Æ ¸ Æ ¸ (Ì Æ ò ¸ Æ 2)

¸ Ò Ò ç y Ó Æ ì Æ; j È Ò « ¾ y S Æ ø | Æ ¸ Æ Æ ò Æ ¸ ¸ ò Ì S ç ÷ Æ ¸ ¸ ò ¾ ò ¾ Ò Ò, « ù Æ ¸ ¸ Æ y ¾ ¸ ¸ Æ S Æ Ò ò p Ø ì Ì ò. p Æ Æ ¼; j Æ Ò Æ ¸ Æ ¸ Æ ¸ Æ ¸ ò: ¸ Ò Ò ç y S Æ ø F ± y Ò ò Æ ¸ ¸ | Æ ¸ Æ Æ Æ; j È; j ø, « ¾ y Æ ¸ ¸ Ç Æ; j ø ± ù Æ Æ ò Ó Æ ì ÷ ò, (x,y,z) ± y Ò ò Ì È ò Æ ¸ ¼ Æ Ì « ¸ Æ ò Æ ¸ a ± È Ì | ÷; j Æ ¼; j ø, p Æ Æ ¼; j Æ Ò Æ ¸ Æ ¸ Æ; j È Ò F = ma ± y È; j Ì ò.

$\rho \hat{A} \hat{i} \hat{j} \hat{k} \hat{m} \pm \hat{y} \hat{A} \hat{D} \hat{O} \hat{\pm} \hat{n} \frac{1}{2} \hat{A} \hat{i} \hat{E} \hat{A} \hat{i} \hat{j} \hat{o}$ (scalar constant). $\rho \hat{D} \hat{S} \hat{A} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{y} \hat{E} \hat{o} \hat{A} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{o}$. (Basic equation in Dynamics).

$\rho \hat{A} \hat{i} \hat{j} \hat{k} \hat{a} \pm \hat{y} \hat{A} \hat{D} \hat{D} \hat{S} \hat{C} \hat{o} \hat{\pm} \hat{n} \frac{1}{4} \hat{i} \hat{j} \hat{o}$ $\frac{3}{4} \hat{E} \hat{C} \hat{O} \hat{I} \hat{i} \hat{j} \hat{k} \hat{o}$. (Absolute acceleration).



A 4-3-1

$\underline{a}, \underline{F} \pm \hat{y} \hat{U} \hat{o} \hat{O} \hat{I} \hat{i} \hat{j} \hat{k} \hat{o}$, $\hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{o} \hat{\pm} \hat{S} \hat{A} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{o} \hat{E} \hat{A} \hat{i} \hat{j} \hat{k} \hat{A} \hat{o} \hat{S} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{o}$, $\hat{D} \hat{S} \hat{U} \hat{z} \hat{U} \hat{E} \hat{S} \hat{A} \hat{V} \pm \hat{y} \hat{U} \hat{o} \frac{3}{4} \hat{C} \hat{o} \hat{S} \hat{A} \hat{D} \hat{D} \hat{y} \hat{F} \hat{A} \hat{i} \hat{j} \hat{k} \hat{o} \hat{I} \hat{j} \hat{k} \hat{S} \hat{A} \hat{E} \hat{i} \hat{j} \hat{k} \hat{A} \hat{o} \hat{C} \hat{o}$
 $\rho \hat{A} \hat{i} \hat{j} \hat{k} \hat{S} \hat{A} \hat{i} \hat{j} \hat{k} \hat{E} \hat{i} \hat{j} \hat{k} \hat{o} \hat{y} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{o} \hat{E} \hat{A} \hat{i} \hat{j} \hat{k} \hat{A} \hat{o} \hat{S} \hat{A} \hat{i} \hat{j} \hat{k} \hat{P}_1, P, P_2 \pm \hat{y} \hat{U} \hat{o} \hat{A} \hat{i} \hat{j} \hat{k} \hat{C} \hat{o} \hat{x} \hat{o} \hat{A} \hat{i} \hat{j} \hat{k} \hat{A} \hat{o} \hat{A} \hat{o} \hat{D} \hat{o} \hat{S} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{o} \hat{E} \hat{O} \hat{U} \hat{C} \hat{A} \hat{i} \hat{j} \hat{k} \hat{U} \hat{P} \hat{A} \hat{i} \hat{j} \hat{k} \hat{o}$.

$\hat{S} \hat{A} \hat{O} \hat{o}$, $\underline{a}, \underline{F} \pm \hat{y} \hat{A} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{S} \hat{A} \hat{i} \hat{j} \hat{k} \hat{A} \hat{o} \hat{C} \hat{o} \hat{I} \hat{j} \hat{k} \hat{A} \hat{o} \hat{A} \hat{i} \hat{j} \hat{k} \hat{P} \hat{A} \hat{i} \hat{j} \hat{k} \hat{o} \underline{F} = m \underline{a} \pm \hat{y} \hat{U} \hat{o} \hat{O} \hat{A} \hat{i} \hat{j} \hat{k} \hat{D} \hat{o} \hat{I} \hat{j} \hat{k} \underline{F} = m \underline{a} \ll \hat{o} \hat{A} \hat{D} \hat{m} = \frac{\underline{F}}{\underline{a}} \pm \hat{y} \hat{U} \hat{o} \hat{\pm} \hat{D} \hat{S} \hat{A} \hat{i} \hat{j} \hat{k} \hat{o}$.

$m \pm \hat{y} \hat{A} \hat{D} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{A} \hat{i} \hat{j} \hat{k} \hat{\pm} \hat{n} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{D} \hat{i} \hat{j} \hat{k} \hat{o} \hat{A} \hat{i} \hat{j} \hat{k} \hat{C} \hat{o} \hat{x} \hat{O} \hat{I} \hat{i} \hat{j} \hat{k} \hat{o} \hat{S} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{U} \hat{C} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{o} \hat{E} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{E} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{E} \hat{D}$. $\rho \hat{D} \hat{S} \hat{A} \hat{i} \hat{j} \hat{k} \hat{y} \hat{A} \hat{i} \hat{j} \hat{k} \hat{D} \hat{S} \hat{C} \hat{y} \hat{z} \hat{C} \hat{o} \hat{E}$ (mass) $\pm \hat{E} \hat{i} \hat{j} \hat{k} \hat{U} \hat{C} \hat{O} \hat{A} \hat{i} \hat{j} \hat{k} \hat{o}$. $\rho \hat{D} \hat{D} \hat{S} \hat{C} \hat{y} \hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{D} \hat{A} \hat{o} \hat{D} \hat{o} \hat{S} \hat{A} \hat{i} \hat{j} \hat{k} \hat{A} \hat{o} \hat{A} \hat{i} \hat{j} \hat{k} \hat{o} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{I} \hat{j} \hat{k} \hat{O} \hat{A} \hat{i} \hat{j} \hat{k} \hat{D} \hat{S} \hat{U} \hat{i} \hat{j} \hat{k}$, $\rho \hat{D} \hat{\pm} \hat{U} \hat{A} \hat{i} \hat{j} \hat{k} \hat{D} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{E} \hat{i} \hat{j} \hat{k} \hat{\pm} \hat{n} \frac{1}{2} \hat{A} \hat{i} \hat{j} \hat{k} \hat{o}$.

$m_1, m_2 \pm \hat{y} \hat{U} \hat{o} \hat{z} \hat{C} \hat{o} \hat{E} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{U} \hat{E} \hat{P}_1, P_2 \pm \hat{y} \hat{U} \hat{o} \hat{P} \hat{O} \hat{D} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{S} \hat{A} \hat{o} \underline{F} \pm \hat{y} \hat{U} \hat{o} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{o} \ll \hat{o} \hat{S} \hat{A} \hat{i} \hat{j} \hat{k} \hat{D} \ll \hat{o} \hat{D} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{O} \hat{I} \hat{i} \hat{j} \hat{k} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{\pm} \hat{n} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{D} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{U}$

$$\underline{a}_1 = \frac{\underline{F}}{m_1}; \underline{a}_2 = \frac{\underline{F}}{m_2}$$

$\hat{\pm} \hat{i} \hat{o} \hat{m}_1 > m_2 \hat{\pm} \hat{E} \hat{i} \hat{j} \hat{k} \hat{a}_1 < a_2 \pm \hat{y} \hat{E} \hat{i} \hat{j} \hat{k} \hat{o}$.

$\ll \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{D} \ll \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{E} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{U} \hat{E} \hat{D} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{U} \ll \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{I} \hat{j} \hat{k} \hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{D} \hat{A} \hat{o} \hat{D} \hat{o} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{U} \hat{U} \hat{U} \hat{C} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{x} \hat{o}$,
 $\ll \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{y} \hat{A} \hat{i} \hat{j} \hat{k} \hat{U} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{\ll} \hat{o} \hat{D} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{C} \hat{o} \hat{z} \hat{C} \hat{o} \hat{O} \hat{I} \hat{i} \hat{j} \hat{k} \hat{o}$, $\hat{A} \hat{i} \hat{j} \hat{k} \hat{U} \hat{E} \hat{D} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{C} \hat{o} \hat{z} \hat{C} \hat{o} \hat{O} \hat{I} \hat{i} \hat{j} \hat{k} \hat{o} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{I} \hat{j} \hat{k} \hat{O} \hat{E} \hat{O} \hat{o} \hat{I} \hat{j} \hat{k} \hat{E} \hat{x} \hat{A} \hat{o} \hat{E} \hat{O} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{y} \hat{E} \hat{i} \hat{j} \hat{k} \hat{E} \hat{D}$.

$\rho \hat{A} \hat{i} \hat{j} \hat{k} \hat{U} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{D} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{U} \hat{I} \hat{j} \hat{k} \hat{o} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{x} \hat{C} \hat{E} \hat{D}$.

$\hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{i} \hat{j} \hat{k} \hat{\pm} \hat{n} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{D} \hat{o}$, $\hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{O} \hat{o} \hat{\pm} \hat{n} \hat{I} \hat{j} \hat{k} \hat{\pm} \hat{E} \hat{S} \hat{A} \hat{i} \hat{j} \hat{k} \hat{\ll} \hat{D} \hat{\pm} \hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{O} \hat{A} \hat{i} \hat{j} \hat{k} \hat{I} \hat{j} \hat{k} \hat{o}$.
 $\hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{\mu} \hat{\pm} \hat{O} \hat{D} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{D} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{U} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{I} \hat{j} \hat{k} \hat{E} \hat{A} \hat{i} \hat{j} \hat{k} \hat{o}$. $\hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{U} \hat{E} \hat{C} \hat{O} \hat{o} \hat{A} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{U} \hat{i} \hat{j} \hat{k} \hat{\ll} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{y} \hat{A} \hat{i} \hat{j} \hat{k} \hat{U} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{U} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{I} \hat{j} \hat{k} \hat{O} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{U} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{O} \hat{U} \hat{C} \hat{C} \hat{o} \hat{\pm} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{S} \hat{z} \hat{i} \hat{j} \hat{k} \hat{A} \hat{i} \hat{j} \hat{k} \hat{O} \hat{A} \hat{i} \hat{j} \hat{k} \hat{o}$.

4.3.3.2.1 $\vec{a} \ll \vec{v} \ll \vec{u}$.

$\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units)

\vec{a} (Newton)

$\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units) $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units), $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units), $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units)

"M.K.S." $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units) $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units)

$$1 \vec{a} \ll \vec{v} \ll \vec{u} = 1 \text{ m/s}^2 \text{ } \vec{a} \ll \vec{v} \ll \vec{u} \text{ } \vec{a} \ll \vec{v} \ll \vec{u}$$

4.3.3.3 $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units)

$\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units) $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units) $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units)

$\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units) $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units) $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units)

(i) $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units) $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units) $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units)

$$F = ma \text{ } \vec{a} \ll \vec{v} \ll \vec{u}$$

$\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units) $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units) $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units)

$$F' = -F = ma \text{ } \vec{a} \ll \vec{v} \ll \vec{u}$$

$F' = -ma$ (Inertia force) $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units) $\vec{a} \ll \vec{v} \ll \vec{u}$ (absolute units)

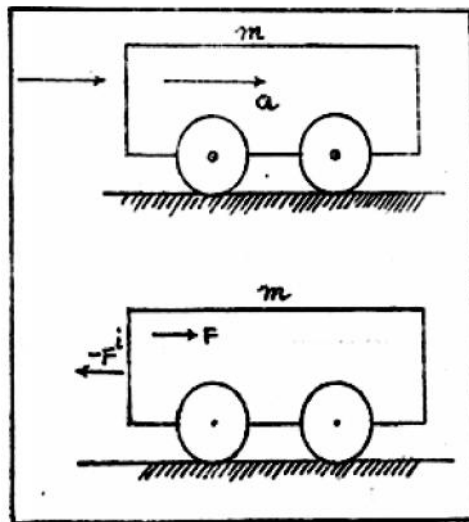


Figure 4-3-2 (a) & b

$\underline{F} + \underline{F}^i = 0 \pm \underline{y} \hat{A} \dots \frac{3}{4}, \ll \hat{A} \ddot{E} \ddot{y} \pm \ddot{n} \frac{1}{2} \hat{O} \hat{A} \dots \times \dots \zeta_i \dots \hat{A} \hat{c} \hat{i} \hat{l} \hat{o} \hat{S} \hat{A} \hat{i} \hat{D},$

$$X\underline{i} + Y\underline{j} + Z\underline{k} - m \frac{d^2x}{dt^2} \underline{i} - m \frac{d^2y}{dt^2} \underline{j} - m \frac{d^2z}{dt^2} \underline{k} = 0$$

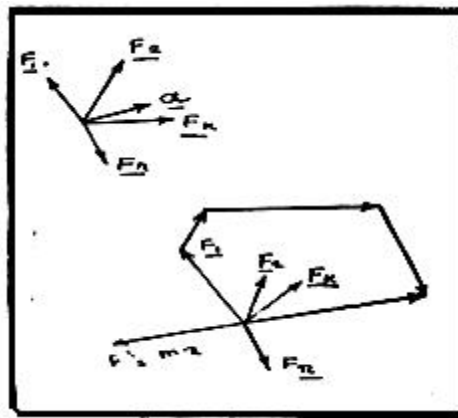
$\ll \frac{3}{4} \hat{i} \hat{A} \hat{D},$

$$X - m \frac{d^2x}{dt^2} = 0; Y - m \frac{d^2y}{dt^2} = 0; Z - m \frac{d^2z}{dt^2} = 0$$

$\neg \hat{l} \hat{o}. \hat{p} \hat{i} \hat{A} \hat{S} \hat{C} \hat{D} \hat{C} \hat{y} \hat{p} \hat{A} \hat{i} \hat{i} \hat{o} \hat{A} \hat{y} \hat{A} \hat{i} \hat{l} \hat{o} \hat{C} \hat{i} \hat{l} \hat{o}.$

$\frac{3}{4} \hat{A} \hat{o} \hat{A} \hat{i} \hat{o} \hat{E} \hat{y} \frac{3}{4} \hat{o} \hat{D} \hat{A} \hat{o} \dots \frac{3}{4} \hat{o} \hat{D} \hat{C} \hat{y} \hat{S} \hat{A} \hat{o} \hat{A} \hat{o} \hat{A} \hat{i} \hat{o} \hat{A} \hat{c} \hat{i} \hat{o} \hat{C} \hat{y}$
 $\frac{3}{4} \hat{i} \hat{l} \hat{o} \hat{y} \hat{E} \hat{u} \hat{l} \hat{o} \hat{A} \hat{A} \hat{y} \hat{A} \hat{i} \hat{o} \frac{3}{4} \hat{A} \hat{i} \hat{o}.$

$\hat{A} \frac{1}{4} \hat{o} (4.3.4) - \hat{o} \dots \hat{i} \hat{o} \hat{E} \hat{A} \hat{A} \hat{i} \hat{U} \underline{F}_1, \underline{F}_2, \dots, \underline{F}_n \pm \hat{n} \hat{t} \hat{o} \hat{w} \hat{A} \hat{c} \hat{i} \hat{o} \hat{u}, m \pm \hat{y} \hat{U} \hat{o}$
 $\hat{c} \hat{i} \hat{o} \hat{E} \hat{i} \hat{o} \hat{A} \hat{o} \hat{i} \hat{A} \hat{u} \hat{U}, P \pm \hat{y} \hat{U} \hat{A} \hat{c} \hat{i} \hat{o} \hat{u} \hat{C} \hat{D} \hat{C} \hat{o} \hat{A} \hat{o} \hat{A} \hat{i} \hat{o} \hat{A} \frac{3}{4} \hat{i} \hat{l} \hat{o} \hat{i} \hat{u} \hat{o}.$



$\hat{A} \frac{1}{4} \hat{o} 4-3-4$

$\ll \hat{u} \hat{A} \hat{c} \hat{i} \hat{o} \hat{u}, \hat{D} \hat{C} \hat{o} \hat{a} \pm \hat{y} \hat{U} \hat{o} \hat{o} \hat{A} \hat{c} \hat{i} \hat{o} \hat{C} \times \hat{O} \hat{l} \hat{i} \hat{o} \dots \frac{3}{4} \text{ (Resultant acceleration), } \hat{z} \hat{u} \hat{A} \hat{i} \hat{o} \hat{D} \hat{A} \frac{3}{4} \hat{i} \hat{l} \hat{o} \hat{i} \hat{u} \hat{o}.$

$\ll \hat{o} \hat{S} \hat{A} \hat{i} \hat{D}$

$$\sum_{k=1}^n \underline{F}_k = m \underline{a}$$

$\ll \frac{3}{4} \hat{i} \hat{A} \hat{D},$

$$\sum_{k=1}^n \underline{F}_k - m \underline{a} = 0$$

$\ll \hat{o} \hat{A} \hat{D}, \sum_{k=1}^n \underline{F}_k + \underline{F}_i = 0 \neg \hat{l} \hat{o}.$

$\hat{p} \hat{i} \hat{l} \underline{F}^i = -m \underline{a} \pm \hat{y} \hat{A} \hat{D} \hat{o} \frac{1}{4} \hat{o} \hat{D} \hat{A} \hat{A} \hat{c} \hat{i} \hat{o} \pm \hat{E} \hat{o} \hat{A} \hat{i} \hat{o}. \frac{3}{4} \hat{A} \hat{o} \hat{A} \hat{i} \hat{o} \hat{E} \hat{y} \hat{i} \hat{u} \hat{o} \hat{A} \hat{y} \hat{A} \hat{E},$

$\underline{F}_1, \underline{F}_2, \dots, \underline{F}_k, \dots, \underline{F}_n \pm \hat{y} \hat{U} \hat{o} \hat{A} \hat{c} \hat{i} \hat{o} \hat{o} \frac{3}{4} \hat{i} \hat{l} \hat{o} \hat{O} \hat{o}, \underline{F}^i \pm \hat{y} \hat{U} \hat{o} \hat{o} \frac{1}{4} \hat{o} \hat{D} \hat{A} \hat{A} \hat{c} \hat{i} \hat{o} \hat{O} \hat{o} \hat{S} \hat{o} \hat{o} \hat{D}$

$\hat{A} \frac{1}{4} \hat{o} (4.3.4) - \hat{o} \dots \hat{i} \hat{o} \hat{E} \hat{A} \hat{A} \hat{i} \hat{U}, \hat{p} \hat{A} \hat{i} \hat{o} \hat{A} \hat{c} \hat{i} \hat{o} \hat{A} \hat{u} \hat{o} \hat{A} \hat{c} \hat{i} \hat{o} \hat{A} \hat{A} \hat{O} \hat{u} \hat{C} \hat{E}.$

$\pm \hat{E} \hat{S} \hat{A}, \hat{p} \hat{u} \hat{A} \hat{c} \hat{i} \hat{o} \hat{C} \hat{i} \hat{o} \hat{E} \hat{o} \hat{D} \hat{i} \hat{l} \hat{o},$

$$\left[\left\{ \underline{F}_k \right\} k = 1, 2, \dots, n, \underline{F}^i \right]$$

2. ÜË¼jÉ ÷ Ö ÄË òð Àø§, j ½ð ÷ ¼ Ä Æó¼jø, « Ð ÷ Ö ã ÊÄ - ÖÄð ÷ ¼ð Ì ÄÜð.

ŞÄÖð, ÷ Ö Ó ÷ ÉÄË òð Ì ¼jÌ ¼ðÌ Ì - jÄ òÁjË ÆÏ òÁýÄjÏ ÷ Ç, [{F_k} k=1,2,.....n, F^i] ±ý Ûð Ì ¼jÌ ¼ðÌ Ì ò ÄÄýÄÏ ò¼,

$$\sum_{k=1}^n F_{kx} - m \frac{d^2x}{dt^2} = 0$$

$$\sum_{k=1}^n F_{ky} - m \frac{d^2y}{dt^2} = 0$$

$$\sum_{k=1}^n F_{kz} - m \frac{d^2z}{dt^2} = 0$$

±ý Ûð þÄÏ, ÄË òÄÄø òÁýÄjÏ ÷ Ç ò ÄËÄjð.

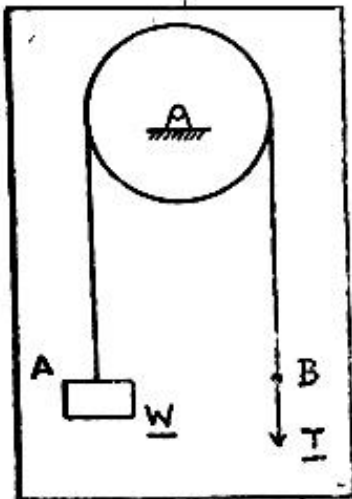
±ÉŞÄ Ð, Çý þÄÏ, ÄË òÄÄø ½ðÌ Ì ÛÌ Ì jÄð¼Éý þÄñ ¼jÄÐ Ä¼Ë ÆŞÄj, « øÄÐ ¼ÄðÄjðÉý ¼ðÐÄð ÷ ¼ð ÄÄýÄÏ ò¼ðŞÄj, þÄÏ, ÄË òÄÄø òÁýÄjÏ ÷ Ç Ä ÆÄÜðÐ, « ÄÜËÛÌ ¼Æ × j ½Äjð.

¼ÄðÄjðÉý ¼ðÐÄð ÷ ¼ð ðËÛÌ ò, ÄjÏÛ, ÛÌ Ì ò « øÄÐ, ðËÛÌ ò ÄjÏÛ, Çý Ì ¼jÌ ¼ðÌ Ì ò ÄÄýÄÏ ò¼Äjð.

4.3.5 Äj¼ðj¼ ½ðÌ Ì

4.3.5.1 ÷ Ö jË ÆÄjÉ, ÄÆÄÆðÄjÉ, þŞÄðjÉ ÷ òÄÄý ÄÐ Ì òøÖð ÄÛ òÌ ÄøÄj¼ ÷ Ö AB ±ý Ûð, ÄÜËý A ±ý Ûð Ó ÷ ÉÄø w ± ÷ ¼ðÛÇ, ð ÷ ¼ÄjÉÐ þ ÷ ½ðÌ òÄðÏ, B ±ý Ûð ÄÛjËjÏ ÑÉÄø, ð ÷ ¼ ŞÄø§jÌ Ì Ä ¼Ë òÄø a ±ý Ûð ÓÏ Ì ò ÷ ¼ð Ì ÄÜÄjÛ ÷ Ö T ±ý Ûð ÄË òÄjÉÐ Ä¼ð (4.3.5)-ø ÷ ðËÄÄjÛ ÄÄýÄÏ ò¼ðÄÏ Ì Ì ¼Éø, « ùÄË òÄý ±ñ Ä¼ð ÷ Äì ÷ ñ.

ÄÜËý þøÄË ÷ Ä T ±Éì Ì jÛ. ÷ òÄÄ ÄÆÄÆðÄj, þÖðÄ¼jø, þùÄøÄË, ÄÛ ÓøÄ¼ð ò ÆÄjÄÏÌ Ì ò.

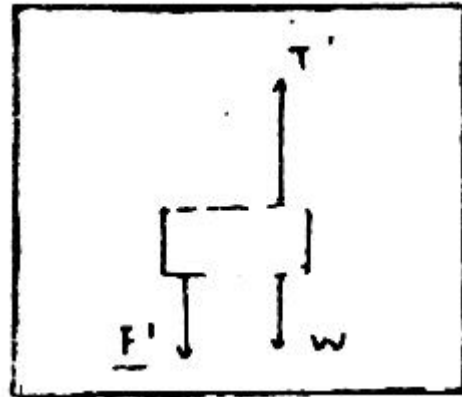


Ä¼ð 4-3-5

À¼õ 4.3.6-ø ð'' ¼ÄjÉÐ ¼ÉöÄÏ ð¼öÄðÏ, « ¼Ûÿ, ùÀ ¼'' ¼ÄüÈ | ÄjÖü ÄÇi ðÄ¼õ ÿjð¼öÄðÏ üÇÐ.

ð'' ¼Äÿ ç'' È $m = \frac{w}{g}$ - Ì õ.

ð'' ¼Äÿ ŞÁø « ¼ÿ ±'' ¼ w↓ Öõ, ÄüÈÿ pØÄ'' ° T' õ |°ÄøÄÏ ÿÿÈÈ. ð'' ¼ ŞÁøÿçjì ÿÄ ¼'' °Äø pÄí ÿç, a ±ÿÜõ ÓÏ ì ð'' ¼ö | ÄüÜüÇ¼jø $F' = -ma$ ±ÿÜõ °¼ðÄÄ'' ° ÿÛÿçjì ÿç ±Ï ì ðÄÏ õ.



À¼õ 4-3-6

±ÉŞÄ $w \downarrow, T' \downarrow, F' \uparrow$, ±ÿÜõ Ä'' °, ù ð'' ¼'' Äð ¼ÄöÄjðÈÿ | ÿjü'' ÿÄÿ ÄÈ °Äç'' ÄÄø'' Äì ÿÿÈÈ.

$$W + T' + F' = 0$$

$$-W + T' + ma = 0$$

$$T' = W + ma$$

$$= W + \frac{W}{g} a$$

$$= W \left(1 + \frac{a}{g} \right)$$

ŞÄÖö B ±ÿÜÄ¼ð¼ø ŞÁøÿçjì ÿç |°ÄøÄÏ ö T' ±ÿÜõ pØÄ'' °, BÄø ÿÛÿçjì ÿç |°ÄøÄÏ ö ¼jì ÿÄ'' ° T-ì |°ÄÄjì õ.

±ÉŞÄ $T = T' = W \left(1 + \frac{a}{g} \right)$ - Ì õ.

4.3.6 | ÿjÏ ì ðÄð¼ Ä'' °, Çjø ¼jì ì üÈ Ð, Çÿ pÄí ì Ä'' Ä'' Äì ÿjì ¼ø.

À¼õ (4.3.7)-ø ÿjðÈÄÄjÜ, F ±ÿÜõ Ä'' °, m ç'' ÈÖüÇ Ð, Çö ¼jì ì Ä¼jì | ÿjü. t ±ÿÜõ ŞÄð¼ø, Ð, Çÿ ç'' Ä'' Ä $OP = r(t)$ ±ÿÜõ ç'' Äð¼'' °ÄÄ'' ÄÄÜð¼jì | ÿjü. $OP = r(t)$

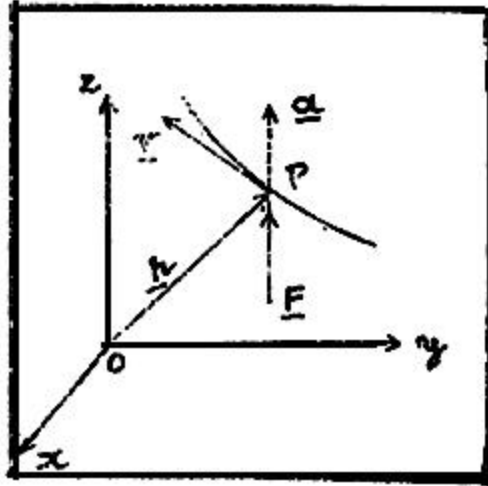


Fig. 4-3-7

For a particle of mass m acted upon by a force \underline{F} ,

$$m\underline{a} = \underline{F}$$

« For a particle, $m \frac{d^2 \underline{r}}{dt^2} = \underline{F}$ is the equation of motion.

For a particle acted upon by several forces $\underline{F}_1, \underline{F}_2, \dots, \underline{F}_k, \dots, \underline{F}_n$, the equation of motion is $m \frac{d^2 \underline{r}}{dt^2} = \sum_{k=1}^n \underline{F}_k$.

where $\{F_k\}$ for $k=1, 2, \dots, n$ are the components of the forces \underline{F}_k along the x, y, z axes.

$$\underline{R} = \sum_{k=1}^n \underline{F}_k$$

is the resultant force

$$m \frac{d^2 \underline{r}}{dt^2} = \sum_{k=1}^n \underline{F}_k$$

where $\underline{F}_k = F_{kx} \underline{i} + F_{ky} \underline{j} + F_{kz} \underline{k}$ is the force vector in Cartesian coordinates.

(i) The force vector \underline{F} can be written as $\underline{F} = F_x \underline{i} + F_y \underline{j} + F_z \underline{k}$.

$$\begin{aligned} \underline{F} &= F_x \underline{i} + F_y \underline{j} + F_z \underline{k} \\ &= \left(\sum_{k=1}^n F_{kx} \right) \underline{i} + \left(\sum_{k=1}^n F_{ky} \right) \underline{j} + \left(\sum_{k=1}^n F_{kz} \right) \underline{k} \\ \underline{R} &= R_x \underline{i} + R_y \underline{j} + R_z \underline{k} \end{aligned}$$

« ôŞÄjĐ ŞÄüÜÈĀ °ÁýÄjÎ Ÿü Ó'' ÈŞÄ

$$m(\ddot{x}_i + \ddot{y}_j + \ddot{z}_k) = F_x i + F_y j + F_z k$$

$$m(\ddot{x}_i + \ddot{y}_j + \ddot{z}_k) = R_x i + R_y j + R_z k \quad \text{— İ ö.}$$

þÄü'' È ±ñ ½ð À Ÿ× ŸÇj Ÿ « '' Äì Ì õŞÄjĐ Ó'' ÈŞÄ,

$$m\ddot{x} = F_x; m\ddot{y} = F_y; m\ddot{z} = F_z \quad \text{±ýÜõ}$$

$$m\ddot{x} = R_x = \sum_{k=1}^n F_{kx}; m\ddot{y} = R_y = \sum_{k=1}^n F_{ky}; m\ddot{z} = R_z = \sum_{k=1}^n F_{kz}$$

±ýÜõ °ÁýÄjÎ Ÿü Ÿ'' ¼ì Ì ö.

(ii) Ä'' °Äý ÜÜŸü Ÿ¼jÎ ŞjÎ , Ÿí Ì ðĐì ŞjÎ Ÿ¼'' °Çø Ÿ¼jÎ Ä'' Ä, Ÿí Ì ðĐì ŞjÎ ðĀ Ÿ¼jÎ Ÿü Ÿü. $\underline{F} = \underline{F}_t + \underline{F}_n$ Ä'' °Äý Ÿ¼jÎ Ä'' Ä, Ÿí Ì ðĐì ŞjÎ ðĀ Ÿ¼jÎ Ÿü Ÿü. $\underline{F}_t; \underline{F}_n \pm \dot{E} \text{ İ } \underline{u}_s$.

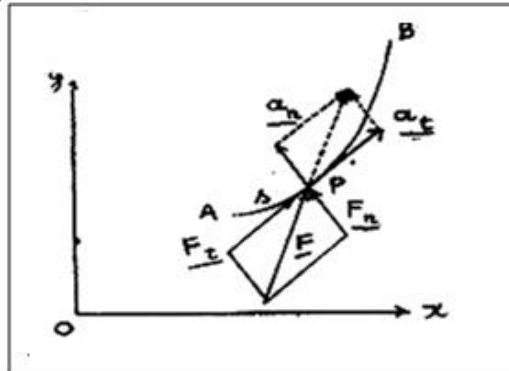
$$\therefore \underline{F} = \underline{F}_t + \underline{F}_n$$

$$\underline{a} = \underline{a}_t + \underline{a}_n$$

$$\therefore m\underline{a} = \underline{F} \quad \text{±ýÜõ °ÁýÄjÎ ,}$$

$$m(a_t i_t + a_n i_n) = F_t i_t + F_n i_n$$

« øÄĐ $ma_t = F_t, ma_n = F_n$ ±ýÜõ — İ ö.



Ä¼õ 4-3-8

ĐŸü þÄî Ì ö Ä'' ÇŞjĐÈø, Ÿí Ì ÈøÄø¼ Ÿ¼'' ÄÄjÉ A ±ýÜõ ðüÇÄÄöóĐ, Ä¼õ 4.3.8-ø ŸjĐÈÄÄjÜ. Äø Ÿ¼jÎ Ä× $\widehat{AP} = s \pm \dot{E}$

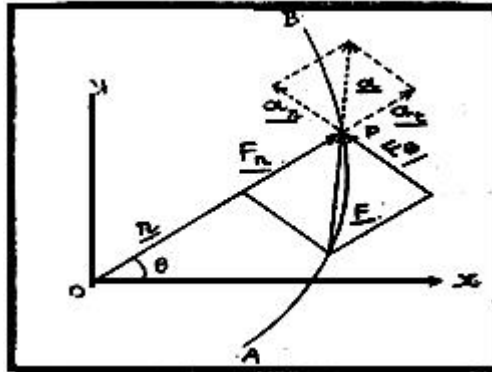
« ÇÄ¼øÄø¼jø, $v = \frac{ds}{dt}, a = \frac{d^2s}{dt^2}$ ±ýÈì ö.

« ôŞÄjĐ þÄî ŸÄø °ÁýÄjÎ Ÿü

$$m \frac{d^2s}{dt^2} = F_t,$$

$$m \left(\frac{1}{p} \right) \left(\frac{ds}{dt} \right)^2 = F_n \quad \text{±ýÈì ö.}$$

(iii) $\vec{F} = F_t \hat{t} + F_n \hat{n}$ $\vec{a} = a_t \hat{t} + a_n \hat{n}$ $\vec{v} = v \hat{t}$ $\vec{r} = r \hat{r}$ $\hat{t} = \dot{\theta} \hat{\phi}$ $\hat{n} = -\hat{\phi}$
 $\ll \vec{F} = m \vec{a}$



A 4-3-9

$\ll \vec{F} = m \vec{a}$

$$\vec{F} = F_t \hat{t} + F_n \hat{n}$$

$$\vec{a} = a_t \hat{t} + a_n \hat{n}$$

$$(f'' + 2f' \dot{\theta})$$

$$m \vec{a} = \vec{F}$$

$$m(\ddot{r} - r \dot{\theta}^2) \hat{t} + m(r \ddot{\theta} + 2\dot{r} \dot{\theta}) \hat{n} = F_t \hat{t} + F_n \hat{n}$$

$$\left. \begin{aligned} m(\ddot{r} - r \dot{\theta}^2) &= F_t \\ m(r \ddot{\theta} + 2\dot{r} \dot{\theta}) &= F_n \end{aligned} \right\}$$

$\ll \vec{F} = F(t, r, \dot{r})$ $\vec{a} = \ddot{\vec{r}}$

$\vec{r} = r \hat{r}$ $\vec{v} = \dot{r} \hat{r} + r \dot{\theta} \hat{\phi}$ $\vec{a} = \ddot{r} \hat{r} + 2\dot{r} \dot{\theta} \hat{\phi} + r \ddot{\theta} \hat{\phi} - r \dot{\theta}^2 \hat{r}$
 (t), $\vec{a} = \ddot{\vec{r}}$ $\vec{r} = r \hat{r}$ $\vec{v} = \dot{r} \hat{r} + r \dot{\theta} \hat{\phi}$ $\vec{a} = \ddot{r} \hat{r} + 2\dot{r} \dot{\theta} \hat{\phi} + r \ddot{\theta} \hat{\phi} - r \dot{\theta}^2 \hat{r}$
 $\ll \vec{F} = m \vec{a}$

$$\vec{F} = F(t, r, \dot{r}) \hat{t} + F_n \hat{n}$$

$\ll \vec{F} = m \vec{a}$

$$m \ddot{\vec{r}} = \vec{F}$$

$$m(a_t + a_n) = F_t + F_n$$

$$m(a_r + a_{\theta}) = F_r + F_{\theta}$$

$\vec{r} = r(t, c_1, c_2)$ $\vec{v} = \dot{r} \hat{r} + r \dot{\theta} \hat{\phi}$ $\vec{a} = \ddot{r} \hat{r} + 2\dot{r} \dot{\theta} \hat{\phi} + r \ddot{\theta} \hat{\phi} - r \dot{\theta}^2 \hat{r}$
 (Vector Integration) $\vec{r} = r(t, c_1, c_2)$ $\vec{v} = \dot{r} \hat{r} + r \dot{\theta} \hat{\phi}$ $\vec{a} = \ddot{r} \hat{r} + 2\dot{r} \dot{\theta} \hat{\phi} + r \ddot{\theta} \hat{\phi} - r \dot{\theta}^2 \hat{r}$
 $\ll \vec{F} = m \vec{a}$

$$y = \frac{1}{2} \times 9.81(1.835)^2 + 18 \times (1.835) + 1.8$$

$$= 18.31 \text{ m}$$

At $y=0$, $y = 0$

$$\therefore 0 = -\frac{1}{2} \times 9.81t^2 + 18t + 1.8$$

$$\text{« } \Delta \text{ } 4.905t^2 - 18t - 1.8 = 0 \text{ } \rightarrow \text{ } t = 0$$

$$t = \frac{18 \pm 18.955}{9.81}$$

$$t_1 = \frac{18 + 18.955}{9.81} = 3.767 \text{ s}; \text{ « } \Delta \text{ } t_2 = -\frac{0.955}{9.81}$$

$t > 0$ \Rightarrow $t = 3.767$ s

4.3.7.2 80 m/s \rightarrow $v = 9 \text{ m/s}$ \rightarrow $\mu = 0.25$ \rightarrow $R = W$ \rightarrow $\frac{w}{g} \ddot{x} = -w$

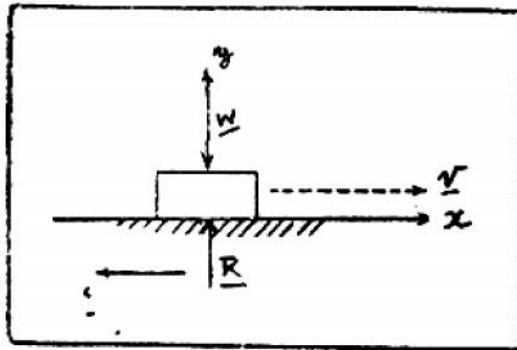


Figure 4-3-10

At $y=0$, $y = 0$ \rightarrow $R = W$ \rightarrow $\frac{w}{g} \ddot{x} = -w$

$$F = -F_i = -R_i = -w_i \text{ } \rightarrow \text{ } \frac{w}{g} \ddot{x} = -w$$

$$\ddot{x} = -0.25g = -\frac{1}{4}g$$

$$\therefore \ddot{x} = -\frac{1}{4}gt + c_1$$

$$t = 0 \text{ } \rightarrow \text{ } \dot{x} = v_0 = 9$$

$$\dot{x} = v_0 = 9$$

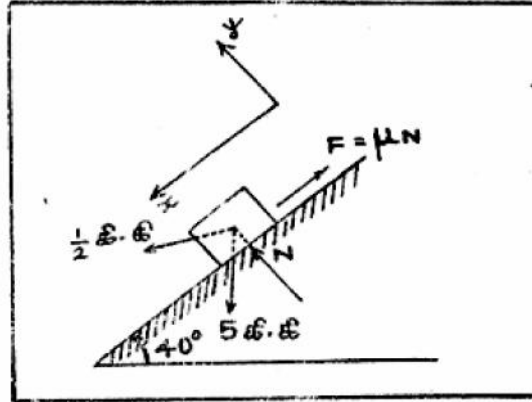


Fig. 4-3-11

Free-body diagram of a block on an inclined plane. The incline is at 40° . A coordinate system (x, y) is shown with x parallel to the incline and y perpendicular to it. Forces acting on the block are: weight $(5g)$ acting vertically downwards, normal force (N) acting perpendicular to the incline, friction force $(F = \mu N)$ acting up the incline, and a horizontal force $(\frac{1}{2}g)$ acting to the left. The weight is decomposed into components $5g \cos 40^\circ$ perpendicular to the incline and $5g \sin 40^\circ$ parallel to the incline.

$$\sum F_{ky} = 0$$

$$-5 \cos 40^\circ + N - \frac{1}{2} \sin 40^\circ = 0$$

$$N = 5 \cos 40^\circ + \frac{1}{2} \sin 40^\circ = 4.1514$$

$$F = \mu N = 0.10 \times 4.1514$$

$$F = 0.41514$$

Free-body diagram of a block on an inclined plane. The incline is at 40° . A coordinate system (x, y) is shown with x parallel to the incline and y perpendicular to it. Forces acting on the block are: weight $(5g)$ acting vertically downwards, normal force (N) acting perpendicular to the incline, friction force $(F = \mu N)$ acting up the incline, and a horizontal force $(\frac{1}{2}g)$ acting to the left. The weight is decomposed into components $5g \cos 40^\circ$ perpendicular to the incline and $5g \sin 40^\circ$ parallel to the incline.

$$m \sum F_{kx} = 5g \sin 40^\circ - \frac{1}{2} \cos 40^\circ - 0.41514$$

$$\frac{w}{g} \ddot{x} = 5 \sin 40^\circ - \frac{1}{2} \cos 40^\circ - 0.41514$$

$$\frac{5}{9.81} \ddot{x} = 2.41586$$

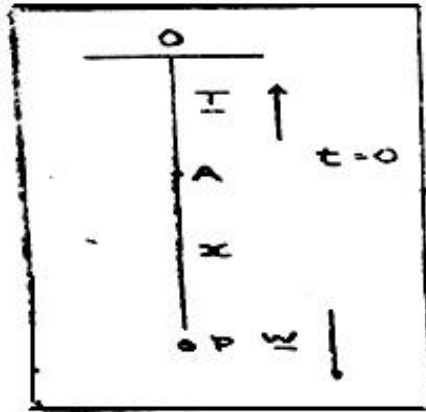
$$\ddot{x} = \frac{2.41586 \times 9.81}{5}$$

$$= 4.704 \frac{m}{s^2}$$

Free-body diagram of a block on an inclined plane. The incline is at 40° . A coordinate system (x, y) is shown with x parallel to the incline and y perpendicular to it. Forces acting on the block are: weight $(5g)$ acting vertically downwards, normal force (N) acting perpendicular to the incline, friction force $(F = \mu N)$ acting up the incline, and a horizontal force $(\frac{1}{2}g)$ acting to the left. The weight is decomposed into components $5g \cos 40^\circ$ perpendicular to the incline and $5g \sin 40^\circ$ parallel to the incline.

4.3.7.5 The block starts from rest at the top of the incline. The distance traveled down the incline is 5.4 m. The time taken to travel this distance is t . The acceleration of the block is 4.704 m/s². The distance traveled down the incline is 5.4 m. The time taken to travel this distance is t . The acceleration of the block is 4.704 m/s².

4. $\ddot{x} = g - T$, $\dot{x} = 5.4 - (5.4 + 0.27t^2)$
 $\dot{x} = 0.4905t^2$
 $x = 0.4905 \frac{t^3}{3} + c_2$
 $t=0, x=0 \Rightarrow 0 = 0 + c_2$
 $x = -0.1635 \frac{t^4}{4} + c_2$
 $t=0, x=0 \Rightarrow 0 = 0 + c_2$
 $\therefore x = -0.1635 \frac{t^4}{4}$
 $t=4 \Rightarrow \dot{x} = -10.464 \text{ м/с}^2$



4-3-12

$$m\ddot{x} = mg - T$$

$$\frac{5.4}{9.81} \ddot{x} = 5.4 - (5.4 + 0.27t^2)$$

$$\ddot{x} = 0.4905t^2$$

$$\dot{x} = 0.4905 \frac{t^3}{3} + c_2$$

$$t=0, x=0 \Rightarrow 0 = 0 + c_1$$

$$0 = 0 + c_1$$

$$x = -0.1635 \frac{t^4}{4} + c_2$$

$$t=0, x=0 \Rightarrow 0 = 0 + c_2$$

$$\therefore x = -0.1635 \frac{t^4}{4}$$

$$t=4 \Rightarrow \dot{x} = -10.464 \text{ м/с}^2$$

$$\dot{x} = -0.1635 \times 64 = -10.464 \text{ м/с}^2$$

« $\dot{x} = -10.464 \text{ м/с}^2$ (при $t=4$)

$$x = -0.1635 \times \frac{(4)^2}{4} = -10.464 \text{ м}$$

5. Δt_{flight} (Time of Flight)

$\Delta t_{\text{flight}} = \frac{2v_0 \sin \theta}{g}$, $\Delta x = v_0 \cos \theta \Delta t_{\text{flight}} = \frac{2v_0^2 \sin \theta \cos \theta}{g} = \frac{v_0^2 \sin 2\theta}{g}$

4.3.8.3 Δt_{flight} Δx Δy Δz Δt_{flight}

$\Delta t_{\text{flight}} = \frac{2v_0 \sin \theta}{g}$, $\Delta x = v_0 \cos \theta \Delta t_{\text{flight}} = \frac{2v_0^2 \sin \theta \cos \theta}{g} = \frac{v_0^2 \sin 2\theta}{g}$

$\Delta y = v_0 \sin \theta \Delta t_{\text{flight}} - \frac{1}{2} g \Delta t_{\text{flight}}^2 = 0$

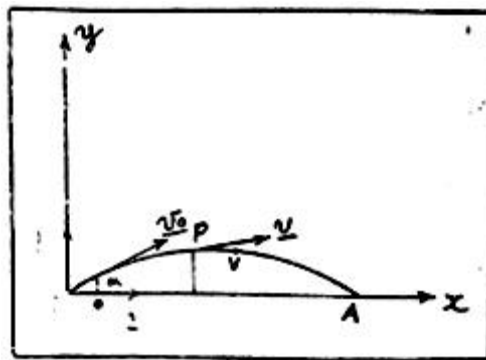


Figure 4-3-13

Projectile motion in a coordinate system with x and y axes. The initial velocity v_0 is at an angle θ to the x -axis. The velocity v is shown at the peak of the path. The horizontal range is x and the vertical displacement is y .

$$v_0 = v_0 \cos \theta \hat{i} + v_0 \sin \theta \hat{j}$$

The acceleration is $\underline{a} = -g \hat{j}$. The force is $\underline{F} = m \underline{a} = -mg \hat{j}$.

$$\underline{W} = -mg \hat{j}$$

Position vector $\underline{r} = x \hat{i} + y \hat{j}$

Force $\underline{F} = m \underline{a} = -mg \hat{j}$

$$m \frac{d^2 \underline{r}}{dt^2} = -mg \hat{j}$$

Acceleration $\frac{d \underline{v}}{dt} = -g \hat{j}$

Initial velocity $\underline{v}_0 = v_0 \cos \theta \hat{i} + v_0 \sin \theta \hat{j}$

$$\int_{v_0}^v dv = \int_0^t -g \hat{j} dt$$

$$\underline{v} - \underline{v}_0 = -gt \underline{j}$$

« ØÄÐ $\underline{v} = -gt \underline{j} + \underline{v}_0 \pm \underline{y} \hat{U} \circ \circ \text{Á} \underline{y} \hat{A}_i \hat{I} \dots \frac{1}{4} \hat{I} \circ$.

$\hat{p} \hat{i} \circ \text{Á} \underline{y} \hat{A}_i \hat{I} \dots \hat{D} \dots \hat{C} \hat{y} \dots \hat{S} \hat{A} \dots \hat{o} \dots \frac{3}{4} \dots \pm \underline{y} \hat{U} \circ \hat{S} \hat{z} \hat{A} \hat{o} \frac{3}{4} \hat{o} \hat{A} \dots \hat{A} \hat{A} \hat{U} \hat{i} \dots \hat{E} \hat{D}$.

$$\frac{d\underline{r}}{dt} = \underline{v} = -gt \underline{j} + \underline{v}_0 \pm \underline{y} \hat{U} \circ \circ \text{Á} \underline{y} \hat{A}_i \hat{I} \hat{o} \dots \frac{1}{4} \hat{A} \hat{U} \hat{O} \dots \hat{E} \dots \frac{3}{4} \hat{i} \dots \hat{A} \hat{I} \dots \hat{o} \frac{3}{4} \hat{o}$$

$$\underline{r} = \int_0^t (-gt \underline{j} + \underline{v}_0) dt$$

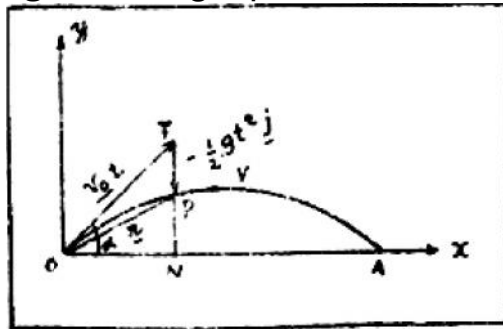
$$= -g \frac{t^2}{2} \underline{j} + \underline{v}_0 t \pm \underline{y} \hat{E}_i \hat{I} \hat{o}$$

$\pm \hat{E} \hat{S} \hat{A} t \pm \underline{y} \hat{U} \circ \hat{S} \hat{z} \hat{A} \hat{o} \frac{3}{4} \hat{o} \dots \hat{D} \dots \hat{C} \hat{y} \dots \hat{z} \hat{C} \dots \hat{A} \dots \hat{A}$

$$r = -\frac{1}{2} - gt^2 \underline{j} + \underline{v}_0 t \pm \underline{y} \hat{U} \circ \hat{z} \hat{C} \dots \hat{A} \hat{o} \frac{3}{4} \hat{C} \dots \hat{o} \hat{A} \hat{C} \hat{A} \dots \hat{A} \hat{A} \hat{U} \hat{i} \dots \hat{E} \hat{D}$$

$\hat{p} \hat{D} \hat{S} \hat{A} \dots \hat{o} \hat{A} \hat{C} \hat{O} \dots \hat{E} \hat{A} \hat{o} \hat{D} \dots \hat{C} \hat{y} \hat{A} \hat{I} \hat{A}_i \dots \frac{3}{4} \dots \hat{A} \ll \hat{E} \hat{C} \hat{A} \hat{I} \dots \hat{E} \hat{D}$.

$\hat{p} \hat{i} \circ \text{Á} \underline{y} \hat{A}_i \hat{I} \hat{o} \dots \frac{1}{4} \hat{I} \dots \hat{A} \hat{E} \hat{A}_i \dots - \hat{A}_i \hat{o} \hat{o} \frac{3}{4} \hat{i} \hat{o} \dots \hat{A} \underline{y} \hat{A} \hat{O} \hat{o} \dots \hat{A}_i \hat{O} \hat{U} \hat{A} \hat{C} \hat{i} \dots \hat{o} \dots \frac{3}{4} \hat{o}$
 $\hat{A} \hat{E} \hat{A}_i \hat{o} \dots t \pm \underline{y} \hat{U} \circ \hat{S} \hat{z} \hat{A} \hat{o} \frac{3}{4} \hat{o} \dots \hat{A} \hat{I} \hat{A}_i \dots \frac{3}{4} \hat{A} \hat{C} \hat{o} \dots \hat{D} \dots \hat{C} \hat{y} \dots \hat{z} \hat{C} \dots \hat{A} \hat{O} \hat{o} \dots (P) \ll \hat{o} \hat{D} \dots \hat{U}$
 $\hat{A} \hat{C} \dots \hat{S} \hat{A} \hat{D} \hat{A} \underline{y} \hat{E} \hat{C} \dots \hat{S} \hat{A} \hat{o} \hat{A}_i \hat{E} \hat{p} \hat{A}_i \hat{o} \hat{D} \frac{1}{4} \hat{y} \ll \hat{S} \frac{3}{4} \hat{S} \hat{z} \hat{A} \hat{p} \dots \frac{1}{4} \hat{A} \hat{C} \hat{A} \hat{o} \dots \frac{3}{4} \hat{i} \hat{I} \hat{o}$
 $\frac{3}{4} \hat{i} \hat{I} \hat{A} \dots \hat{A} \hat{o} \hat{A}_i \hat{I} \hat{o} \dots \hat{A}_i \hat{S} \dots \hat{i} \hat{o} \hat{E} \hat{o} \hat{I} \hat{E} \hat{o} \hat{A} \hat{o} \frac{1}{4} \hat{z} \hat{C} \dots \hat{A} \dots (T) \dots \hat{y} \dots \hat{E} \ll \dots \frac{1}{4} \hat{o} \hat{D} \dots \ll \hat{o} \frac{3}{4} \hat{S} \hat{z} \hat{A}$
 $\hat{p} \dots \frac{1}{4} \hat{A} \hat{C} \hat{A} \hat{o} \ll \hat{o} \hat{o} \hat{U} \hat{C} \hat{A} \hat{A} \hat{O} \hat{o} \hat{D} \dots \mu \hat{o} \times \dots \hat{z} \hat{C} \dots \hat{A} \hat{A} \hat{o} \dots \hat{O} \hat{E} \hat{o} \hat{A} \hat{o} \hat{I} \dots \hat{O} \hat{A} \hat{A} \hat{E} \hat{o} \hat{o}$
 $\hat{A} \hat{C} \dots \hat{A} \hat{C} \hat{E}_i \hat{o} \ll \dots \frac{1}{4} \hat{y} \hat{E} \hat{z} \hat{C} \dots \hat{A} \hat{O} \hat{o} \dots \hat{y} \hat{E}_i \hat{I} \hat{o}$.



A 4-3-14

$\hat{z} \hat{I} \hat{E} \hat{E} \hat{o} \dots \hat{o} \hat{A} \hat{C} \dots \hat{o} \hat{o} \dots \hat{o} \hat{A} \hat{o} \hat{A} \frac{1}{4} \hat{A} \hat{A} \hat{C} \hat{O} \hat{o} \frac{3}{4} \hat{i} \hat{o} \dots t \pm \underline{y} \hat{U} \circ \hat{S} \hat{z} \hat{A} \hat{o} \frac{3}{4} \hat{o} \hat{D} \dots \hat{U}$
 $T \pm \underline{y} \hat{U} \circ \hat{o} \hat{o} \hat{U} \hat{C} \hat{C} \dots \hat{A} \ll \dots \frac{1}{4} \hat{o} \hat{D} \hat{A} \frac{1}{4} \hat{o} \hat{4.3.14} \hat{o} \dots \hat{i} \hat{o} \hat{E} \hat{A} \hat{A}_i \hat{U}$,

$$\underline{OT} = \underline{v}_0 \hat{i} \pm \underline{y} \hat{U} \circ \hat{p} \frac{1}{4} \hat{o} \hat{A} \hat{A} \hat{I} \hat{o} \hat{C} \dots \hat{A} \hat{o} \hat{I} \hat{A} \hat{U} \hat{E} \hat{C} \hat{O} \hat{i} \hat{I} \hat{o} \hat{S} \hat{A} \hat{O} \hat{o} \ll \frac{3}{4} \hat{y} \pm \dots \frac{1}{4}$$

$\ll \hat{S} \frac{3}{4} \hat{S} \hat{z} \hat{A} \hat{o} \frac{3}{4} \hat{o} \dots \ll \dots \frac{3}{4} \hat{z} \hat{C} \dots \hat{A} \hat{i} \hat{I} \hat{o} \frac{3}{4} \hat{i} \hat{I} \dots \hat{U} \hat{S} \hat{z} \hat{i} \hat{I} \hat{z} \hat{C} \dots TP = g \frac{t^2}{2} \pm \underline{y} \hat{U} \circ \hat{p} \frac{3}{4} \hat{i} \dots \hat{A} \times \hat{i} \hat{I}$

$\frac{3}{4} \hat{i} \hat{U} \hat{o} \frac{3}{4} \hat{o} \hat{p} \hat{O} \hat{i} \hat{I} \hat{o} \dots \ll \frac{3}{4} \hat{I} \hat{A} \hat{D} \dots \hat{D} \dots \hat{U} \dots T \hat{A} \hat{C} \hat{A} \hat{O} \hat{o} \hat{D} \dots TP = \frac{1}{2} g t^2 \underline{j} \pm \underline{y} \hat{U} \circ \hat{A} \hat{U} \hat{I} \hat{E}_i \hat{O}$

$\hat{p} \frac{1}{4} \hat{o} \hat{I} \hat{A} \hat{A} \hat{I} \hat{o} \hat{C} \dots \hat{A} \hat{o} \hat{I} \hat{A} \hat{U} \hat{E} \hat{C} \hat{O} \hat{i} \hat{I} \hat{o}$.

±ÉŞÅ, t ±ýÛõ ŞĴÀð¼Ø, Ð, ÇŸ ĵĴ· Ä· Å, $v_0 t = \frac{1}{2} g t^2 \underline{j}$ ±ýÛõ
 ÄĴ· Ç×ð¼Ĵ· °ÄĴ « ÈĴÄĴ, ĴĴ. - Éĵø, « Ş¼ŞĴÀð¼Ø, Ð, ÇŸ ĵĴ· Äð¼Ĵ· °ÄĴ
 $OP = r \pm \underline{y} \hat{\Lambda} \frac{3}{4} \hat{i} \hat{o}$, $r = v_0 t - \frac{1}{2} g t^2 \underline{j}$ ±ýÈĵ, ĴĴ.

þíĴ $\underline{r} = x \hat{i} + y \hat{j}$

$$v_0 = v_0 \cos r \hat{i} + v_0 \sin r \hat{j}$$

±ýĴ¼ĵø, ĵĴ· Äð¼Ĵ· °ÄĴ °ÁýÄĵðËý ±ñ ½Ĵõ Ä, Ç×, Ç þÕðËÓõ ´õÄ¼,
 $x = v_0 \cos r t$

$$y = v_0 \sin r t - \frac{1}{2} g t^2$$

±ýÛõ ±ñ ½ĴĴ °ÁýÄĵĴ, Çõ ĴĴÈĴõ. þÄÛÈĴÕóÐ t ±ýÛõ Ð ½
 « ÄĴ, ÄĴĴ, Ĵ¼,

$$y = v_0 \sin r \left(\frac{x}{v_0 \cos r} \right) - \frac{1}{2} g \left(\frac{x^2}{v_0^2 \cos^2 r} \right)$$

$$= x \tan r - \frac{g x^2}{2 v_0^2 \cos^2 r}$$

-Ĵõ.

þí°ÁýÄĵð ¼õ ÄĴ ÄÕÄĵ ÄĵÛÈĴ ±Ø¼Äĵõ

$$x^2 - \frac{2 v_0^2}{g} \sin r \cos r = - \frac{2 v_0^2 \cos^2 r y}{g}$$

$$\left(x - \frac{v_0^2 \sin r \cos r}{g} \right)^2 = \frac{v_0^4 \sin^2 r \cos^2 r}{g^2} - \frac{2 v_0^2 \cos^2 r y}{g}$$

$$= \frac{-2 v_0^2 \cos^2 r}{g} \left(y - \frac{v_0^2 \sin^2 r}{2g} \right)$$

« ¼ĴÄĴ,

$$\left(x - \frac{v_0^2 \sin 2r}{2g} \right) = \frac{-2 v_0^2 \cos^2 r}{g}$$

$$\left(y - \frac{v_0^2 \sin 2r}{2g} \right)$$

þí°ÁýÄĵĴ, $\frac{v_0^2 \sin 2r}{2g}, \frac{v_0^2 \sin^2 r}{2g}$ ±ýÛõ - ĴĴ· ÄÕõ (vertex) $\frac{2 v_0^2 \cos^2 r}{g}$ ±ýÛõ
 ĴõÄĴ, Äð¼Ĵõ (Latus rectum) ĴĴñ ¼ ´Õ ÄÄĴ· Ç· ÄĴ ĴÈĴõ. « ¼ý
 « ĴĴ ĴõĴ¼Ĵõ, ŞĴĴĴĴõ - ũĴĴ.

- (i) $v_x = v_0 \cos r$ (4.21) - v_x is constant throughout the motion.
(ii) $S_x = v_x t = v_0 \cos r t$ (focus)

$$v_x = \frac{1}{4} \times v_0 \cos r$$

$$= \frac{1}{4} \left(\frac{2v_0^2 \cos^2 r}{g} \right)$$

$$= \frac{v_0^2 \cos^2 r}{2g}$$

(iii) $v_x = v_0 \cos r$ (constant)

At any time t , the horizontal distance travelled is $S_x = v_x t = v_0 \cos r t$. The vertical distance travelled is $S_y = v_0 \sin r t - \frac{1}{2} g t^2$. The particle is at the same vertical level as the launch point when $S_y = 0$.
(iv) $v_x = v_0 \cos r$ (constant)

At any time t , the horizontal distance travelled is $S_x = v_x t = v_0 \cos r t$. The vertical distance travelled is $S_y = v_0 \sin r t - \frac{1}{2} g t^2$. The particle is at the same vertical level as the launch point when $S_y = 0$.

(v) $S_x = v_0 \cos r t$, $y = 0 \pm \frac{1}{2} g t^2$ when $x = 0$

« $S_x = \frac{2u^2 \sin r \cos r}{g} = u^2 \frac{\sin 2r}{g}$ (horizontal range) OA (horizontal range) OA

$x = 0$ at $t = 0$ and $t = \frac{2v_0 \sin r}{g}$. The horizontal range is $S_x = u^2 \frac{\sin 2r}{g}$ (horizontal range) OA (horizontal range) OA

4.3.8.4 To find the total time of flight

At any time t , the vertical distance travelled is $S_y = v_0 \sin r t - \frac{1}{2} g t^2$

$y = v_0 \sin r t - \frac{1}{2} g t^2$
 $v_0 \sin r t - \frac{1}{2} g t^2 = 0$

At any time t , the vertical distance travelled is $S_y = v_0 \sin r t - \frac{1}{2} g t^2$. The particle is at the same vertical level as the launch point when $S_y = 0$.
 $S_y = 0$

$$0 = v_0 \sin r T - \frac{1}{2} g T^2$$

« $S_x = \frac{2v_0 \sin r}{g}$

$T = 0$ and $T = \frac{2v_0 \sin r}{g}$. The total time of flight is $T = \frac{2v_0 \sin r}{g}$.

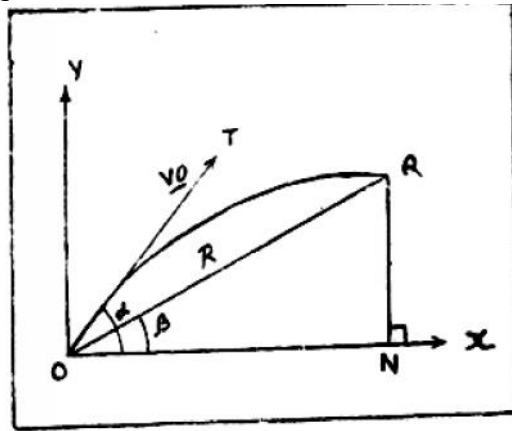
$$v \cos r = v_0 \cos r$$

$$\pm \text{É} \text{Ş} \hat{A}, v = \sqrt{v_0^2 - gh}$$

$$\tan r = \frac{\sqrt{v^2 \sin^2 r - 2gh}}{v_0 \cos r} \rightarrow \text{İ} \text{ö}.$$

4.3.8.12 ±ÉŞĀ, Éò¼Ÿ ĀĒŞĀ |°øÖö ˆÖ °iö¼Çò¼Ÿ ĀĐŪÇ ĀĦ ˆ°i ˆıİ ¼ø.

ˆ° ¼ø¼ÇòĐ¼Ÿ s ±ŸÉ Şıİ ½ò¼ø °iöö¼Öİ İ ö Āĉ, ôİ ĀİĀ °iö×İ Şıİ ÖÉŸ (line of greatest slope) ĀĒĀİ, İ |°øÖö |°ıİ òĐò ¼Çò¼ø ˆ° ¼Āö¼İ Şıİ ÖÉŸ r Şıİ ½ °iöĀø v_0 ±Ÿ Ūö ¼ĉ ˆ°ŞĀ, òĐ¼Ÿ ˆÖ Đ, Ū ±ÉĀôĀĀ Ā¼ıİ İ |ıİ Ū.



Ā¼ö 4-3-18

Ā¼ö 4.3.18-ø, O ±ŸĀĐ ±ÉŞĀİİ ˆ.

Đ, Ū, °iö¼Çò ˆ¼ Q ±Ÿ Ū Āĉ¼ø¼ø ¼ıİ ˆİ ö. OQ ±ŸĀĐ °iö¼Çò¼Ÿ ĀĐŪÇ ĀĦİ ˆİ ö.

O ˆĀò |¼ıİ ˆòŪÇĀİ, ×ö, O-ĀĒĀİ, İ |°øÖö ˆ° ¼Āö¼, ĉĉ Āİ İ òĐİ Şıİ Ā ˆŞ « İİ ˆŞı, ×ö |ıİ Ū.

$$\text{İ} \text{ö} \text{Đ, ÇŸ ĀĦ Āİ ˆ¼ĀŸ °ĀŸ ĀİĀ, } y = x \tan r - \frac{gx^2}{2v_0^2 \cos^2 r} \rightarrow \text{İ} \text{ö}.$$

$$OQ = R \pm \text{É} \text{Ÿ, } Q(R \cos s, R \sin s) \pm \text{Ÿ} \text{Ūö òŪÇ ħĀİ İ Ā ˆĀĉöŪÇ ¼ıø,$$

$$R \sin s = R \cos s \tan r - g \frac{R^2 \cos^2 s}{2v_0^2 \cos^2 r}$$

$$\ll \text{¼ı} \text{ĀĐ } R = \frac{2v_0^2 \sin(r-s) \cos r}{g \cos^2 s} \rightarrow \text{İ} \text{ö}.$$

$$\text{İ} \text{ö} \text{ö} s = 0 \pm \text{É} \text{Ÿ ˆ° ¼ĀĦİ = \frac{2v_0^2 \sin r \cos r}{g} \rightarrow \text{İ} \text{ö}.$$

4.3.8.13 $\circ_i \ddot{o} \times \frac{3}{4} \zeta \ddot{o} \frac{3}{4} \zeta \ddot{o} \ddot{O} \ddot{D} \pm \ddot{E} \zeta \ddot{A}_i \ddot{O} \zeta \ddot{y} \ddot{A} \zeta - \ddot{A} \div \times \ddot{o} \mid \frac{3}{4} i \ddot{A} \ddot{A} \ddot{i} \zeta \frac{1}{2} \ddot{o}$.

$\circ_i \ddot{o} \times \frac{3}{4} \zeta \ddot{o} \frac{3}{4} \zeta \ddot{o} \ddot{O} \ddot{D}$, $\ddot{D} \ddot{u} \ddot{A} \zeta - \ddot{A} \div \times \ddot{o} \mid \frac{3}{4} i \ddot{A} \ddot{A} \ddot{O} \ddot{u} \zeta \ddot{S} \ddot{A}_i \ddot{D}$, « $\frac{3}{4} \ddot{u} \ddot{l} \hat{i}$
 $\mid \circ_i \ddot{l} \ddot{o} \ddot{D} \ddot{o} \frac{3}{4} \zeta \ddot{o} \ddot{A} \zeta$, $\ddot{D} \zeta \ddot{y} \ddot{O} \ddot{E} \times \ddot{S} \ddot{A}_s \ddot{o} \hat{a} \hat{i} \circ \ddot{A} \ddot{A}_i \ddot{l} \ddot{o}$. $\pm \ddot{E} \ddot{S} \ddot{A}$, $\circ_i \ddot{o}$
 $\frac{3}{4} \zeta \ddot{o} \frac{3}{4} \zeta \ddot{o} \ddot{O} \ddot{D} \ddot{A} \zeta - \ddot{A} \div \times \ddot{o} \mid \frac{3}{4} i \ddot{A} \times Y \pm \ddot{E} \ddot{y}$,

$$0 = v_0^2 \sin^2(r - s) - 2g \cos s \cdot Y$$

$$Y = \frac{v_0^2 \sin^2(r - s)}{2g \cos s}$$

4.3.8.14 $\circ_i \ddot{o} \frac{3}{4} \zeta \ddot{o} \frac{3}{4} \zeta \ddot{o} \mid \ddot{A} \ddot{O} \ddot{A} \ddot{A} \ddot{f} \ddot{l} \ddot{i} \circ_i \zeta \frac{1}{2} \ddot{o}$.

$R \pm \ddot{y} \ddot{A} \ddot{D} \circ_i \ddot{o} \frac{3}{4} \zeta \ddot{o} \frac{3}{4} \zeta \ddot{o} \ddot{y} \ddot{A} \ddot{D} \ddot{u} \zeta \ddot{A} \ddot{f} \ddot{l} \pm \ddot{E} \ddot{o}$,

$$R = \frac{2v_0^2 \sin(r - s) \cos r}{g \cos^2 s} = \frac{v_0^2}{2g \cos^2 s} [\sin(2r - s) - \sin s]$$

$\rho \hat{i} \hat{l}$, $v_0, s \pm \ddot{y} \ddot{A} \ddot{A} \mid \frac{3}{4} i \ddot{o} \frac{3}{4} \zeta \ddot{o} \frac{1}{2} \ddot{A} \hat{i} \zeta \ddot{u}$.

$\pm \ddot{E} \ddot{S} \ddot{A} R - \ddot{y} \mid \ddot{A} \ddot{O} \ddot{A} \ddot{o} \ddot{A} \ddot{o} \mid \ddot{A} \ddot{E}$, $\sin(2r - s) \pm \ddot{y} \ddot{A} \ddot{D} \ddot{A} \zeta \ddot{o} \mid \ddot{A}_i \zeta \ddot{A} \ddot{A} \frac{3}{4} \ddot{o} \ddot{A}$
 « $\ddot{A} \ddot{S} \ddot{A} \hat{n} \hat{i} \ddot{o}$. $\neg \ddot{E} \zeta \ddot{o} \sin(2r - s) - \ddot{A} \ddot{y} \ddot{A} \zeta \ddot{o} \mid \ddot{A}_i \zeta \ddot{A} \ddot{A} \frac{3}{4} \ddot{o} \ddot{D} \ddot{y} \ddot{E} \zeta \hat{l} \ddot{o}$.

« $\ddot{o} \ddot{S} \ddot{A}_i \ddot{D}$, $2r - s = 90^\circ$

« $\ddot{o} \ddot{A} \ddot{D} r = 45^\circ + \frac{s}{2} \neg \hat{l} \ddot{o}$.

$\pm \ddot{E} \ddot{S} \ddot{A} \pm \ddot{E} \zeta \ddot{S} \zeta \frac{1}{2} \ddot{o} 45^\circ + \frac{s}{2} \pm \ddot{y} \ddot{E} \zeta \ddot{o}$, $\circ_i \ddot{o} \frac{3}{4} \zeta \ddot{o} \frac{3}{4} \zeta \ddot{o} \ddot{A} \ddot{A} \ddot{O} \ddot{o} \ddot{A} \ddot{f} \ddot{l} \mid \ddot{A} \ddot{O} \ddot{A} \ddot{o} \ddot{A} \frac{3}{4}$
 « $\ddot{A} \ddot{O} \ddot{o}$.

$$\cdot \mid \ddot{A} \ddot{O} \ddot{A} \ddot{A} \ddot{f} \ddot{l} = \frac{v_0^2}{g \cos^2 s} (1 - \sin s)$$

$$= \frac{v_0^2}{g(1 + \sin s)}$$

$\ddot{S} \ddot{A} \ddot{O} \ddot{o} 2r - s = 90^\circ \neg \hat{l} \ddot{o} \ddot{S} \ddot{A}_i \ddot{D}$,

$$r - s = 90^\circ - r$$

« $\frac{3}{4} i \ddot{A} \ddot{D} \tau \hat{o} \hat{Q} = Y \hat{O} T$

$\pm \ddot{E} \ddot{S} \ddot{A} \mid \ddot{A} \ddot{O} \ddot{A} \ddot{A} \ddot{f} \ddot{l} \hat{i} \hat{l} \mid \zeta \ddot{A} \frac{3}{4} \zeta \ddot{o}$, $\zeta \ddot{A} \ddot{A} \hat{i} \hat{l} \ddot{o} \ddot{D} \ddot{o} \frac{3}{4} \zeta \ddot{o}$, $\circ_i \ddot{o} \frac{3}{4} \zeta \ddot{o} \pm \ddot{y} \hat{U} \ddot{o}$
 $\rho \hat{A} \hat{n} \hat{E} \hat{u} \hat{l} \ddot{A} \zeta \frac{1}{4} \ddot{S} \ddot{A} \neg \hat{u} \zeta \zeta \frac{1}{2} \ddot{o} \frac{3}{4} \rho \hat{O} \circ \ddot{A} \ddot{A}_i \zeta \hat{i} \zeta \ddot{S} \zeta \ddot{o} \ddot{A} \zeta \hat{i} \hat{l} \ddot{o}$.

4.3.8.15 $\mid \zeta \hat{i} \hat{l} \hat{i} \hat{o} \hat{A} \hat{O} \frac{1}{4} \pm \ddot{E} \zeta \frac{1}{4} \ddot{o} \ddot{S} \ddot{A} \ddot{o} \ddot{D} \frac{1}{4} \ddot{y} \mid \zeta \hat{i} \hat{l} \hat{i} \hat{o} \hat{A} \hat{O} \frac{1}{4} \neg \hat{O} \circ_i \ddot{o} \frac{3}{4} \zeta \ddot{o}$
 $\hat{A} \hat{f} \hat{i} \hat{l} \hat{i} \hat{l}$, $\hat{z} \hat{u} \hat{A} \rho \hat{O} \frac{3}{4} \zeta \ddot{o} \hat{u} \neg \zeta$. « $\ddot{A} \zeta \hat{u} \mid \ddot{A} \ddot{O} \ddot{A} \ddot{A} \ddot{f} \ddot{l} \ddot{o} \frac{3}{4} \zeta \ddot{o} \circ_i \hat{l} \hat{i} \hat{o} \ddot{A} \ddot{A}_i \zeta$
 $\circ_i \ddot{o} \ddot{D} \ddot{u} \zeta \ddot{E} \pm \ddot{E} \hat{i} \zeta \frac{1}{4} \ddot{o}$
 $\circ_i \ddot{o} \frac{3}{4} \zeta \ddot{o} \frac{3}{4} \zeta \ddot{o} \hat{A} \hat{f} \hat{i} \hat{l}$,

$$R = \frac{v_0^2}{g \cos^2 s} [\sin(2r - s) - \sin s]$$

$$\therefore \sin(2\alpha - \beta) = \frac{g \cos^2 \beta}{v_0^2} + \sin \beta$$

πίλ g, R, v_0, β εστανλ $\hat{A}_s \hat{u}$ λ $\hat{E} \hat{O} \hat{A} \hat{C} \hat{O} \hat{A} \hat{C}$ $\hat{E} \hat{o}$ | $\hat{A} \hat{U} \hat{A} \hat{j} \hat{o}$,

$$\sin(2\alpha - \beta) s \pm \hat{y} \hat{A} \hat{D} \hat{O} \hat{A} \hat{j} \hat{E} \hat{C} \hat{A} \hat{j} \hat{l} \hat{o}.$$

· $(2r_1 - \beta)$ εστανλ $\hat{A} \hat{j} \hat{u}$ $180^\circ - \hat{l} \hat{l} \hat{l}$ $\hat{E} \hat{o} \hat{A} \hat{j} \hat{o} \hat{u}$ $\hat{n} \hat{l}$. « $\hat{A}_s \hat{u}$

$$r_1, r_2 \pm \hat{y} \hat{E} \hat{j} \hat{o},$$

$$\sin(2r_1 - s) = \sin(2r_2 - s)$$

$$\therefore 2r_1 - s = 180 - (2r_2 - s)$$

$$r_1 - \frac{s}{2} = 90 - r_2 + \frac{s}{2}$$

$$r_1 - \left(45 + \frac{s}{2}\right) = \left(45 + \frac{s}{2}\right) - r_2$$

· $\hat{E} \hat{j} \hat{o}$ $45^\circ + \frac{s}{2}$ $\pm \hat{y} \hat{U} \hat{o}$ $\hat{s}_{s,j} \frac{1}{2} \hat{o}$, | $\hat{A} \hat{O} \hat{A}$ $\hat{o} \hat{j} \hat{o} \hat{C}$ $\hat{A} \hat{f}$ $\hat{o} \hat{o}$ | $\hat{A} \hat{U} \hat{A} \hat{j} \hat{o}$ $\hat{j} \hat{C} \hat{A}$ $\hat{j} \hat{o}$ $\hat{A} \hat{A} \hat{U} \hat{o} \hat{A} \hat{j} \hat{o}$, $\hat{A} \hat{u} \hat{E}$ $\hat{p} \hat{O} \hat{A} \hat{j} \hat{o} \hat{u}$ $\hat{p} \hat{o} \hat{D} \hat{y}$ $\hat{o} \hat{A} \hat{j} \hat{E}$ $\hat{s}_{s,j} \frac{1}{2} \hat{l}$ \hat{u} « $\hat{A} \hat{i} \hat{s} \hat{y} \hat{E} \hat{E}$.

4.3.9 $\hat{A} \hat{j} \hat{o} \hat{C} \hat{i} \hat{s} \frac{1}{2} \hat{l} \hat{u}$.

4.3.9.1 $\hat{O} \hat{D} \hat{s} \hat{C} \hat{j} \hat{E} \hat{D}$ $\hat{A} \hat{o} \hat{A} \hat{j} \hat{E}$ $\hat{A} \hat{A} \hat{o}$ (level ground), $\hat{O} \hat{D} \hat{u} \hat{C} \hat{A} \hat{C} \hat{O} \hat{D}$, $\hat{A} \hat{C} \hat{j} \hat{E} \hat{l}$ $84 \hat{A} \hat{o} \hat{A} \hat{j} \hat{o}$ $\pm \hat{y} \hat{U} \hat{o}$ $\hat{s} \hat{A} \hat{o} \hat{s} \hat{j} \hat{l}$, $\hat{s} \hat{C} \hat{i} \hat{s} \hat{j} \hat{o} \hat{l} \hat{y}$ 30° $\hat{s}_{s,j} \frac{1}{2} \hat{l} \hat{o} \hat{j} \hat{o} \hat{A} \hat{o} \hat{E} \hat{C} \hat{A} \hat{o} \hat{A} \hat{l} \hat{o}$. « \hat{D} (1) « $\hat{A} \hat{o} \hat{A} \hat{j} \hat{o} \hat{A} \hat{j} \hat{C} \hat{A} \hat{A} \hat{o} \hat{O}$ (2) $\hat{A} \hat{E} \hat{o} \hat{O}$ $\hat{s}_{s,j} \hat{A} \hat{o} \hat{O}$ (3) $\hat{s} \hat{C} \hat{i} \hat{s} \hat{j} \hat{o} \hat{C} \hat{o} \hat{y}$ $\hat{A} \hat{D} \hat{u} \hat{C}$ $\hat{A} \hat{f}$ $\hat{o} \hat{o}$ (4) $60 \hat{A} \hat{o} \hat{A} \hat{j} \hat{o}$ $\hat{A} \hat{A} \hat{o} \hat{A} \hat{j} \hat{o}$ $\hat{p} \hat{O} \hat{l} \hat{o} \hat{A} \hat{j} \hat{o} \hat{D}$ « $\hat{s} \hat{y} \hat{s} \hat{A} \hat{o} \hat{O}$, $\hat{p} \hat{A} \hat{i} \hat{s} \hat{o} \hat{A} \hat{o} \hat{s} \hat{j} \hat{n}$.
($g = 9.8 \hat{A} \hat{l} \hat{A} \hat{C}^2 \hat{s} \hat{E} \hat{l} \hat{s} \hat{j} \hat{u}$.)

πίλ $v_0 = 84 \hat{A} \hat{l} \hat{A} \hat{C}$ $r = 30^\circ$

$$(1) \quad \hat{A} \hat{o} \hat{A} \hat{j} \hat{o} \hat{A} \hat{j} \hat{C} \hat{A} \hat{A} \hat{o} = \frac{v_0^2 \sin^2 r}{2g}$$

$$= 84 \times 84 \times \frac{1}{2} \times \frac{1}{2} \times \frac{1}{2} \times \frac{1}{9.8}$$

$$= 90 \hat{A} \hat{o} \hat{A} \hat{j} \hat{o} \hat{u}$$

$$(2) \quad \hat{A} \hat{E} \hat{o} \hat{O} \hat{s}_{s,j} \hat{A} \hat{o} = \frac{2v_0 \sin r}{g}$$

$$= 2 \times 84 \times \frac{1}{2} \times \frac{1}{9.8}$$

$$= \frac{60}{7} \hat{A} \hat{C} \hat{j} \hat{E} \hat{s} \hat{j} \hat{u}$$

$$\begin{aligned}
(3) \quad v_0 \sin r &= \frac{v^2 \sin r}{g} \\
&= 84 \times 84 \times \frac{\sqrt{3}}{2} \times \frac{1}{9.8} \\
&= 420\sqrt{3} \text{ m/s}
\end{aligned}$$

(4) $v^2 = v_0^2 - 2gh$ \rightarrow $v = \sqrt{v_0^2 - 2gh}$

príklad: $v_0 = 84, h = 60$

$$v^2 = 84 \times 84 - 2 \times 9.8 \times 60 = 6048$$

$$v = \sqrt{6048} = 12\sqrt{42} = 77.772 \text{ m/s}$$

$$\tan r = \frac{\sqrt{v_0^2 \sin^2 r - 2gh}}{v_0 \cos r}$$

$v_0 = 84, h = 60, r = 30^\circ$

$$\tan r = \frac{\sqrt{84 \times 84 \times \frac{1}{2} \times \frac{1}{2} - 2 \times 9.8 \times 60}}{84 \times \frac{\sqrt{3}}{2}}$$

$$= \frac{7\sqrt{12}}{42\sqrt{3}} = \frac{2}{3}$$

$\therefore r = 33^\circ 42'$

4.3.9.2 \rightarrow $R = \frac{V_0^2 \sin 2r}{g}$ \rightarrow $V_0^2 = \frac{gR}{\sin 2r}$

$$\begin{aligned}
\text{Kinetic energy} &= \frac{1}{2}mv^2 \\
&= \frac{1}{2}m v_0^2 \\
&= \frac{1}{2}m \frac{gR}{\sin 2r}
\end{aligned}$$

• Дуга AC AF OC \rightarrow UEA ; ED , $\sin 2r = \frac{y}{\text{AD}}$ AC , O ; A ; CA $\text{A}^{\frac{3}{4}} \text{O}$ A ; AU OS ; D U AI O . « OS ; D $\sin 2r = 1$ « OD $r = 45^\circ$ \rightarrow I O .

$$= \frac{m}{2} \times gR \text{ AF } \text{OC} \rightarrow \text{UEO}$$

$$\text{SAO} \text{O } v_0^2 = gR$$

Дуга AC AF OC \rightarrow UEA ; ED , $\sin 2r = \frac{y}{\text{AD}}$ AC , O ; A ; CA $\text{A}^{\frac{3}{4}} \text{O}$ A ; AU OS ; D U AI O . « OS ; D $\sin 2r = 1$ « OD $r = 45^\circ$ \rightarrow I O .

$$\text{pí l } h = \frac{gR}{2g} = \frac{R}{2} \rightarrow \text{I} \text{ O.}$$

$\pm \text{E}$ SA , D , U , C $\frac{1}{4} \text{AF}$ OC A ; CA \times I I O AA ; E A O $\frac{3}{4}$ « $\frac{1}{4} \text{AI}$ U I O .

4.3.9.3 O D , U AE ; EI I 14AO $\frac{1}{4}$ SA , O $\frac{3}{4} \text{O}$ $\pm \text{E}$ AO AI , C $\frac{1}{4} \text{AI}$, 10AO $\frac{1}{4}$ $\frac{1}{4} \text{I}$ AA O « EO $\frac{3}{4} \text{I}$ O , D , U I I pO $\pm \text{E}$ O O , U U CE $\pm \text{E}$ I , I A .

$$\frac{3}{4} \text{AO} \text{O} \frac{1}{4} \frac{3}{4} \text{C} \text{SA} \text{O} = 14 \text{AI} \text{A}$$

$$\frac{3}{4} \text{AO} \text{O} \frac{1}{4} \text{C} \frac{1}{4} \text{AF} \text{I} = 10 \text{AE}$$

Дуга AC AF OC \rightarrow UEA ; ED , $\sin 2r = \frac{y}{\text{AD}}$ AC , O ; A ; CA $\text{A}^{\frac{3}{4}} \text{O}$ A ; AU OS ; D U AI O .

$$R = \frac{v_0^2 \sin 2r}{g} \rightarrow \text{I} \text{ O.}$$

$$\sin 2r = \frac{gR}{v_0^2}$$

$$\frac{9.8 \times 10}{14 \times 14} = \frac{1}{2}$$

$$2r = 30^\circ \ll \text{OD} \ 150^\circ$$

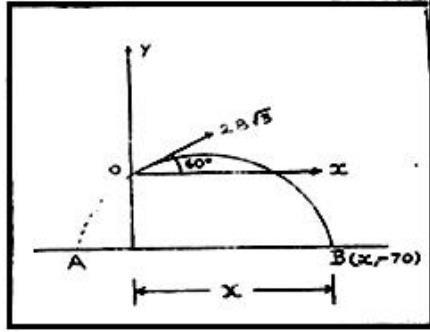
« OD $r = 15^\circ$ « OD 75° \rightarrow I O
 $\pm \text{E}$ SA D , U , pO $\pm \text{E}$ O O , C O ; AU U C D .

4.3.9.4 70AO $\frac{1}{4}$ AA O U C O S ; I O AO $\frac{3}{4} \text{O}$ I O CA AO O O AE ; EI I $28 \sqrt{3}$ 3AO $\frac{1}{4}$ $\frac{3}{4} \text{C}$ SA , O $\frac{3}{4} \text{O}$ 60° UEO $\frac{3}{4} \text{O}$ O AO D $\pm \text{E}$ AO AI O Y ED . « I S ; I O AO $\frac{3}{4} \text{O}$ O O « AO D $\frac{3}{4}$ A A « EI I O OU CA O C $\frac{1}{4} \text{O}$; $\frac{3}{4} \text{I}$ A \times , $\frac{3}{4} \text{C}$ SA , O , pAI , O $\frac{3}{4} \text{C}$ O CA U EI , I I .

$$\text{pí l } v = 28\sqrt{3}$$

$$r = 60^\circ \rightarrow \text{I} \text{ O.}$$

Дуга AC $\frac{3}{4}$ A A $B(x, -70)$ $\pm \text{Y}$ U O OU CA O AO $(4.3.20)$ - O S ; I O EA A ; U « EI , I O .



A 4-3-20

$$y = x \tan \Gamma - \frac{gx^2}{2u^2 \cos^2 \Gamma}$$

$$-70 = x \tan 60^\circ - \frac{9.8x^2}{2 \times 28 \times 28 \times 3 \times \cos^2 60^\circ};$$

« 3/4 j A D,

$$70 = x\sqrt{3} - \frac{x^2}{120}$$

« 3/4 j A D $x^2 - 120\sqrt{3}x - 8400 = 0 \rightarrow \hat{I} \hat{o}$

$$x = \frac{120\sqrt{3} \pm 160\sqrt{3}}{2}$$

$\therefore x = -20\sqrt{3}$ « \hat{o} A D $x = 140\sqrt{3}$ $\rightarrow \hat{I} \hat{o}$.

$\therefore x = -20\sqrt{3}$ \hat{o} E \hat{i} $\frac{1}{2}$ \hat{u} \hat{o} A \hat{o} I,

$x = 140\sqrt{3}$ $\pm \hat{y}$ $\hat{U} \hat{o}$ A $\hat{3}/4 \hat{u} \hat{o}$ $\hat{z} \hat{u}$ \hat{o} A $\hat{I} \hat{o}$.

B $\pm \hat{y}$ $\hat{U} \hat{A} \hat{1}/4 \hat{o} \hat{3}/4 \hat{u} \hat{o}$ D $\hat{C} \hat{y}$ $\hat{3}/4 \hat{u} \hat{o}$ \hat{o} S $\hat{A} \hat{o}$ \hat{o} $v \pm \hat{E} \times \hat{o}$, « D $\hat{u} \hat{C} \hat{1}/4 \hat{o} \hat{3}/4 \hat{u} \hat{o}$ \hat{o} $\hat{O} \hat{1}/4 \hat{y}$, „
 $S \hat{u} \hat{i} \hat{1}/2 \hat{i} \hat{o}$ $\hat{i} \hat{C} \hat{A} \hat{u} \hat{o} \hat{3}/4 \hat{u} \hat{o}$ $\hat{A} \hat{I} \hat{A}$ « $\hat{E} \hat{o} \hat{A} \hat{3}/4 \hat{u} \hat{o}$ $\times \hat{o}$ $\hat{i} \hat{u} \hat{o}$.

« \hat{o} S $\hat{A} \hat{i} \hat{D}$, $v^2 = v_o^2 - 2gh$

$$= 28 \times 28 \times 3 - 2 \times (9.8) \times (-70)$$

$$= 2352 + 1372$$

$$= 3724$$

$$\therefore v = 14\sqrt{9} \hat{A} \hat{f} / \hat{A} \hat{C}$$

$$\tan \mu = \frac{\sqrt{v_o^2 \sin^2 \Gamma - 2gh}}{v_o \cos \Gamma}$$

$$= \frac{\sqrt{28 \times 28 \times 3 \times \frac{3}{4} - 2 \times 9.8 \times (-70)}}{28 \times \sqrt{3} \times \frac{\sqrt{3}}{2}}$$

$$= \frac{\sqrt{2352 + 1372}}{28 \times \sqrt{3} \times \frac{\sqrt{3}}{2}}$$

$$= \sqrt{2/3}$$

$$\therefore \mu = 39^\circ 13'$$

$y = \frac{1}{2}gt^2$; $\frac{dy}{dt} = gt$; $\frac{dv}{dr} = 0 \Rightarrow \frac{dy}{dr} = 0$
 $\frac{dy}{dr} = \frac{dy}{dt} \cdot \frac{dt}{dr} = gt \cdot \frac{1}{v} = 0$

$$a \sec^2 r - \frac{ga^2}{2v_o^2} \cdot 2 \sec r \cdot \sec r \cdot \tan r = 0$$

$$a \sec^2 r \left(\frac{1 - ga \tan r}{v_o^2} \right) = 0$$

$$\therefore \tan r = \frac{v_o^2}{ga}$$

$H = \frac{1}{2}gt^2$; $\frac{dH}{dt} = gt$; $\frac{dH}{dr} = \frac{dH}{dt} \cdot \frac{dt}{dr} = gt \cdot \frac{1}{v} = 0$

$$H = a \cdot \frac{v_o^2}{ga} - \frac{ga^2}{2v_o^2} \left(1 + \frac{v_o^4}{g^2 a^2} \right)$$

$$= \frac{v_o^2}{g} - \frac{ga^2}{2v_o^2} - \frac{v_o^2}{2g}$$

$$\frac{v_o^2}{2g} - \frac{ga^2}{2v_o^2}$$

$\frac{dH}{dr} = \frac{dH}{dt} \cdot \frac{dt}{dr} = gt \cdot \frac{1}{v} = 0$

$$= \frac{v_o^2 \sin^2 r}{2g}$$

$$= \frac{v_o^2}{2g} \cdot \frac{1}{\cos^2 r}$$

$$= \frac{v_o^2}{2g} \cdot \frac{1}{(\cot^2 r)}$$

$$= \frac{v_o^2}{2g \left(1 + \frac{g^2 a^2}{2v_o^4} \right)}$$

$$= \frac{v_o^2}{2g(v_o^4 + g^2 a^2)}$$

4.3.9.7 $\frac{dH}{dr} = \frac{dH}{dt} \cdot \frac{dt}{dr} = gt \cdot \frac{1}{v} = 0$, $400 \text{ m} - \frac{1}{2}gt^2 = 252$ (Solving for t)
 $\frac{1}{2}gt^2 = 148$; $t^2 = \frac{148}{g}$; $t = \sqrt{\frac{148}{g}}$
 $v = gt = g \sqrt{\frac{148}{g}} = \sqrt{148g}$
 $\frac{dH}{dr} = \frac{dH}{dt} \cdot \frac{dt}{dr} = gt \cdot \frac{1}{v} = \frac{gt}{\sqrt{148g}} = \frac{t}{\sqrt{148}}$
 $\frac{dH}{dr} = 0 \Rightarrow \frac{t}{\sqrt{148}} = 0 \Rightarrow t = 0$
 $\frac{dH}{dr} = \frac{dH}{dt} \cdot \frac{dt}{dr} = gt \cdot \frac{1}{v} = 0$

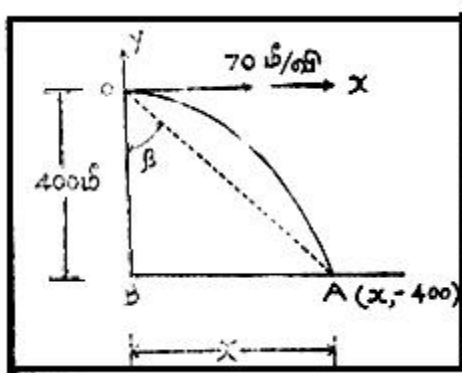
pril A y U A d p A i l - u C j s i | s i u s .

$$v_0 = \frac{252 \times 1000}{60 \times 60} = 70 \text{ m/s}$$

$$r = 0^\circ$$

$$A(x_1 - 400) \text{ y U o } \theta \text{ u C t}$$

$$y = x \tan r - \frac{g^2 x^2}{2u^2 \cos^2 r};$$



A d 4-3-21

y U o p A i l A A A o - u C j s i o ,

$$-400 = 0 - \frac{9.8x^2}{2 \times 70 \times 70 \times 1};$$

$$\ll \text{ j A D , } x^2 = \frac{400 \times 2 \times 70 \times 70}{9.8}$$

$$= 400,000$$

$$x = 200\sqrt{10} \text{ m}$$

4.3.9.8 S A S A i o A o A d (4.3.9.7) y U o 1/2 i o

(1) i n l A A o A i o S A j D , A A j E o j O o p A i o O o S o i l o
 i j i i o A j i A i S j i (Initial line of sight) i A i l o D i S j i o i y
 j i l o s y U o S j i 1/2 o j i n

(2) i n l p A i o E i l o j O 1/2 o A A j E o u A A o A O i l o?

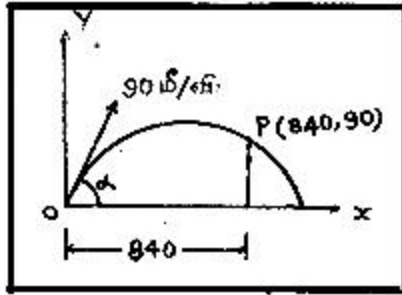
$$(1) \tan s = \frac{BA}{BO} = \frac{200\sqrt{10}}{400} = 1.581$$

$$\therefore s = 57^\circ 41'$$

(2) A A j E o p A i l o j O 1/2 o A A o , u A A o j A A o A j i A A j o ,
 « D A 1/2 i 252 A o S A S A i n l p A i o E i l o
 j O 1/2 o « U j A i o A E o D j i n E O i l o .

4.3.9.9 ĐòÄì ÷ Çì Äì ý Û ÄÉì Èì Ì 98Äð¼ ÷ ±ý Û ò Ó, òð §Ä, òð¼ý (muzzle velocity) ±ð¼ç ðÄç ò Ì ñ ÷¼î Ìð¼ç, « ð 840 Äð¼ ÷ ÷¼ì ÷ ÄÄç, 90 Äð¼ ÷ - ÄÄç Û Ç ò §, ÷ Äð¼ý ÷ î ðÄç ÷ Äì ÷ ÄðÈÖì Ì ò μ ÷ þÄì ÷, « Èì Ì ò ±Éì ÷ ÷ ñ ÷. Äí Äì ÷¼Äý ðÄý Äì Ì

$$y = x \tan r - \frac{gx^2}{2v_0^2 \cos^2 r}$$



Ä¼ç 4-3-22

Ä¼ç (4.3.22)-ð ÷ ðÈÄÄì Û, P(840,90) ò Û Ç Äì ÷¼Äç ÷ Û Ç¼ì ç,

$$90 = 840 \tan r = \frac{9.8 \times 840 \times 840}{2 \times 98 \times 98 \times \cos^2 r}$$

« ÷¼ì Äð, $90 = 840 \tan r - 360(1 + \tan^2 r)$

« ÷¼ì Äð, $3 = 28 \tan r - 12(1 + \tan^2 r)$

« ÷¼ì Äð,

$$12 \tan^2 r - 28 \tan r + 15 = 0;$$

$$\therefore \tan r = \frac{28 \pm \sqrt{28 \times 28 - 4 \times 12 \times 15}}{24};$$

$$= \frac{28 \pm 8}{24};$$

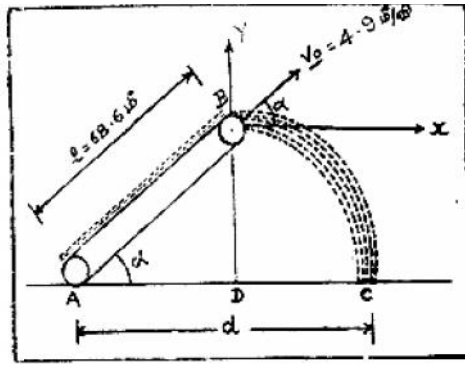
$$\therefore \tan r = \frac{36}{24} \ll \text{ðÄð} \frac{20}{24}$$

$$\frac{3}{2} \ll \text{ðÄð} \frac{5}{6}$$

$$r = \tan^{-1}\left(\frac{3}{2}\right) \ll \text{ðÄð} \tan^{-1}\left(\frac{5}{6}\right)$$

$$= 56^\circ 19' \ll \text{ðÄð} 39^\circ 48'$$

4.3.9.10 þÖ þ ÷¼Äì É Ì Ä ÷ Çý ÷ î ð ÷ Ç - Äì öóð ÷ ðÖÄì Û ò Äóð ±ÈÄóÄì ý Èð. Ó¼ç Ì Ä ÷ "a" - ÄÄç Û Ç¼ì Öò, ±È¼ì É ò¼ç ÄÖóð "b" ÷¼ì ÷ ÄÄç ÷ Û Çð. þñ ÷¼ì Äð Ì Ä ÷ "b" - ÄÄç ÷¼Ä¼ì Öò ±È¼ì É ò¼ç ÄÖóð "a" ÷¼ì ÷ ÄÄç ÷ Û Çð. Äó¼ý Äì ÷¼ þÖ Ì Ä ÷ Û Ì ò §ç ÷ Ì ò¼ì É



À¼õ 4-3-26

B - A - l - 68.6 m, B - A - y - U - o - A - C - l - E - o, x - y « - i - C - x - o - u - . AB - y - U - o - A - C - l - E - o, r - y - U - o - s - i - 1/2 - i - o - i - c - A - o - A - u - u - C - 3/4 - i - i - u - . « - o - S - A - D, 3/4 - i - E - A - A - 1/2 - u - u - A - y - U - o, B - A - A - O - o - D, v_0 - y - U - o - 3/4 - o - S - A - o - 3/4 - o - o, r - y - U - o - ± - E - S - i - 1/2 - o - 3/4 - o - o - A - u - U - p - A - i - l - E - D. 3/4 - i - E - A - o - 3/4 - y - C - 1/4 - o - 3/4 - o - A - A - i - o

x = y_0 cos r t ± y - U - o - A - y - A - i - o - 1/4 - i - o - A - A - U - i - o - A - i - o.

3/4 - i - E - A - o - B - A - A - O - o - D - C - A - « - 1/4 - A - ± - l - o - 3/4 - S - A - o - t - ± - E - o

$$DC = d - l \cos r = v_0 \cos r t - l$$

$$\therefore \cos r = \frac{d}{l + v_0 t}$$

3/4 - i - E - A - o - 3/4 - y - C - A - i - l - o - D - o - 3/4 - o - A - o - p - A - i - o

$$v_0 \sin r t - \frac{1}{2} g t^2$$

± y - U - o - A - y - A - i - o - 1/4 - i - o - A - A - U - i - o - A - i - o

$$BD = -l \sin r = v_0 \sin r t - \frac{1}{2} g t^2$$

$$\therefore \sin r = \frac{g t^2}{2(l + v_0 t)}$$

$$\sin^2 r + \cos^2 r = 1 \pm y - A - 3/4 - o - A - A - y - A - i - o - 3/4$$

$$d^2 = (l + v_0 t)^2 - g^2 t^4 - l^2 \mp l \cdot o.$$

d - - E - D - t - A - y - o - i - A - A - E - i - C - E - D.

$$p - i - l = 68.6 \text{ m}$$

$$v_0 = 4.9 \text{ m/s}$$

$$g = 9.8 \text{ m/s}^2$$

$$\therefore d^2 = (68.6 + 4.9t)^2 - \frac{(9.8)^2}{4} t^4$$

$$= (49)^2 ((4 + t)^2 - t^4)$$

(ii) $\tan^{-1} \frac{v_0}{v_0} = \frac{v_0}{v_0} = 1 \Rightarrow \theta = 45^\circ$

(iii) $s = 41.8'$

4.3.10.9 $\frac{1}{2}gt^2 = \frac{1}{2}v_0^2 \Rightarrow t = \frac{v_0}{g}$. $s = v_0 t = \frac{v_0^2}{g}$. $v_0 = \sqrt{2gh}$. $s = \frac{2gh}{g} = 2h$. $h = \frac{s}{2} = \frac{41.8}{2} = 20.9'$

$$\left[\frac{1}{2}gt^2 = \frac{1}{2}v_0^2, x = v_0 t, v = \sqrt{v_0^2 - 2gh}, \theta = \tan^{-1} \left(\frac{2gh}{v_0^2} \right) \right]$$

4.3.10.10 $\frac{1}{2}gt^2 = \frac{1}{2}v_0^2 \Rightarrow t = \frac{v_0}{g}$. $s = v_0 t = \frac{v_0^2}{g}$. $v_0 = \sqrt{2gh}$. $s = \frac{2gh}{g} = 2h$. $h = \frac{s}{2} = \frac{41.8}{2} = 20.9'$

(iii) $v_0 = 108.5$ ft/sec $r = 45^\circ$

4.3.10.11 $\frac{1}{2}gt^2 = \frac{1}{2}v_0^2 \Rightarrow t = \frac{v_0}{g}$. $s = v_0 t = \frac{v_0^2}{g}$. $v_0 = \sqrt{2gh}$. $s = \frac{2gh}{g} = 2h$. $h = \frac{s}{2} = \frac{41.8}{2} = 20.9'$

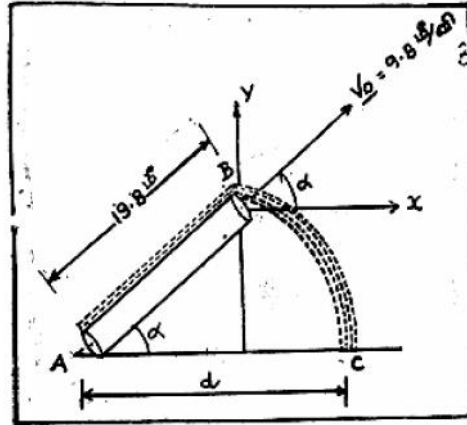
4.3.10.12 $\tan^{-1} \left(\frac{3}{4} \right) \Rightarrow \theta = 36.87^\circ$. $\frac{1}{2}gt^2 = \frac{1}{2}v_0^2 \Rightarrow t = \frac{v_0}{g}$. $s = v_0 t = \frac{v_0^2}{g}$. $v_0 = \sqrt{2gh}$. $s = \frac{2gh}{g} = 2h$. $h = \frac{s}{2} = \frac{41.8}{2} = 20.9'$

(iii) $s = 34.293$ ft

4.3.10.13 $\frac{1}{2}gt^2 = \frac{1}{2}v_0^2 \Rightarrow t = \frac{v_0}{g}$. $s = v_0 t = \frac{v_0^2}{g}$. $v_0 = \sqrt{2gh}$. $s = \frac{2gh}{g} = 2h$. $h = \frac{s}{2} = \frac{41.8}{2} = 20.9'$

$$\left(\frac{1}{2}gt^2 = \frac{1}{2}v_0^2 \Rightarrow \theta = \tan^{-1} \left(\frac{3}{4} \right) \right)$$

4.3.10.14 $\frac{1}{2}gt^2 = \frac{1}{2}v_0^2 \Rightarrow t = \frac{v_0}{g}$. $s = v_0 t = \frac{v_0^2}{g}$. $v_0 = \sqrt{2gh}$. $s = \frac{2gh}{g} = 2h$. $h = \frac{s}{2} = \frac{41.8}{2} = 20.9'$



À¼õ 4-3-28

($g = 9.8 \text{ Áf}(\text{ÁÉ} \text{ j} \text{ Ê})^2 \pm \text{É} \text{ ì } \text{ñ} \text{ } \text{.}$)

($\text{Á} \text{ } \text{¼} Td = 33.94 \text{ Áfr} = 30^\circ$)

4.3.10.15 Ð, ù ´ýËý þÁì ò´ ¼ $x = t^2 + 5t, y = t^3 - 8t^2 + 2$ ±ýÁ´ Á « ÈÁÏ ÿËË (x,y ÁÐ¼÷ « ÇÁÖö t ÁÉjÊÁÖö « ÇÁ¼öÁÏ ÿËË) $t = 2$ ÁÉjÊÁì ÿ ùÇŞÁjÐ Ð, Çÿ ¼´ °ŞÁ ò ÁüÜö ÓÍ ì ò ÿ ÿÁü´ Èð ¼ÉÁjÉÏ, ×ö.

($\text{Á} \text{ } \text{¼} V = 21.932 \text{ m/s}; \alpha = 65.77^\circ$
 $a = 4.472 \text{ m/s}^2; \beta = 63.44^\circ$)

4.3.10.16 Ð, ù ´ýÚ $N = 20t^2 - 100t + 50$ ±ýË ¼´ °ŞÁ ò¼ö þÁí ì ÿÈÐ. ÓÍ ì ò ÿ ÿÁü´ Èð ¼ö¼ö¼ö « òjÁjÖÇÿ ¼´ °ŞÁ ò ±ýË? ($\text{Á} \text{ } \text{¼} V = 75 \text{ m/s}^2$)

4.3.10.17 Ð, ù ´ýËý þ¼öjÁÁ÷í ° $s = 2t^3 - 30t^2 + 100t - 50, v = 0$ ±ýÚüÇ ŞÁjÐ ŞjÄð´ ¼ (t) ¼ÉÁjÉÏ.

4.3.13.18 s « í ° ÖjÁjÖü þÁí ì öŞÁjÐ « ¼ý ¼´ °ŞÁ ò $N = 2 + 5t^{3/2}$ ±É t=4 ±ýÚüÇŞÁjÐ, þ¼öjÁÁ÷í °(s) ¼´ °ŞÁ ò(v) ÁüÜö ÓÍ ì ò(a) ÿ ÿÁü´ Èì ñ Èì.

($\text{Á} \text{ } \text{¼}: s = 72 \text{ Áf}, v = 42 \text{ Áf}(\text{ÁÉ} \text{ j} \text{ Ê}), a = 15 \text{ Áf}(\text{ÁÉ} \text{ j} \text{ Ê})^2$)

4.3.10.19 x-y ¼ö¼ö, Ð, Çÿ ¼´ °Áç´ Ä ŞjÄö $t = 3.60$ ÁÉjÊ ±ýÚüÇŞÁjÐ $(2.76i - 3.28j)$ Áf $t = 3.62$ ÁÉjÊ ±ýË ¼ö¼ö¼ö "¼´ °Áç´ Ä þüÁ´ ¼jÁçÁö Ð, Çÿ °Áj °ç ŞÁ ò¼ý ÁÖÁ´ ÉÖö, « Ð x « í¼ý ²üÁ òÐö Şj¼ö « Ç´ Á´ Áöö ÿñ.

($\text{Á} \text{ } \text{¼}: N = 2.92 \text{ Áf}(\text{ÁÉ} \text{ j} \text{ Ê}) \theta = -59^\circ$)

4.3.10.20 $\vec{v} = 0.4 \hat{r} - \hat{\theta}$ $\vec{a} = \frac{1}{2} \hat{r} + \frac{1}{2} \hat{\theta}$ $\rho = 1$ $\dot{\rho} = 0$ $\dot{\theta} = 0.4$ $\ddot{\rho} = 0$ $\ddot{\theta} = 0$ $\vec{a} = -0.4 \hat{r} + 0.8 \hat{\theta}$ $a_r = -0.4$ $a_\theta = 0.8$

$$(\ddot{r} = 0; \ddot{\theta} = 0.8 \text{ rad/s}^2)$$

4.3.10.21 $\vec{v} = 240 \hat{r} - 30 \hat{\theta}$ $\vec{a} = 30 \hat{r} + 240 \hat{\theta}$ $\rho = 240$ $\dot{\rho} = 30$ $\dot{\theta} = -0.125$ $\ddot{\rho} = 30$ $\ddot{\theta} = -0.25$ $\vec{a} = 30 \hat{r} + 240 \hat{\theta}$ $a_r = 30$ $a_\theta = 240$

$$[\ddot{r} = 30; a_\theta = -2.39 \text{ rad/s}^2]$$

4.3.10.22 $\vec{v} = 15 \hat{r}$ $\vec{a} = 3 \hat{r}$ $\rho = 15$ $\dot{\rho} = 0$ $\dot{\theta} = 0$ $\ddot{\rho} = 3$ $\ddot{\theta} = 0$ $\vec{a} = 3 \hat{r}$ $a_r = 3$ $a_\theta = 0$

$$[\ddot{r} = 3; a_\theta = 0]$$

$$a_n = \frac{v^2}{\rho} = 2.025 \text{ rad/s}^2$$

$$a = 3/62 \text{ rad/s}^2$$

4.3.10.23 $y = \frac{1}{20} x^2$ $\vec{v} = x \hat{i} + y \hat{j}$ $\vec{a} = 2x \hat{i} + \hat{j}$ $\rho = \sqrt{x^2 + y^2}$ $\dot{\rho} = \frac{1}{20} x$ $\dot{\theta} = \frac{1}{20} \frac{y}{x}$ $\ddot{\rho} = \frac{1}{20}$ $\ddot{\theta} = -\frac{1}{20} \frac{y}{x^2}$ $\vec{a} = 2x \hat{i} + \hat{j}$ $a_r = 2x \cos \theta + \sin \theta$ $a_\theta = 2x \sin \theta - \cos \theta$ $a = \sqrt{(2x \cos \theta + \sin \theta)^2 + (2x \sin \theta - \cos \theta)^2}$

$$v_A = 6 \text{ rad/s}$$

$$a = 2.37 \text{ rad/s}^2$$

2

4.3.10.24 $\vec{r} = 4(1 + \sin t) \hat{r}$ $\vec{v} = 4 \cos t \hat{r} - 4 \sin t \hat{\theta}$ $\vec{a} = -4 \sin t \hat{r} - 4 \cos t \hat{\theta}$ $\rho = 4(1 + \sin t)$ $\dot{\rho} = 4 \cos t$ $\dot{\theta} = -1$ $\ddot{\rho} = -4 \sin t$ $\ddot{\theta} = 1$ $\vec{a} = -4 \sin t \hat{r} - 4 \cos t \hat{\theta}$ $a_r = -4 \sin t$ $a_\theta = -4 \cos t$

4.3.10.25 $\vec{r} = 2 + 3t^2 \hat{r}$ $\vec{v} = 6t \hat{r}$ $\vec{a} = 6 \hat{r}$ $\rho = 2 + 3t^2$ $\dot{\rho} = 6t$ $\dot{\theta} = 0$ $\ddot{\rho} = 6$ $\ddot{\theta} = 0$ $\vec{a} = 6 \hat{r}$ $a_r = 6$ $a_\theta = 0$

$$(\ddot{r} = 6; v = 26.62 \text{ rad/s})$$

$$a_n = -2343 \text{ rad/s}^2$$

$$a_t = 411 \text{ rad/s}^2$$

4.3.10.30 (a) $\vec{F} \cdot \hat{r} = ma_n \Rightarrow F \cos 14.04 - N \sin 14.04 = \frac{10}{9.81}$

$$\nearrow \sum F_n = ma_n \Rightarrow F \cos 14.04 - N \sin 14.04 = \frac{10}{9.81}$$

$$\nwarrow \sum F_r = ma_r \Rightarrow F \sin 14.04 + N \cos 14.04 = \frac{10}{9.81} a_r$$

$$a_r = \ddot{r} - r \dot{\theta}^2 = 5.25 \text{ (A} \hat{e}_r \text{)}^2$$

$$a_r = r'' + 2\dot{r}\dot{\theta} = 6 \text{ (A} \hat{e}_r \text{)}^2$$

$$\therefore F = 6.68 \text{ N}$$

$$N = 4.64 \text{ N}$$

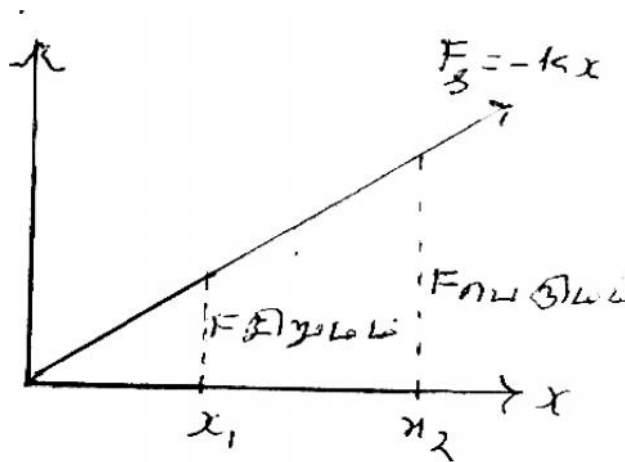
4.3.10.30 (b) $\vec{v} \cdot \hat{r} = 0$ (satellite) $\Rightarrow \dot{r} = 0$ $\Rightarrow \ddot{r} = -r \dot{\theta}^2 = -\sqrt{2gR} \dot{\theta}^2$

$$[\dot{\theta} = \sqrt{2gR}] \Rightarrow \ddot{r} = -\sqrt{2gR} \dot{\theta}^2 = -\sqrt{2gR} \dot{\theta}^2$$

$$R = \frac{v^2}{g} - \frac{v^2}{g} = 0$$

4.3.10.31 $\vec{F} = -kx \hat{i}$ $\Rightarrow \vec{v} = v \hat{i}$ $\Rightarrow \vec{a} = -\frac{k}{m} x \hat{i}$ $\Rightarrow \ddot{x} = -\frac{k}{m} x$ $\Rightarrow \int_{x_1}^{x_2} F dx = \frac{1}{2} k (x_2^2 - x_1^2)$

$$(\text{A} \hat{e}_r \text{)} \cdot \vec{F} = -kx \Rightarrow \int_{x_1}^{x_2} F dx = \frac{1}{2} k (x_2^2 - x_1^2)$$



4.3.10.32 "É « ÄöÄ:Éý" (D' Alembert) ¾ðÐÄð ÷ ¾î Û Û, ?

Äç ¼: | ÄÇŞÄÖüÇ Äç ° ü ÄüÜö - üÄç ° ü - ÄÄüÉý Äç ° ð | ¾î | ¾ç
´ Ö Ð ç Çì ° Äç ÄÄö ÷ Äð¾ÄÖî | Û Û ö ± Èì Ö¾Äî ö. | ÄÇÄç ° Çý
Äç Ç× ´ ÖÐ Çö | ° ÄöÄî ö ŞÄî Ð, äî ° Ä Ä¾ö Äö | ÄÉ; ÄÄÖî ì ö
Şç Äð¾Äö, « ðÐ ü ÞÄî ÄÄü ° Äç ÄÄö ÞÖöÄ¾î | | ü ÇöÄî ö.
Þð¾ðÐÄŞÄ "É « ÄöÄ:Éý ¾ðÐÄö" ± ý Û Û ÈöÄî ç ÈÐ.

4.3.10.33. Şç ü Û ì | Ä | ç Ççý Ä¾ç ü (Kepler's Laws of Planetary Motran) Ä; Ä?

Ä¾ç 1: ¾ÄÄ´ Èì | ÄÄÄî | | ç ñ Î Şç ü ç ç Äö¼í ç Ç Ä´ Ä çý ÈÈ.

Ä¾ç 2: ¾ÄÄ´ ÄÉ ÄÖóÐ Şç ü ç ý Èüì Ä´ ÄÄöÄî ö. - ´ Äð¾ç ° Äç ° ÄÄî É
Şç Äð¾Äö ° ÄÄî É ÄÄöÄÇ´ Ä ŞÄ Äî | ° ö ç ÈÐ.

Ä¾ç 3: Şç ü Çý ç ÄÄö¼í Çý Ä÷ì í ü « ö¾ö¾ Şç ü ´ Øì | Çý
orbits « Ä ŞÄî | ç Çý ÖöÄÉ Û ì Äç ¾ ° ÄÄî É « ÇÄö ÞÖî ÷ ¾î É.

Ä¾ç ÞÄñ Éý ÄÈ Şç ü ´ ü | Äî ý Èüì ö ÄÄöÄÇ× ŞÄ ö. (areal velocity);

$\frac{1}{2}r^2$, $\mu \div Ä; ÈÄÄî ö. ÄüÜö Şç Çö | ° ÄöÄî ö Äç ° Äçý | Û ì | | Ä Û Û
äî ° ÄÄî ö. ± ÈŞÄ Şç ü ç ý Èý ŞÄö | ° ÄöÄî ö Äç ° - ´ Äð¾ç ° Äçý
ç ÇÄî ö Èö Äöî ŞÄ | ° ÄöÄî ö. ± ÈŞÄ ÞüÄç ° ´ ÄÄÄî É Äç ° Äî ö
¾ÄÄ´ Èì ÄÄÄî | | ç ñ Î Şç ü ÞÄî | ö Ä; ¾´ Ä´ ÄÄ´ Øì | ± Èì
Û ÈöÄî ö.$

Şç Çý ŞÄö | ° ÄöÄî ö Ä÷ì ° Äç °, Şç Û ì ö ¾ÄÄÛ ì ö
Þ´ ¼öÄö¼ | ¾î ´ ÄÄý ÞÖÄÈ ¾´ Äü « ØÄÐ Şç Äî Ü Äç ¾ð¾Äö ÞÖî ÷
¾î Ð Ä¾ç-1 Þ´ ¾ð¾î ý | ¾Ç× Äî öÐ ç ÈÐ.

ÞÐŞÄ ç ä ö¼Éý ¾´ Ä ç Ä÷ì Ä¾ç (Inverse Square Law) - ì ö.

4.3.10.34 ÖÄç ŞÄüÄÄöÄÖðÐ 320 ç.ÄÈ ðÐ - ÄÄð¾ö, ¾ç ° ŞÄ ö 36,000
ç.ÄýÄ½ç - ü ÇÄî Ü Şç ü ç ý Ü ± ÈÄöÄî ç ÈÐ. (launched) ÄÞç ± ÈÄöÄî ö
Şç Äð¾Äö Şç ü ÞÄî | ö Ä; ¾, ÖÄÄý ŞÄüÄÄöÄüì Þ´ ½Äî « ´ Ä ç ÈÐ.
ÖÄÄý ŞÄüÄÄöð Şç ÇÄÉÄö - ü ÇÐ ± Èì | ç ñ Î (- Äö 640 ç.ÄÞ)

Äý ÄÖÄÄÉ Äü´ È¾ÉÄî É ç × ö

1. Şç Çý Äî ö Ä; ¾
2. ´ Øì | Şç Äö (Orbital time)
3. ¾öÄöÐì | ç ü Ü ö ¾ç ° ° ŞÄ ö
4. Äö¼ | Äî Øì | Ä¾ç ° ° ŞÄ ö.

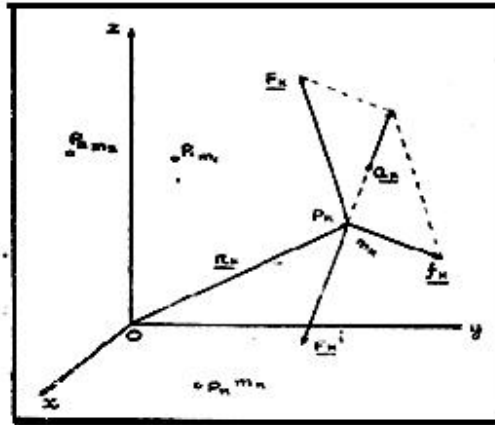
4.3.10.35 ´ Ö Şç ö Èö ÞÄî | ö ÄüÜö ´ ŞÄ ç Äî Ü ´ ¼Ä ç Äî É Ä ç ° ç ç °
ÞÄî | ç ü ÞÄñ Éý Äç Ç× ´ Ö ç Äî É Ä ç ° ç ç ° ÞÄî | ÄÉ ç ÇÜ × ç.

ç Ð ç | Ø } ÞÄü´ ç Çö ç ÞÄü´ Èö´ ¼Ä ÄÜ ç ý Ü « ¾ý
ç ì ö ö ç Äö¼öüç ç ç Èö´ ¼Ä ´ ÖÐ ç ç | ç ñ Î ç ÇÐ. « ¾ý ÞÄü´
ç Çö¾üì ÞÖÄ¼í |, « ¾ý ÑÈç´ ç ç ÄÄî ´ ÄöÐ ç ÈÈ, « ¾´ È ´ Ö

4.3.10.41 $r \sim \dots \tilde{A} \tilde{O} \dots \frac{1}{4} \tilde{A} \ll \dots \tilde{A} \tilde{i} \tilde{S} \dots \tilde{C} \tilde{o} \frac{3}{4} \tilde{y} \tilde{A} \tilde{D} \ll \dots \tilde{A} \tilde{i} \tilde{S} \dots \tilde{C} \tilde{o} \frac{3}{4} \tilde{y} \ll \tilde{S} \frac{3}{4} \tilde{A} \tilde{D} \frac{1}{4} \ll \tilde{E} \tilde{A} \tilde{D} \sim \dots \tilde{A}, h \sim \tilde{A} \tilde{A} \tilde{O} \dots \frac{1}{4} \tilde{A} \sim \tilde{O} \tilde{A} \tilde{D} \frac{1}{4} \times \tilde{O} \tilde{D} \dots \frac{1}{4} \tilde{i} \dots \tilde{i} \tilde{n} \frac{1}{4} \circ \tilde{A} \tilde{i} \tilde{E} \ll \frac{1}{4} \div \tilde{o} \frac{3}{4} \tilde{O} \dots \frac{1}{4} \tilde{A} \frac{3}{4} \tilde{n} \tilde{A} \tilde{o} \sim \tilde{y} \tilde{U} \dots \tilde{o} \tilde{A} \tilde{o} \tilde{A} \tilde{D} \tilde{E} \tilde{O} \tilde{i} \tilde{D} \tilde{E} \tilde{D}. n = h\sqrt{2} \pm \tilde{y} \tilde{U} \tilde{p} \tilde{O} \tilde{o} \tilde{A} \tilde{y} \ll \dots \tilde{A} \tilde{i} \tilde{S} \dots \tilde{C} \tilde{o} \frac{3}{4} \tilde{y} \tilde{O} \tilde{E} \tilde{o} \tilde{A} \tilde{A} \tilde{o} \tilde{D} \dots \tilde{C} \frac{1}{4} \tilde{o} \frac{3}{4} \tilde{C} \tilde{o} \dots \frac{3}{4} \tilde{o} \dots \frac{3}{4} \tilde{i} \tilde{D} \tilde{I} \pm \tilde{o} \tilde{C} \dots \tilde{A} \tilde{A} \tilde{C} \tilde{O} \tilde{o} \circ \tilde{A} \tilde{C} \dots \tilde{A} \tilde{A} \tilde{C} \tilde{O} \tilde{i} \tilde{I} \dots \tilde{A} \tilde{E} \tilde{i} \dots \tilde{i} \tilde{D} \tilde{I} \dots$

4.3.10.42 $\tilde{O} \dots \tilde{o} \tilde{i} \tilde{l} \tilde{o} \tilde{D} \tilde{i} \tilde{S} \dots \tilde{D} \tilde{E} \tilde{o} \tilde{p} \tilde{o} \tilde{A} \tilde{i} \frac{3}{4} \tilde{p} \tilde{O} \tilde{D} \tilde{u} \tilde{C} \tilde{U} \tilde{i} \tilde{C} \dots \frac{1}{4} \tilde{A} \tilde{C} \tilde{o} \tilde{D} \tilde{A} \tilde{C} \circ \tilde{o} \tilde{A} \tilde{i} \tilde{o} \tilde{C} \tilde{D} \frac{1}{4} \tilde{p} \tilde{A} \tilde{A} \tilde{i} \frac{3}{4} \circ \tilde{A} \tilde{i} \tilde{E} \tilde{A} \tilde{C} \tilde{U} \sim \tilde{y} \tilde{U} \dots \frac{3}{4} \tilde{i} \tilde{l} \tilde{D} \tilde{E} \tilde{D}. \ll \tilde{D} \dots \tilde{i} \tilde{u} \tilde{U} \tilde{o} \tilde{A} \tilde{A} \tilde{y} \dots \tilde{i} \div \tilde{E} \tilde{C} \tilde{A} \tilde{y} \circ \tilde{A} \tilde{y} \tilde{A} \tilde{i} \tilde{o} \dots \frac{1}{4} \tilde{i} \dots \tilde{i} \tilde{n} \dots \tilde{N} \tilde{E} \tilde{C} \dots \tilde{C} \sim \tilde{y} \tilde{U} \tilde{S} \circ \tilde{o} \tilde{D} \tilde{o} \tilde{I} \tilde{o} \tilde{A} \tilde{i} \tilde{I} \tilde{a} \sim \dots \tilde{A} \tilde{A} \tilde{D} \frac{1}{4} \dots \tilde{o} \tilde{A} \tilde{A} \tilde{D} \dots \tilde{o} \tilde{A} \tilde{A} \tilde{y} \tilde{a} \tilde{y} \tilde{E} \tilde{o} \tilde{p} \tilde{O} \tilde{A} \tilde{i} \tilde{l} \tilde{A} \tilde{i} \dots \tilde{o} \frac{3}{4} \tilde{o} \dots \frac{3}{4} \tilde{i} \tilde{I} \tilde{o} \tilde{A} \tilde{E} \dots \frac{3}{4} \tilde{i} \tilde{l} \tilde{o}$

$$\circ \tilde{i} \dots \tilde{A} \tilde{C} \sim \tilde{y} \tilde{E} \tilde{y} \tilde{C} \tilde{C} \tilde{o} a \left[\frac{3}{\log(2+\sqrt{3})} + \frac{4f}{3} \right] \pm \tilde{E} \tilde{i} \dots \tilde{i} \tilde{D} \tilde{I} \dots$$



Билд 4-4-1

K- \rightarrow $\hat{A}D$ \hat{D}_s $\hat{C}\hat{y}$ $\hat{S}\hat{A}\hat{\emptyset}$ | $\hat{A}\hat{u}\hat{A}\hat{I}$ \hat{o} $\hat{D}\hat{E}\hat{A}\hat{C}$ \hat{o}_s \hat{u} , $\hat{u}\hat{A}\hat{C}$ \hat{o}_s \hat{u} \rightarrow $\hat{C}\hat{A}\hat{u}\hat{E}\hat{C}\hat{y}$
 $\hat{A}\hat{C}$ $\hat{C}\times$ $\hat{A}\hat{C}$ \hat{o}_s \hat{C} \hat{O} $\hat{E}\hat{S}\hat{A}$ $\underline{F}_k, \underline{f}_k \pm \hat{E}\hat{i}$ | \hat{s} | \hat{u} . « $\hat{D}\hat{D}_s$ $\hat{C}\hat{y}$ $\hat{O}\hat{I}$ \hat{i} \hat{o} \hat{t}_k \rightarrow $\hat{E}\hat{D}$
 $\underline{F}_k, \underline{f}_k = m_k \hat{t}_k \pm \hat{y}$ $\hat{U}\hat{o}$ $\hat{O}\hat{A}\hat{y}\hat{A}_i \hat{\emptyset} \hat{y}_i \hat{\emptyset}$ \hat{A} $\hat{A}\hat{u}\hat{i}$ \hat{o} $\hat{A}\hat{I}$ \hat{o} .

$\underline{F}_k = -m_k \hat{t}_k \pm \hat{E}\hat{i}$ | \hat{s} | \hat{u} . « $\hat{o}\hat{S}\hat{A}_i \hat{D}$ K- \rightarrow $\hat{A}D$ \hat{D}_s $\hat{C}\hat{y}$ $\hat{p}\hat{A}\hat{i}$ \hat{o} $\hat{y}_i \hat{u}\hat{i}$ | \hat{A}
 $\hat{O}\hat{A}\hat{y}\hat{A}_i \hat{I}$ $\underline{F}_k + \underline{f}_k + \underline{F}_k' = 0$ (1) \rightarrow \hat{I} \hat{o}

$\hat{p}\hat{i}$ \hat{I} $\underline{F}_k' = -m_k \hat{a}_k \pm \hat{y}$ $\hat{A}D$ K- \hat{D}_s $\hat{C}\hat{y}$ $\hat{S}\hat{A}\hat{\emptyset}$ | $\hat{A}\hat{u}\hat{A}\hat{I}$ \hat{o} \hat{o} $\hat{y}_i \hat{D}\hat{A}$
 $\hat{A}\hat{C}$ $\hat{O}\hat{A}_i \hat{I}$ \hat{o} . (Inertia force) (1)- \rightarrow $\hat{A}D$ $\hat{O}\hat{A}\hat{y}\hat{A}_i \hat{\emptyset}\hat{E}\hat{y}$ $\hat{A}\hat{A}\hat{o}\hat{D}\hat{E}\hat{o}$ $\hat{a}\hat{i}$ $\hat{O}\hat{A}\hat{A}_i \hat{A}_i \hat{\emptyset}$,
 $\underline{F}_k, \underline{f}_k, \underline{F}_k' \pm \hat{y}$ $\hat{U}\hat{o}$ $\hat{A}\hat{C}$ \hat{o}_s \hat{u} , « $\hat{D}\hat{D}_s$ \hat{C} $\hat{p}\hat{A}\hat{i}$ \hat{s} $\hat{A}\hat{C}$ $\hat{O}\hat{A}\hat{u}$ $\hat{O}\hat{A}_i \hat{C}$ $\hat{A}\hat{A}\hat{\emptyset}$
 $\hat{A}\hat{O}\hat{A}_i \hat{s}$ \hat{I} \hat{o} $\hat{O}\hat{y}_i \hat{A}\hat{I}$ \hat{o} .

$\hat{S}\hat{A}\hat{O}\hat{o}$, $\pm \hat{y}$ $\hat{U}\hat{o}$ | $\hat{y}_i \hat{y}_i$ \hat{o} $\hat{D}\hat{u}\hat{C}\hat{C}$ $\hat{A}\hat{u}\hat{E}\hat{C}$, « $\hat{u}\hat{A}\hat{C}$ \hat{o}_s $\hat{C}\hat{y}$ $\hat{y}_i \hat{O}\hat{o}\hat{D}$
 $\hat{y}_i \hat{E}\hat{i}$ \hat{s} $\hat{C}\hat{i}$ $\hat{y}_i \hat{I}$ \hat{o} $\hat{S}\hat{A}_i \hat{D}$, $\underline{r}_k \wedge \underline{F}_k + \underline{r}_k \wedge \underline{f}_k + \underline{r}_k \wedge \underline{F}_k' = 0$(2) \rightarrow \hat{I} \hat{o} .

$\hat{S}\hat{A}\hat{u}\hat{U}_i \hat{A}$ (1), (2) - $\pm \hat{y}$ $\hat{U}\hat{o}$ $\hat{O}\hat{A}\hat{y}\hat{A}_i \hat{I}$ \hat{u} , | $\hat{y}_i \hat{I}$ $\hat{y}_i \hat{A}\hat{O}\hat{u}\hat{C}$ \hat{u} | $\hat{A}_i \hat{O}$ \hat{D} $\hat{U}\hat{i}$ \hat{o}
 $\hat{A}_i \hat{O}\hat{D}\hat{A}_i \hat{A}_i \hat{\emptyset}$, « $\hat{I}\hat{O}\hat{A}\hat{y}\hat{A}_i \hat{I}$ $\hat{C}\hat{y}$ \hat{I} $\hat{E}\hat{C}\hat{A}\hat{u}$ $\hat{U}\hat{o}\hat{I}$ \hat{o} | \hat{y}_i \hat{s} $\hat{U}\hat{o}$
 $\hat{a}\hat{i}$ $\hat{O}\hat{A}\hat{A}_i \hat{I}$ \hat{o} .

« $\hat{y}_i \hat{A}D$, $\sum_{k=1}^n (\underline{F}_k + \underline{f}_k + \underline{F}_k') = 0$,

« $\hat{y}_i \hat{A}D$, $\sum_{k=1}^n \underline{F}_k + \sum_{k=1}^n \underline{f}_k + \sum_{k=1}^n \underline{F}_k' = 0$(3)

$\sum_{k=1}^n \underline{f}_k \pm \hat{y}$ $\hat{A}D$ $\hat{u}\hat{A}\hat{C}$ \hat{o}_s $\hat{C}\hat{y}$ | $\hat{y}_i \hat{I}$ $\hat{A}\hat{A}$ $\hat{E}\hat{i}$ \hat{I} $\hat{E}\hat{C}\hat{A}_i \hat{\emptyset}$, « \hat{y} $\hat{A}\hat{A}\hat{O}\hat{D}$
 $\hat{a}\hat{i}$ $\hat{O}\hat{A}\hat{A}_i \hat{I}$ \hat{o} , $\hat{S}\hat{A}\hat{O}\hat{o}$ $\sum_{k=1}^n \underline{F}_k = R \pm \hat{y}$ $\hat{A}\hat{y}_i \hat{\emptyset}$, (3)- $\hat{A}D$ $\hat{O}\hat{A}\hat{y}\hat{A}_i \hat{I}$,

$$\underline{R} + \sum_{k=1}^n \frac{F_k}{k} = 0$$

$$\ll \frac{3}{4} \text{Å} \text{Đ} \cdot \underline{R} - \sum_{k=1}^n m_k \underline{a}_k = 0 \quad \neg \text{İ} \text{õ}.$$

$$\text{Ş} \text{Ä} \text{Ö} \text{õ} \sum_{k=1}^n \underline{r}_k \wedge (\underline{F}_k + \underline{f}_k + \underline{F}_k') = 0 \quad \neg \text{İ} \text{õ}.$$

$$\ll \frac{3}{4} \text{Å} \text{Đ} \sum_{k=1}^n \underline{r}_k \wedge \underline{F}_k + \sum_{k=1}^n \underline{r}_k \wedge \underline{f}_k + \sum_{k=1}^n \underline{r}_k \wedge \underline{F}_k' = 0$$

$$\ll \frac{3}{4} \text{Å} \text{Đ} \sum_{k=1}^n \underline{r}_k \wedge \underline{F}_k + \sum_{k=1}^n \underline{r}_k \wedge \underline{F}_k' = 0$$

$$\ll \frac{3}{4} \text{Å} \text{Đ} \underline{M}_o - \sum_{k=1}^n \underline{r}_k \wedge m_k \underline{a}_k = 0 \dots \dots \dots (5) \quad \neg \text{İ} \text{õ}.$$

$$(4) \text{ Å} \text{Đ} \text{ °} \text{Á} \text{ý} \text{À} \text{İ} \text{ ð} \text{È} \text{ø}, - \sum_{k=1}^n m_k \underline{a}_k \pm \text{ý} \text{Å} \text{Đ},$$

$\frac{1}{4} \text{ð} \text{Đ} \text{Ä} \text{ Å} \text{ ¸} \text{ Ç} \text{ý} \text{ Å} \text{ ¸} \text{ Ç} \text{Ä} \text{İ} \text{ ð} \neg \text{Ş} \text{Ä} \text{,} \text{Đ} \text{ ð} \text{İ} \text{¼} \text{İ} \text{¼} \text{Ä} \text{ø} \text{İ} \text{°} \text{Ä} \text{ü} \text{Ä} \text{İ} \text{ ð} \text{ ð} \text{È} \text{ Å} \text{ ¸} \text{ Ç} \text{ý} \text{ Å} \text{ ¸} \text{ Ç} \text{×} \text{ Å} \text{ ¸} \text{ °} \text{Ö} \text{õ}, \ll \text{ ð} \text{İ} \text{¼} \text{İ} \text{¼} \text{Ä} \text{İ} \text{İ} \text{Ç} \text{Ä} \text{ °} \text{¼} \text{ð} \text{Đ} \text{Ä} \text{ Å} \text{ ¸} \text{ Ç} \text{ý} \text{ Å} \text{ ¸} \text{ Ç} \text{×} \text{ø} \text{Ş} \text{°} \text{÷} \text{ø} \text{Đ} \text{,} \text{Đ} \text{ ð} \text{İ} \text{¼} \text{İ} \text{¼} \text{Ä} \text{ ¸} \text{Ä} \text{ þ} \text{Ä} \text{İ} \text{,} \text{þ} \text{Ä} \text{ø} \text{ °} \text{Ä} \text{¸} \text{ ¸} \text{Ä} \text{Ä} \text{ø} \text{ ¸} \text{Ä} \text{ð} \text{¼} \text{Ö} \text{İ} \text{İ} \text{ ð} \pm \text{ý} \text{Å} \text{Đ} \text{İ} \text{Ä} \text{È} \text{ö} \text{Ä} \text{İ} \text{ ð} \text{ þ} \text{Đ} \text{Ş} \text{Ä} \text{,} \text{Đ} \text{ ð} \text{İ} \text{¼} \text{İ} \text{¼} \text{Ä} \text{İ} \text{É} \text{¼} \text{Ä} \text{ö} \text{Ä} \text{İ} \text{ ð} \text{È} \text{ý} \text{¼} \text{ð} \text{Đ} \text{Ä} \text{Ä} \text{İ} \text{ ð}$
 (4) (5) $\neg \text{Å} \text{Đ} \text{ °} \text{Á} \text{ý} \text{À} \text{İ} \text{ ð} \text{È} \text{Ä} \text{ ¸} \text{ü}, \text{ ð} \text{È} \text{Ä} \text{ ¸} \text{ü}, \text{¼} \text{ð} \text{Đ} \text{Ä} \text{ Å} \text{ ¸} \text{ü} \neg \text{Ç} \text{Ä} \text{ ¸} \text{Ä} \text{ ð} \text{ ð} \text{İ} \text{¼} \text{İ} \text{¼} \text{Ä} \text{ø} \text{İ} \text{°} \text{Ä} \text{ü} \text{Ä} \text{ö} \text{İ} \text{ «} \text{ ð} \text{İ} \text{¼} \text{İ} \text{¼} \text{Ä} \text{ ¸} \text{Ä} \text{ þ} \text{Ä} \text{İ} \text{,} \text{þ} \text{Ä} \text{ø} \text{ °} \text{Ä} \text{¸} \text{ ¸} \text{Ä} \text{Ä} \text{ø} \text{ ¸} \text{Ä} \text{ð} \text{¼} \text{Ö} \text{İ} \text{İ} \text{ ð} \pm \text{ý} \text{Å} \text{Đ} \text{¼} \text{İ} \text{Ä} \text{Ç} \text{ö} \text{Ä} \text{İ} \text{ ð} \text{Đ} \text{,} \text{ý} \text{È} \text{É} \text{.} \ll \text{Ä} \text{ü} \text{È} \text{ý} \text{ ±} \text{ñ} \text{¼} \text{ð} \text{Ä} \text{,} \text{Ç} \text{×} \text{,} \text{Ç} \text{ö} \text{ö}, \text{Ä} \text{ý} \text{Ä} \text{ö} \text{Ä} \text{İ} \text{Ü} \text{İ} \text{Ä} \text{È} \text{Ä} \text{İ} \text{ ð}.$

$$\underline{R}_k - \sum m_k \underline{a}_k = 0 \pm \text{ý} \text{Å} \text{Đ},$$

$$R_x - \sum_{k=1}^n m_k \frac{d^2 x_k}{dt^2} = 0; R_y - \sum_{k=1}^n m_k \frac{d^2 y_k}{dt^2} = 0; R_z - \sum_{k=1}^n m_k \frac{d^2 z_k}{dt^2} = 0$$

$\pm \text{ý} \text{Ü} \text{õ} \text{ ä} \text{ý} \text{Ü} \pm \text{ñ} \text{¼} \text{ð} \text{°} \text{Á} \text{ý} \text{À} \text{İ} \text{ ð} \text{È} \text{ Ç} \text{Ä} \text{ ¸} \text{Ä} \text{Ü} \text{İ} \text{,} \text{ý} \text{È} \text{É}.$

$$\ll \text{ü} \text{Ä} \text{İ} \text{Ş} \text{È} \underline{M}_o - \sum m_k \underline{r}_k \wedge \underline{a}_k = 0 \pm \text{ý} \text{Å} \text{Đ} \underline{M}_{o,x} \underline{i} + \underline{M}_{o,y} \underline{j} + \underline{M}_{o,z} \underline{k} - \sum m_k$$

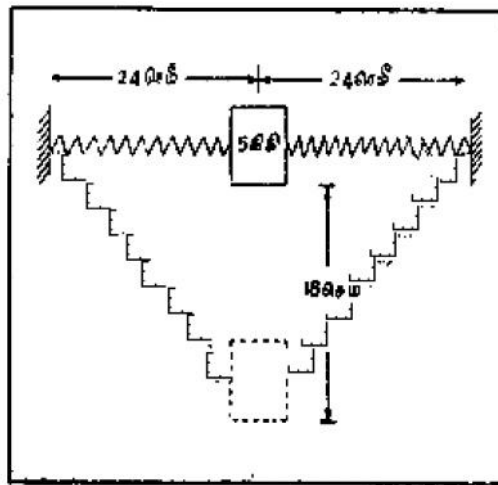
$$\begin{pmatrix} \underline{i} & \underline{j} & \underline{k} \\ xk & yk & zk \\ \frac{d^2 x_k}{dt^2} & \frac{d^2 y_k}{dt^2} & \frac{d^2 z_k}{dt^2} \end{pmatrix} = 0,$$

"ŞA'' Ä-üÈø" Ş, j ðÄ; ðËýÄË,

$$\frac{1.25v_A^2}{9.8 \times 4} = 30$$

$$\therefore v_A = 3.068 \text{ ÅÏÄË j Ë}$$

4.4.4.2 5 ŞÄ; Ä; ð ± ¼ÛÇ |Ä; Õ; ÇýÚ þ Õ ¾ÛÏ î Í ÕüÄø ü Ä; ½î ðÄøÏ ÛÇË. Ä¼ø 4.4.3ø j ðËÄÄ; Ú, Í ÕüÄø ü Ç ¼Ä; ÛÇŞÄ; ð « ð |Ä; Õü µö×ç ÄÄÄÛóð ÄÏ Äü ðÄÏ ÇË. |¾; ¼î ð¾ø Û; Ä; ýÚø 2, Ç, Ç þøÄ; ° Äø |ÄüÜüÇð, « ð |Ä; ÕÇ; Ëð 18 {[10⁻²]Ş} |¾; Ä× üŞç; ì ç þÄí Ì øŞÄ; ð, « ¾ý ¾ç °ŞÄ; ð ¾î ç; ñ. Í ÕüÄø Û; Ä; ýÚø k=0.5, Ç, Ç / {[10⁻²]Ş} ±ý Ûø ÄøÄ; ÈÄ; Äø |ÄüÜüÇ¾; ì | ç; Û.



Ä¼ø 4-4-3

ç ÄÄø ¾ÛÏ î Í ÕüÄø Û; Ä; ýÈÛø x₁ |°ÄË « Ç× çðø 2üÄÏ ÇË¾ËË T = kx₁; 2 = 0.5x₁; x₁ = 4 {[10⁻²]Ş} |Ä; ÕÇ; Ëð 18 |°ÄË {[10⁻²]Ş} üŞç; ì ç ðÄí ÄüŞÏç, ¾ÛÏ î Í Õü Û; Ä; ýÈÛø 2üÄø¼ çðø Ä x₃ |°ÄË ±Ë × ø x₂ = √(24² + 18² - 20) = 10 {[10⁻²]Ş} ±Ë × ø |Ä; ÕÇý ¾ç °ŞÄ; ð ¾î ç; ñ v |°ÄËÄË j Ë ±Ë × ø ç; Û. ±Ë ŞÄ ¾ÛÏ î Í Õü Û; Ä; ýÚø |°ö¾ŞÄ'' Ä = ½k(x₁² - x₃²) = -21, Ç, Ç {[10⁻²]Ş}.

$$5, Ç, Ç ± ¼ÛÇ |Ä; Õü |°ö¾ ŞÄ'' Ä = 5 \times 18 = 90, Ç, Ç |°ÄË {[10⁻²]Ş}$$

$$\therefore v_{1-2} \text{ Ä; °, Ç; Ë ððø |°ö¾ ŞÄ'' Ä} = 2 \times (-21 + 90) = 48, Ç, Ç {[10⁻²]Ş}$$

$$\text{þÄí } \text{üÈø Ä; üÈø} = \frac{1}{2} \times \frac{5}{981} \times v^2 - 0 = \frac{5}{1962} v^2$$

±y Ū ò šžÄð¼ø p₁, p₂ ±y Ū ò , ð'' ¼, ū (a₁, y₁)(a₂, y₂) ±y Ū Á¼í , Çç Ä'' ÁÄ¼j, ì | , j Ū .

dt ±y Ū ò Äç, î ò ÈÄ šžÄð¼ø dw ±y Ū ò ' Ö ò ÈÄ š, j ½ p¼ð | ÄÄ:î ò ç ²üÄî ò šÄjÐ,

dy₁ = a₁dw, dy₂ = -a₂dw ±y Ū ò p¼ð | ÄÄ:î ò ç , ð'' ¼, ū Ó'' ÈšÄ šžžjì , Öð, šÄøšžjì , Öð | ÄÚ , çÝ ÈÉ.

$$\therefore \frac{dy_1}{dt} = a_1 \frac{dw}{dt}, \frac{dy_2}{dt} = -a_2 \frac{dw}{dt} \quad \text{-- } \text{ì } \text{õ}.$$

$$\text{šÄÖö } \frac{d^2y_1}{dt^2} = a_1 \frac{d^2w}{dt^2}, \frac{d^2y_2}{dt^2} = -a_2 \frac{d^2w}{dt^2} \quad \text{-- } \text{ì } \text{õ}.$$

$$\therefore \frac{d^2y_1}{dt^2} / \frac{d^2y_2}{dt^2} = -\frac{a_1}{a_2}$$

$$\ll \text{øÄÐ } \frac{f_1}{f_2} = -\frac{a_1}{a_2};$$

$$\ll \text{øÄÐ } f_2 = -\frac{a_1}{a_2} f_1; \quad \text{±y Èjì } \text{õ}.$$

f₁ ±y Ū ò Óî ì , ò šžžjì , Öðç¼jø, , ð'' ¼, çÝ šÄø | ÄüÄî ò ò¼ðÐÄÄç'' ò , ū (inertia forces) Ó'' ÈšÄ

$$F_1' = \frac{1}{g} w_1 f_2;$$

$$F_2' = \frac{1}{g} w_2 f_2 = -\frac{a_2 w_2}{a_1 g} f_1 \dots \dots (1)$$

$$= -a_2 \frac{w_2}{g} \quad \text{-- } \text{ì } \text{õ}.$$

« ò¼'' Ä ò¼ðÐÄ Äç'' ò ū | ÄüÄî ò çç'' ò ū Ä¼ö (4.4.12) -ø j ðÈöüçÄjÜ - üçÉ. « Äü'' Èöð ðÈÄç'' ò , šçjî š ò:ì ì öšÄjÐ, šÄjÖð | ¼jì çç pÄî , pÄø « '' Á¼ç çç ÄÄÄÖî ì ò. Ö-ÄüÈç « ùÄç'' ò , çç¼ Öððð¼çÉí , '' çì , ½ì , ¼,

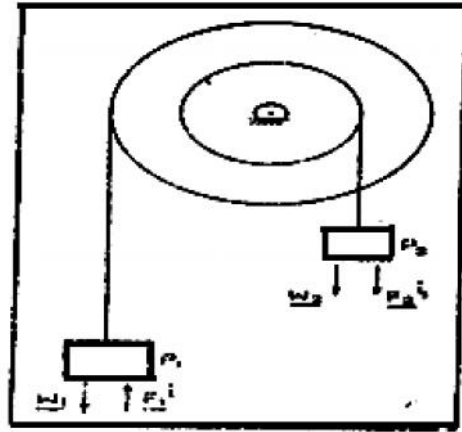
$$(w_1 - F_1') a_1 = (w_2 - F_2') a_2 \dots \dots (2) \quad \text{±y ÄÐ , ç'' ¼ì ì } \text{õ}$$

(1), (2) ±y Ū ò °ÁýÄjî ū ù ì ì ò ç¼ç × , jî ò šÄjÐ,

$$f_1 = \left\{ \frac{w_1 a_1 - w_2 a_2}{w_1 a_1^2 + w_2 a_2^2} \right\} a_{1,g}$$

$$f_2 = - \left\{ \frac{w_1 a_1 - w_2 a_2}{w_1 a_1^2 - w_2 a_2^2} \right\} a_{2,g} \dots \dots (3)$$

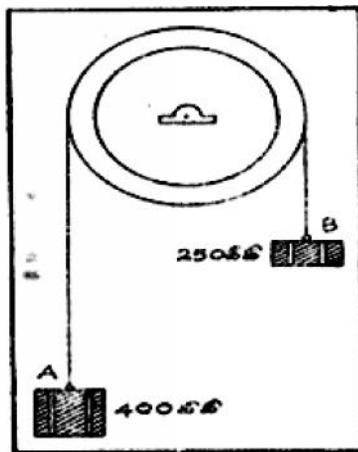
-- ì ò.



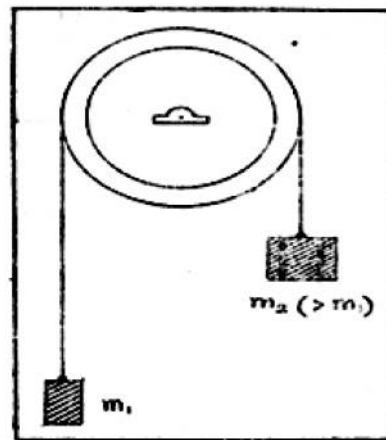
À¼õ 4-4-12

4.4.5 ÀÁÙ°

4.4.5.1 400, 250, $\pm \frac{1}{4}$, \hat{U} $\frac{1}{4}$ \hat{A} , $B \pm \hat{y} \hat{U} \hat{o}$ $\hat{p} \hat{O}$ \hat{u} \hat{O} \hat{z} $\hat{A} \hat{A}_i \hat{E}$
 $\hat{A} \hat{E} \hat{A} \hat{E} \hat{o} \hat{A}_i \hat{E}$, $\hat{p} \hat{S} \hat{A} \hat{o}_i \hat{E}$ $\hat{o} \hat{A} \hat{C} \hat{A} \hat{y}$ $\hat{A} \hat{D}$ $| \hat{o} \hat{O} \hat{o}$ $\hat{A} \hat{C} \hat{U} \hat{i}$ $\frac{3}{4} \hat{A} \hat{U} \hat{E}$ (inextensible)
 $\mu_i \hat{C} \hat{E} \hat{A} \hat{C} \hat{E}_i \hat{o}$ \hat{p} $\frac{1}{2} \hat{i}$ $\hat{o} \hat{A} \hat{D} \hat{I}$, $\hat{A} \hat{¼} \hat{o}$ (4.4.4) \hat{o} \hat{z} $\hat{E} \hat{A} \hat{A}_i \hat{U}$, $\mu \times \hat{z}$ $\hat{A} \hat{A} \hat{C} \hat{A} \hat{O} \hat{o} \hat{D}$
 $\hat{A} \hat{C} \hat{I}$ $\hat{A} \hat{C}$ $\hat{o} \hat{A} \hat{I}$ $\hat{y} \hat{E} \hat{E}$, \hat{A} $\pm \hat{y} \hat{U} \hat{o}$ \hat{u} $\frac{1}{4}$ $10 \hat{A} \hat{E}$ $| \frac{3}{4} \hat{i}$ \hat{A} $\hat{A} \hat{i}$ $\frac{1}{4} \hat{i}$ $\hat{o} \hat{S} \hat{A}_i \hat{D} \ll \hat{D}$
 $| \hat{A} \hat{U} \hat{o}$ $\frac{3}{4} \hat{C}$ $\hat{o} \hat{S} \hat{A}_i \hat{U}$ \hat{i} \hat{n}
 ($\hat{A} \hat{C}$ $\frac{1}{4}$: 7.314 $\hat{A} \hat{E} / \hat{A} \hat{C} \hat{E}_i \hat{E}$)



À¼õ 4-4-4



À¼õ 4-4-5

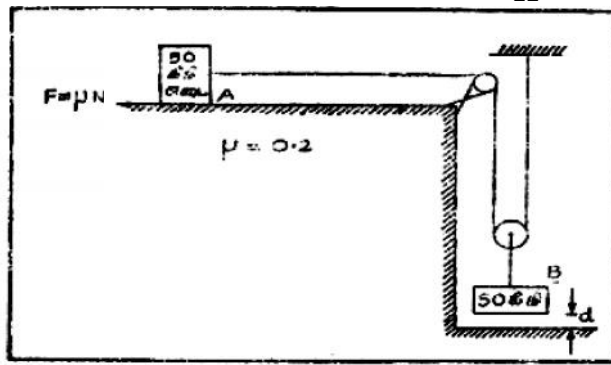
4.4.5.2 « $\hat{o} \times \hat{o} \pm \hat{o} \frac{3}{4} \hat{A} \hat{O}$ (Atwood's Machine) $\pm \hat{y} \hat{U} \hat{o}$ $| \hat{A}_i \hat{C} \hat{A}_i \hat{E} \hat{D}$ $g \hat{A} \hat{C} \hat{y}$
 $\hat{A} \frac{3}{4} \hat{O}$ $\hat{A} \hat{o}$ $| \hat{A} \hat{E} \hat{o}$ $\hat{A} \hat{A} \hat{y} \hat{A} \hat{I}$ $\hat{o} \frac{3}{4} \hat{o} \hat{A} \hat{I}$ \hat{o} , « $\frac{3}{4} \hat{y} \pm \hat{C} \hat{A}$ $\hat{A} \hat{E} \hat{A}$ « $\hat{A} \hat{o} \hat{O}$, $\hat{A} \hat{¼} \hat{o}$ 4.4.5 -
 \hat{o} \hat{z} $\hat{E} \hat{A} \hat{A} \hat{D} \hat{I}$ $\hat{u} \hat{C} \hat{D}$. \hat{u} \hat{o} $\frac{1}{4}$ $\hat{C} \hat{y}$ \hat{z} \hat{C} \hat{E} \hat{z} \hat{C} $m_1, m_2 (m_2 > m_1)$ $\pm \hat{E} \times \hat{o}$ $\hat{o} \hat{A} \hat{C} \hat{A}_i \hat{E} \hat{D}$
 $\hat{p} \hat{S} \hat{A} \hat{o}_i \hat{x} \hat{o}$, $\hat{A} \hat{E} \hat{A} \hat{E} \hat{o} \hat{A}_i \hat{x} \hat{o}$ $\hat{u} \hat{C} \hat{D}$ $\pm \hat{E} \times \hat{o}$ $| \hat{i}$ \hat{n} \hat{I} , $\hat{o} \times \hat{z}$ $\hat{A} \hat{A} \hat{C} \hat{A} \hat{O} \hat{o} \hat{D}$ \hat{h} $\hat{A} \hat{E}$
 $| \frac{3}{4} \hat{i}$ $\hat{A} \times$, $m_2 \pm \hat{y} \hat{U} \hat{o}$ \hat{z} \hat{C} \hat{E} $\hat{u} \hat{S} \hat{z} \hat{i}$ \hat{z} $\hat{p} \hat{A} \hat{i}$ \hat{z} , v $\hat{A} \hat{E} \hat{A} \hat{C} \hat{E}_i \hat{E}$ $\pm \hat{y} \hat{U} \hat{o}$

3/4... 0 S A, 0... 3/4 0 | A U A 3/4 j, 0, g - A y A 3/4 0... A (m1, m2, v, h) - , C A u E y A j A A j, i
 s, i n s.

$$[\text{I } \ddot{E} \text{ 0 0 } (m_1 - m_2)h = \frac{1}{2}m_1v^2 + \frac{1}{2}m_2v^2]$$

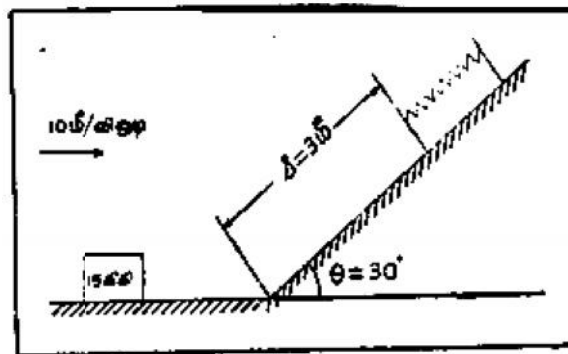
$$\text{A c' } 1/4: g = \left(\frac{m_2 + m_1}{m_2 - m_1}\right) \frac{v^2}{2h} \text{ A y A c' E j E}^2$$

4.4.5.3 A 1/4 0 4.4.6 0 s, i 0 E 0 u C « ... A 0... A 0 | A u E | A j 0 0 | 1/4 j l 3/4 0 y U m o x
 z c' A A c A 0 0 0 A c l A c i 0 A I 0 E D, B y U o | A j 0 u d A e | 3/4 j... A x u S z i l s c
 p A i A x 1/4 y 3/4... A... A p E 0 D, A u U o A l 3/4... A 0 | 3/4 j o A j i l 0 E D (slack).
 A y U o | A j 0 u | A j 0 3/4 A j, 5 A e | 3/4... A x p A i s c, o x z c' A... A
 « ... 1/4, 0 E | 3/4 j E 0, d - y A 3/4 0... A i s, i n s. (A c' } 1/4: d = 25/22 A)



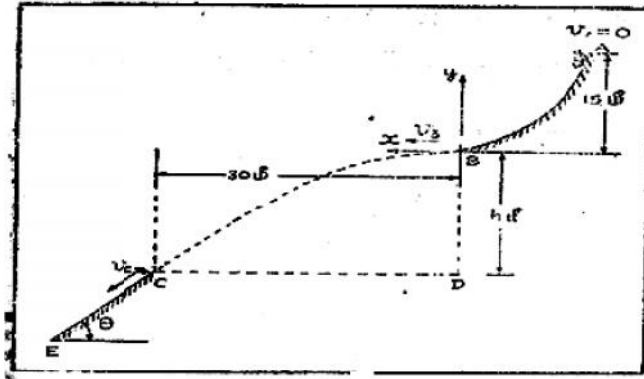
A 1/4 0 4-4-6

4.4.5.4 W=15 ±... 1/4 0 u C | A j 0 | C j y U, A e A e 0 A j E s c' 1/4 0 3/4 C 0 3/4 0,
 A c' E j E i l 10 A e S A, 0 3/4 0 A 1/4 0 4.4.7-0 s, i 0 E A A j U p A i l 0 S A j D,
 s c' 1/4 0 3/4 C 0 3/4 0 l



A 1/4 0 4-4-7

2 u E i s, i 1/2 0... 3/4 0 | A u U u C A e A e 0 A j E o j 0 3/4 C 0 3/4 0, S A 0 S z i l s C A A j S E
 A 0 A j E c A c k=2, C, V | 0. A e - u C 3/4 0 l i l 0 u A 0 y... E S A j D, 0 E D. s=3 A e
 ± E 0 « 0 | A j 0 u o j 0 3/4 C 0 3/4 0 | o y E z c' A i l 0 D A A A j D ± E i s, i n s.
 (A c' } 1/4: 1.365 A y A c' E j E)

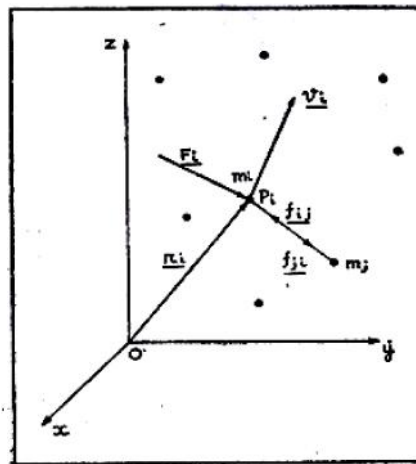


À¼õ 4-4-9

4.4.6 Ð, ù, ÇÛÝ |¾|¾ | - ;ÇÁ ŠÁ" Ä-ñ üÈø °ÁÝÄ;Î (Work-Energy Equation for a system of particles)

n Ð, ù, ÇÛÝ |¾|¾ |¾ÇÁ;ÉÐ À¼õ (4.4.13) - ø, ;ðÈÄÁ;Ú þÕ; ðÎ ò mi, i=1,2,3,...,n ±ÝÄÐ i--ñ ÄÐ Ð, ÇÛÝ ;Ç" ÈÄ;Î ò. « Ð ri ±ÝÛõ ;Ç" Äð¾Ç" °ÄÇ" Äð;ÄüÈ pi ±ÝÛõ òùÇÇÄø t ±ÝÛõ §;Äð¾Çø þÕð¾; ; |¾;Û.

Fi ±ÝÄÐ mi±ÝÛõ Ð, ÇÛø |°ÄüÄÎ ò òÈÄÇ" °, ÇÛÝ |¾|¾ |ÄÄÝ ÄÇ" °" Äî |ÈÇ, ðÎ ò. f_{ij}, (j=1,2,...,n, j≠i) ±ÝÄÐ i--ñ ÄÐ Ð, ù j--ñ ÄÐ Ð, ÇÛÄÕóÐ |ÄÜõ - ùÄÇ" °" Äî |ÈÇ, ðÎ ò. þð¾" , Ä ÄÇ" °, Ç;ø mi ±ÝÛõ Ð, ù ;¾; |¾, òÄðÎ, « Ð v_i ±ÝÛõ ;Ç" ° ŠÁ, ò¾Çø þÁÍ |¾;É¾; ; |¾;Û.



À¼õ 4-4-13

mi ±ÝÛõ Ð, ù ò òÈÄÇ" °¾ - òÄ « " ÄðÄÇÄÕóÐ (from one configuration) Äü;É;Ö |ÈÄÇ" °¾ - òÄ « " Äðð;Î |¾ (to another configuration) ≥§¾Û |Á;Ö Ä; "¾Äø |øÄ¾; ;ø, « òÐ, Û;Î |¾ "ŠÁ" Ä-ñ üÈø" °ÁÝÄ;Î ,

$$\therefore \frac{dr_i}{dt} = \frac{dr_0}{dt} + \frac{dp_i}{dt}$$

« $\frac{1}{2} \dot{A} \dot{B} \quad \underline{v}_1 = \underline{v}_c + \underline{p}_1$

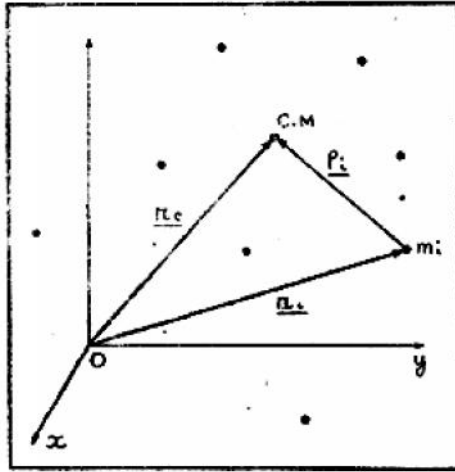


Figure 4-4-13

Let \underline{v}_i be the velocity of mass m_i relative to the origin O , \underline{v}_c be the velocity of the center of mass relative to O , and \underline{p}_i be the velocity of mass m_i relative to the center of mass. (velocity relative to the mass centre) $\underline{v}_i = \underline{v}_c + \underline{p}_i$.

Let \underline{v}_i be the velocity of mass m_i relative to the origin O , \underline{v}_c be the velocity of the center of mass relative to O , and \underline{p}_i be the velocity of mass m_i relative to the center of mass. $\underline{v}_i = \underline{v}_c + \underline{p}_i$.

$$\begin{aligned} &= \frac{1}{2} \sum_{i=1}^n m_i (\underline{v}_i \cdot \underline{v}_i) \\ &= \frac{1}{2} \sum_i m_i (\underline{v}_c + \underline{p}_i) \cdot (\underline{v}_c + \underline{p}_i) \\ &= \frac{1}{2} \sum_i m_i (v_c^2 + 2\underline{v}_c \cdot \underline{p}_i + p_i^2) \\ &= \frac{1}{2} \sum m_i v_c^2 + \sum m_i \underline{v}_c \cdot \underline{p}_i + \frac{1}{2} \sum m_i p_i^2 \\ &= \frac{1}{2} (\sum m_i) v_c^2 + \underline{v}_c \cdot \sum m_i \underline{p}_i + \frac{1}{2} \sum m_i p_i^2 \end{aligned}$$

Let \underline{v}_i be the velocity of mass m_i relative to the origin O , \underline{v}_c be the velocity of the center of mass relative to O , and \underline{p}_i be the velocity of mass m_i relative to the center of mass. $\underline{v}_i = \underline{v}_c + \underline{p}_i$.

$$\sum m_i \underline{p}_i = \sum m_i \frac{d}{dt} (\underline{p}_i) = \frac{d}{dt} \sum m_i \underline{p}_i$$

Let \underline{v}_i be the velocity of mass m_i relative to the origin O , \underline{v}_c be the velocity of the center of mass relative to O , and \underline{p}_i be the velocity of mass m_i relative to the center of mass. $\underline{v}_i = \underline{v}_c + \underline{p}_i$.

Let \underline{v}_i be the velocity of mass m_i relative to the origin O , \underline{v}_c be the velocity of the center of mass relative to O , and \underline{p}_i be the velocity of mass m_i relative to the center of mass. $\underline{v}_i = \underline{v}_c + \underline{p}_i$.

$\sum m_i \underline{p}_i = \pm \dot{y} \Delta D \quad \frac{3}{4} \times \dots \hat{A} \hat{o} \hat{l} \hat{E} \hat{o} \hat{D} \pm \hat{l} \hat{l} \hat{o}$
 (First moment about the mass centre).
 $\pm \dot{E} \hat{S} \hat{A} \hat{D} \hat{o} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D}$

$$= \frac{1}{2} M v_c^2 + \frac{1}{2} \sum m_i P_i^2$$

$\hat{S} \hat{A} \hat{D} \hat{o} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D}$
 $\hat{S} \hat{A} \hat{D} \hat{o} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D}$

$$\frac{1}{2} M v_c^2 \pm \dot{y} \Delta D \quad \hat{S} \hat{A} \hat{D} \hat{o} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D}$$

$\hat{S} \hat{A} \hat{D} \hat{o} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D}$
 $\hat{S} \hat{A} \hat{D} \hat{o} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D}$
 (Kinetic energy due to translation of the system)

$$\hat{S} \hat{A} \hat{D} \hat{o} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D}$$

$\hat{S} \hat{A} \hat{D} \hat{o} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D}$
 $\hat{S} \hat{A} \hat{D} \hat{o} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D}$
 (Kinetic energy of the motion of particles relative to the mass centre)

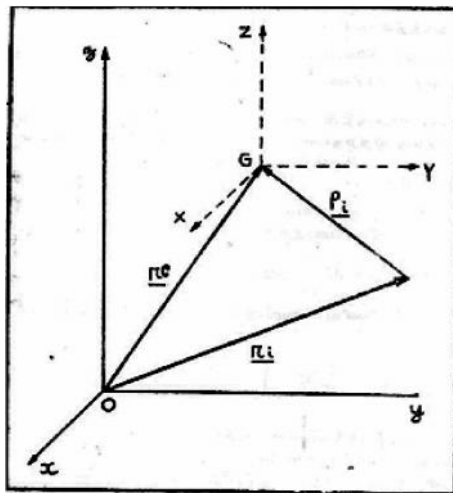


Figure 4-4-15

$$\pm \dot{E} \hat{S} \hat{A} \hat{D} \hat{o} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D}$$

Kinetic energy of the system = Kinetic energy of the Centre of mass + Kinetic energy about the Centre of mass

$$P_i^2 - \pm \dot{y} \Delta D \quad \hat{S} \hat{A} \hat{D} \hat{o} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D} \hat{l} \hat{E} \hat{o} \hat{D}$$

$$P_i^2 = \left[\left(\frac{dP_i}{dt} \right)_{xyz} \right]^2 = \left[\left(\frac{dP_i}{dt} \right)_{xyz} \right]^2$$

$$= \left[\left(\frac{dP_i}{dt} \right)_{xyz} + \underline{w} \wedge \underline{P}_i \right]^2$$

Ó· È· Àì Ì Èñ Ì ò. Á¼õ (4.4.15) - ³ ò Àì ÷ Ì

$\underline{w} \pm \dot{y} \Delta D$ ç· ÄÄ_jÉ xyz Ì ÈòÀö¼íÎ « ·· Áö·· Àî °_j÷òÐ pÁî Ì ò XYZ-
ý §_j ½ð³¼ç· °ŠÄ_jÁ_j Ì ò.

4.4.8 ¼ç½çx ·· ÄÄð¼çý « ÈðÀ· ¼Äç Ð_j ù_j Çý |¼ì ¼ç ýÈù Ì ²üÈ¼_jÉ
"ŠÄ· Ä- ùÈø" §_j ·· Ä_j ·· Çì_j Ì ¼ø: (Work-kinetic energy expressions
based on centre of mass)

çäð¼Éý pÁñ ¼_jÄÐ Ä¼òÀÈ, Ð_j ù_j Çý |¼ì ¼ç ýÈù ·· ¼Ä

¼ç½çx ·· ÄÄð¼çý pÁî Ì ò $\underline{F} = M \frac{d^2 r_c}{dt^2} = M v_c$ Ì ò.

« ò¼· ·· Ä ¼ç½çx ·· ÄÄð¼çù Ì Ä "ŠÄ· Ä- ùÈø" °Áý À_jÎ

$$\int_1^2 \underline{F} \cdot d\underline{r}_c = \left(\frac{1}{2} M v_c^2 \right)_2 - \left(\frac{1}{2} M v_c^2 \right)_1 \dots (1)$$

pí Ì ÄÄÐÈð¼öùç Ä¼òò, Ð_j ù_j Çý |¼ì ¼ç | Ä_jý Ù | ÄÜò, Ó¼ø
Ä Ì ¼ç_jÉ (First part) pÁî Ì ùÈÄý §ÄÜ_jð· ¼ì Ì Èñ_jÈÐ. pùÄ¼
pÁî Ì ùÈø Ä Ì ¼çÄ_jÉÐ, Ð_j ù_j Çý |Ä_jð¼ ç· È_j ·· Çò | ÄüÜò, ¼ç½çx
·· ÄÄð¼çÄ ·· Áóðò Ì ùç_j ·· ùÄ_j ·· ÉÄ_jÉ Ð Çý §Äø, òÈ Ä_j ·· Ç_j ·· Éððò
| òòòò §Ä_j ·· Áö¼ý |¼_j¼÷òòÄ Ì ò¼òÄ Ì ùç_j ·· ¼, (1) ±ý Üò °Áý À_jÎ
| ÄçòÄ Ì òð_jÈÐ.

pÁî Ì ùÈÄý Äü Ì È_jò Ä Ì ¼ç Ì ò, Ä_j ·· ù Ì Ì Óùç
|¼_j¼÷ ·· Ä Ì_j ½, m_j ±ý Üò 21 ç· Èò· ¼Ä Ì Ì ÄÐ Ð_j Çý pÁî Ì ùÈø
°Áý À_jð· ¼ Ì Ä_j Ä §Äñ ÈÄò ÈÐ.

çäð¼Éý pÁñ ¼_jÄÐ Ä¼òÀÈ, --- ±ý Üò Ð_j Çý pÁî Ì ò^¼
Ä ·· ÄÄÜ Ì Ì °Áý À_jÎ

$$\underline{F}_i + \sum_{j=1}^n \underline{f}_{ij} = m_i \frac{d^2 r_i}{dt^2} = m_i \frac{d v_i}{dt} \text{ Ì ò.}$$

pí Ì \underline{f}_{ij} ±ý ÄÐ, j- Ì ÄÐ Ð_j ù_j, i- Ì ÄÐ Ð_j Çý §Äø | °ÄüÄ Ì òðò Ì ù
Ä_j ·· À Ì Ì Èñ_jÈÐ. §Áöò, Ä¼ò (9.23)ø_j ðÈÄÄ_jÜ.

$$\underline{r}_i = \underline{r}_c + \underline{P}_i$$

$$d \underline{r}_i = d \underline{r}_c + d \underline{p}_i$$

(2),(3) ±ý Üò °Áý À_jÎ ç·ø « ·· Áöò ¼ç· °Ä_j Çý ±ñ ½òò
| Äò Ì ç· Ä_j ·· ÄÄÜòÐ, -- ÄÐ Ì ÖÄ « ·· ÁòÄÄöóò, 2ÄÐ Ì ÖÄ_j ·· Äò Ì Ì, --

±ý Ū õ Ð, ù ²§¾Ū | Á; Ō Á; ·¾ÄÄÄí ì õ§Á; Ð, «¾ù ò ²üÈ¾; É "§Ä · Ä-
 -üÈø" °ÁýÄ; í |¾; ·, Ññ, ½¾ Ó · ÈôÄÉ,

$$\begin{aligned} & \int_1^2 \left(\underline{F}_i + \sum_{j=1}^n \underline{f}_{ij} \right) (d\underline{r}_c + d\underline{P}_i) \\ &= \int_1^2 m_i \frac{d\underline{v}_i}{dt} \cdot d\underline{r}_i \\ &= \int_1^2 m_i \frac{d\underline{v}_i}{dt} \cdot \frac{d\underline{r}_i}{dt} dt \\ &= \int_1^2 m_i \left(\frac{d\underline{v}_i}{dt} \cdot \underline{v}_i \right) dt \\ &= \frac{1}{2} \int_1^2 m_i \frac{d}{dt} (\underline{v}_i \cdot \underline{v}_i) dt \\ &= \frac{1}{2} \int_1^2 m_i d(\underline{v}_i \cdot \underline{v}_i) = \frac{1}{2} \int_1^2 m_i d(v_i^2) = \frac{1}{2} \int_1^2 m_i \left\{ (v_i^2)_2 - (v_i^2)_1 \right\} \end{aligned}$$

í = - Ä Ð Ð Çý þÄì, -üÈø Á; üÈÄ; ì õ.
 þüÄ¾ "§Ä · Ä-üÈø" °ÁýÄ; í, ù | Á; Ō Ð, ù ì ì õ | Á; Ō ó Ð Á¾; ø,
 §ÄüÜÉÄ °ÁýÄ; ðÉý Ū ð ì ò |¾; ·, Ä; ø, n-Ð, ù, Çý |¾; ì |¾; ì |Ä
 "§Ä · Ä-üÈø" °ÁýÄ; ð · ¼ø | ÄÈÄ; ð. -¾Ä; ø,

$$\begin{aligned} \sum_{i=1}^n \left(\underline{F}_i + \sum_{j=1}^n \underline{f}_{ij} \right) \cdot (d\underline{r}_c + d\underline{P}_i) &= \frac{1}{2} \sum_{i=1}^n m_i (v_i^2)_2 - \frac{1}{2} \sum_{i=1}^n m_i (v_i^2)_1; \\ \sum_{i=1}^n \int_1^2 \underline{F}_i \cdot d\underline{r}_c + \sum_{i=1}^n \int_1^2 \underline{F}_i \cdot d\underline{P}_i \\ \sum_{i=1}^n \int_1^2 \sum_{j=1}^n \underline{f}_{ij} \cdot d\underline{r}_c + \sum_{i=1}^n \int_1^2 \sum_{j=1}^n \underline{f}_{ij} \cdot d\underline{P}_i \end{aligned}$$

$$\begin{aligned} \text{Ð, ù, ù} &\ll \cdot \cdot \cdot \text{É} \text{ } \text{¾ù} \text{ì} \text{ } \text{Ä; É} \text{ } \text{þÄì}, -\text{üÈø}, \text{Ä; üÈÄ; ì} \text{ } \text{õ} \\ &= \Delta [KE]_{1,2} \\ &= \Delta \left\{ \frac{1}{2} M v_c^2 + \frac{1}{2} \sum m_i P_i^2 \right\} \\ &= \Delta \left(\frac{1}{2} M v_c^2 \right) + \Delta \left(\frac{1}{2} \sum m_i P_i^2 \right) \end{aligned}$$

§ÄÖö,

$$\sum_{i=1}^n \int_1^2 \underline{F}_i \cdot d\underline{r}_c = \Delta \left(\frac{1}{2} M v_c^2 \right) = \sum_{i=1}^n \int_1^2 \sum_{j=1}^n \underline{f}_{ij} \cdot d\underline{r}_c = \int_1^2 \left(\sum_{i=1}^n \sum_{j=1}^n \underline{f}_{ij} \right) \cdot d\underline{r}_c$$

$$= \int_1^2 \underline{0.drc}, ; = 0(-\hat{u} \hat{A} \hat{c} \hat{o}, \hat{c} \hat{y} \hat{l} \hat{E} \hat{A} \hat{A} \hat{o} \hat{U} \hat{o} \hat{l} \hat{o} | \hat{3}_i \hat{r} \hat{a} \hat{i} \hat{o} \hat{A} \hat{A} \hat{l} \hat{o})$$

$$\sum_{i=1}^n \int_1^2 \sum_{j=1}^n \underline{fij.dPi} = \int_1^2 \sum_{i=1}^u \sum_{j=1}^n (\underline{fij.dPi}); \pm 0; \pm y \hat{A} \hat{3}_i \hat{o},$$

(4) $\pm y \hat{U} \hat{o} \hat{o} \hat{A} \hat{y} \hat{A}_i \hat{o} \hat{E} \hat{y} \hat{p} \hat{U} \hat{3}_i \hat{A}_i \hat{E} \hat{z} \hat{c} \hat{r} \hat{A}$

$$\sum_{i=1}^n \int_1^2 \underline{Fi.dP1} + \sum_{i=1}^n \int_1^2 \sum_{j=1}^n (\underline{fi.dP1});$$

$$\Delta \left(\frac{1}{2} \sum miPi^2 \right) \dots \dots \dots (5)$$

$\hat{r} \hat{S} \hat{A}, (1) - \pm y \hat{U} \hat{o} \hat{o} \hat{A} \hat{y} \hat{A}_i \hat{l}, \hat{o} \hat{E} \hat{A} \hat{c} \hat{o}, \hat{c} \hat{y} \hat{A}_i \hat{A} \hat{A}_i \hat{r}, \hat{3}_i \hat{c} \hat{1} \hat{2} \hat{c} \hat{x} \hat{r} \hat{A} \hat{A} \hat{o} \hat{3}_i \hat{y}$
 $\hat{p} \hat{A} \hat{i} \hat{o} \hat{r} \hat{3}_i \hat{A} \hat{A}_i \hat{c} \hat{E} \hat{D}. \hat{r} \hat{E} \hat{j} \hat{o} (5) - \pm y \hat{U} \hat{o} \hat{o} \hat{A} \hat{y} \hat{A}_i \hat{l}, \hat{o} \hat{E}, \hat{r} \hat{u} \hat{\pm} \hat{y} \hat{E}$
 $\hat{p} \hat{O} \hat{A} \hat{r} \hat{A}_i \hat{E} \hat{A} \hat{c} \hat{o} \hat{u} \hat{l} \hat{o} \hat{o} \hat{S} \hat{A} \hat{r} \hat{A} \hat{c} \hat{y} \hat{o}, \hat{3}_i \hat{c} \hat{1} \hat{2} \hat{c} \hat{x} \hat{r} \hat{A} \hat{A} \hat{o} \hat{r} \hat{3}_i \hat{r} \hat{o} \hat{D},$
 $\hat{D} \hat{u} \hat{c} \hat{y} \hat{p} \hat{A} \hat{i} \hat{o} \hat{r} \hat{3}_i \hat{A} \hat{c} \hat{i} \hat{l} \hat{E} \hat{D}.$

4.4.9 $\hat{A}_i \hat{3}_i \hat{c} \hat{i} \hat{r} \hat{1} \hat{2} \hat{l} \hat{u}$

4.4.9.1 $2 \hat{c} \hat{c} \hat{6} \hat{c} \hat{c} \hat{z} \hat{c} \hat{E} \hat{r} \hat{C} \hat{o} \hat{l} \hat{A} \hat{u} \hat{E} \hat{p} \hat{O} \hat{l} \hat{A}_i \hat{O} \hat{u} \hat{u}, \hat{z} \hat{c} \hat{r} \hat{A} \hat{A}_i \hat{E} \hat{A} \hat{E} \hat{A} \hat{o} \hat{A}_i \hat{E},$
 $\hat{p} \hat{S} \hat{A}_i \hat{o} \hat{i} \hat{E} \hat{r} \hat{O} \hat{o} \hat{A} \hat{A} \hat{y} \hat{A} \hat{D} \hat{l} \hat{o} \hat{o} \hat{O} \hat{o} \hat{A} \hat{c} \hat{A} \hat{o} \hat{A}_i \hat{3}_i \hat{A} \hat{U} \hat{r} \hat{y} \hat{E} \hat{o} \hat{p} \hat{r} \hat{1} \hat{2} \hat{l} \hat{o} \hat{A} \hat{O} \hat{l}$
 $\hat{r} \hat{S} \hat{A} \hat{A} \hat{o} \hat{3}_i \hat{A} \hat{O} \hat{o} \hat{D} \hat{A} \hat{c} \hat{r} \hat{A} \hat{c} \hat{u} \hat{o} \hat{A} \hat{l} \hat{r} \hat{y} \hat{E} \hat{E}. 100: \{ [10^{-2}] \hat{D} \} \hat{3}_i \hat{r} \hat{A} \times \hat{p} \hat{A} \hat{i} \hat{r} \hat{A} \hat{A} \hat{y},$
 $\ll \hat{o} \hat{l} \hat{3}_i \hat{l} \hat{3}_i \hat{c} \hat{l} \hat{A} \hat{U} \hat{o} \hat{3}_i \hat{c} \hat{o} \hat{S} \hat{A} \hat{o} \hat{r} \hat{3}_i \hat{l} \hat{r} \hat{n}.$
 $\hat{p} \hat{l} \hat{l} \hat{A}_i \hat{O} \hat{u} \hat{c} \hat{y} \hat{\pm} \hat{r} \hat{1} \hat{4} \hat{u} \hat{A} \hat{o} \hat{l} \hat{S} \hat{A} \hat{S} \hat{A} \hat{r} \hat{A} \hat{r} \hat{l} \hat{o} \hat{o} \hat{r} \hat{y} \hat{E} \hat{E}. \hat{\pm} \hat{E} \hat{S} \hat{A},$
 $\hat{\pm} \hat{r} \hat{1} \hat{4} \hat{u} \hat{l} \hat{o} \hat{o} \hat{3}_i \hat{S} \hat{A} \hat{r} \hat{A}$

$$[2(-1.0) \times 9.81 + 6(1.0) \times 9.81] f \hat{r} \hat{o} \hat{u}$$

$$= 39.24 f \hat{r} \hat{o} \hat{u}.$$

$\hat{A} \hat{U} \hat{A} \hat{u} \hat{o} \hat{l} \hat{3}_i \hat{A} \hat{u} \hat{E} \hat{3}_i \hat{r} \hat{A}_i \hat{o}, \hat{p} \hat{O} \hat{l} \hat{A}_i \hat{O} \hat{u} \hat{c} \hat{y} \hat{S} \hat{A} \hat{r} \hat{u} \hat{o} \hat{A} \hat{A}_i \hat{l} \hat{o} ((V: \hat{E} \hat{u} \hat{o})$
 $\hat{\pm} \hat{E} \hat{S} \hat{A},$
 $\hat{p} \hat{A} \hat{i} \hat{r} \hat{u} \hat{E} \hat{A} \hat{o} \hat{A}_i \hat{u} \hat{E} \hat{o}$

$$\hat{p} \hat{U} \hat{3}_i \hat{p} \hat{A} \hat{i} \hat{r} \hat{u} \hat{E} \hat{o} - \hat{l} \hat{3}_i \hat{1} \hat{4} \hat{l} \hat{u} \hat{p} \hat{A} \hat{i} \hat{r} \hat{u} \hat{E} \hat{o} = \frac{1}{2} (2+6)v^2 - 0 = 4v^2$$

" $\hat{S} \hat{A} \hat{r} \hat{A} - \hat{u} \hat{E} \hat{o}$ " $\hat{3}_i \hat{o} \hat{D} \hat{A} \hat{o} \hat{A} \hat{E},$

$$4v^2 = 3924$$

$$v^2 = 9.81$$

$$v = 3.132 \hat{A} \hat{r} \hat{A} \hat{E} \hat{j} \hat{E}$$

4.4.9.2 $6 \hat{c} \hat{c} \hat{\pm} \hat{r} \hat{1} \hat{4} \hat{o} \hat{o}, 1.8 \hat{A} \hat{E} \hat{j} \hat{C} \hat{O} \hat{u} \hat{c} \hat{o} \hat{l} \hat{A} \hat{A} \hat{y} 1.2 \hat{A} \hat{o} \hat{3}_i \hat{c} \hat{c} \hat{O} \hat{u} \hat{c} \hat{A} \hat{l} \hat{3}_i \hat{c}$
 $\hat{A} \hat{E} \hat{A} \hat{o} \hat{A} \hat{u} \hat{E} \hat{S} \hat{A} \hat{r} \hat{A} \hat{y} \hat{A} \hat{D} \ll \hat{r} \hat{A} \hat{O} \hat{A}_i \hat{U} \hat{o}, \hat{A} \hat{3}_i \hat{O} \hat{u} \hat{c} 0.6 \hat{A} \hat{E} \hat{A} \hat{l} \hat{3}_i \hat{c} \hat{A} \hat{E} \hat{A} \hat{o} \hat{A}_i \hat{E}$
 $\hat{S} \hat{A} \hat{r} \hat{A} \hat{y} \hat{A} \hat{c} \hat{c} \hat{o} \hat{o} \hat{A} \hat{E} \hat{A}_i \hat{l} \hat{l} \hat{o} \hat{o} \hat{3}_i \hat{A} \hat{o} \hat{l} \hat{l} \hat{3}_i \hat{l} \hat{A} \hat{A} \hat{r} \hat{1} \hat{2} \hat{o} \ll \hat{r} \hat{A} \hat{3}_i \hat{c} \hat{z} \hat{c} \hat{A} \hat{A} \hat{o},$
 $\hat{A} \hat{1} \hat{4} \hat{o} 4.4.16 \hat{o} \hat{j} \hat{o} \hat{E} \hat{A} \hat{A}_i \hat{U}, \hat{r} \hat{A} \hat{i} \hat{o} \hat{A} \hat{o} \hat{l} \hat{u} \hat{c} \hat{E}. \hat{r} \hat{A} \hat{i} \hat{o} \times \hat{l} \hat{l} \hat{o} 0.3 \hat{o} \hat{l} \hat{c} \hat{c}$

$m_i, i=1,2 \dots n$ ±ý Ûõ ç· È· Çõ|ÀüÈ n Ð, ù, ù « ¼í, ÇÁ |¾í| Ñ
 ´ý· È\$çí| Ì · « ò|¾í| ¾ÇÁý - ùÁç· °, ù, ÞÃð· ¼, Çí, (in pairs) ´\$π
 \$ç±\$çí ðÈø °ÁÛõ ±¾ÇÁíø | °ÁüÁî Á¾íø « ÁüÈý | ÈÇÁü ÛÍ ¾ó
 âî °ÇÁí| ò. « ò|¾í| ¾ÇÁø | °ÁüÁî ò ðÈÁç· °, Çý |¾í| ÁÁý Áç· ° ÁF
 ±Éì |¾í| ù.

çã ð¼Èý ÞÃñ ¼í ÁÐ ÁÇÁøÀÈ, « ò|¾í| ¾ÇÁý ÞÃì, ò· ¾,

$$F = \sum_{i=1}^n m_i \frac{d v_i}{dt};$$

±ý Ûõ °Áý Àí| Á· ÁÁÜì ÷ÈÐ. Þð¾·, Á Áç· °, Ð, ù, Çý
 |¾í| ¾ÇÁý \$Áø, (t₂ - t₁) ç· Ä« ÇÁü| î | °ÁüÁî ÁíÁý,

$$\begin{aligned}
 \int_{t_1}^{t_3} F dt &= I \cdot \Delta E = \int_{t_1}^{t_3} \left(\sum_{i=1}^n m_i \frac{d v_i}{dt} \right) dt \\
 &= \int_1^2 \sum_{i=1}^n d(m_i v_i) \\
 &= \sum_{i=1}^n \int_1^2 d(m_i v_i) \\
 &= \left(\sum_{i=1}^n m_i v_i \right)_2 - \left(\sum_{i=1}^n m_i v_i \right)_1
 \end{aligned}$$

±É\$Á, Ð, ù |¾í| ¾ÇÁý \$Áø, ° Ì ÈÇÁø¼ ç· Ä« ÇÁü| î | °ÁüÁî ò
 ðÈÁç· Ç× Áç· °Áý ¾í| Ç· Á (Impulse) « ì ç· Ä Þ· ¼ | ÁÇÁø Ð, ù, Çý
 \$ç±\$çí ðÈ - ó¾ð¾ø ç· ÄüÁî ò ÁíÜÁí, Çý Ûð| ò |¾í| Ì î °Áí| ò.
 | ÁøöÁíø, |¾í| ¾ÇÁ¼í ÇÁ Ð, ù, ù ç· ÄíýÈý ÞÃì, ò· ¾ø
 « ÈÇÁñ ÈÁ ç· Á· Á, ù ÞÃíÐ. | Áíø¾ø¾ø |¾í| ¾ÇÁý ÞÃì, ò· ¾ø ÁüÈÇÁ
 ÁÇÁí \$Ç \$¾· ÁðÁî ò. « ùÁç· ç· Á· Á, Çø, |¾í| ¾ÇÁý ¾Ç¼×
 · ÁÁð¾ý ÞÃì \$Á °Èð· Áò | ÁÜò.

¾Ç¼× · ÁÁð¾ý ç· Á· Á· ÁÁÜì Ì ò °Áý Àí| ,

$$M r_c = \sum_{i=1}^n m_i r_i - \dot{L} \cdot \vec{o}.$$

\$ÁüÜÈÇÁ °Áý Àí| ð· ¼ t - çí| ÈøÐ °Ó· È Á·, Áñ | °öø\$ÁíÐ
 (differentiating once with respect to t)

$$M v_c = \sum_{i=1}^n m_i v_i$$

±ý ÁÐ ç· ¼í, ÷ÈÐ.

Þí °Áý Àí| , Ð, ù, Çý |¾í| ¾ÇÁ | ÇÁ | Áíø¾ - ó¾ð, Ð, ù, Çý | Áíø¾
 ç· È· Áò | ÁÜÜò, ¾Ç¼× · ÁÁð¾ø· ÁóÐò. « ò¾¼× · ÁÁð¾ý

$\frac{3}{4} \text{c} \cdot \text{S} \hat{A} \text{ o} \cdot \frac{3}{4} \hat{o} \quad | \hat{A} \hat{u} \hat{U} \hat{o}, \quad \hat{u} \hat{A} \cdot \hat{E} \hat{A}_i \hat{o} \quad - \hat{O} \hat{A}_i \hat{i} \quad \hat{o} \hat{A} \hat{o} \frac{1}{4} \hat{D} \hat{A}_i \hat{E} \quad \hat{D} \hat{u} \quad \hat{y} \hat{E} \hat{y}$
 $- \hat{o} \frac{3}{4} \hat{o} \frac{3}{4} \hat{u} \hat{i} \hat{i} \hat{o} \hat{A} \hat{A}_i \hat{i} \hat{o} \pm \hat{y} \hat{A} \cdot \frac{3}{4} \ll \hat{E} \hat{A} \hat{u} \hat{i} \hat{o} \hat{E} \hat{D}.$
 (1)- $\hat{A} \hat{D} \quad \hat{o} \hat{A} \hat{y} \hat{A}_i \hat{o} \hat{E} \hat{y} \quad \hat{A} \hat{A} \hat{o} \hat{D} \hat{E} \quad \hat{A} \frac{3}{4} \hat{o} \cdot \hat{A}, \quad (2)\text{-}\hat{A} \hat{D} \quad \hat{o} \hat{A} \hat{y} \hat{A}_i \hat{o} \frac{1}{4} \hat{i} \hat{o}$
 $\hat{O} \hat{I} \quad | \hat{o} \hat{O} \hat{o} \hat{S} \hat{A}_i \hat{D},$

$$= \int_{t_1}^{t_2} \underline{F} dt = \underline{I} = M (\underline{v}_c)_2 - M (\underline{v}_c)_1 \pm \hat{y} \hat{A} \hat{D} \quad \hat{u} \hat{c} \cdot \frac{1}{4} \hat{i} \hat{o} \hat{E} \hat{D}.$$

$\pm \hat{E} \hat{S} \hat{A}, \quad \hat{O} \hat{E} \hat{o} \frac{3}{4} \hat{i} \hat{i} \hat{o} \hat{C} \cdot \hat{A} \hat{A}_i \hat{o} \quad | \hat{o} \hat{A} \hat{u} \hat{A} \hat{o} \hat{I} \quad \hat{p} \hat{A} \hat{i} \hat{i} \hat{o}, \quad \hat{D} \hat{u} \hat{C} \hat{y} \quad | \frac{3}{4} \hat{i} \hat{i} \frac{3}{4} \hat{c}$
 $\hat{y} \hat{E} \hat{o} \hat{z} \hat{u} \hat{A} \hat{i} \hat{o} \quad - \hat{o} \frac{3}{4} \hat{A}_i \hat{u} \hat{E} \hat{o}, \quad \hat{D} \hat{u} \hat{C} \hat{y} \quad | \hat{A}_i \hat{o} \frac{3}{4} \hat{z} \hat{c} \cdot \hat{E} \cdot \hat{A} \hat{o} \quad | \hat{A} \hat{u} \hat{U} \hat{o}, \quad | \frac{3}{4} \hat{i} \hat{i} \frac{3}{4} \hat{c} \hat{i} \hat{i} \hat{c} \hat{A}$
 $\frac{3}{4} \hat{c} \frac{1}{2} \hat{c} \times \quad \hat{A} \hat{A} \hat{o} \frac{3}{4} \hat{c} \hat{y} \quad \hat{p} \hat{A} \hat{i} \hat{o} \quad \hat{o} \frac{3}{4} \hat{o} \quad | \hat{A} \hat{u} \hat{U} \hat{o} \quad \hat{u} \hat{A} \cdot \hat{E} \hat{A}_i \hat{o} \quad - \hat{O} \hat{A}_i \hat{i} \quad \hat{o} \hat{A} \hat{o} \frac{1}{4} \hat{D} \hat{A}_i \hat{E}$
 $\hat{D} \hat{u} \hat{y} \hat{E} \hat{o} \hat{z} \hat{u} \hat{A} \hat{i} \hat{o} \quad - \hat{o} \frac{3}{4} \hat{A}_i \hat{u} \hat{E} \hat{o} \frac{3}{4} \hat{u} \hat{i} \hat{i} \hat{o} \hat{A} \hat{A}_i \hat{i} \hat{o}.$

$\hat{p} \hat{i} \hat{U} \hat{u} \cdot \hat{E} \quad \hat{p} \hat{A} \hat{i} \quad \hat{A} \hat{c} \cdot \hat{o} \hat{A} \hat{A} \hat{o} \quad \hat{A} \hat{A} \hat{E} \hat{C} \hat{u} \hat{i} \hat{o} \quad \hat{A} \cdot \hat{A} \hat{c} \quad \hat{A} \hat{y} \hat{A} \hat{O} \hat{A}_i \hat{U} \hat{o}$
 $| \frac{3}{4} \hat{i} \hat{c} \hat{O} \hat{A} \hat{D} \hat{A} \hat{E} \hat{i} \hat{o}.$

$\hat{O} \hat{i} \hat{E} \hat{o} \hat{A} \hat{o} \frac{1}{4} \quad \hat{u} \hat{i} \hat{A} \quad \hat{p} \cdot \frac{1}{4} \hat{A} \hat{C} \hat{A} \hat{o} \quad \hat{D} \hat{o} \frac{1}{4} \hat{i} \hat{i} \frac{3}{4} \hat{c} \quad \hat{y} \hat{E} \hat{y} \quad \frac{3}{4} \hat{c} \frac{1}{2} \hat{c} \times$
 $\cdot \hat{A} \hat{A} \hat{o} \frac{3}{4} \hat{c} \quad \hat{z} \hat{u} \hat{A} \hat{i} \hat{o} \quad - \hat{o} \frac{3}{4} \hat{A}_i \hat{u} \hat{E} \hat{o}, \quad \ll \hat{o} \frac{1}{4} \hat{i} \hat{i} \frac{3}{4} \hat{c} \hat{A} \hat{y} \quad \hat{S} \hat{A} \hat{o} \quad | \hat{o} \hat{A} \hat{u} \hat{A} \hat{i} \hat{o}$
 $\hat{O} \hat{E} \hat{o} \frac{3}{4} \hat{i} \hat{i} \hat{o} \hat{C} \cdot \hat{A} \hat{C} \hat{y} \quad \hat{U} \hat{I} \quad \frac{3}{4} \hat{O} \hat{i} \hat{i} \hat{i} \hat{o} \hat{A} \hat{A}_i \hat{i} \hat{o}.$

$\hat{i} \hat{E} \hat{A} \hat{H} \quad \hat{O} \cdot \hat{E} \hat{A} \hat{o}, \quad \hat{p} \hat{i} \hat{U} \hat{u} \hat{U}$

$$\sum_{i=1}^n \underline{I}_i = (\sum m_i) (\underline{v}_c)_2 - (\sum m_i) (\underline{v}_c)_1$$

$\pm \hat{y} \hat{U} \hat{o} \quad \hat{o} \hat{A} \hat{y} \hat{A}_i \hat{o} \frac{1}{4} \hat{i} \hat{o} \hat{A} \cdot \hat{A} \hat{A} \hat{U} \hat{i} \quad \hat{o} \hat{A} \hat{i} \hat{o}.$

4.4.11 $\hat{o} \frac{3}{4} \hat{i} \hat{i} \hat{o} \hat{O} \ll \hat{o} \hat{A} \hat{D} \quad \frac{3}{4} \hat{c} \frac{1}{2} \hat{c} \times \quad \hat{S} \hat{A} \hat{u} \hat{i} \hat{o} \hat{O}$ (Conservation of Momentum)

$\frac{3}{4} \hat{O} \frac{3}{4} \hat{i} \hat{i} \hat{o} \hat{S} \hat{z} \hat{A} \hat{o} \frac{3}{4} \hat{c} \hat{o} \quad \hat{D} \hat{u} \hat{C} \hat{y} \quad | \frac{3}{4} \hat{i} \hat{i} \frac{3}{4} \hat{c} \hat{A}_i \hat{E} \hat{D} \quad \pm \hat{u} \hat{A} \hat{o} \hat{o} \quad \hat{O} \hat{E} \hat{A} \hat{c} \cdot \hat{U} \hat{i} \hat{i} \hat{o}$
 $\hat{O} \hat{i} \hat{o} \hat{A} \frac{1}{4} \hat{i} \hat{i} \hat{o} \hat{A} \hat{A} \hat{O} \hat{i} \hat{i} \hat{i} \hat{o} \hat{A} \hat{E} \hat{o}, \quad \ll \hat{o} \hat{S} \hat{z} \hat{A} \hat{o} \frac{3}{4} \hat{c} \hat{o} \quad | \frac{3}{4} \hat{i} \hat{i} \frac{3}{4} \hat{c} \hat{A} \hat{o} \quad \hat{z} \hat{u} \hat{A} \hat{i} \hat{o} \quad - \hat{o} \frac{3}{4} \hat{A}_i \hat{u} \hat{E} \hat{o}$
 $\hat{a} \hat{i} \hat{o} \hat{A} \hat{A}_i \hat{i} \hat{o}.$

$$\ll \frac{3}{4} \hat{i} \hat{i} \hat{A} \hat{D}, \quad \int_{t_1}^{t_2} \underline{F} dt = \left(\sum_{i=1}^n m_i \underline{v}_i \right)_2 - \left(\sum_{i=1}^n m_i \underline{v}_i \right)_1 \pm \hat{y} \hat{U} \hat{o}$$

$\hat{o} \hat{A} \hat{y} \hat{A}_i \hat{o} \hat{E} \hat{o}, \quad \underline{F} = 0; \quad \neg \hat{A} \frac{3}{4} \hat{i} \hat{o},$

$$\int_{t_1}^{t_2} \underline{F} dt = 0 \quad \neg \hat{i} \hat{o}.$$

$$\pm \hat{E} \hat{S} \hat{A}, \quad \left(\sum_{i=1}^n m_i \underline{v}_i \right)_2 - \left(\sum_{i=1}^n m_i \underline{v}_i \right)_1 = 0$$

$\ll \frac{3}{4} \hat{i} \hat{i} \hat{A} \hat{D}, \quad \hat{o} \frac{3}{4} \hat{A}_i \hat{u} \hat{E} \hat{o} \quad \hat{a} \hat{i} \hat{o} \hat{A} \hat{A}_i \hat{i} \hat{o} \hat{E} \hat{D},$

$\neg \hat{u} \hat{S} \hat{A}, \quad \underline{F} = 0 \quad \pm \hat{y} \hat{U} \hat{u} \hat{C} \hat{S} \hat{A}_i \hat{D},$

$$\left(\sum m_i \underline{v}_i \right)_2 - \left(\sum m_i \underline{v}_i \right)_1 = \hat{o} \hat{A}_i \hat{E} \hat{C} \hat{A} \hat{A}_i \hat{i} \hat{o}.$$

$\hat{p} \hat{D} \hat{S} \hat{A} \quad \hat{S} \hat{z} \hat{z} \hat{S} \hat{u} \hat{i} \hat{o} \hat{I} \quad - \hat{o} \frac{3}{4} \hat{i} \hat{i} \hat{o} \hat{O} \hat{A} \hat{c} \hat{c}$ (Law of conservation of Linear Momentum) $\pm \hat{E} \hat{o} \hat{A} \hat{i} \hat{o}.$ $\hat{p} \hat{u} \hat{A} \hat{o} \hat{o} \quad \hat{A} \hat{o} \hat{A} \hat{y} \hat{A} \hat{O} \hat{A}_i \hat{U} \hat{o} \quad \hat{A} \cdot \hat{A} \hat{A} \hat{U} \hat{i} \quad \hat{A}_i \hat{o}.$

$\vec{v}_c = \frac{1}{2} \vec{v}_1 + \frac{1}{2} \vec{v}_2$

$M(\vec{v}_c)_2 - M(\vec{v}_c)_1 = 0 \rightarrow \vec{v}_c = 0$

$\ll \frac{1}{4} \vec{A} \vec{D}, M(\vec{v}_c)_2 - M(\vec{v}_c)_1 = 0 \rightarrow \vec{v}_c = 0$

$\rightarrow \frac{1}{4} \vec{A}_i \vec{D}, \vec{A}_i \vec{D} \vec{O} \vec{U} \vec{U} \vec{E} \vec{O} \rightarrow \frac{1}{4} \vec{E} \vec{E} \vec{A}_i \vec{D} \rightarrow \vec{A} \vec{E} \vec{O} \vec{A} \vec{I} \vec{O}$

$\pm \vec{u} \vec{A} \vec{D} \vec{O} \rightarrow \vec{O} \vec{E} \vec{A} \vec{C} \vec{O} \rightarrow \vec{U} \vec{I} \vec{I} \vec{O} \rightarrow \vec{O} \vec{I} \vec{O} \vec{A} \vec{I} \vec{D} \rightarrow \vec{D} \vec{O} \vec{I} \vec{D} \rightarrow \vec{y} \vec{E} \vec{y}$

$\frac{1}{4} \vec{v}_1 \vec{v}_2 \times \vec{A} \vec{A} \vec{O}, \vec{O} \vec{S}_2 \div \vec{S}_1 \vec{D} \vec{E} \vec{S} \vec{A} \vec{S} \vec{A} \vec{O} \vec{A}_i \vec{E} \vec{S} \vec{A} \vec{D} \vec{O} \vec{D} \vec{y} \vec{p} \vec{A} \vec{I} \vec{O}$

4.4.12 $\vec{A} \vec{A} \vec{U} \vec{O}$

4.4.12.1(1) $0-\vec{D} \vec{A} \vec{U} \vec{E} \vec{A} \vec{I} \vec{D} \vec{O} \vec{A} \vec{D} \vec{O} \vec{A} \vec{C} \vec{O} \vec{E} \vec{O} \vec{A}_i \vec{E} \vec{O} \vec{A} \vec{A} \vec{I} \vec{D} \vec{O} \vec{I} \vec{S}_1 \vec{D} \vec{O} \vec{A} \vec{C} \vec{I}$

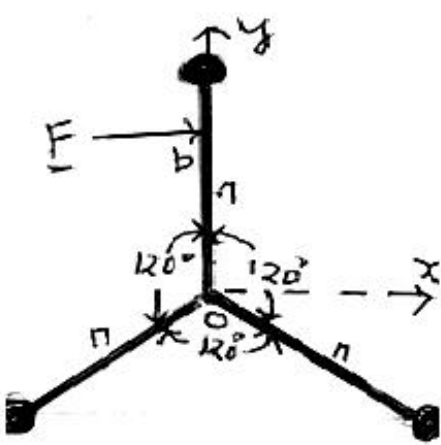
$\vec{I} \vec{E} \vec{A}_i \vec{E} \vec{C} \vec{E} \vec{I} \vec{I} \vec{D} \vec{O} \vec{A}_i \vec{y} \vec{E} \vec{O}, \vec{S} \vec{A} \vec{m} \vec{C} \vec{E} \vec{I} \vec{I} \vec{D} \vec{O} \vec{A} \vec{y} \vec{U} \vec{A} \vec{O} \vec{D} \vec{O} \vec{U}$

$\vec{A} \vec{I} \vec{D} \vec{O} \vec{A} \vec{C} \vec{O} \vec{I} \vec{D} \vec{E} \vec{A} \vec{A}_i \vec{U} \ll \vec{A} \vec{O} \vec{D} \vec{U} \vec{C} \vec{D} \rightarrow \vec{p} \vec{u} \vec{A} \vec{A} \vec{O} \vec{I} \vec{D} \vec{O} \vec{A} \vec{E} \vec{A} \vec{E} \vec{O} \vec{A}_i \vec{E}$

$\vec{C} \vec{I} \vec{A}_i \vec{E} \vec{S} \vec{A} \vec{U} \vec{A} \vec{A} \vec{O} \vec{O} \vec{y} \vec{E} \vec{O} \vec{C} \vec{A}_i \vec{I} \vec{I} \vec{D} \vec{O} \vec{U} \vec{C} \vec{D} \rightarrow \pm \vec{v}_1 \vec{A}_i \vec{A}_i \vec{D} \vec{C} \vec{A} \vec{A} \vec{O}$

$\vec{C} \vec{I} \vec{A}_i \vec{D} \vec{A} \vec{C} \vec{O} \vec{F} \vec{y} \vec{U} \vec{A} \vec{D} \vec{O} \vec{y} \vec{E} \vec{O} \vec{A} \vec{I} \vec{D} \vec{O} \vec{A} \vec{C} \vec{O} \vec{I} \vec{D} \vec{E} \vec{A} \vec{A}_i \vec{U}$

$\vec{A} \vec{A} \vec{y} \vec{A} \vec{I} \vec{D} \vec{O} \vec{A} \vec{I} \vec{D} \vec{E} \vec{D}$



(a) $0-\vec{D} \vec{U} \vec{C} \vec{A} \vec{y} \vec{O} \vec{I} \vec{I} \vec{D} \vec{O}$ (b) $\vec{D} \vec{O} \vec{A} \vec{C} \vec{O} \vec{y} \vec{S}_1 \vec{D} \vec{O} \vec{I} \vec{I} \vec{D} \vec{O} \rightarrow \vec{A} \vec{A} \vec{U} \vec{O} \vec{E} \vec{O}$

$(\vec{A} \vec{C} \vec{O} \vec{D} \vec{O} (a) \vec{a} = \frac{F}{3m} \vec{i}; (b) \vec{a} = \frac{fb}{3mn^2} \vec{i})$

(2) $\vec{a} \vec{y} \vec{U} \vec{A} \vec{I} \vec{D} \vec{O} \vec{U} \vec{O} \vec{A} \vec{I} \vec{D} \vec{O} \vec{A} \vec{C} \vec{O} \vec{E} \vec{O} \vec{A}_i \vec{E} \vec{O} \vec{A} \vec{A} \vec{I} \vec{D} \vec{O} \vec{I} \vec{S}_1 \vec{D} \vec{O} \vec{A} \vec{C} \vec{I}$

(a) (b) $\vec{S}_1 \vec{D} \vec{O} \vec{A} \vec{C} \vec{O} \vec{U} \vec{A} \vec{I} \vec{D} \vec{O} \vec{U} \vec{I} \vec{I} \vec{D} \vec{O} \vec{A} \vec{I} \vec{D} \vec{O} \vec{A} \vec{I} \vec{D} \vec{O} \vec{U} \vec{A} \vec{I} \vec{D} \vec{O} \vec{y} \vec{E} \vec{E} \rightarrow \pm \vec{E} \vec{S} \vec{A}$

$t = 2.2 \vec{A} \vec{C} \vec{E} \vec{I} \vec{E} \vec{A} \vec{C} \vec{O}, 5 \vec{D} \vec{O} \vec{U} \vec{C} \vec{y} \vec{I} \vec{D} \vec{O} \vec{A} \vec{C} \vec{O} \vec{y} \vec{S}_2 \div \vec{S}_1 \vec{D} \vec{O} \vec{I} \vec{D} \vec{O} \vec{A} \vec{C} \vec{O} \vec{y} \vec{S} \vec{A} \vec{D} \vec{O} \frac{G}{2.2}$

$\vec{i} - 2.6 \vec{j} + 4.6 \vec{k} \text{ kgm/s } \pm \vec{y} \vec{U} \vec{U} \vec{C} \vec{D} \rightarrow t = 2.4 \vec{A} \vec{C} \vec{E} \vec{I} \vec{E} \vec{A} \vec{C} \vec{O} \vec{S}_2 \div \vec{S}_1 \vec{D} \vec{O} \vec{I} \vec{D} \vec{O} \vec{A} \vec{C} \vec{O} \vec{y} \vec{S} \vec{A} \vec{D} \vec{O}$

$\frac{G}{2.4} = 3.7 \vec{i} - 2.2 \vec{j} + 4.9 \vec{k} \text{ kg.m/s } \pm \vec{y} \vec{U} \vec{A} \vec{I} \vec{D} \vec{O} \vec{U} \vec{A} \vec{I} \vec{D} \vec{O} \vec{E} \vec{D} \rightarrow \vec{S}_2 \div \vec{S}_1 \vec{D} \vec{O} \vec{I} \vec{D} \vec{O} \vec{A} \vec{C} \vec{O} \vec{y} \vec{S} \vec{A} \vec{D} \vec{O}$

$$T_f - T_i = 350 \text{ N}$$

$$[(v_A)_f = (v_B)_f = N]$$

$$U_{i-f} = T_f - T_i = 11536.56 = 350N^2 - 0$$

$$\therefore N = 5.741 \text{ m/s}$$

(1) $N^2 = N_0^2 + 2as$

$$(5.741)^2 = 0 + 2a(3.5)$$

$$\therefore a = 4.708 \text{ m/s}^2$$

$$T + 420a - 4120.2 = 0$$

$$T = 2142.84 \text{ N}$$

4.4.12.12 A block of mass 600 kg is pushed up a smooth inclined plane of length 4.5 m and height 1.5 m. Find the work done by the pushing force.

« $W = mgh = 600 \times 9.8 \times 1.5 = 8820 \text{ J}$ »
 (Answer: 8820 J)

4.4.12.13 A block of mass 750 N is pushed up a rough inclined plane of length 1500 N and height 1500 N. The coefficient of friction is 0.2. Find the work done by the pushing force.

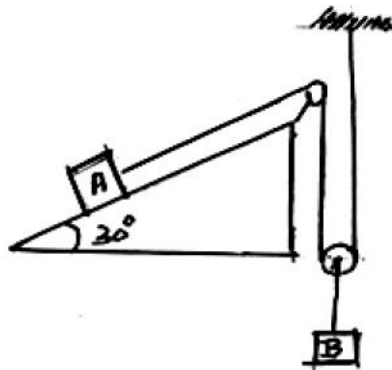


Figure 4-4-19

$$v_A = 2.532 \text{ m/s}$$

4.5. Движение частицы (IMPULSE MOMENTUM PRINCIPLE OF PARTICLE)

Одним из основных законов механики является закон сохранения импульса. Импульс частицы определяется произведением ее массы на скорость. Вектор импульса совпадает по направлению с вектором скорости. Закон сохранения импульса гласит, что суммарный импульс системы частиц сохраняется, если на систему не действуют внешние силы. Вектор импульса является вектором, поэтому его можно складывать по правилу сложения векторов. Импульс является векторной величиной, поэтому его можно складывать по правилу сложения векторов. Импульс является векторной величиной, поэтому его можно складывать по правилу сложения векторов.

4.5.1 Импульс (Impulse)

Импульс \vec{I} определяется как изменение импульса \vec{p} за время Δt : $\vec{I} = \vec{p}_1 - \vec{p}_0 = m(\vec{v}_1 - \vec{v}_0)$. Импульс является векторной величиной, поэтому его можно складывать по правилу сложения векторов. Импульс является векторной величиной, поэтому его можно складывать по правилу сложения векторов.

$$\vec{I} = \vec{F}(t_1 - t_0) = \vec{F}\Delta t$$

Вектор импульса совпадает по направлению с вектором силы. Импульс является векторной величиной, поэтому его можно складывать по правилу сложения векторов. Импульс является векторной величиной, поэтому его можно складывать по правилу сложения векторов.

Импульс является векторной величиной, поэтому его можно складывать по правилу сложения векторов. Импульс является векторной величиной, поэтому его можно складывать по правилу сложения векторов. Импульс является векторной величиной, поэтому его можно складывать по правилу сложения векторов.

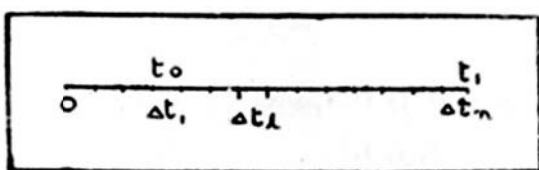


Рис. 4-5-1

« Если на частицу действует сила \vec{F} , то ее импульс \vec{p} изменится на $\vec{I} = \vec{F}\Delta t$. Импульс является векторной величиной, поэтому его можно складывать по правилу сложения векторов. Импульс является векторной величиной, поэтому его можно складывать по правилу сложения векторов.

$$\vec{I} = \sum_{i=1}^n \vec{F}_i \Delta t_i$$

ŞAÖö, $\underline{F}_i, i=1,2,\dots,n$ ±ýÀ" Å "ÖÖ" É Å" ° Çjì ö. « ÄüËý |¾jì ÀÄý Å" °, \underline{R} -ì ö. ¾ÄôÀð¼ (t_i-t₀) ,jÄ þ" ¼|ÄÇÄø, |¾jì ÀÄý Å" °Äý ¾jì Ç" Ä, Å" ° ü "ü|ÄjýËüì ö -jÄ ¾jì Ç" ÄÄý ÌÈÄÄø ÜðÍ ò|¾jì ìì î °ÄÄjì ö.

\underline{L} ±ýÄð, |¾jì ÀÄý Å" °ì ÌjÄ ¾jì Ç" Ä ±Éø,

$$\begin{aligned} \underline{L} &= \int_{t_0}^{t_1} \underline{R} dt = \int_{t_0}^{t_1} \left(\sum_{i=1}^n \underline{F}_i \right) dt \\ &= \sum_{i=1}^n \int_{t_0}^{t_1} \underline{F}_i dt \\ &= \underline{I}_1 + \underline{I}_2 + \dots + \underline{I}_n \end{aligned}$$

-ì ö.

4.5.2. Å" Ä¼ Ö" ÈÄø ¾jì Ç" Å" Äì ½ì ¼ø:

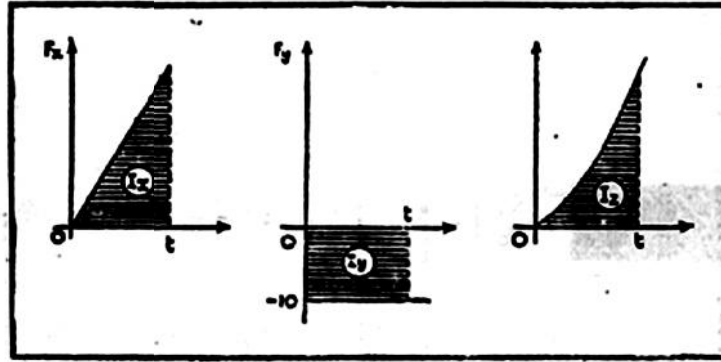
"Ö Å" °Äý ¾jì Ç" Ä "Å" °-jÄ" Å" Ä¼ø¼ø, (Force-time graph), T ,jÄ « ÇÄø, t = 0, t = T ±ýÜö Ìð¾jìÄí Üì Ì þ" ¼ôÀð¼ ÄôÄjø ÌÈü ,ôÄì ö. ±î òðì ,jð¼j, $\underline{F} = 4t\underline{i} - 9\underline{j} + 6t^2\underline{k}$ ±ýÜö Å" ° "Ö ð Çø t = 0, t = T ±ýÜö þ" ¼,jÄ ŞjÄð¼ø |°ÄüÄÄ ¾jì |,jü. \underline{F} ý Ç,Ä¾jì Ç" Ä

$$\begin{aligned} \underline{L} &= \int_0^T \underline{F} dt = \int_0^T (4t\underline{i} - 9\underline{j} + 6t^2\underline{k}) dt \\ &= 2T^2\underline{i} - 9T\underline{j} + 2T^3\underline{k} \end{aligned}$$

-ì ö.

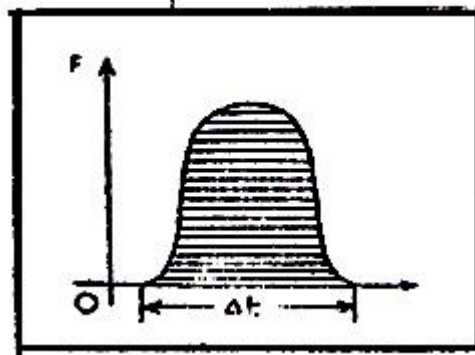
þì Ì ¾jì Ç" ÄÄý Ä,Ç×,ü, ŞjÄð" ¾î °j÷óð (4.5.2)-ø ,jðÈÄÄjÜ Å" °ôÄ,Ç× Å" Ç×ôÄj" ¾î Ì ö, t « îìì ö, t = T ±ýÜö Ç" Äì Ş,jðÍ ìì ö þ" ¼ÄöüÇ ÄôÄÇ× Å" ÄÄÜì Ì ö.

Ç" ¼Ö" Èì ½ì Ì Çø, Å" °Äý ÄÈÄ" Äòð |¾jìÄjÄŞÄŞÄ, « ¾ý ¾jì Ç" ÄÄjÉð « ÇÄ¼ì ÜÈÄð. ±î òðì ,jð¼j, Äð" ¼ ýËjø (bat) "Ö Äó" ¾ « Èì Ì öŞÄjð, ÄÄýÄì ð¾ôÀð¼ Å" °" Ä Å" ÄÄÜôÄð ,ÈÉÄjì ö. « üÄ¼ Å" °Äý ±ñ Ä¼ôÄø ²üÄì ö ÄjÜÄjÄ, Ä¼ö (4.5.3)-,jðÈÄÄjÜ þÖì Ì Üî ö. ¾jì ð ŞjÄð Ä,î °ÈÄ¾jì þÖòÄÜö, Å" °ÄjÉð |ÄjÄ¾jì þÖì Ì Üî Äj¾Äjø, ¾jì Ç" Ä "Ö Ì ÈöÀð¼ « Ç× Ä¼ö" Äò |ÄÈð¾jì ¾jì ,üÇð.



À¼õ 4-5-2

±ÉŞÅ ¼¼ì Ç Á - - ó¼ Ó È (Impulse - Momentum Method) Åø, Åç ° Çý Å¼õø Ç « ÈÅ;ÅŞÅŞ, « Å, ù Åç ÇÅ Ì õ - ó¼ Å;üÈø ¼ « Çó¼ÈÅ ÓÈõ.



À¼õ 4-5-3

4.5.3.Ð Ù Ì Ì Å ¼¼ì Ç Á - - ó¼ò ¼òÐÅò ¼ « ÈÅ Ì õ °Áý Å;ø ¼ Å ÆÅÜò¼ø.

m ç È Æ Å Ð ù ý Èø, $F = \pm y \dot{U} \delta$ Åç ° ÅüÅ Æ¼¼ì Ì ù. ç ä ø¼ Èý þ Æñ ¼ Å;Ð Å¼õÅÈ

$$F = ma \rightarrow \delta.$$

ç È Æ Å;ÈÅ;¼¼ø,

$$F = m \frac{dv}{dt} = \frac{d}{dt}(mv) \pm \text{É} \times \delta \text{ È} \text{ Å;ø.}$$

þ Ì (mv) ±ý Ùø çç °Å;ÉÐ, $S_{z \pm} S_{z; \delta} \text{È}$ - ç¼ø (Linear momentum) ±ÉøÅ Æ. ±ÉŞÅ, ç ä ø¼ Èý þ Æñ ¼ Å;Ð Å¼ç Å Ì ù Ì Ì õ ÅÈç¼; Õ Å Æ “ Æ Ì Å; ÕÇý - ó¼ Å; ÙÅ; Æ¼Å;ÉÐ, « ¼ý ÅÐ ÅøÅ Æ Åç ò Ì $S_{z \pm} \text{Å} \text{¼} \text{°} \text{Å;ø} \ll \text{Å} \text{Å} \text{¼} \text{Å} \ll \text{ù} \text{Åç} \text{°} \text{ÅüÅ} \text{ø} \text{¼ç} \text{°} \text{Å} \text{ŞÅ} \text{Ş} \text{Å} \text{-} \text{ó¼} \text{Å;} \text{ÙÅ; Æ} \text{ø} \text{üÅ} \text{ø} \text{.} \text{”}$

ŞĂÖõ, $\underline{F} = \frac{d}{dt}(m\underline{v})$ « ÇĂüî ò Ð ÇÛŞÁø | °ÄüÂî ÁĭÂŷ, Ññ ½¼ Ó· ÈÄø, $\underline{F} = \frac{d}{dt}(m\underline{v})$ ±ý Ûõ °Áý Àĭ ð ¼ ò | ¼ĭ · · ÄĬ õŞĀĭÐ,

$$\begin{aligned} \underline{I} &= \int_{t_0}^{t_1} \underline{F} dt = \int_{t_0}^{t_1} \frac{d}{dt}(m\underline{v}) dt \\ &= \int_{v_0}^{v_1} d(m\underline{v}) \\ &= m\underline{v}_1 - m\underline{v}_0 \end{aligned}$$

±ý ÄÐ - ó¼ĀĭüÈĀĭ ò.

±ÉŞĀ, - ó¼ĀĭüÈð¼ĭø, ¼ĭ ÷ Ç· Ā « ÇĂ¼ôÂî õ ±ý ÄÐ ç· ¼ĭ ÇÈÐ. ñ ŞĀ, çä ð¼Éŷ þĀñ ¼ĭĀÐ Ā¼Ĭ ì ò ÄŷĀÖõ ĀĒĀð¼ø ÄÇì õ | ĭĬ ì Āĭ ð.

¼ĭĬ ì õÄð¼ ō ŞĀð¼ø, Ð ÇÛŞÁø - ó¼ĀĭüÈõ, « ¼· É Ā· ÇĂĬ ì Ā· °Äŷ ¼ĭ ÷ Ç· ĀĬ Ĭ °ÁĒĭ ð, « Ş¼ ¼Ĭ · °ÄÄÖĬ ì õ.

4.5.4 Ð ū ŷËŷ Ā· ò ð¼ĭ ÷ ç ŷÛ | °ÄüÂî õŞĀĭÐ, ¼ĭ ÷ Ç· Ā - ¼ð ¼ðÐĀ ð ¼ ĀÇĬ ì ¼ø.

m ç· Èõ ¼Ā Ð ū ŷ $\{F_i\}, i=1,2,\dots,u$ ±ý Ûõ Ā· ° ū | °ÄüÂî Ā¼ĭ ì

| ĭ ū · « ÄüËŷ | ¼ĭ ĀĀ· É, $\underline{R} = \sum_{i=1}^n \underline{F}_i$ ±ý Ûõ ç· °ÄĀ· ĀĀŪĬ ì õ.

çä ð¼Éŷ þĀñ ¼ĭĀÐ Ā¼Ĭ ì ĀĒ,

$$\underline{R} = \sum_{i=1}^n \underline{F}_i = m\underline{a} \quad \text{ñ ì õ.}$$

« ùĀ· ò ð¼ĭ ÷ ç Ð ÇÛø $(t_1 - t_0)$ ĭĬ « ÇĂüî Ĭ | °ÄüÂî ÁĭÂŷ, Ññ ½¼ Ó· ÈÄø,

$$\underline{I} = \int_{t_0}^{t_1} \underline{R} dt = \int_{t_0}^{t_1} \left(\sum_{i=1}^n \underline{F}_i \right) dt = \int_{t_0}^{t_1} m \underline{a} dt$$

« ¼ĭĀÐ

$$\begin{aligned} I &= \sum_{i=1}^n \int_{t_0}^{t_1} \underline{F}_i dt = \int_{t_0}^{t_1} m \frac{d\underline{v}}{dt} dt \\ &= \int_{v_0}^{v_1} m d\underline{v} \end{aligned}$$

« 3/4 j ĀĐ

$$\underline{I} = \sum_{i=1}^n \underline{I}_i = m \underline{v}_1 - m \underline{v}_0 = \text{ó} \frac{3}{4} \hat{A}_i \ddot{u} \hat{E} \hat{A}_i \hat{l} \hat{o}.$$

±É ŠĀ, | 3/4 j ĩ ĀĀý Āċ'' °Āċý 3/4 j ĩ , Ç'' ĀŌō - ó 3/4 Ā_i üĒ ò 3/4 j ∅ « Ç ĀĈŌĀĪ ō.

4.5.5. 3/4 j ĩ , Ç'' Ā - - ó 3/4 ò 3/4 ò ĐĀĪ °Āý Ā_i ðĒý ±ñ 1/2 ō Ā_s Ĉ × , Ç ĩ , j ĩ 3/4 ∅.

$$\underline{I} = \int_{t_0}^{t_1} \underline{F} dt = m \underline{v}_1 - m \underline{v}_0$$

Āċ'' °, 3/4 ċ'' ° ŠĀ_s ō - , (ĀĀüĒċý Ā_s Ĉ × , ũ, i, j, k 3/4 ċ'' °, Ç ∅,

$$\underline{F} = X \underline{i} + Y \underline{j} + Z \underline{k} \pm \underline{E} \times \underline{o}$$

$$\underline{v} = v_x \underline{i} + v_y \underline{j} + v_z \underline{k}$$

$$\underline{v} = v_x \underline{i} + Y \underline{j} + Z \underline{k} \pm \underline{E} \times \underline{o} | , j \hat{u} \hat{C} \hat{o} \hat{A} \hat{l} \hat{o}.$$

±É ŠĀ,

$$\int_{t_0}^{t_1} (X \underline{i} + Y \underline{j} + Z \underline{k}) dt = m (v_x \underline{i} + v_y \underline{j} + v_z \underline{k})$$

$$- m (v_{0x} \underline{i} + v_{0y} \underline{j} + v_{0z} \underline{k}),$$

« 3/4 j ĀĐ,

$$\underline{i} \int_{t_0}^{t_1} X dt + \underline{j} \int_{t_0}^{t_1} Y dt + \underline{k} \int_{t_0}^{t_1} Z dt = m (v_{1x} - v_{0x}) \underline{i} + m (v_{1y} - v_{0y}) \underline{j} + m (v_{1z} - v_{0z}) \underline{k}$$

→ ĩ ō.

$$\therefore \int_{t_0}^{t_1} X dt = m (v_{1x} - v_{0x})$$

$$\int_{t_0}^{t_1} Y dt = m (v_{1y} - v_{0y})$$

$$\int_{t_0}^{t_1} Z dt = m (v_{1z} - v_{0z})$$

±ý Ū ō ±ñ 1/2 ō °Āý Ā_i Ī ũ , Ĉ'' 1/4 ĩ , ŋĒĒ.

[Ī ĒŌŌ: 3/4 j ĩ , Ç'' Ā - - ó 3/4 Ī °Āý Ā_i Ī , Āċ'' ° ĩ ō 3/4 ċ'' ° ŠĀ_s ò 3/4 ũ ĩ ō - ũ Ç | 3/4 j 1/4 ÷ Ā | Ā Ç ŌĀĪ ò Đ_s ĈĐ. « ũ Ā 3/4 Ī °Āý Ā_i ðĒü ĩ ò 3/4 Ĉ × , j 1/2, | °ĀüĀĪ ō Āċ'' , F - É Đ, Ā_i Ē_i Āċ'' °Ā_i , ŠĀ_j « ∅ĀĐ Š_s Ā ò 3/4 ċý °_i ÷ ĀĒÉ_i , ŠĀ_j pŌ ĩ , ŠĀñ Ī ō.]

4.5.6. $\frac{3}{4}i \text{ } \frac{1}{2}j \text{ } \hat{A} = \int \hat{A} \cdot d\vec{l} = \int (2i - 20j + 9k) \cdot (dx \hat{i} + dy \hat{j} + dz \hat{k})$
 $\therefore [I] = [F \times T] = [FT] = \text{J} \cdot \text{m}^{-1}$

ŞAÖö, $\frac{3}{4}i \text{ } \frac{1}{2}j \text{ } \hat{A} \cdot \hat{n} = \int \hat{A} \cdot \hat{n} \, dV = \int (2i - 20j + 9k) \cdot (dx \hat{i} + dy \hat{j} + dz \hat{k})$
 $\hat{A} \cdot \hat{n} = 2x - 20y + 9z$
 $\int_V (2x - 20y + 9z) \, dV = \int_0^1 \int_0^1 \int_0^1 (2x - 20y + 9z) \, dx \, dy \, dz$
 $= [M] \times [L/T]$

4.5.7 $\hat{A} = \frac{3}{4}i \text{ } \frac{1}{2}j \text{ } \hat{A}$

4.5.7.1 $\int_C \hat{A} \cdot d\vec{l} = \int_C (2i - 20j + 9k) \cdot (dx \hat{i} + dy \hat{j} + dz \hat{k})$
 $\int_C (2x - 20y + 9z) \, d\vec{l} = \int_0^5 (2x - 20y + 9z) \, dt$
 $\int_0^5 (2x - 20y + 9z) \, dt = \int_0^5 (2x - 20y + 9z) \, dt$

$$\frac{1}{25} (12i - 20j + 9k) \cdot \hat{l} = \frac{1}{25} (12i - 20j + 9k)$$

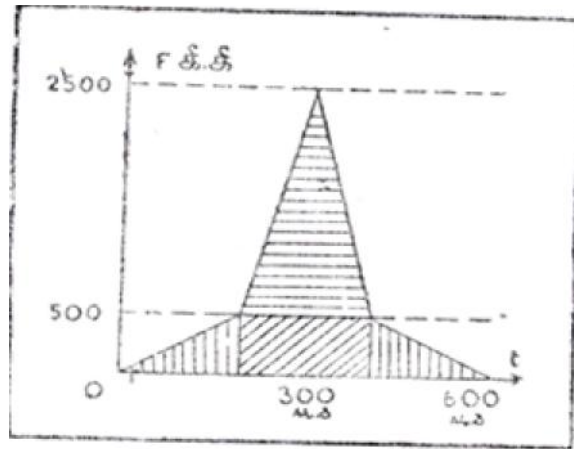
$$\begin{aligned} \therefore I_z &= \int_0^5 (F \cdot k) \, dt \\ &= \int_0^5 \frac{12}{25} (12i - 20j + 9k) \cdot k \, dt \\ &= \frac{108}{25} \int_0^5 dt \\ &= 21.6k \cdot \hat{l} \\ \therefore I_z &= 21.6 \cdot \hat{l} \end{aligned}$$

4.5.7.2 $\int_C \hat{A} \cdot d\vec{l} = \int_C (2i - 20j + 9k) \cdot (dx \hat{i} + dy \hat{j} + dz \hat{k})$

$\hat{A} \cdot \hat{n} = (2x - 20y + 9z) \cdot (dx \hat{i} + dy \hat{j} + dz \hat{k})$
 $\int_V (2x - 20y + 9z) \, dV = \int_0^1 \int_0^1 \int_0^1 (2x - 20y + 9z) \, dx \, dy \, dz$

$\hat{A} = \hat{A} \cdot \hat{n} = \int_C \hat{A} \cdot d\vec{l} = \int_C (2i - 20j + 9k) \cdot (dx \hat{i} + dy \hat{j} + dz \hat{k})$

$$\begin{aligned} &= \left(\frac{1}{2} \times 200 \times 500 + 200 \times 500 + \frac{1}{2} \times 200 \times 2000 + \frac{1}{2} \times 200 \times 500 \right) \cdot \hat{l} \\ &= 0.4 \cdot \hat{l} \end{aligned}$$



À¼õ 4-5-4

4.5.7.3. 100 t $\text{S}\ddot{\text{A}}\text{i}$ $\text{Q}\ddot{\text{A}}\text{i}$ o \pm $\frac{1}{4}$ $\text{O}\ddot{\text{U}}\text{C}$ o $\ddot{\text{O}}$ $\frac{1}{4}$ $\text{A}\ddot{\text{I}}\text{Y}\ddot{\text{U}}$, $\text{A}\ddot{\text{I}}\text{o}\times\text{i}$ i o 0.2 \pm $\text{Y}\ddot{\text{U}}\text{C}$ $\text{A}\ddot{\text{E}}\text{A}\ddot{\text{E}}\text{o}\text{A}\ddot{\text{U}}\text{E}$ o C $\frac{1}{4}$ $\text{C}\ddot{\text{O}}\text{C}$ o $\mu\ddot{\text{o}}\times$ C $\text{A}\ddot{\text{A}}\text{O}\ddot{\text{U}}\text{C}$. 75 t C $\text{A}\ddot{\text{C}}\text{o}$ \pm n $\text{A}\ddot{\text{A}}\text{o}$ i i n $\frac{1}{4}$ $\text{A}\ddot{\text{C}}\text{o}$ $\text{Y}\ddot{\text{U}}\text{C}$ $\frac{1}{4}$ $\text{S}\ddot{\text{I}}\text{O}\ddot{\text{E}}\text{U}\ddot{\text{I}}$ 30° $\text{Z}\ddot{\text{U}}\text{A}\ddot{\text{I}}$ $\text{S}\ddot{\text{I}}\frac{1}{2}$ i $\text{A}\ddot{\text{O}}$ $\text{A}\ddot{\text{A}}\text{o}$ (4.5.5) o $\text{S}\ddot{\text{I}}\text{O}\ddot{\text{E}}\text{A}\ddot{\text{A}}\text{i}\text{U}$, o $\frac{1}{4}$ $\text{A}\ddot{\text{Y}}$ SAo 3 $\text{A}\ddot{\text{E}}\text{i}\text{E}$ u i $\text{A}\ddot{\text{U}}\text{A}\ddot{\text{I}}$ $\text{C}\ddot{\text{E}}\text{D}$. « o $\text{S}\ddot{\text{I}}\text{O}\ddot{\text{E}}\text{A}\ddot{\text{A}}\text{i}\text{U}$ o $\frac{1}{4}$ $\text{A}\ddot{\text{U}}\text{E}$ $\text{p}\ddot{\text{U}}\text{C}$ $\text{S}\ddot{\text{A}}$ o $\text{A}\ddot{\text{I}}\text{D}$?

$$N \pm \text{Y}\ddot{\text{A}}\text{D} \pm \frac{3}{4} \text{C} \frac{3}{4} \text{i} \text{A}\ddot{\text{C}}\text{o}$$

$$F = -N \pm \text{Y}\ddot{\text{A}}\text{D} - \text{A}\ddot{\text{I}}\text{o} \times \text{A}\ddot{\text{C}}\text{o} \text{A}\ddot{\text{I}}\text{o}$$

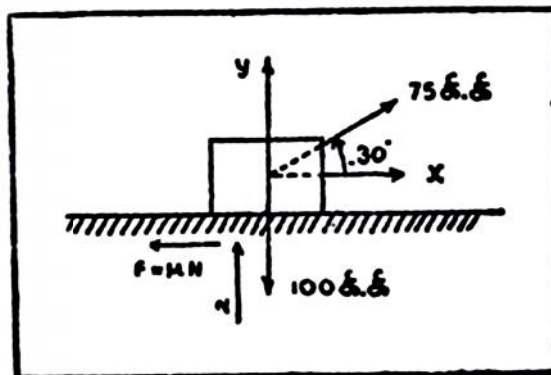
$$\text{o}$$

$$\sum f_{iy} = 0 - \text{i} \text{o}$$

$$\therefore 75 \times \frac{1}{2} - 100 + N = 0$$

$$\pm \text{E} \text{S}\ddot{\text{A}}, N = 62.5 \text{ t}$$

$$F = N = 0.2 \times 62.5 = 12.50 \text{ t}$$



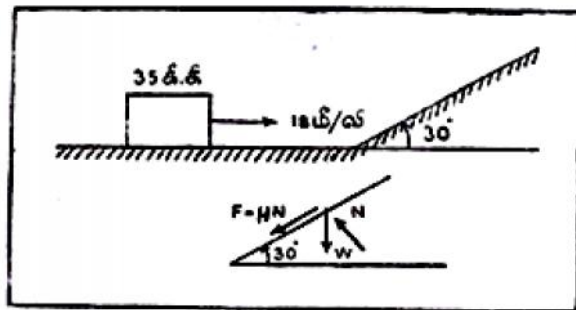
À¼õ 4-5-5

$$\begin{aligned}
 &= 75 \cos 30^\circ - N \\
 &= 75 \times \frac{\sqrt{3}}{2} - 12 \cdot 50 \\
 &= 52.44 \text{ t. t. } \ddot{\text{A}}\text{t}^\circ \\
 \therefore \int_0^3 F dt &= m v_1 - m v_0
 \end{aligned}$$

±ý Á¾jø,

$$\begin{aligned}
 \int_0^3 52.44 dt &= \frac{100}{9.81} v_1 - 0 \\
 \therefore v &= \frac{9.81}{100} \times 52.44 \times 3 \\
 &= 15.44 \text{ Á/ ÁÉ jÉ.}
 \end{aligned}$$

4.5.7.4. 35 t. t. Ájõ ±üüÇ | Ájõ | ÇjýÚ ÁÉjÉì | 18 Ájõ ÷
 ŠÁjõ pÁì | ŠÁjõ « Ð 30° züÈì Šj½î°jÇ Áõ | ÀüÈ ÁÆÁÆòÀüÈ
 °jõÇò¾ « üÇÉÐ, - Ájõxì | ø 0.3 ±Éø, « ò | Ájõü °jõÇò¾
 µöüÇ Á Áõ | ÁÚÁ¾ü ±îì | õŠjõ Ájõ?



Ájõ 4-5-6

°jõÇò¾üì î | íì òÐò¾Ç °Áø | ÁjõÜì | pÁì ÁøÁjõ ÁÁjõ, $\sum f_{iy} = 0$
 -î õ.

$$\therefore N - W \cos 30^\circ = 0$$

«¾jÁÐ,

$$N = 35 \times \frac{\sqrt{3}}{2} = 30.31 \text{ t. t.}$$

$$F = \mu N$$

$$= \mu N$$

$$= 0.3 \times 30.31 = 9.093 \text{ t. t.}$$

$t \int_0^t (-35 \sin 30^\circ - 9.093) dt = 0 - \frac{35}{9.81} \times 18$

$$\int_0^t (-35 \sin 30^\circ - 9.093) dt = 0 - \frac{35}{9.81} \times 18$$

$$(17.5 + 9.093)t = \frac{70}{1.09}$$

$$\therefore t = \frac{70}{1.09 \times 26.593}$$

$$= 2.415 \text{ s}$$

4.5.7.5 108 N, $\mu = 0.2$, $\theta = 42^\circ$, $P = 56 \text{ N}$, $AB = 45 \text{ cm}$, $BC = 108 \text{ cm}$, $AC = 117 \text{ cm}$. P is applied at A at an angle of 42° to the horizontal. T_1 and T_2 are tensions in the strings AB and BC respectively. C is a pulley. $\mu = 0.2$.

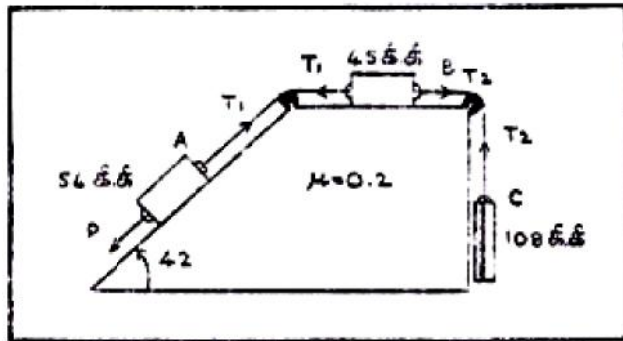


Figure 4-5-7

The block is on a horizontal surface. The force P is applied at A at an angle of 42° to the horizontal. The tensions in the strings are T_1 and T_2 .

The force P is applied at A at an angle of 42° to the horizontal. The tensions in the strings are T_1 and T_2 .

The force P is applied at A at an angle of 42° to the horizontal. The tensions in the strings are T_1 and T_2 .

The force P is applied at A at an angle of 42° to the horizontal. The tensions in the strings are T_1 and T_2 .

Σ M_A:

$$= [P + 54 \sin 42^\circ - 0.2(54 \cos 42^\circ) - T_1] \times 20$$

$$= \frac{54}{9.81}(6-3)$$

Σ M_B:

$$[T_1 - T_2 - 0.2(45)] \times 20 = \frac{45}{9.81}(6-3),$$

Σ M_C:

$$[T_2 - 108] \times 20 = \frac{108}{9.81}(6-3),$$

Σ M_o = 0

$$[P + 54 \sin 45^\circ - 0.2(54 \cos 45^\circ) - 9 - 108 \times 20]$$

$$= \frac{(54 + 45 + 108)}{9.81} \times 3$$

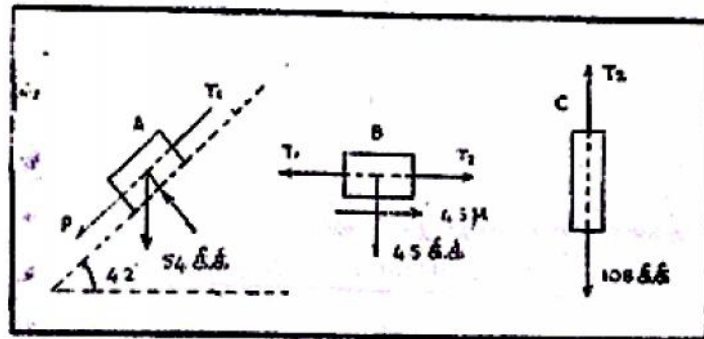


Figure 4-5-8

Σ M_o:

$$(P + 36 \cdot 130 - 8.026 - 9 - 108) \times 20$$

$$= \frac{207 \times 3}{9.81}$$

$$\therefore P - 88.896 = 3.120$$

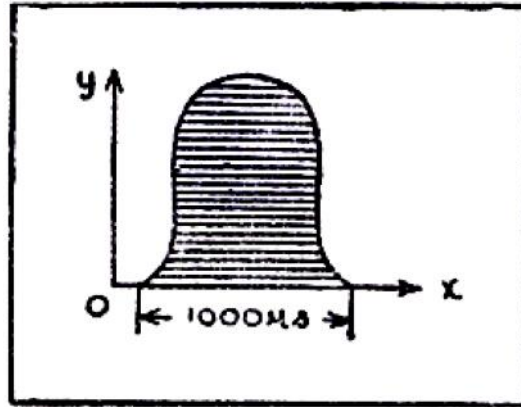
$$\therefore P = 3.120 + 88.896 = 92.016$$

$$P = 3.120 + 88.896 = 92.016$$

4.5.8 \vec{A} \vec{u}

4.5.8.1 \vec{O} \vec{A} \vec{u} 1000 \vec{A} \vec{S} \vec{A} \vec{E} \vec{E} \vec{C} \vec{O} , \vec{A} (4.5.9) \vec{u} \vec{E} \vec{A} \vec{A} \vec{U} , 500 \vec{C} \vec{a} \vec{d} \vec{y} - \vec{A} \vec{E} \vec{E} « \vec{C} \vec{x} \vec{u} \vec{C} \vec{A} \vec{i} \vec{C} \vec{A} \vec{A} \vec{z} \vec{u} \vec{A} \vec{O} \vec{u} \vec{C} \vec{D} \vec{E} \vec{O} , « \vec{u} \vec{A} \vec{y} \vec{A} \vec{i} \vec{O} \vec{i} \vec{t} \vec{n} \vec{A} \vec{O} \vec{A} \vec{D} ?

[\vec{A} \vec{u} : 5×10^5 \vec{C} \vec{a} \vec{d} \vec{y}]



\vec{A} (4.5.9)

4.5.8.2 \vec{O} \vec{S} \vec{A} \vec{u} \vec{A} \vec{u} \vec{C} \vec{D} \vec{S} \vec{C} \vec{i} \vec{y} \vec{U} \vec{A} \vec{i} \vec{O} \vec{u} \vec{C} \vec{A} \vec{O} \vec{x} \vec{C} \vec{A} \vec{O} \vec{u} \vec{C} \vec{D} . \vec{S} \vec{A} \vec{O} \vec{A} \vec{i} \vec{O} \vec{D} \vec{A} \vec{i} \vec{U} \vec{E} \vec{A} $\vec{F} = t^2 \vec{i} + (6t + 10) \vec{j} + 1.6t^3 \vec{k}$ \vec{C} \vec{C} \vec{y} \vec{U} \vec{O} \vec{A} \vec{u} « \vec{y} \vec{S} \vec{A} \vec{O} \vec{A} \vec{O} \vec{A} \vec{D} . 5 \vec{A} \vec{E} \vec{E} \vec{u} \vec{y} \vec{E} \vec{A} \vec{y} , \vec{D} \vec{C} \vec{O} \vec{S} \vec{A} \vec{O} \vec{A} \vec{i} \vec{u} .

[\vec{A} \vec{u} : $(41.666\vec{i} + 125\vec{j} + 250\vec{k})$ \vec{A} \vec{E} \vec{E}]

4.5.8.3 3.27 \vec{S} \vec{A} \vec{u} \vec{A} \vec{u} \vec{C} \vec{D} \vec{S} \vec{C} \vec{i} \vec{y} \vec{E} \vec{O} , $\vec{F} = t^2 \vec{i} - 2\vec{j} + 0.4t\vec{k}$ \vec{S} \vec{A} \vec{u} \vec{A} \vec{u} \vec{C} \vec{D} . \vec{S} \vec{A} \vec{O} $t = 3$ \vec{A} \vec{E} \vec{E} \vec{u} \vec{C} \vec{S} \vec{A} \vec{D} , \vec{D} \vec{C} \vec{i} \vec{E} \vec{D} , $\vec{v}_0 = (3\vec{i} - 2\vec{j} + \vec{k})$ \vec{A} \vec{E} / \vec{A} \vec{E} \vec{E} \vec{y} \vec{U} \vec{O} \vec{S} \vec{A} \vec{O} \vec{A} \vec{u} \vec{U} \vec{C} \vec{D} . $t = 3$ \vec{A} \vec{E} \vec{E} \vec{u} \vec{C} \vec{S} \vec{A} \vec{D} , « \vec{y} \vec{S} \vec{A} \vec{O} \vec{A} \vec{i} \vec{u} .

[\vec{A} \vec{u} : $(30\vec{i} - 20\vec{j} + 6.4\vec{k})$ \vec{A} \vec{E} \vec{E}]

4.5.8.4 98.1 \vec{S} \vec{A} \vec{u} \vec{A} \vec{u} \vec{C} \vec{D} \vec{S} \vec{O} \vec{A} \vec{i} \vec{y} \vec{U} , \vec{A} \vec{E} \vec{A} \vec{O} \vec{A} \vec{E} \vec{u} \vec{C} \vec{S} \vec{A} \vec{D} \vec{A} \vec{i} \vec{y} \vec{E} \vec{O} \vec{x} \vec{C} \vec{A} \vec{O} \vec{u} \vec{C} \vec{D} . « \vec{y} \vec{S} \vec{A} \vec{O} $(10 - 2t)$ \vec{S} \vec{A} \vec{u} \vec{A} \vec{u} \vec{C} \vec{D} . \vec{A} \vec{u} \vec{y} \vec{U} , \vec{S} \vec{A} \vec{O} \vec{A} \vec{u} \vec{C} \vec{D} . « \vec{O} \vec{D} \vec{u} \vec{O} \vec{S} \vec{A} \vec{O} \vec{S} \vec{A} \vec{O} , \vec{A} \vec{C} \vec{O} \vec{A} \vec{A} \vec{S} \vec{A} \vec{O} \vec{A} \vec{U} \vec{O} ? « \vec{O} \vec{S} \vec{A} \vec{D} « \vec{y} \vec{S} \vec{A} \vec{O} \vec{A} \vec{i} \vec{u} .

[\vec{A} \vec{u} : 5 \vec{A} \vec{E} \vec{E} \vec{u} : \vec{i} \vec{O} \vec{S} \vec{A} \vec{O} = \vec{A} \vec{E} \vec{E}]

4.5.8.5 3 $\text{SÄ}_j, \text{Ä}_j \text{ö}$ z^{c} ÈÖüç $\text{D}_s \text{ü}$ $\text{y}^{\text{E}} \text{y}^{\text{S}} \text{A} \text{ø}$, $14t^2$ $\text{SÄ}_j, \text{Ä}_j \text{ö}$
 $\pm \text{n}$ $\text{Ä}^{\text{c}} \text{ö} \text{üç}$ Ä^{c} ö y^{U} , $(3i - 6j + 2k)$ $\pm \text{y}^{\text{U}} \text{ö}$ S^{c} $\text{ö} \text{Ä}^{\text{c}} \text{I}$ p ö $\text{Ä}_j \text{ü}$
 $\text{I}^{\text{c}} \text{ö} \text{Ä}^{\text{c}} \text{I}$ $\text{ö} \text{E} \text{D}$. $t = 0$ $\pm \text{y}^{\text{U}} \text{ö}$ $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$, $(6i + 9j + 5k)$ $\text{Ä}^{\text{c}} \text{ö} \text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$
 $\text{p} \text{Ä}^{\text{c}} \text{I}$ I $\text{Ä}^{\text{c}} \text{ö}$, $t = 3$ $\text{Ä}^{\text{c}} \text{E}_j \text{E} \text{Ä}_j \text{ü}$ $\text{üç} \text{S}^{\text{c}} \text{Ä}_j \text{D}$, $\ll \text{y}^{\text{c}} \text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö} \text{Ä}_j \text{D}?$

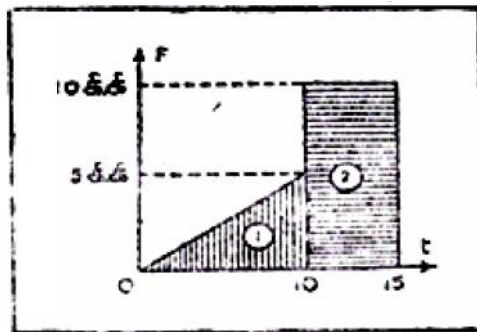
[Ä^{c} ö $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$: $(182 \cdot 58i - 344 \cdot 16j + 122 \cdot 72k)$ $\text{Ä}^{\text{c}} \text{E}_j \text{E}$]

4.5.8.6. 50 $\text{SÄ}_j, \text{Ä}_j \text{ö}$ z^{c} ÈÖ^{c} $\text{Ä}^{\text{c}} \text{D}_s \text{ü}$ $\text{y}^{\text{E}} \text{ö}$, t $\text{Ä}^{\text{c}} \text{E}_j \text{E}$ $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$ $\text{I}^{\text{c}} \text{ö} \text{Ä}^{\text{c}} \text{I}$ ö
 $(1.5696i - 1.5j + 2.7468k)$ Ä^{c} $\text{ö} \text{I}^{\text{c}} \text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$ Ä^{c} $\text{ö} \text{ç} \times$ Ä^{c} ö $F = 3t^2i - 7k$ ö
 Ä^{c} $\text{ö} \text{Ä}_j \text{ö}$. $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$ $t = 0$ $\pm \text{y}^{\text{U}} \text{üç} \text{S}^{\text{c}} \text{Ä}_j \text{D}$, $\text{D}_s \text{ü}$ $v_n = 1.5j$ $\text{Ä}^{\text{c}} \text{E}_j \text{E}$ $\pm \text{y}^{\text{U}} \text{ö}$
 $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö} \text{D} \text{y}$ $\text{p} \text{Ä}^{\text{c}} \text{I}$ I $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$, $t = 2$ $\text{Ä}^{\text{c}} \text{E}_j \text{E} \text{Ä}_j \text{ü}$ $\text{üç} \text{S}^{\text{c}} \text{Ä}_j \text{D}$, $\ll \text{y}^{\text{c}}$
 $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö} \text{I}^{\text{c}} \text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$.

[Ä^{c} ö $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$: $\text{Ä}^{\text{c}} \text{E}_j \text{E}$]

4.5.8.7. $\text{m} \times \text{z}^{\text{c}}$ $\text{Ä}^{\text{c}} \text{ö} \text{üç}$ $\text{D}_s \text{ü}$ $\text{ç} \text{y}^{\text{E}} \text{y}^{\text{S}} \text{A} \text{ø}$, $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$ $\text{I}^{\text{c}} \text{ö} \text{D}$ $\text{Ä}_j \text{U} \text{ö}$ Ä^{c} ö
 $\text{y}^{\text{E}} \text{y}^{\text{S}} \ll \text{Ä}^{\text{c}} \text{ö}$, $\text{Ä}^{\text{c}} \text{ö}$ (4.5.10) ö $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$ $\text{üç} \text{D}$. $\text{D}_s \text{ç} \text{y}^{\text{E}}$ z^{c} È 3
 $\text{SÄ}_j, \text{Ä}_j \text{ö}$ $\pm \text{E} \times \text{ö}$ $\ll \text{D}$ ö $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$ $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$, Ä^{c} ö $\text{I}^{\text{c}} \text{ö} \text{Ä}^{\text{c}} \text{I}$ ö $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$
 $\text{z}^{\text{c}} \text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö} \times \text{ö}$ $\text{I}^{\text{c}} \text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$, 15 $\text{Ä}^{\text{c}} \text{E}_j \text{E}$ $\text{ç} \ll \text{D}$ $\text{Ä}^{\text{c}} \text{U} \text{ö}$ $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$ $\text{I}^{\text{c}} \text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$.

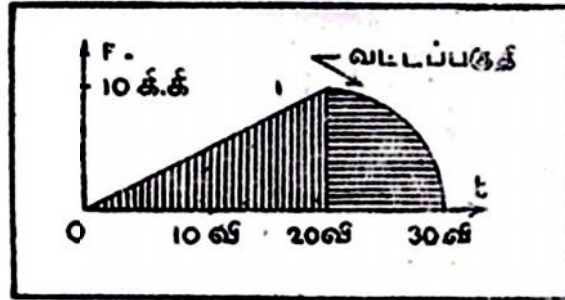
[Ä^{c} ö $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$: $(1.5696i - 1.5j + 2.7468k)$ $\text{Ä}^{\text{c}} \text{E}_j \text{E}$]



$\text{Ä}^{\text{c}} \text{ö}$ 4- 5-10

4.5.8.8 ö $\text{I}^{\text{c}} \text{ö} \text{Ä}^{\text{c}} \text{ö}$ $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$ $\text{I}^{\text{c}} \text{ö} \text{Ä}^{\text{c}} \text{I}$ ö Ä^{c} ö y^{U} 2 $\text{SÄ}_j, \text{Ä}_j \text{ö}$
 z^{c} $\text{È} \text{Ä}^{\text{c}} \text{ö} \text{I}^{\text{c}} \text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$ $\text{D}_s \text{ü}$ y^{E} . $\ll \text{D}$ $\text{m} \times \text{z}^{\text{c}}$ $\text{Ä}^{\text{c}} \text{ö}$ $\text{üç} \text{S}^{\text{c}} \text{Ä}_j \text{D}$ $\text{I}^{\text{c}} \text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$.
 $\ll \text{Ä}^{\text{c}}$ $\text{ö} \text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$ $\text{I}^{\text{c}} \text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$ $\text{Ä}^{\text{c}} \text{ö}$, $\text{Ä}^{\text{c}} \text{ö}$ (4.5.11)- ö $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$ $\text{Ä}^{\text{c}} \text{ö} \text{Ä}^{\text{c}} \text{ö}$
 $\text{Ä}^{\text{c}} \text{ö} \text{Ä}^{\text{c}} \text{ö}$ $\text{I}^{\text{c}} \text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$ $\pm \text{E}$, 30 $\text{Ä}^{\text{c}} \text{E}_j \text{E}$ ü $\text{y}^{\text{E}} \text{Ä}^{\text{c}} \text{y}$, $\text{D}_s \text{ü}$ $\text{Ä}^{\text{c}} \text{U} \text{ö}$ $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$ $\text{I}^{\text{c}} \text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$.

[Ä^{c} ö $\text{S}^{\text{c}} \text{Ä}^{\text{c}} \text{ö}$: 89.27 $\text{Ä}^{\text{c}} \text{E}_j \text{E}$]



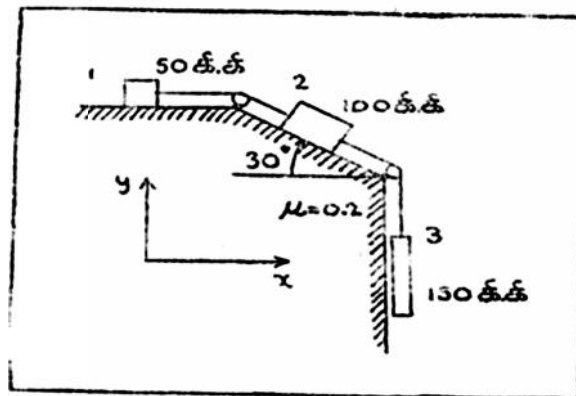
À¼õ 4-5-11

4.5.8.9 À¼õ (4.5.12)-ð ðËÄÄ;Ù, |Ä;Õð|¼;|¼Ï ÿÙ, µö× ÒËÄÄ;Ù 10 ÄÉ;Ë ðÿË Äÿ, « ÄËÿ¼Ï ÑÄ;ð¼; ðÿ.

4.5.8.8 Ò |ËÄÄ;¼¼Ï ðÿÏ ÄÏ ðÿÙ 2 ÑÄ;¼;¼; ÒËÄÄ;Ù ÄËË ðÿË. « ð µö× ÒËÄÄ;Ù ÒËÄÄ;Ù ðÿË. « ÒÄÿÏ Äÿ¼;Ï Ä Ä¼Ï, À¼õ (4.5.11)-ð ðËÏËÏ ÄÄÄ;Ä;ð ÄÄÄ;Ù ðÿË, 30 ÄÉ;Ë ðÿË Äÿ, ðÿÄÏ ÑÄ;ð¼; ðÿ.

[Äÿ¼: 89.27 ÄÄÉ;Ë]

4.5.8.9 À¼õ (4.5.12)-ð ðËÄÄ;Ù, |Ä;Õð|¼;|¼Ï ÿÙ, µö× ÒËÄÄ;Ù 10 ÄÉ;Ë ðÿË Äÿ, « ÄËÿ¼Ï ÑÄ;ð¼; ðÿ.



À¼õ 4-5-12

ðÄ;Ù ÄÄ;¼¼Ï ÄËË ÄËË, ðÄ;Ù ÄÄÄ;Ù ÄËË ÄËË. [Äÿ¼: 56.45 ÄÄÉ;Ë]

4.5.9 ðË¼;¼; |ÄÿÏ (Impulsive Forces)

m çċ' ÈÔ' ¼Ā |À;Õû 'ýÈÿ ÁÐ P - ±ýÛō Āċ' °Ā;ÉÐ, T
 SĶĀð¾ĀÛ ò ¾jì Ì Ā¾j;ì |;j;Û. Þó¾ SĶĀð¾Āÿ |¾j;¼ì ,ò¾ĀÏō ÞÛ¾ĀĀÏō
 « ò|À;ÕÇÿ ŞĀ' í , ù Ó' ÈŞĀ ^{v₁,v₂} ±Éì |;j;Û.

$$Pt = m(v_2 - v_1)$$

¾Āð' ¾ĀĠ °ÈÈ¾j;ì Ą |;j;ñ Ī Āċ' °' Çō |À;¾j;ì Ą |;j;ñ Ī ò
 |°øÏōŞĀ;Ð, « ĀüÈÿ |ĀÏì ò ÓĒ×ÛÇ¾j; ÞÏì ì ÛĪ ò. « ò¾' Ā
 Āß|ĀÏ Āċ' °Āÿ Āċ' Ç×, « ùĀċ' ° Āċ' ÇĀĀ Ī ò - ó¾Ā;üÈð¾j;ø
 « ÈĀĀĀĪ ò. - , ŞĀ, Ī Û,Ā ,¾Āð¾Āø |°ĀüĀĪ ò Āß|ĀÏĀċ' °Ā;ÉÐ
 ,½ð¾j;ì Āċ' ° ±ÉðĀĪ ò.

Ā' ĀĀ' È

'Ï ,½ð¾j;ì Āċ' ° 'Ï Āċ' °ÈĀ SĶĀð¾ĀŞĀ ¾j;ì Ì ,ÿÈ 'Ï
 Āċ' ò|À;Ā Āċ' °Ā;Ī ò. - ĀĀÛ ò. « ùĀċ' ° 'Ï Ð ,ÇÿÁÐ ¾j;ì Ì ò SĶĀð¾Āø
 « òÐ ,Çÿ çċ' ĀĀ;üÈø (change in position) ÒÈì ,½Ą ,òĀ¼Ā;ò. « ¾ÿ
 ÓøĀċ' Ç× ò « ¾ÿ - ó¾Ā;üÈð¾j;ø « ÇĀĀðĀĪ ò.

- ñ 'ĀĀø « ò¾' Ā ÓĒĀÛ Āċ' Ì Û,Ā 'Ï ,¾Āð¾ĀÛ ò
 ¾j;ì Ì ,ÿÈ Āċ' ò|À;Ā 'Ï Āċ' °' Āð |ĀÛĀÐ ÓĒĀ;¾¾Ī ò. - ĀĀÛ ò
 °òĀðĒĀ;ø |;j;Ī ì ,òĀĪ ò ¾j;ì Ì , ,Ą |;ø Āó¾Āÿ ÁÐ Āó¾ĒÈì ò Āð' ¼
 |;j;Ī Ì ò « È - ,Ā' Ā « ò¾' Ā ,½ð¾j;ì Āċ' °' Çō |À;Ðð
 'ð¾ĀÏì ì ÛĒĀ ±Ī òÐì ,j;ðĪ ,Ç;Ī ò.

4.5.10 ÞÏ ĀĒĀĒòĀ;É |À;Õû ,Çÿ ŞĀ;Ð' ,

A , B ±ýÛō ÞÏ |À;Õû , ù 'ýŞÈ;|¼ÿÛ ŞĀ;ÐðŞĀ;Ð çċ' ð¾Ēÿ
 āÿÈ;ĀÐ ÞĀì ,Ā¾ĀĒĒ, « 'Ā 'ý'È;Ā;ÿÛ |¾Ī Ī ò 'ù|Ā;Õ
 ,½ð¾ĀÏō, B Āÿ ÁÐÛÇ A ÿ ¾j;ì ,Ç' Ā, A Āÿ ÁÐÛÇ B ĀĒÉÐ
 ¾j;ì ,Ç' Āì Ī Ī °ĀÛ |Ā¾ĀĀ;ĀĀÏì ò. Þ¾ĀĀÏð B ĀĒÉÐ - ó¾Ā;üÈð, A
 ĀĒÉÐ - ó¾Ā;üÈð¾ĀÛ Ī °ĀÛ |Ā¾ĀĀ;ĀĀÏì |ĀÿĀÐ |ĒÈĀĪ ò. - , ŞĀ
 ÞÛĀ¾Ā Ā;üÈĪ ,Çÿ |Ā;ð¾Ā, |Ā;ÐĪ |°í S;Ī ðĪ ¾ċ' °Āø « Çì ,òĒÿÿ
 āĪ°ĀĀ;Ī ò. ±ÉŞĀ « ùĀÏ |À;Õû , Û' ¼Ā - ó¾Ā;üÈð 'ŞĀ ¾ċ' °Āø

« ĀüÈÿ ŞĀ;Ð' ,Ā;ø Ā;È;Ð. « ¾ĀĀÐ $mu+mu' = mv+mv'$ ÞĪ°ĀÿĀ;Ī ,
 'SĶ÷S;Ī ðĪ - ó¾Ā;üÈð¾Āø ±Éì ÛÈĀĪ ò.

4.5.11 'Ï Ì ñ Ī , ÐòĀ;ì ,Ç - ,ĀĀüÈÿ ÞĀì , ò

'Ï ÐòĀ;ì ,Ç |ĒÈ ñ '¼Ā ĪĪ ,ÈÐ. « ò|Ā;øÐ « ¾Û ù ÞÏ Ì ò ò ù
 ¾ĄÈ |ĒÈ Āċ' ×Ā÷ó¾ « øð¾ð¾Āø Ā;ăĀ; Ā;Èð¾ÿ Āċ'Ā;ø « ¾Û ù Ç
 Ī ñ '¼ |ĀÇŞĀ |°ÏðÐ ,ÈÐ. « Ī Ì ñ Ī ÐòĀ;ì ,Ç ĀĀðĪ |ĀÇĄ ,Çðð
 Óÿ Ā;Ş¾Û |Ā;Õ ,½ð¾Āø « ¾ÿĀĀÐ ÓÛĀì ,Ā; , ²üĀð¼ Āċ' °

$$\therefore u = \frac{7}{10} \text{ m/s}$$

$$\therefore 0 - \frac{1}{2} \times \frac{20 \times 1000}{9.8} \times \frac{7}{10} \times \frac{7}{10} = -2 \times 1000 s$$

– üËø §, j ðÀi ðËý ÆË, ÆËí, ÇËý þÚ¼Ç þËî, – üËø-ÆËí, ÇËý |¼j¼î, þËî, – üËø = ÇËý É Êò ÆËË° |°ö¼ ±¼Ç-§ËË° Æ.

$$\therefore s = 25 \text{ s. } \text{Æ}$$

4.5.12.3 5000 ÇËj ð ±¼¼ÛÇ ° ÆËí, ÇËî ñ Î, ÆËÉjËË, ù 500 ÆË¼÷ §ËËð§¼jÎ |ÆËË, òËËË ÆËË. «¼ý þËî, – üËË° Æ ±¼¼ÛÇ, ÇËø, jñ. « òËËË, ÇËî 100 Ç. Ç. ÇËË° ÆËË ÆËË¼Û ì, ðËËý ° ÆËË (Free of Recoil) ñ |¼ËË, «¼ý ÆËËÉÊò – üËË° ÆËË, jñ.

$$\text{ÆËí, ÇËî ñ ËË þËî, – üËø}$$

$$= \frac{1}{2} \times 5000 \times 500 \times 500 \times 10^4$$

$$= 625 \times 10^{10} \text{ J}$$

ÆËí, ÇËý ÆËËÉÊò §ËË, ò u ñ ð.

∴ ñ ð¼ËË, jò ÆËËËËË.

$$5000 \times 500 \times 100 = 100 \times 1000 \times u$$

$$\therefore u = 2500 \text{ m/s}$$

ÆËí, ÇËý ÆËËÉÊò ÆËË

$$\frac{1}{2} \times 100 \times 1000 \times 2500 \times 2500$$

$$= 3125 \times 10^8 \text{ J}$$

4.5.12.4 ÆËÉjËË ì 28 ÆË¼÷¼Ç° §ËËðË¼ý, ÇË¼ËË, þËî ð 155 ÇËj ð ÇËË° ÆËËÛÇ ° ÇËË, j ð ÆËË §ËËËË, ÆËÉjËË ì 16 ÆË¼÷¼Ç° §ËËðË¼ý

¼ËËËË « ËË, òËËË ÆËË. ÆË¼ËË ð ÆËË¼ ÆËË¼ ð |¼jÎ ð §ËËË ð 18 ÆËÉjËË |ÆËË ÆË¼ËË ð ÆËË¼ |ÆËË ð ð ð ÆËË¼, j¼ð¼ËË ì ÆËË° ÆËË, jñ.

$P = \frac{1}{2} \rho A v^3$ $\rho = 1000 \text{ kg/m}^3$ $A = 0.5 \text{ m}^2$ $v = 2800 \text{ m/s}$

$$I = \frac{1}{2} \rho A v^3 t = 155 [2800 - (-1600)]$$

$$= 155 \times 4400 \text{ J} = 682000 \text{ J}$$

$I = Pt$

$$\therefore P = \frac{I}{t} = \frac{155 \times 4400}{\left(\frac{1}{18}\right)} = 18 \times 155 \times 4400$$

$$= \frac{18 \times 155 \times 4400}{981} = 12.513 \text{ W}$$

4.5.12.5 12 m/s 25 m 7 m/s 50 m 240 m 1000 kg $g = 9.81 \text{ m/s}^2$

$\Delta v = 240 \text{ m/s}$ $v = 1000 \text{ m/s}$ $\cos r = \frac{240}{1000} = 0.24$

$$50 \times 240 \times v = 10 \times 1000 \times v \cos r = 10 \times 1000 \times v \times \frac{24}{25}$$

$$\therefore v = 125 \text{ m/s}$$

$\Delta v = 240 \text{ m/s}$ $v = 125 \text{ m/s}$

$$\therefore 0^2 = 125^2 - 2 \times 981 \times \frac{7}{25} s$$

$$= -g \sin r = -981 \times \frac{7}{25}$$

$$\therefore s = 28.44 \text{ m}$$

$$(M + m)v = Mu \dots\dots(1)$$

ζÄð¼ P ζäð¼ý | ÇÉø, Ä¼ç, jø à ñ ζÄð¼ü ù | °øÄ¼ð

$$\frac{1}{2} \hat{I} \ddot{\theta} = P - (M + m)g$$

¬ üÈø, jøðð¼ðÄð¼ý ÄÊ,

$$\begin{aligned} \frac{1}{2}(M + m)v^2 &= [P - (M + m)g]a \\ \therefore P &= (M + m)g + (M + m)\frac{v^2}{2a} \\ &= (M + m)g + \frac{M + m}{2a} \frac{M^2 u^2}{(M + m)^2} \\ &= (M + m)g + \frac{M^2 u^2}{(M + m)2a} \\ &= (M + m)g + \frac{M^2}{(M + m)} \frac{2gh}{2a} \\ &= (M + m)g + \frac{M^2}{(M + m)} \frac{gh}{a} \dots\dots\dots(2) \end{aligned}$$

ζÄð¼¼ÄÊ jø²üÄÊ ò ±¼ç: ÓÏ ì, ò f ÄÄÊ; Ê² ±Éì |, ü.

ŞÄð¼¼ ì òÄý - üÇ v ±ý Üò ŞÄ¼ÄÊ Ð 'a' |¼¼ Ä× - ðÏ ó¼×¼ý
âî°ÄÄ¼Ä¼ø,

$$0 = v^2 - 2fa$$

$$\therefore f = \frac{v^2}{2a} \dots\dots\dots(3) \text{ ¬ ì ö.}$$

« òà ñ pÄî, ð¼ÄÖó¼ ŞÄö t ±Éø,

$$0 = v - ft$$

$$\therefore t = \frac{v}{f} = \frac{v}{v^2} 2a = \frac{2a}{v}$$

$$\therefore t = \frac{2a(M + m)}{M\sqrt{2gh}} = \frac{(M + m)a}{M} \sqrt{\frac{2}{gh}} \dots\dots\dots(4)$$

ŞÄö (1)-ÄÖóð $v = \frac{Mu}{M + m} = \frac{M}{M + m} \sqrt{2gh}$

ŞÄð¼¼ ÄÖüÇ pÄî, ¬ üÈÄÊøð,

$$\begin{aligned}
&= \frac{1}{2}(m + M) \cdot \frac{m^2 u^2}{(m + M)^2} \\
&= \frac{1}{2} \frac{m^2 u^2}{(m + M)} \\
&= \frac{1}{2} \left(\frac{m}{m + M} \right) m^2 u^2
\end{aligned}$$

Þrí $\frac{m}{m + M} < 1$ ±ý Á¼íø, ŞÁíÐ'' , ì òÀý ²üÄî õ ÞÁî , ñ üÈø, ŞÁíÐ'' , ì ì

Óý - ûç $\frac{1}{2} m u^2$ ±ý Ûõ ÞÁî , ñ üÈ'' ÄÄ¼î ì '' È×Äî õ.

±ÈŞÅ
ŞÁíÐ'' , Äíø ²üÄî õ ÞÁî , ñ üÈø ÞÆòð

$$\begin{aligned}
&= \frac{1}{2} \left(\frac{m}{m + M} \right) m u^2 - \frac{1}{2} m u^2 \\
&= \frac{1}{2} m u^2 \left[\frac{m}{m + M} - 1 \right] \\
&= - \frac{m M u^2}{2(m + M)}
\end{aligned}$$

ÞüÄ¼ ÞÆòð ²üÄî Ä¼íø, ñ üÈø Ş , ðÄíø'' ¼ (Principle of Energy),
 , ½ð¼í ì Ä'' ° , ù |¼í¼÷ÄíÉ , ½ì ì , Çø ÄÄýÄî ð¼í Û¼íÐ.

4.5.14 Ä¼íø ½ì ì , ù

4.5.14.1 m' ç'' Èòûç 'õ ì ñ î m'' ç'' Èòûç 'õ ÐòÄí ì , ÄÄöóð

ÄÉíÈì ì v' ŞÅ, ð¼ø ç'' ¼Äí, î í¼òÄòî , « ì ñ î / ç'Çóø, m' ç'' Èòø
 ì , ñ ¼ 'õ ¼Éç ° °ø Ş , ç'ø'' ¼ « Èì , ÈÐ. ÐòÄí ì ç' íðÉýÈç
 ÞÁí ì Ä¼í, ì ì ñ î

(i) « ¼ý ÄýÉÈòð ŞÅ, õ
(ii) ç'' Äì ì ð¼íÉ ç'' Äò¼ý ° °ø « '' Äì ì õ Ş , ½ò (Angle of Displacement for the Pendulum).

(iii) ŞÁíÐ'' , ì ì òÀý , Þ'' ÄÄø | °ÄøÄî õ ÞøÄ'' ° , ñ ÄÄü'' Èì , ñ .

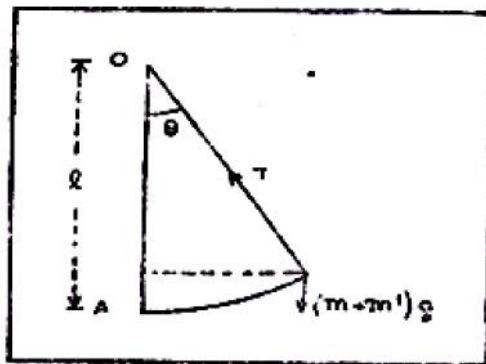
ÐòÄí ì ç' , ðÉýÈç v'' ±ý Ûõ ¼'' ° ŞÅ, ðð¼ÉÄí ì Ä¼í, ì ì ù .
 Şç' ì Ş , ðî - ó¼í , ì ðò Ä¼ÄýÄÈ,

$$m'' v'' + m' v' = 0$$

$$\therefore v'' = - \left(\frac{m'}{m''} \right) v'$$

$\vec{v} = \frac{m'}{m+m'} v' \rightarrow \vec{0}$.
 $\therefore v = \left(\frac{m'}{m+m'} \right) v' \rightarrow \vec{0}$.

t ±y Ūō 2S¾Ū | Á; Ō S¾Äð¾Ō, ¾ÉŌ ° °ø Œ· Äì ì òÐì S¾; ðĪ ¼ý Á¼ō
 (4.5.13) -ø Œ; ðĒÄ; Ū „ ±y Ūō ° °Ä; Ī Ō S¾; ½ð¾ ¾ 2üĀ òÐÄ¾; ì
 | Œ; Ū.



Ä¼ō 4-5-3

« ôŞÄ; Ð - üĒø Œ; òÐ Ä¾Ä; ÄĒ

$$\frac{1}{2}(m+m')v^2 = (m+m')gl(1-\cos \theta)$$

« ¾; ÄÐ $\cos \theta = \frac{2gl-v^2}{2gl} \rightarrow \vec{0}$. $(m+m') \pm y \hat{U} \circ \text{Œ} \cdot \hat{E} \cdot \hat{A} \circ | \hat{A} \hat{U} \hat{E} \hat{D} \hat{S} \hat{U} \hat{O}$

±y Ūō Œ· ÄòüŒ· Ä · ÄÄ; ì | Œ; ñ Ī . Ō Œ· Äì ì òÐ Äð¾ôÄì ¾ÄŌ
 « · ÄxŪÄ¾; ø Œäð¾ÉŸ þÄñ ¼; ÄÐ Ä¾ôÄĒ þ· ÄĒŌ | °ÄŌĪ Ō T
 ±y Ūō þŌÄŒ· °Ä; ÉÐ.

$$T - (m+m')g = (m+m')a_n = (m+m')\frac{v^2}{l}$$

$$\therefore T = (m+m')\left(g + \frac{v^2}{l}\right) \pm y \hat{E} \hat{I} \hat{O}$$

4.5.14.2 56 SÄ; Ä; Œ· ÈŌ· ¼Ä Ō °ôÄðĒ 1.6Äð¾; | ¾; · ÄÄÄŌóÐ
 ÄŌóÐ þŌðð Œ· È Ÿ· È « Èð¾ÄŸ µöÄ· ¼; ĒÐ. « È Œ; úó¾ S¾ÄŌ $\frac{1}{40}$
 ÄÉ; Ē. « ĩ°ô ÄðĒÄ; ø þŌðÄŸÄÐ ÄÄŸĀĪ ò¾ôÄð¾ ½ð¾; ì Ī ÄŒ· °
 Ä; Ē; | ¾Éì | Œ; ñ Ī « ¾· Ēì Œ; ñ . (g=9.8 ÄŸ ÄÉ; Ē) °ÄÄðĒ þŌðð

$v = \sqrt{2gh} = (2 \times 9.8 \times 1.6)^{\frac{1}{2}} = 5.6 \text{ m/s}$
 $\Delta t = \frac{v}{g} = \frac{5.6}{9.8} = 0.57 \text{ s}$
 $\Delta t = 0.57 \text{ s}$

$$v = \frac{1}{2} a t^2 \Rightarrow 5.6 = \frac{1}{2} a (0.57)^2$$

$$\begin{aligned} \therefore a &= \frac{2 \times 5.6}{(0.57)^2} \\ &= \frac{11.2}{0.3249} \\ &= 34.47 \text{ m/s}^2 \end{aligned}$$

$P = \frac{1}{2} m v^2 = \frac{1}{2} \times 56 \times (5.6)^2 = 878.08 \text{ J}$
 $\Delta t = 0.57 \text{ s}$

$$P = \frac{W}{t} = \frac{878.08}{0.57} = 1539.97 \text{ W}$$

$$\therefore (P - 56 \times 9.8) t = I = \Delta t \cdot C \cdot A$$

$$\therefore P - 56 \times 9.8 = \frac{56 \times 5.6}{\frac{1}{40} \times 9.8} = \frac{56 \times 5.6 \times 40}{9.8} = 1280$$

$$P = 1280 + 56 \times 9.8 = 1828.8 \text{ W}$$

4.5.14.3 $m = \rho V = \rho A s$, $M = \rho A s$, $\Delta t = \frac{1}{2} a t^2$
 $\Delta t = \frac{1}{2} a t^2 \Rightarrow 5.6 = \frac{1}{2} a (0.57)^2$
 $\Delta t = 0.57 \text{ s}$

$\Delta t = \frac{1}{2} a t^2 \Rightarrow 5.6 = \frac{1}{2} a (0.57)^2$
 $\Delta t = 0.57 \text{ s}$

$$0 - \frac{1}{2} m u^2 = -F \cdot s$$

$$\therefore \frac{1}{2} m u^2 = F s$$

$\Delta t = \frac{1}{2} a t^2 \Rightarrow 5.6 = \frac{1}{2} a (0.57)^2$
 $\Delta t = 0.57 \text{ s}$

$$(M + m) v = m u + M O = m u \quad \dots\dots\dots(ii)$$

$\Delta t = \frac{1}{2} a t^2 \Rightarrow 5.6 = \frac{1}{2} a (0.57)^2$
 $\Delta t = 0.57 \text{ s}$

$$\frac{1}{2}mv^2 - \frac{1}{2}mu^2 = -F(x+y) \quad \dots\dots\dots(iii)$$

→ üËø §, i ðÄi ðËÿÀË , ð'' ¼'' ¼'' Âî °i ðóð.

$$\frac{1}{2}Mv^2 - 0 = Fy \quad \rightarrow \dot{\bar{1}} \bar{o} \quad \dots\dots\dots(iv)$$

(iii) (iv) → , ÇÄü'' Èì Ü ð¼

$$\frac{1}{2}(m+M)v^2 - \frac{1}{2}mu^2 = -Fx$$

$$\ll \text{¼}i \text{Äð} \frac{1}{2}(m+M) \frac{m^2u^2}{(m+M)^2} - \frac{1}{2} \cdot 2Fs = -Fx$$

$$\frac{1}{2} \frac{m(2Fs)}{(m+M)} - \frac{1}{2} \cdot 2Fs = -Fx$$

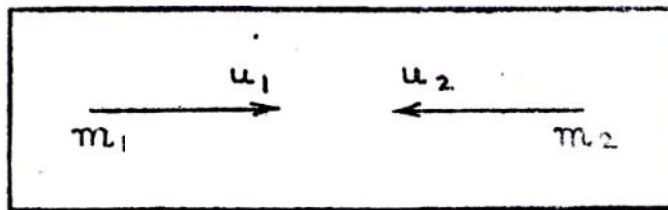
$$\therefore x = \frac{Ms}{M+m}$$

4.5.14.4 ' Õ ì ñ Î | ÄËòð m₁, m₂ ±ÿ Û ð ç'' È, Û'' ¼Ä p Õðñ Î , Çi , Äççì , ðÄÎ , ÿËÈ. « '' Ä Ó'' ÈÏÄ u₁, u₂ ±ÿ Û ð | ¼i ¼i ð ¼ç'' °ÏÄ, í , Û ¼ÿ ±¼ç: ð¼ç'' ° , Çç pÄì ì , ÿËË. p¼Ë ç pÄì , ñüËç.

$$\frac{1}{2} \frac{m_1, m_2}{m_1 + m_2} (u_1 + u_2)^2$$

« Ç × Äç ÄÄÿ ñ üÇð ±Ë ç Û × ,

ñ ó¼i §, i ðÄi ðËÿÀË



$$m_1u_1 - m_2u_2 = 0.$$

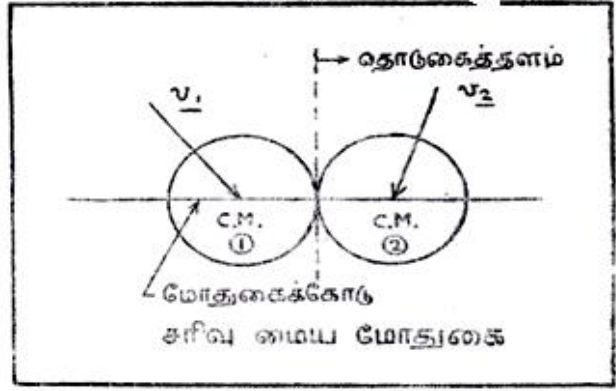
ì ñ Î | ÄËò¼üì Óÿ pÄì , ñüËø = 0

ì ñ Î | ÄËò¼Äÿ pÄì , ñüËø.

$$= \frac{1}{2}m_1u_1^2 + \frac{1}{2}m_2u_2^2$$

$$(m_1 + m_2)(m_1u_1^2 + m_2u_2^2) = (m_1u_1 - m_2u_2)^2 + m_1m_2(u_1 + u_2)^2 = m_1m_2(u_1 + u_2)^2$$

$v_1 > v_2$ எனில் v_1 மீது v_2 இடையே உள்ள வேக வேறுபாடு $v_1 - v_2$ ஆகும். இதை v_{rel} எனக் குறிக்கலாம். இவ்வேக வேறுபாடு v_{rel} இன் e பங்கு $v_1 - v_2$ ஆகும். $v_1 < v_2$ எனில் $v_2 - v_1$ ஆகும். இதை v_{rel} எனக் குறிக்கலாம். இவ்வேக வேறுபாடு v_{rel} இன் e பங்கு $v_2 - v_1$ ஆகும்.



À¼õ 4-5-15

4.5.16.4 e (Coefficient of restitution)

m_1, m_2 ஆகிய நிறைகள் v_1, v_2 வேகங்களில் நகர்ந்துள்ள இரண்டு பந்துக்களின் மீட்டிங் வேக வேறுபாடு $v_1 - v_2$ ஆகும். மீட்டிங் பின்னர் அவற்றின் வேக வேறுபாடு $v_1' - v_2'$ ஆகும். e என்பது $v_1' - v_2'$ இன் $v_1 - v_2$ இன் விகிதம் ஆகும். $v_1 > v_2$ எனில் $v_1 - v_2$ ஆகும். $v_1 < v_2$ எனில் $v_2 - v_1$ ஆகும்.

$v_1 > v_2$ எனில் $v_1 - v_2$ ஆகும். $v_1 < v_2$ எனில் $v_2 - v_1$ ஆகும். e என்பது $v_1' - v_2'$ இன் $v_1 - v_2$ இன் விகிதம் ஆகும். $v_1 > v_2$ எனில் $v_1 - v_2$ ஆகும். $v_1 < v_2$ எனில் $v_2 - v_1$ ஆகும். e என்பது $v_1' - v_2'$ இன் $v_1 - v_2$ இன் விகிதம் ஆகும்.

$$\underline{v}_1' - \underline{u} = e(\underline{u} - \underline{v}_1) \dots\dots\dots(6)$$

±ýËjì õ

« ùÁjşÈ m₂ ±ýÛõ ç' ÈÔ' ¼Ã pÃñ ¼jÁĐ Đ, Û ì ò

$$e = \frac{I_R}{I_C} = \frac{m_2(\underline{v}_2' - \underline{u})}{m_2(\underline{u} - \underline{v}_2)} \ll \text{øÄĐ}$$

$$\underline{v}_2^1 - \underline{u} = e(\underline{u} - \underline{v}_2) \pm \text{ýËjì õ} \dots\dots\dots(7)$$

(7)-ÁĐ °ÁýÀjõ' ¼ (6)-ÁĐ °ÁýÀjõÈÄÖóĐ, Æñ.

« øÄĐ

$$e = -\frac{\underline{v}_1' - \underline{v}_2'}{\underline{v}_1 - \underline{v}_2} = -\frac{\text{ÄçÖõ ç' °ŞÄ, õ (Velocity of separation)}}{\text{"i ì õ ç' °ŞÄ, õ (Velocity of approach)}} \dots\dots\dots(8)$$

¬ ì õ

e- ¬ ÉĐ ´Ö ÀjÁj ½ÁüÈ, ½ÄÁjì õ.

$$[\text{ì Èöò} \text{(i)}] \underline{I}_R = e \underline{I}_C = \frac{m_1 m_2}{m_1 + m_2} (\underline{v}_1 - \underline{v}_2)$$

$$\text{(ii)} \quad \text{¼Ájõç' ç' ç' } \underline{I}_C \text{ } \hat{A}$$

$$= \underline{I}_C + \underline{I}_R$$

$$= (1+e) \underline{I}_C = \frac{(1+e)m_1 m_2}{(m_1 + m_2)} (\underline{v}_1 - \underline{v}_2)$$

(iii) $\underline{u} = -\hat{i} \text{ ç' } \hat{A} - \hat{O} \hat{A} j \hat{u} \hat{E} \text{ ç' } \hat{y} \hat{S} \hat{A} j \hat{D} \ll \text{óşç'Äðç'ø } \hat{D}, \hat{u}, \hat{U} \text{ } \hat{¼} \hat{A} \text{ } \hat{¼} \hat{A} j \hat{D} \text{ ç' } \hat{ç' } \hat{S} \hat{A}, \hat{o}.$

$$= \frac{m_1 v_1 + m_2 v_2}{m_1 + m_2} = \frac{m_1 v_1' + m_2 v_2'}{m_1 + m_2} \pm \text{ýËjì õ]$$

ç' ÈÄÖóÔ' ¼Ã şÁjĐ' Äø pÚì ç' Äò ç' ì ç' ÄÖõ Äðç' Äò ç' ì ç' ÄÖõ °ÁÁjì õ. ±ÉŞÄ e-ý Áç'öò ´ýËjì õ. Äðç' ÈÈ şÁjĐ' Äø e-Äý Áç'öò âî °ÄÁjì õ. « ôşÁjĐ

$$\underline{v}_1' = \underline{v}_2' \text{ } \neg \text{ } \hat{i} \text{ } \hat{o}.$$

« ç' jÁĐ ðjõü, ù pÃñ ì õ ç' ç' ðì ì ç' jñ ş¼ ´şÄ ç' °ŞÄ, õç'ÄÄí ì õ.

4.5.16.6 ŠÁj^{3/4}Öi_j É Á^{3/4}ú

±øÄj^{3/4}Á^{3/4}ŠÁj^{3/4}ø_j Û ö_j lü_j ñ_j ¼^{3/4}ð^{3/4}Áí_j Û ì ðÄî ö.

(1) ĸä^{3/4}ð^{3/4}Éÿ_j Áj^{3/4}Š^{3/4} É Á^{3/4}ú

pŌ|Äj^{3/4}Öü_j ú_j ´ý_j È|Äj^{3/4}ý_jÚ_j š_jÄj^{3/4} ŠÁj^{3/4}Éj^{3/4}ø_j ŠÁj^{3/4}Đ^{3/4} ì_j ò_j
 Äÿ_j Û_j ç_j « ÄüËÿ_j °j^{3/4} Š^{3/4}ö_j ŠÁj^{3/4}Đ^{3/4} ì_j Óý_j Û_j ç_j « ÄüËÿ_j
 °j^{3/4} Š^{3/4}ö_j ů_j Ő_j Äj^{3/4}Ëj^{3/4}Á^{3/4}ö_j ±_jÄ^{3/4}ö_j Ä^{3/4}ö_j pŌ|Äj^{3/4} ÄÉ_j
 Áj^{3/4}Š^{3/4} É Áj^{3/4}Äj^{3/4} ĸä^{3/4}ð^{3/4}ý_j ñ_j ¼_j.

« ô|Äj^{3/4}Öü_j ú_j °j^{3/4}ö_j ŠÁj^{3/4}Éj^{3/4}ø_j ŠÁj^{3/4}Đ^{3/4} ì_j ò_j Äÿ_j « ÄüËÿ_j |Äj^{3/4}Đ_j
 |°í_j š_j ðËý_j Ä_j Š^{3/4}ö_j « ð^{3/4} Ä^{3/4}Š^{3/4}Ä^{3/4} ŠÁj^{3/4}Đ^{3/4} ì_j Óý_j
 Ä_j Š^{3/4}ö_j °j^{3/4} Š^{3/4}ö_j ů_j Ő_j Äj^{3/4}Ëj^{3/4}Á^{3/4}ö_j ±_jÄ^{3/4} È^{3/4}Ö^{3/4}É^{3/4}Ö^{3/4} ì_j ö.
 pŌ|Äj^{3/4}Ëj^{3/4}Á^{3/4}Š^{3/4} Ä^{3/4}ö_j ì_j ½_j ö « øÄ_j ĸ^{3/4} ÄÄ^{3/4} |_j øÄj^{3/4} ì_j ö.

(2) ŠÁj^{3/4}Đ^{3/4} ì_j š_j ðËý_j Ä_j pŌ|Äj^{3/4}Öü_j ç_j ý_j pÄî_j ö

pŌ|Äj^{3/4}Öü_j ç_j ý_j ŠÁj^{3/4}Đ^{3/4} Ä_j « Ä_j ±_jÄ^{3/4} ðËÄ^{3/4} ÒËÄ^{3/4} Ò_j Û ì_j ö
 - ðÄ^{3/4} ÄÄ^{3/4} Ä^{3/4} Ä^{3/4} ŠÁj^{3/4}Đ^{3/4} ì_j š_j ðËý_j Ä_j ç_j - ö^{3/4}ð^{3/4}ý_j |Äj^{3/4}ð^{3/4}ö_j
 Óý_j Û_j ò_j Äÿ_j Û_j ö °ÄÄj^{3/4} ì_j ö.

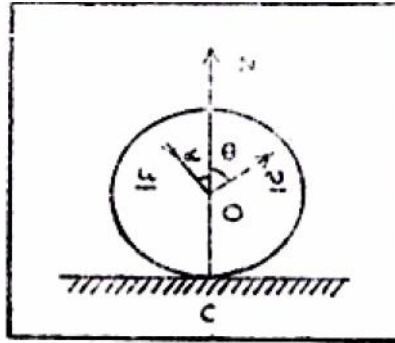
(3) ÄÉÄ^{3/4}öÄj^{3/4}É pŌ|Äj^{3/4}Öü_j ŠÁj^{3/4}Đ^{3/4} ì_j š_j ðËÿ_j ù_j |°í_j ð^{3/4}ö_j pÄî_j Á.

ÄÉÄ^{3/4}öÄj^{3/4}É pŌ|Äj^{3/4}Öü_j ú_j ´ý_j È|Äj^{3/4}ý_jÚ_j ŠÁj^{3/4}Đ^{3/4}ø_jŠÁj^{3/4}Đ_j
 « ÄüËË^{3/4} Š^{3/4}Ä^{3/4} |_j š_j ðËÿ_j ð^{3/4}ö_j Äj^{3/4}ĐÄ^{3/4} Ä_j - š^{3/4}Ä^{3/4} |Äj^{3/4}Öü_j Û ì_j ò_j
 p^{3/4} Š^{3/4}Ä^{3/4} Öü_j ç_j - ù_j ç_j Ö^{3/4} ì_j ö (Stress) ÓüË^{3/4} Ö^{3/4} « ÄüËÿ_j |Äj^{3/4}Đ_j |°í_j ð^{3/4}ö_j
 š_j ðËý_j Ä_j ç_j - ù_j ç_j Ä_j ±É_j Š^{3/4}Ä^{3/4} « ì_j š_j ðËý_j |°í_j ð^{3/4}ö_j ±_jÄ^{3/4} Ä^{3/4}ö^{3/4}
 Ä^{3/4}ö^{3/4} Ä_j « ^{3/4}Ä_jĐ_j |_j š_j ðËÿ_j ð^{3/4}ö_j ±_jÄ^{3/4} Ä^{3/4}ö^{3/4} Ä^{3/4}ö^{3/4}
 |°ÄüÄ^{3/4} Ä^{3/4}ö^{3/4} Ä_j - ^{3/4}Äj^{3/4}ø_j |_j š_j ðËÿ_j ð^{3/4}ö_j Š^{3/4}Ä^{3/4} Äj^{3/4}üË^{3/4} Ö^{3/4}ö_j ç_j ¼_j Äj^{3/4}Đ_j.
 ±É_j Š^{3/4}Ä^{3/4} |Äj^{3/4}Đ_j |°í_j š_j ðËÿ_j ð^{3/4}ö_j |°í_j ð^{3/4}ö_j É^{3/4} Ä^{3/4}ö^{3/4}, ´ü|Äj^{3/4}Ö_j |Äj^{3/4}Ö_j ç_j Û_j ¼_j Ä_j
^{3/4}ö^{3/4} Š^{3/4}Ä^{3/4}ö^{3/4} Ä_j × ŠÁj^{3/4}Đ^{3/4} Äj^{3/4}ø_j Äj^{3/4}Ëj^{3/4}ÄÄ^{3/4} Ö^{3/4} ì_j ö. Ä^{3/4}ö^{3/4} |Äj^{3/4}Öü_j ç_j ø_j
 ŠÁj^{3/4}Đ^{3/4} Ä_j ý_j |Äj^{3/4} ½_j Äj^{3/4} ²_j Ä^{3/4} ì_j ö pÄî_j Äj^{3/4}üË^{3/4} Ö^{3/4}ö_j Äÿ_j Ä^{3/4}ö^{3/4} ĸ^{3/4} Ä^{3/4} Ä_j ç_j ø_j
 |_j ½_j Äj^{3/4} ö.

4.5.17 ĸ^{3/4} ÄÄj^{3/4}É^{3/4} ç^{3/4}ð^{3/4}ý_j Ä_j ŠÁj^{3/4}Đ^{3/4} ì_j ö

m ĸ^{3/4} ÈÖ^{3/4}ö e-±ý_j Û_j ö ĸ^{3/4} ÄÄ^{3/4} |_j øÄ^{3/4}ö_j |ÄüË ÄÉÄ^{3/4}öÄj^{3/4}É š_j ç_j ö
 « øÄ_j Đ_j |_j ç_j ý_j Ú_j ĸ^{3/4} ÄÄ^{3/4} ÄÉÄ^{3/4}öÄj^{3/4}É ^{3/4} ÄÄÿ_j Ä_j °j^{3/4} öÄj^{3/4} ŠÁj^{3/4}Đ^{3/4} ì_j ö.
 ŠÁj^{3/4}Đ^{3/4} ì_j ö Äÿ_j « ^{3/4}ý_j pÄî_j ð^{3/4}ö_j |_j ¼_j ø_j. Ä^{3/4}ö^{3/4} (4.5.18)-ø_j
 š_j ðËÿ_j Öü_j ç_j Äj^{3/4}Ú_j ĸ^{3/4} Ä^{3/4} ì_j ð^{3/4}ö_j š_j ðËÿ_j ð^{3/4}ö_j r š_j ½_j ð^{3/4}ö_j u ±ý_j Û_j ö
 Š^{3/4}Ä^{3/4}ö^{3/4} ý_j pÄî_j ì_j ö ŠÁj^{3/4}Đ^{3/4} š_j ç_j ö ĸ^{3/4} ÄÄj^{3/4}É^{3/4} ç^{3/4}ð^{3/4}ý_j Ä_j « ð^{3/4} ç^{3/4}ð^{3/4} ü_j CN
 ±ý_j Û_j ö |°í_j ð^{3/4}ö_j š_j ð^{3/4}ö_j ¼_j Ä^{3/4} Ä_j. « ì_j š_j ðËÿ_j Öü_j ç_j ÄÄ^{3/4}ö^{3/4}ý_j
 ÄÉ^{3/4}Š^{3/4}Ä^{3/4} |°ø^{3/4} Ö^{3/4}ö_j ŠÁj^{3/4}Đ^{3/4} ì_j ö Äÿ_j š_j ç_j ö ĸ^{3/4} Ä^{3/4} ì_j ð^{3/4}ö_j ^{3/4}ö^{3/4}ý_j „ ±ý_j Û_j ö
 š_j ½_j ð^{3/4}ö_j v ±ý_j Û_j ö Š^{3/4}Ä^{3/4}ö^{3/4} ý_j pÄî_j ì_j ö Ä^{3/4}ü_j |_j ç_j ö_j ¼_j ç_j Ö^{3/4}ö_j š_j ç_j Ö^{3/4}ö_j

- $\vec{A}_i \vec{A} \vec{u} \vec{e} \vec{O} \vec{O} \vec{A} \vec{3}_i \vec{\theta}$ $\vec{S} \vec{A}_i \vec{D} \vec{r}$ $\vec{A} \vec{y} \vec{S} \vec{A}_i \vec{D}$ $\vec{1}_2 \vec{O} \vec{3}_i \vec{i}$ $\vec{A} \vec{C} \vec{r} \vec{O}$ $\vec{y} \vec{U} \vec{3}_i \vec{y}$ $\vec{A}_i \vec{D}$
 $\vec{i} \vec{o} \vec{i} \vec{S}_i \vec{D} \vec{I}$



$\vec{A} \vec{1}_4 \vec{o} \vec{4} \vec{5} \vec{1} \vec{8}$

$\vec{A} \vec{E} \vec{S} \vec{A}$ $\vec{i} \vec{o} \vec{A} \vec{O} \vec{A} \vec{I}$ $\vec{C} \vec{E} \vec{D}$. \vec{r} $\vec{S} \vec{A}$ $\vec{A}_i \vec{D}$ $\vec{i} \vec{3}_i \vec{I}$ $\vec{S}_i \vec{i} \vec{D} \vec{E} \vec{y}$ $\ll \vec{3}_i \vec{A} \vec{D}$ $\vec{3}_i \vec{C} \vec{o} \vec{3}_i \vec{u} \vec{i}$
 $\vec{p} \vec{r}$ $\vec{1}_2 \vec{A}_i \vec{E}$ $\vec{3}_i \vec{C} \vec{r}$ $\vec{O} \vec{A} \vec{C}$, $\vec{S} \vec{A}$ \vec{i} $\vec{C} \vec{C} \vec{o}$ $\vec{A}_i \vec{U} \vec{3}_i \vec{O}$ $\vec{2} \vec{u} \vec{A} \vec{1}_4 \vec{D}$.

$$\therefore v \sin \alpha = u \sin r \quad \dots\dots\dots(1)$$

$\vec{C} \vec{a} \vec{D} \vec{1}_4 \vec{E} \vec{y}$ $\vec{A}_i \vec{C} \vec{S} \vec{o} \vec{i} \vec{3}_i \vec{r}$ \vec{E} $\vec{A} \vec{C} \vec{O} \vec{A} \vec{E}$.

$$v \cos \alpha = e u \cos r \quad \dots\dots\dots(2)$$

$\vec{r} \vec{i} \vec{o}$.

(1) (2)- $\pm \vec{y} \vec{A} \vec{A} \vec{u} \vec{E} \vec{y}$ $\vec{A} \vec{i} \vec{i}$ $\vec{i} \vec{U} \vec{I}$ $\vec{3}_i \vec{O}$,

$$v^2 = u^2 (\sin^2 r + e^2 \cos^2 r) \vec{r} \vec{i} \vec{o}$$

$$\therefore v = u \sqrt{\sin^2 r + e^2 \cos^2 r} \quad \dots\dots\dots(3)$$

(2) $\vec{3}$ (1) $\vec{r} \vec{o} \vec{A} \vec{i} \vec{i}$ \vec{r} ,

$$\cot \alpha = e \cot r \quad \dots\dots\dots(4)$$

$\pm \vec{y} \vec{A} \vec{D}$ $\vec{C} \vec{r}$ $\vec{1}_4 \vec{i} \vec{i} \vec{o}$.

(3) (4)- $\pm \vec{y} \vec{U} \vec{o}$ $\vec{o} \vec{A} \vec{y} \vec{A}_i \vec{I}$ \vec{u} , $\vec{S} \vec{A}_i \vec{D} \vec{r}$ $\vec{i} \vec{i} \vec{o} \vec{A} \vec{y}$ $\vec{S}_i \vec{i} \vec{C} \vec{o} \vec{3}_i \vec{y}$ $\vec{p} \vec{A} \vec{i}$ $\vec{u} \vec{o} \vec{r}$ $\vec{3}_i$
 $\vec{A} \vec{r}$ $\vec{A} \vec{A} \vec{U} \vec{i}$ \vec{r} $\vec{y} \vec{E} \vec{E}$. $\vec{A} \vec{y} \vec{A} \vec{O} \vec{o} \vec{D} \vec{r}$ $\vec{1}_2 \vec{O} \vec{E} \times \vec{r}$ $\vec{C} \vec{O} \vec{o}$ (Corollaries) $\vec{A} \vec{E} \vec{A}_i \vec{o}$.

(i) $\vec{S} \vec{A}_i \vec{D} \vec{r}$ $\vec{S}_i \vec{A}_i \vec{A} \vec{y}$ $r = 0$

$\ll \vec{3}_i \vec{A}_i \vec{D}$ $\vec{S}_i \vec{i} \vec{C} \vec{o}$ $\vec{3}_i \vec{C} \vec{o} \vec{r}$ $\vec{3}_i \vec{S}_i \vec{A} \vec{E} \vec{A}_i$ $\vec{S} \vec{A}_i \vec{D} \vec{o} \vec{S} \vec{A}_i \vec{D}$, $\ll \vec{D}$ $\vec{A}_i \vec{D}$ $\vec{i} \vec{o} \vec{i} \vec{S}_i \vec{i} \vec{D} \vec{E} \vec{y}$
 $\vec{A} \vec{E} \vec{S} \vec{A}$ $\pm \vec{3}_i \vec{C} \vec{o} \vec{r}$ $\vec{O} \vec{A} \vec{C}$ $\vec{S} \vec{A}_i \vec{D} \vec{r}$ $\vec{i} \vec{i} \vec{o} \vec{A} \vec{y}$, $e u \pm \vec{y} \vec{U} \vec{o}$ $\vec{S} \vec{A}_i \vec{D} \vec{1}_4 \vec{E} \vec{A} \vec{i} \vec{i} \vec{o}$.

(ii) $e = 1$ $\pm \vec{y} \vec{E}_i \vec{o}$ $\vec{r} = r$; $v = u \vec{r} \vec{i} \vec{o}$.

$\ll \vec{3}_i \vec{A}_i \vec{D}$ $\vec{C} \vec{r}$ $\vec{E} \vec{A} \vec{D} \vec{O} \vec{r}$ $\vec{1}_4 \vec{A}$ $\vec{S}_i \vec{i} \vec{C} \vec{o} \vec{3}_i \vec{y}$ $\vec{A} \vec{I}$ $\vec{S}_i \vec{i} \vec{1}_2 \vec{O} \vec{o}$ $\vec{3}_i \vec{E} \vec{C} \vec{S}_i \vec{i} \vec{1}_2 \vec{O} \vec{o}$ $\vec{o} \vec{A} \vec{A}_i \vec{i} \vec{o}$.
 $\vec{S} \vec{A} \vec{O} \vec{o}$ $\vec{S} \vec{A}_i \vec{3}_i \vec{A}_i \vec{o}$ $\vec{S} \vec{A}_i \vec{o} \vec{3}_i \vec{y}$ $\pm \vec{r}$ $\vec{A} \vec{3}_i \vec{O} \vec{O}$ $\vec{A}_i \vec{U} \vec{A} \vec{3}_i \vec{O} \vec{r}$ \vec{A} .

(iii) $e = 0$ $\pm \vec{y} \vec{U} \vec{o}$ $\vec{r} = 90^\circ$; $v = u \sin r \vec{r} \vec{i} \vec{o}$.

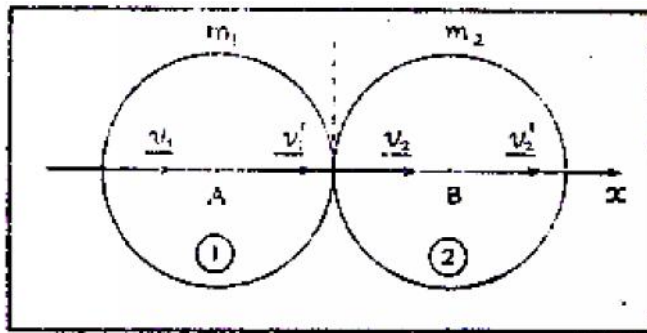
$p_1 \pm \frac{1}{2} \mu v_1 \cos^2 \theta$, $S_{ij} \text{ } \dot{\Delta}_j \text{ } p_{Ai} - \dot{u} \dot{E} \dot{A} \text{ } \dot{z} \dot{u} \dot{A} \text{ } \dot{o} \text{ } p_{E \dot{o}} \dot{A}$
 $\ll \dot{E} \dot{A} \dot{C} \dot{E} \dot{D} \text{ } \pm \dot{E} \dot{S} \dot{A} \text{ } p_{Ai} - \dot{u} \dot{E} \dot{A} \text{ } \dot{z} \dot{u} \dot{A} \text{ } \dot{o} \text{ } p_{E \dot{o}} \dot{o}$,
 $= \frac{1}{2} (1 - e^2) \mu v^2 \cos^2 \theta$

$[\dot{I} \dot{E} \dot{o} \dot{o}: e = 1 \pm \dot{E} \text{ } \dot{S}_{ij} \text{ } \dot{C} \dot{o} \text{ } \dot{z} \dot{C} \dot{E} \dot{A} \dot{D} \dot{o} \dot{C} \dot{O} \dot{C} \dot{A} \dot{I} \dot{o} \ll \dot{o} \dot{S} \dot{A} \dot{I} \dot{D} \text{ } p_{Ai} - \dot{u} \dot{E} \dot{A} \dot{y}$
 $\dot{A}_j \dot{u} \dot{E} \dot{o} \dot{a} \dot{i} \dot{C} \dot{A} \dot{A}_j \dot{o} \ll \dot{z} \dot{A}_j \dot{A} \dot{D} \text{ } p_{Ai} - \dot{u} \dot{E} \dot{A} \text{ } p_{E \dot{o}} \text{ } p_{A_j \dot{D}}$]

4.5.18 $p \dot{O} \dot{S}_{ij} \text{ } \dot{C} \dot{i} \text{ } \dot{C} \dot{y} \text{ } \dot{S}_{ij} \dot{A} \dot{E} \text{ } \dot{S}_{ij} \dot{A} \dot{D}$ (Direct impact of two spheres)

$m_1 \dot{z} \dot{C} \dot{E} \dot{O} \dot{C} \dot{A} \dot{A} \dot{E} \dot{A} \dot{E} \dot{o} \dot{A}_j \dot{E} \text{ } \dot{S}_{ij} \dot{C} \dot{o} \text{ } v_1 \pm \dot{y} \dot{U} \dot{o} \dot{z} \dot{C} \dot{E} \dot{S}_{ij} \dot{D} \dot{D} \dot{y} \text{ } p_{Ai} \dot{o} \dot{S}_{ij} \dot{D}$,
 $\ll \dot{S}_{ij} \dot{C} \dot{E} \dot{O} \dot{C} \dot{A} \dot{A} \dot{E} \dot{A} \dot{E} \dot{o} \dot{A}_j \dot{E} \text{ } m_2$
 $\dot{z} \dot{C} \dot{E} \dot{O} \dot{C} \dot{A} \dot{A} \dot{E} \dot{A} \dot{E} \dot{o} \dot{A}_j \dot{E} \text{ } \dot{S}_{ij} \dot{C} \dot{o} \dot{z} \dot{C} \dot{y} \dot{A} \dot{D} \text{ } \dot{S}_{ij} \dot{A}_j \dot{o} \text{ } \dot{S}_{ij} \dot{D} \dot{y} \dot{E} \dot{D} \text{ } e \pm \dot{y} \dot{A} \dot{D} \text{ } \dot{S}_{ij} \dot{C} \dot{i} \text{ } \dot{C} \dot{y}$
 $\dot{z} \dot{C} \dot{E} \dot{A} \dot{A} \dot{D} \dot{o} \dot{C} \dot{I} \dot{D} \dot{C} \dot{A} \dot{I} \dot{o} \dot{E} \dot{O} \dot{A} \dot{z} \dot{A}_j \dot{o} \text{ } \dot{S}_{ij} \dot{D} \dot{C} \dot{I} \dot{D} \dot{C} \dot{A} \dot{I} \dot{o} \ll \dot{A} \dot{u} \dot{E} \dot{y} \text{ } p_{Ai} \dot{S}_{ij} \dot{C} \dot{i}$
 $\dot{S}_{ij} \dot{I} \dot{z} \dot{A} \dot{D}$.

$\dot{A} \dot{z} \dot{O} \text{ } (4.5.19) \text{ } \dot{A}, \dot{B} \pm \dot{y} \dot{A} \dot{D} \text{ } \dot{S}_{ij} \dot{C} \dot{i} \text{ } \dot{C} \dot{y} \text{ } \dot{A} \dot{A} \dot{I} \dot{C} \dot{i} \dot{I} \dot{E} \dot{O} \dot{A} \dot{z} \dot{A}_j \dot{o} \dot{I} \dot{o} \text{ } \dot{A}, \dot{B}$
 $\pm \dot{y} \dot{A} \dot{D} \text{ } \dot{S}_{ij} \dot{D} \dot{C} \dot{I} \dot{D} \dot{S}_{ij} \dot{z} \dot{A}_j \dot{o} \ll \dot{z} \dot{A}_j \dot{A} \dot{D} \text{ } \dot{I} \dot{A}_j \dot{D} \dot{I} \dot{o} \dot{S}_{ij} \dot{z} \dot{A}_j \dot{o}$.



$\dot{A} \dot{z} \dot{O} \text{ } 4-5-19$

$\dot{S}_{ij} \dot{C} \dot{i} \text{ } \dot{C} \dot{y} \dot{A} \dot{A} \dot{I} \dot{C} \dot{i} \dot{I} \dot{E} \dot{O} \dot{A} \dot{z} \dot{A}_j \dot{o} \dot{I} \dot{o} \dot{A} \dot{E} \dot{A} \dot{E} \dot{o} \dot{A}_j \dot{E} \text{ } \dot{A} \dot{S}_{ij} \dot{C} \dot{i} \dot{E} \dot{z} \dot{A}_j \dot{o} \text{ } \dot{S}_{ij} \dot{D} \dot{C} \dot{I} \dot{D} \dot{C} \dot{A} \dot{I} \dot{o} \dot{y}$
 $\dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{z} \dot{C} \dot{E} \dot{O} \dot{C} \dot{A} \dot{A} \dot{E} \dot{A} \dot{E} \dot{o} \dot{A}_j \dot{E} \text{ } \dot{z} \dot{C} \dot{E} \dot{S}_{ij} \dot{D} \dot{D} \dot{y} \dot{I} \dot{I} \dot{A} \dot{C} \dot{C} \dot{O} \dot{U} \dot{o} \dot{z} \dot{C} \dot{E} \dot{z} \dot{A}_j \dot{o} \text{ } \dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{z} \dot{C} \dot{E} \dot{O} \dot{C} \dot{A} \dot{A} \dot{E} \dot{A} \dot{E} \dot{o} \dot{A}_j \dot{E}$
 $\dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{z} \dot{C} \dot{E} \dot{O} \dot{C} \dot{A} \dot{A} \dot{E} \dot{A} \dot{E} \dot{o} \dot{A}_j \dot{E} \text{ } \dot{S}_{ij} \dot{C} \dot{i} \text{ } \dot{C} \dot{y} \text{ } \dot{z} \dot{C} \dot{E} \dot{S}_{ij} \dot{D} \dot{D} \dot{y} \dot{I} \dot{I} \dot{A} \dot{C} \dot{C} \dot{O} \dot{U} \dot{o} \dot{z} \dot{C} \dot{E} \dot{z} \dot{A}_j \dot{o} \text{ } \dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{z} \dot{C} \dot{E} \dot{O} \dot{C} \dot{A} \dot{A} \dot{E} \dot{A} \dot{E} \dot{o} \dot{A}_j \dot{E}$
 $\dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{y} \text{ } \dot{S}_{ij} \dot{C} \dot{i} \text{ } \dot{C} \dot{y} \text{ } \dot{A}, \dot{B} \pm \dot{y} \dot{U} \dot{o} \dot{S}_{ij} \dot{D} \dot{E} \dot{S} \dot{A} \dot{S} \dot{A} \text{ } p_{Ai} \dot{I} \dot{A} \dot{z} \dot{A}_j \dot{o} \text{ } p \dot{O}$
 $\dot{S}_{ij} \dot{C} \dot{o} \dot{z} \dot{C} \dot{y} \dot{U} \dot{o} \dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{y} \text{ } \dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{z} \dot{C} \dot{E} \dot{O} \dot{C} \dot{A} \dot{A} \dot{E} \dot{A} \dot{E} \dot{o} \dot{A}_j \dot{E} \text{ } \dot{z} \dot{C} \dot{E} \dot{S}_{ij} \dot{D} \dot{D} \dot{y} \dot{I} \dot{I} \dot{A} \dot{C} \dot{C} \dot{O} \dot{U} \dot{o}$
 $\dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{y} \text{ } \dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{z} \dot{C} \dot{E} \dot{O} \dot{C} \dot{A} \dot{A} \dot{E} \dot{A} \dot{E} \dot{o} \dot{A}_j \dot{E} \text{ } \dot{z} \dot{C} \dot{E} \dot{S}_{ij} \dot{D} \dot{D} \dot{y} \dot{I} \dot{I} \dot{A} \dot{C} \dot{C} \dot{O} \dot{U} \dot{o} \dot{z} \dot{C} \dot{E} \dot{z} \dot{A}_j \dot{o} \text{ } \dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{z} \dot{C} \dot{E} \dot{O} \dot{C} \dot{A} \dot{A} \dot{E} \dot{A} \dot{E} \dot{o} \dot{A}_j \dot{E}$
 $\dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{y} \text{ } \dot{S}_{ij} \dot{C} \dot{i} \text{ } \dot{C} \dot{y} \text{ } \dot{A}, \dot{B} \pm \dot{y} \dot{U} \dot{o} \dot{S}_{ij} \dot{D} \dot{E} \dot{S} \dot{A} \dot{S} \dot{A} \text{ } p_{Ai} \dot{I} \dot{o}$.

$\dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{y} \text{ } \dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{z} \dot{C} \dot{E} \dot{O} \dot{C} \dot{A} \dot{A} \dot{E} \dot{A} \dot{E} \dot{o} \dot{A}_j \dot{E} \text{ } \dot{z} \dot{C} \dot{E} \dot{S}_{ij} \dot{D} \dot{D} \dot{y} \dot{I} \dot{I} \dot{A} \dot{C} \dot{C} \dot{O} \dot{U} \dot{o} \dot{z} \dot{C} \dot{E} \dot{z} \dot{A}_j \dot{o} \text{ } \dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{z} \dot{C} \dot{E} \dot{O} \dot{C} \dot{A} \dot{A} \dot{E} \dot{A} \dot{E} \dot{o} \dot{A}_j \dot{E}$
 $\dot{I} \dot{E} \dot{O} \dot{A} \dot{z} \dot{A}_j \dot{o} \text{ } \dot{z} \dot{C} \dot{E} \dot{S}_{ij} \dot{D} \dot{D} \dot{y} \dot{I} \dot{I} \dot{A} \dot{C} \dot{C} \dot{O} \dot{U} \dot{o} \dot{z} \dot{C} \dot{E} \dot{z} \dot{A}_j \dot{o} \text{ } \dot{S}_{ij} \dot{D} \dot{I} \dot{o} \dot{z} \dot{C} \dot{E} \dot{O} \dot{C} \dot{A} \dot{A} \dot{E} \dot{A} \dot{E} \dot{o} \dot{A}_j \dot{E}$.

$$\underline{v_2'} - \underline{v_1'} = -e(\underline{v_2} - \underline{v_1}) \dots \dots \dots (1) \pm \dot{y} \dot{A} \dot{D} \text{ } \dot{z} \dot{C} \dot{E} \dot{z} \dot{A}_j \dot{o} \dot{I} \dot{o}$$

ŞAÖö - ó¼î , ðò Å¼ÅÊ, ÞÕŞ , Çí , Û ö ŞÁ;ÐŞÀ;Ð ŞÁ;Ð'' , Ş , ðËý
 ÁÐÛÇ - ó¼í , Çý , Á;ð¼ö, ŞÁ;Ð'' , ì Ì Óý Û ö Àý Û ö °ÁÁ;ì ö.
 ±É ŞÁ,

$$m_1 \underline{v_1'} + m_2 \underline{v_2'} = m_1 \underline{v_1} + m_2 \underline{v_2} \dots\dots\dots(2)$$

Þí ì $\underline{v_1'}, \underline{v_2'}$ ±ý Æ'' Å¼;ý , ¼;Ç;ì , ½ÇÁ , ù « Åü'' È (1) (2) ±ý Û ö °Áý
 À;î , Û ì ì ö ¼Æ× , ñ î , ÀÈÀ;ö.

→ ŞÁ (2) - (1) × m_2 ±ý Æ'' ¼;ì , ½;ì , Ç¼,

$$(m_1 + m_2) \underline{v_1'} = (m_1 - em_2) \underline{v_1} + (1 + e) m_2 \underline{v_2}$$

$$\underline{v_1'} = \frac{(m_1 - em_2) \underline{v_1} + (1 + e) m_2 \underline{v_2}}{(m_1 + m_2)} \dots\dots\dots(3)$$

→ ì ö.

« ùÁ;ŞÈ (2)+(1) × m_1 ±ý Æ'' ¼;ì , ½;ì , Ç¼,

$$(m_1 + m_2) \underline{v_2'} = (m_2 - em_1) \underline{v_2} + (1 + e) m_1 \underline{v_1}$$

$$\underline{v_2'} = \frac{(m_2 - em_1) \underline{v_2} + (1 + e) m_1 \underline{v_1}}{(m_1 + m_2)} \dots\dots\dots(4)$$

→ ì ö.

(3) (4) ±ý Û ö °Áý À;î , ù, ŞÁ;Ð'' , ì Ì öÀý , Ş , Çí , Çý ¼Ç'' °ŞÁ;í , '' Ç
 Å'' ÅÄÛ; , ý ÈÈ.

4.5.18.1 Ç'' ÈÖ'' ¼Å Ş , Çö¼ý ŞÁø ²üÄî ö ¼;ì , Ç'' Å'' Å;ì , ì ¼ø.

$$I = m_1 \text{ Ç'' ÈÖ'' ¼Å Ş , Çö¼ý ŞÁø ŞÁ;Ð'' , } \underline{v_1} \text{ø ²üÄî ö ¼;ì , Ç'' Å}$$

$$= \ll \text{ ¼ý - ó¼ö¼ø ²üÄî ö } \underline{v_1} \text{üÈö}$$

$$= m_1 \underline{v_1'} - m_1 \underline{v_1}$$

$$= m_1 (\underline{v_1'} - \underline{v_1})$$

$$= m_1 \left[\frac{(m_2 - em_2) \underline{v_1} + (1 + e) m_2 \underline{v_2}}{(m_1 + m_2)} - \underline{v_1} \right]$$

$$= \frac{m_1}{m_1 + m_2} \left[(1 + e) (m_2 \underline{v_2} - m_2 \underline{v_1}) \right]$$

$$= - \frac{m_1 m_2}{m_1 + m_2} (1 + e) (\underline{v_1} - \underline{v_2}), (\underline{v_1} > \underline{v_2})$$

[I] Èòò (i) $m_2 \underline{v}_2' = \underline{v}_2$; $m_1 \underline{v}_1' = \underline{v}_1$ ñ ò. $\pm \frac{1}{2} m_1 \underline{v}_1' = \pm \frac{1}{2} m_2 \underline{v}_2'$ ñ ò. $\pm \frac{1}{2} m_1 \underline{v}_1' = \pm \frac{1}{2} m_2 \underline{v}_2'$ ñ ò. $\pm \frac{1}{2} m_1 \underline{v}_1' = \pm \frac{1}{2} m_2 \underline{v}_2'$ ñ ò.

(ii) $m_2 \underline{v}_2' = \underline{v}_2$; $m_1 \underline{v}_1' = \underline{v}_1$ ñ ò.

(iii); $m_1 - m_2 e = 1 \pm \frac{1}{2} m_1 \underline{v}_1' = \pm \frac{1}{2} m_2 \underline{v}_2'$ ñ ò.

« $\frac{1}{2} m_1 \underline{v}_1' = \frac{1}{2} m_2 \underline{v}_2'$ ñ ò. $\frac{1}{2} m_1 \underline{v}_1' = \frac{1}{2} m_2 \underline{v}_2'$ ñ ò. $\frac{1}{2} m_1 \underline{v}_1' = \frac{1}{2} m_2 \underline{v}_2'$ ñ ò. $\frac{1}{2} m_1 \underline{v}_1' = \frac{1}{2} m_2 \underline{v}_2'$ ñ ò.

(iv) $e=0 \pm \frac{1}{2} m_1 \underline{v}_1' = \pm \frac{1}{2} m_2 \underline{v}_2'$ ñ ò.

$\underline{v}_2' = \underline{v}_1'$ ñ ò.]

4.5.18.2 $\underline{v}_2' = \underline{v}_1'$ ñ ò. $\underline{v}_2' = \underline{v}_1'$ ñ ò.

$m_1, m_2 \pm \frac{1}{2} m_1 \underline{v}_1' = \pm \frac{1}{2} m_2 \underline{v}_2'$ ñ ò. $\frac{1}{2} m_1 \underline{v}_1' = \frac{1}{2} m_2 \underline{v}_2'$ ñ ò. $\frac{1}{2} m_1 \underline{v}_1' = \frac{1}{2} m_2 \underline{v}_2'$ ñ ò. $\frac{1}{2} m_1 \underline{v}_1' = \frac{1}{2} m_2 \underline{v}_2'$ ñ ò.

$$\underline{v}_2' - \underline{v}_1' = -e(\underline{v}_2 - \underline{v}_1)$$

$$m_1 \underline{v}_1' + m_2 \underline{v}_2' = m_1 \underline{v}_1 + m_2 \underline{v}_2$$

$\underline{v}_2' = \underline{v}_1'$ ñ ò. $\underline{v}_2' = \underline{v}_1'$ ñ ò.

$$= \left\{ \frac{1}{2} m_1 (\underline{v}_1' \cdot \underline{v}_1') - \frac{1}{2} m_1 (\underline{v}_1 \cdot \underline{v}_1) \right\} + \left\{ \frac{1}{2} m_2 (\underline{v}_2' \cdot \underline{v}_2') - \frac{1}{2} m_2 (\underline{v}_2 \cdot \underline{v}_2) \right\}$$

$$= \frac{1}{2} m_1 (\underline{v}_1'^2 - \underline{v}_1^2) + \frac{1}{2} m_2 (\underline{v}_2'^2 - \underline{v}_2^2)$$

$$= \frac{1}{2} (m_1 \underline{v}_1'^2 + m_2 \underline{v}_2'^2) - \frac{1}{2} (m_1 \underline{v}_1^2 + m_2 \underline{v}_2^2)$$

$\underline{v}_2' = \underline{v}_1'$ ñ ò. $\underline{v}_2' = \underline{v}_1'$ ñ ò. $\underline{v}_2' = \underline{v}_1'$ ñ ò. $\underline{v}_2' = \underline{v}_1'$ ñ ò.

$$(m_1 + m_2)(m_1 \underline{v}_1'^2 + m_2 \underline{v}_2'^2) = (m_1 \underline{v}_1 + m_2 \underline{v}_2)^2 + m_1 m_2 (\underline{v}_1 - \underline{v}_2)^2$$

$$(m_1 + m_2)(m_1 \underline{v}_1'^2 + m_2 \underline{v}_2'^2) = (m_1 \underline{v}_1' + m_2 \underline{v}_2')^2 + m_1 m_2 (\underline{v}_1' - \underline{v}_2')^2$$

$\underline{v}_2' = \underline{v}_1'$ ñ ò. $\underline{v}_2' = \underline{v}_1'$ ñ ò.

$$= \frac{1}{2} \left[\frac{m_1 m_2}{(m_1 + m_2)} \{ (\underline{v}_1' - \underline{v}_2')^2 - (\underline{v}_1 - \underline{v}_2)^2 \} \right]$$

$$= \frac{m_1 m_2}{2(m_1 + m_2)} [e^2 (\underline{v}_1 - \underline{v}_2)^2 - (\underline{v}_1 - \underline{v}_2)^2]$$

ŞĂÖö ŞĂİĐ·· ÂŞŞĂİĐ Ş,İ 1/2İ ÇŞÁĐ |°ÂÜÂÎ ö 1/2ò¼İ Ş Á·° Ş Ü
 ·· ÂÂÎ Ş,İ ðÊŞĂŞ°ÁÛ ö ±¼ÖÁİö ÞÖÔÁ¼İø « İ Ş,İ ðÊÖÜÇ |Áİò¼ - ó¼ö
 ÁİËİĐ.

±ÉŞĂ

$$m_1 \underline{v}_1' \cos \alpha - m_2 \underline{v}_2' \cos \omega = m_1 \underline{v}_1 \cos \Gamma - m_2 \underline{v}_2 \cos S \dots\dots(4)$$

¬ İ ö.

ŞĂÜÜÈÂ çİÝİ °ÁÝÀİÎ ÇĂÖÓóĐ, $\underline{v}_1', \underline{v}_2', \alpha, \omega$ ±ÝÂÜ·· È Á·· ÂÂÜİ Ş,İ ö.

(3)×m₂+(4) ±ÝÂĐ

$$(m_1 + m_2) \underline{v}_1' \cos \alpha = (m_1 - em_2) \underline{v}_1 \cos \Gamma + (1 + e) m_2 \underline{v}_2 \cos S$$

« ¼İÁĐ,

$$\underline{v}_1' \cos \alpha = \frac{(m_1 - em_2) \underline{v}_1 \cos \Gamma + (1 + e) m_2 \underline{v}_2 \cos S}{(m_1 + m_2)} \dots\dots(5) \quad \neg \text{ İ } \ddot{\circ}.$$

« ùÂİŞÈ.

$$\underline{v}_2' \cos \omega = \frac{(m_1 - em_1) \underline{v}_2 \cos S + (1 + e) m_1 \underline{v}_1 \cos \Gamma}{(m_1 + m_2)} \dots\dots(6) \quad \neg \text{ İ } \ddot{\circ}.$$

4.5.19.1 Ş,İÇÍ Ş Ü ´ÝÈŞÁĐ ÁÜİËİÝÜ ŞĂİĐ·· Âİø |°ÂÜÂÎ ðĐö
 ¼İİ Ş Ç·· Â.

$m_1 \text{ ç·· ÈÖ·· } \frac{1}{4} \hat{A} \text{ Ş,İ } \frac{1}{2} \text{ò¼Ş ÁĐÜÇ ŞĂİĐ·· } \text{ò } \frac{1}{4} \text{İ Ş Ç·· } \hat{A} = \ll \text{ İ Ş,İ Çò¼Ş$

$$- \text{ó¼ } \hat{A} \text{üÈö} = m_1 (\underline{v}_1' \cos \alpha - \underline{v}_1 \cos \Gamma)$$

$$= - \frac{m_1 m_2 (1 + e)}{(m_1 + m_2)} (\underline{v}_1 \cos \Gamma - \underline{v}_2 \cos S) \dots\dots(7) \quad \neg \text{ İ } \ddot{\circ}.$$

[İ Èöò. (i) $m_2 \text{ ç·· ÈÖ·· } \frac{1}{4} \hat{A} \text{ Ş,İ Çò¼Ş } \frac{1}{2} \text{ò¼İİ } \hat{A} \text{·° } m_1 \text{ ÞÁİ İ ö } \frac{1}{4} \text{·° İ } \pm \frac{1}{4} \text{ò¼·° } \hat{A} \text{ø } | \text{° } \hat{A} \text{ÜÂÎ } \hat{A} \frac{3}{4} \text{İø } m_1 \text{ ç·· ÈÖ·· } \frac{1}{4} \hat{A} \text{ Ş,İ Çò¼ø } - \text{ó¼ } \text{ÞÈöò } \text{ZÜÂÎ } \text{ÇÈĐ. } \ll \text{·· } \frac{1}{4} \text{Þİ İ İ·· Èİ İ ÈÇ | } \hat{A} \text{ÇÖÂÎ ðĐ } \text{ÇÈĐ.}$

(ii) $m_1 \text{ ç·· ÈÖ·· } \frac{1}{4} \hat{A} \text{ Ş,İ Çò¼ø } - \text{ó¼ } \hat{A} \text{İ } \frac{3}{4} \text{ZÜÂÎ } \text{ÇÈĐ.}$

(iii) $v_2 = 0 \pm \text{ÉŞ } w = 0 \neg \text{ İ } \ddot{\circ}.$

(iv) $m_1 = m_2, e = 1 \pm \text{ÉŞ}$

$$\underline{v}_1' \cos \alpha = \underline{v}_2 \cos S$$

$$\underline{v}_2' \cos \omega = \underline{v}_1 \cos \Gamma \quad \neg \text{ İ } \ddot{\circ}].$$

4.5.19.2 $\circ_i \times \text{ŞÁ} \hat{D} \cdot \hat{A}_i \varnothing \hat{z} \hat{u} \hat{A} \hat{i} \hat{o} \hat{p} \hat{A} \hat{i} \hat{s} \rightarrow \hat{u} \hat{E} \varnothing \hat{p} \hat{A} \hat{o} \hat{D}$.

$\hat{D} \hat{s} \hat{o} \hat{i} \frac{1}{4} \hat{i} \hat{l} \frac{3}{4} \hat{A} \hat{o} \text{ŞÁ} \hat{D} \cdot \hat{A}_i \varnothing \hat{z} \hat{u} \hat{A} \hat{i} \hat{o} \hat{p} \hat{A} \hat{i} \hat{s} \rightarrow \hat{u} \hat{E} \varnothing \hat{A}_i \hat{u} \hat{E} \hat{o}$,

$$\begin{aligned} &= \left(\frac{1}{2} m_1 \underline{v}_1'^2 + \frac{1}{2} m_1 \underline{v}_2'^2 \right) - \left(\frac{1}{2} m_1 \underline{v}_1'^2 + \frac{1}{2} m_1 \underline{v}_2'^2 \right) \\ &= \frac{1}{2} m_1 (\underline{v}_1'^2 \cos^2 \theta + \underline{v}_1'^2 \sin^2 \theta) + \frac{1}{2} m_2 (\underline{v}_2'^2 \cos^2 \omega + \underline{v}_2'^2 \sin^2 \omega) \\ &= \frac{1}{2} m_1 (\underline{v}_1'^2 \cos^2 r + \underline{v}_1'^2 \sin^2 r) - \frac{1}{2} m_2 (\underline{v}_2'^2 \cos^2 s + \underline{v}_2'^2 \sin^2 s) \end{aligned}$$

$\rightarrow \hat{E}_j \varnothing$, $\hat{p} \hat{i} \hat{l} \hat{s}_i \hat{C} \hat{i} \hat{u} \hat{A} \hat{E} \hat{A} \hat{o} \hat{A}_i \hat{s} \rightarrow \hat{u} \hat{C} \frac{3}{4} \hat{i} \varnothing$. « $\hat{A} \hat{u} \hat{E} \hat{y}$
 $\hat{i} \frac{3}{4} \hat{i} \hat{l} \hat{s}_i \hat{o} \hat{i} \hat{o} \hat{A} \hat{o} \rightarrow \hat{u} \hat{C} \text{ŞÁ} \hat{s} \hat{i} \hat{u} \hat{A}_i \hat{U} \frac{3}{4} \hat{A} \hat{i} \hat{s} \hat{A}_i$.

$$\therefore v_1' \sin \theta = v_1 \sin r; v_2' \sin \omega = v_2 \sin s$$

$\pm \hat{E} \text{ŞÁ} \hat{p} \hat{A} \hat{i} \hat{s} \rightarrow \hat{A}_i \hat{u} \hat{E} \hat{o}$

$$= \frac{1}{2} (m_1 \underline{v}_1'^2 \cos^2 \theta + m_2 \underline{v}_2'^2 \cos^2 \omega) - \frac{1}{2} (m_1 \underline{v}_1'^2 \cos^2 r + m_2 \underline{v}_2'^2 \cos^2 s)$$

$\hat{p} \frac{3}{4} \hat{y} \hat{A} \frac{3}{4} \hat{o} \hat{A} \hat{o} \hat{A} \hat{y} \hat{A} \hat{O} \hat{A}_i \hat{U} \hat{s} \frac{1}{2} \hat{i} \hat{s} \hat{o} \hat{i} \hat{A} \hat{s} \hat{A} \hat{U} \hat{i} \hat{s} \hat{A}_i \hat{o}$.

$$(m_1 + m_2) (m_1 \underline{v}_1'^2 \cos^2 \theta + m_2 \underline{v}_2'^2 \cos^2 \omega) = (m_1 \underline{v}_1' \cos \theta + m_2 \underline{v}_2' \cos \omega)^2 + m_1 m_2 (\underline{v}_1 \cos \theta + \underline{v}_2 \cos \omega)^2$$

$$(m_1 + m_2) (m_1 \underline{v}_1'^2 \cos^2 \theta + m_2 \underline{v}_2'^2 \cos^2 \omega) = (m_1 \underline{v}_1' \cos r + m_2 \underline{v}_2' \cos s)^2 + m_1 m_2 (\underline{v}_1 \cos r - \underline{v}_2 \cos s)^2$$

$\cdot \hat{p} \hat{A} \hat{i} \hat{s} \rightarrow \hat{u} \hat{E} \varnothing \hat{A}_i \hat{u} \hat{E} \hat{o}$

$$= \frac{m_1 m_2}{2(m_1 + m_2)} \left[(v_1' \cos \theta - v_2' \cos \omega)^2 - (v_1 \cos r - v_2 \cos s)^2 \right]$$

$$= \frac{m_1 m_2}{2(m_1 + m_2)} \left[e^2 (v_1 \cos r - v_2 \cos s)^2 - (v_1 \cos r - v_2 \cos s)^2 \right]$$

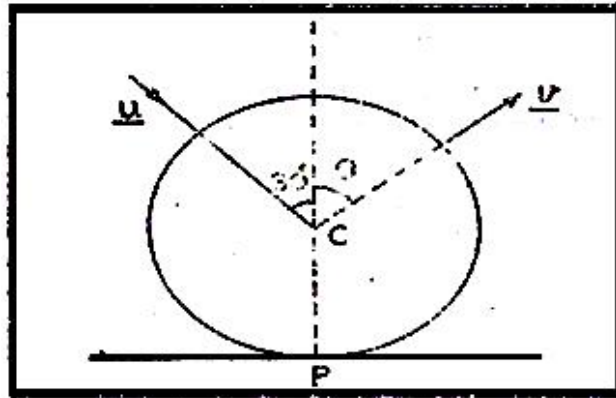
$$= \frac{m_1 m_2}{2(m_1 + m_2)} (1 - e^2) (v_1 \cos r - v_2 \cos s)^2$$

$\rightarrow \frac{3}{4} \hat{A}_i \varnothing \hat{p} \hat{A} \hat{i} \hat{s} \rightarrow \hat{u} \hat{E} \varnothing \hat{p} \hat{A} \hat{o} \hat{D}$

$$= \frac{m_1 m_2}{2(m_1 + m_2)} (1 - e^2) (v_1 \cos r - v_2 \cos s)^2$$

4.5.20 $\hat{A}_i \frac{3}{4} \hat{i} \hat{C} \hat{i} \hat{u} \hat{s} \frac{1}{2} \hat{i} \hat{l} \hat{s} \hat{u}$

4.5.20.1 2, SÄi, Äi ö ç ÈÔÛÇ S, i Ç | Äi ý Ú ÁÆÁÆöÄi É ç ÄÄi É ¼Çò¼Äý ÁÐ, « ò¼Çò¼Äý | öí Ì òÐì S, i ðËÛÌ 30° S, i ½î° öÄö ÄÉ; Èì Ì 20ÁfSÄ, òÐ¼ý Äö, ÇÈÐ e = 1/√3 - Äý SÄi Ð'' , Ì ò Äý



Ä¼ö 4-5-21

S, i Çò¼Äý pÄi , ò'' ¼i , ñ , « ý ÈÖö pÄi , - üÈÄý pÆö'' ÄÖö , ñ , SÄi Ð'' , Ì ò Äý S, i Çö | öí Ì òÐì S, i ðË¼ý , S, i ½î° öÄö v ±ý Ûö SÄ, òÐ¼ ý pÄi Ì Ä¼i , Ì | , i Û ,

$$\underline{u} = 20|30^\circ \left\{ \begin{array}{l} u \sin 30^\circ \rightarrow \\ u \sin 30^\circ \downarrow \end{array} \right\}; \underline{v} = v|_{\underline{u}} = \left\{ \begin{array}{l} u \sin 30^\circ \rightarrow \\ u \sin 30^\circ \downarrow \end{array} \right\}$$

· çä ö¼Éý Äi S°i¼'' É ÄöÄöÄÉ,

$$v \cos_{''}^\circ - 0 = -e(-u \cos 30^\circ - 0) = eu \cos 30^\circ$$

$$v \cos_{''}^\circ = \frac{1}{\sqrt{3}} \times 20 \times \frac{\sqrt{3}}{2} = 10 \quad \dots\dots\dots (i)$$

· ç¼ö¼Çò¼ÄÛÌ p'' ½Äi É ¼ç'' öÄö Äç'' öSÄÐÄö'' Ä ±ý Ä¼i ö

$$v \sin_{''} = u \sin 30^\circ = 20 \times \frac{1}{2} = 10 \quad \dots\dots\dots (ii)$$

· (i) (ii) ±ý Ûö öÁý Äi Î , ÇÄÖÖóÐ

$$v^2 = 100 + 100; \therefore u = 10\sqrt{2} \text{ ÄÄÄ}$$

$$SÄÖö \tan_{''} = 1; \therefore ''^\circ = 45^\circ$$

±ÉSÄ S, i Çö SÄi Ð'' , Ì ò Äý ÄÉ; Èì Ì 10√2 Áf SÄ, ò¼ö | öí Ì òÐì S, i ðËÛÌ 45° S, i ½î° öÄö pÄi Ì ö.

$$SÄi Ð'' , Äi ö pÄi , - üÈÄö ²üÄî ö pÆöð = \frac{1}{2} \mu u^2 \cos^2 r (1 - e^2)$$

PQ, QR, RS ±ý Û õ §, i Î, Û ì, Ç, ¼Ãø « ·· ÁÕõ ÄÄ·· Ç×õ Ä; ·· ¾, ·· Ç
 Ä·· ÄÄ Ð, ù ±Í òÐì |, i ù Û õ §, Äõ t₁, t₂, t₃ - Ì õ. °i ò¾Çò¾Ü Ì î | °í Ì òÐ
 ¾Ç·· °Äø Ð, Çý ÞÄì, ò· ¾ §, ì Ì, t₁ §, Äò¾Çø °i ò¾Çò¾Ü Ì î | °í Ì ò¾i,
 | °ý È |¾i·· Ä× âî °ÄÄ; Ì õ.

±É §Ä

$$0 = eu \cos r t_1 - \frac{1}{2} g \cos r t_1^2;$$

$$\therefore t_1 = \frac{2e \cos r}{g \cos r} = \frac{2eu}{g}$$

« ùÄ; §È

$$t_2 = \frac{2e^2 u}{g}; t_3 = \frac{2e^3 u}{g}$$

±É §Ä Ð, ù ÞÄÄÕóÐ S ±ý Û Ä¼ò·· ¾Ä·· ¼Ä ±Í òÐì |, i ñ ¼ §, Äõ
 = t₁ + t₂ + t₃ = $\frac{2eu}{g}(1+w+w^2)$ Þ¾¾§, Äò¾Çø Ð, | Ç; ý Û °i ò¾Çò¾Çø, ù §, ì, ÄÄ; Û
 ÞÄì, Ä |¾i·· Ä× 4ÄÈ - Ì õ. |¾i ¼ì, ò¾Çø °i ò¾Çò¾Çý, ù §, ì, Ä¾Ç·· °Äø
 u sin r ±ý Û õ §Ä, ò· ¾ò Ð, Ç; È Ð | ÄÜ Û ÇÐ. « ¾ý ®:òð ÓÍ ì, õ g sin r
 - Ì õ.

$$\therefore u \sin r (t_1 + t_2 + t_3) + \frac{1}{2} g \sin r (t_1 + t_2 + t_3)^2 = 4$$

$$\ll \text{¾i ÄÐ} \quad u \sin r \frac{2eu}{g}(1+e_2+e_3) + \frac{1}{2} g \sin r \frac{4e^2 u^2}{g^2}(1+e_2+e_3) = 4$$

$$\ll \text{¾i ÄÐ} \quad \frac{2eu^2 \sin r}{g}(1+e+e) + \frac{2e^2 u^2 \sin r}{g}(1+e+e) = 4$$

$$\ll \text{¾i ÄÐ} \quad \frac{2eu^2 \sin r}{g}(1+e+e^2)[1+e(1+e+e^2)] = 4$$

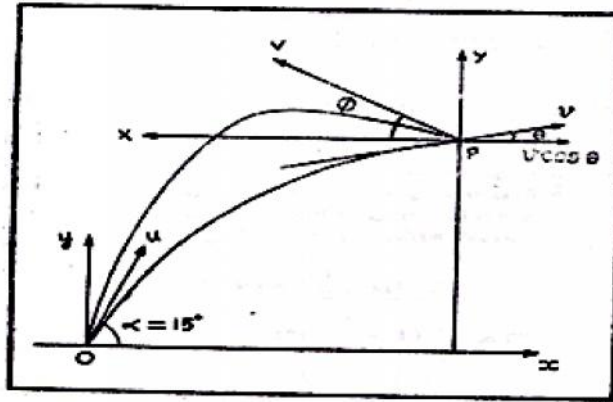
$$\ll \text{¾i ÄÐ} \quad \frac{2eu^2 \sin r}{g}(1+e+e^2)(1+e)(1+e^2) = 4$$

$$\begin{aligned} \therefore e(1+e)(1+e^2)(1+e+e^2) \\ = \frac{3g}{2u^2 \sin r} = \frac{3g}{2 \times 12g \sin 30^\circ} = \frac{1}{4} = 0.25 \end{aligned}$$

4.5.20.6 ´Õ Ä¾¾; ÈÐ 15° ²üÈì §, i ½ò¾Çø 35ÄÈ |¾i·· ÄÄÜÇ´Õ
 ÄÈÄÈòÄ; È Ç·· Äì Ì òÐì Í Ä;ø §Ä;¾Ç, ²ÈÇ òüÇ·· Ä Äñ Í õ « ·· ¼, ÇÈÐ.
 Äò¾Çò¾ ò Í ÄÕì Ì Ä·· ¼§ÄÜÇ Ç·· ÄÄõ°Ç |, ØÄý Ä¾Ç·· Äì, ì, ñ,

$$[g = 9.8 \text{ m/s}^2] \text{ } \pm \text{ } \hat{y} \text{ } \hat{u} \text{ } \hat{v}$$

Óðø ÅÆt : Åó¼jÉÐ ÅÆÁÆðÀjÉ Í ÅjØ P ±ýÛõ þ¼ð¾Ø §ÁjÐÅ¼j,ì
 |,jÛ. « òòÛÇh ÅÆ - Åð¾Ø þÕðÅ¼j,Ø P(25, h) ±ýÛõ òòÛÇ



À¼õ 4-5-25

$$y = x \tan r - \frac{2x^2}{2u^2 \cos^2 r} \pm \hat{y} \hat{u} \hat{v} \text{ } \hat{A} \text{ } \hat{C} \hat{D}$$

$$h = 25 \tan 15 - \frac{9.8 \times 25 \times 25 \times 4(2 - \sqrt{3})}{2 \times 35 \times 35}$$

$$h = 25(2 - \sqrt{3}) - 10(2 - \sqrt{3}) = 15(2 - \sqrt{3})$$

Í Å · Å §ÁjÐð§ÁjÐ Åó¼y §Å, ò, v ±É × ò « ¾ý ¾ç · ò, ç · ¼ì §, j òÍ ¼ý „
 ±ýÛõ §, j ½î òj, ÅØ - ÛÇÐ ±É × ò |, jÛ. §ÁjÐ ·, ì òÀý, Åó¼jÉÐ w
 ²ÛÈì §, j ½ð¾Ø V ÅÆ§Å, òÐ¼ý |¾ÈðÅ¼j,Ø

$$V \cos w = v \cos r = u \cos r$$

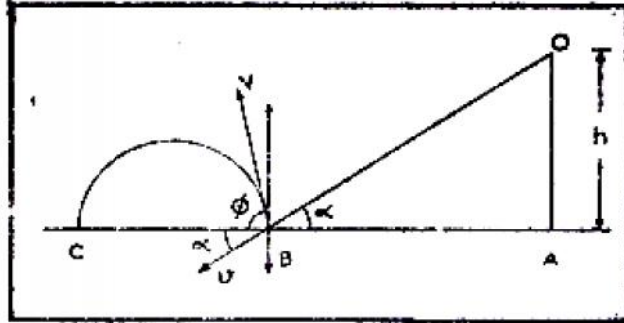
$$V \sin w = v \sin r = \sqrt{u^2 \sin^2 r - 2gh}$$

$$\therefore \tan w = \frac{1}{e} \frac{\sqrt{u^2 \sin^2 r - 2gh}}{u \cos r} = \frac{(2 - \sqrt{3})}{5e}$$

¬ ì õ.

§ÁjÐ ·, ì òÀý Åó¼jÉÐ 0 · · Å « · · ¼Å¾jØ Px, Py ±ýÛõ « î Í, · Çì
 Ì ÈðÐ 0 (25, -15(2 - √3)) ±ýÛõ òòÛÇ $y = x \tan w - \frac{gx^2}{2V^2 \cos^2 w} \pm \hat{y} \hat{u} \hat{v}$

Å · Ç × ò Å · · ¾ÅØ þÕì ì õ.



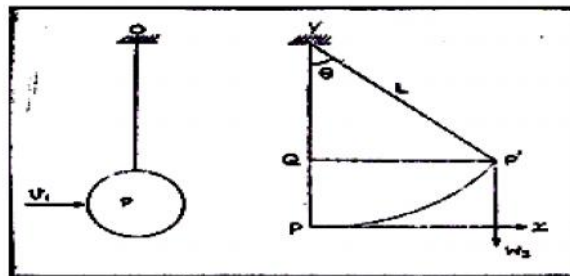
À¼õ 4-5-27

À¼õ (4.5.27)ø ,i ðÊÄÄ;Ú ÀóÐ B³ « '' ¼ÔõŞÄ;Ð « ¾ý ŞÄ,õ $V = \sqrt{2gh}$
 -Ì õ. ,Ç' ¼ò¾Çò¾¼ø B ±ý ÛÁ¼ò¾¼ø ŞÄ;Ð'' ,ì òÄý Àó¾;É Ð W ²üÈì
 Ş,i ½î°;Çø V ±ý Ûõ ŞÄ,òÐ¼ý |¾ÈòÄ¾; ,ø $V \cos w = V \cos r$; $V \sin w = ev \sin r$

BC ±ý ÀÐ ,Ç' ¼ò¾Ç Äî Í ±É ø

$$\begin{aligned}
 BC &= \frac{2(V \cos w)(V \sin w)}{R} \\
 &= \frac{2(v \cos r)(ev \sin r)}{g} \\
 &= \frac{e \cdot 2v^2 \sin r \cdot \cos r}{g} \\
 &= \frac{2e \cdot 2gh \cdot \sin r \cdot \cos r}{g} \\
 &= 4eh \sin r \cos r
 \end{aligned}$$

4.5.20.9 $w_1 = 15$, Ç;õ ±'' ¼ÔûÇ Ä'' Ä 'ý Û À¼õ (4.5.28)ø ,i ðÊÄÄ;Ú 0
 ±ý Ûõ Ç' ÄÄ;É òûÇÄÄ;õóÐ



À¼õ 4-5-28

$L = 0.9 \text{ m}$, $\alpha = 30^\circ$, $W_1 = 10 \text{ N}$, $W_2 = 10 \text{ N}$, $P = 10 \text{ N}$.
 The system is released from rest. Find the velocity of the block of mass W_1 when the string makes an angle of 30° with the vertical.

The block of mass W_1 moves vertically downwards with velocity v_1 . The block of mass W_2 moves vertically upwards with velocity v_2 . The string makes an angle α with the vertical. The velocity of the block of mass W_2 is v_2 . The velocity of the block of mass W_1 is v_1 . The velocity of the block of mass W_2 is v_2 . The velocity of the block of mass W_1 is v_1 .

$$v_1 = 2 \frac{(W_1 + W_2)}{W_1} \sqrt{gL} \sin \frac{\alpha}{2}$$

$$v_1 = 2 \left(\frac{10 + 10}{10} \right) \sqrt{9.81 \times 0.9} \sin 15^\circ$$

$$v_1 = 1026 \text{ cm/s}$$

4.5.20.10 A block of mass 20 kg is suspended from a fixed point by a string of length 16 m . The block is released from rest at an angle of 45° to the vertical. Find the velocity of the block when the string makes an angle of 30° with the vertical.

The block of mass 20 kg moves in a circular path of radius 16 m . The velocity of the block is v . The velocity of the block is v . The velocity of the block is v .

A block of mass 16 kg is suspended from a fixed point by a string of length 16 m . The block is released from rest at an angle of 45° to the vertical. Find the velocity of the block when the string makes an angle of 30° with the vertical.

$1m_1 = 16$	$v_1 = 20 \text{ m/s}$	$\xrightarrow{v_2} = 4$
$2m_2 = 48$	$v_2 = 4 \text{ m/s}$	$\xrightarrow{v_2}$

ΣΑ₁ΑΣΑ Ο^{3/4}Α₁ΑΔ ΑόΔ Σ_ζ÷Σ_ι ðËÖÛÇ þÃñ ¼₁ΑΔ Αó^{3/4} ΣΑ₁¾Α×¼₁ý « Δ
 μö× ζ^{3/4} Ä^{3/4} Ä^{3/4} ¼₁ΑΔ¼₁ý þÃñ ¼₁ΑΔ ΑόΔ u ±ý Û ð Σ_Α ðΣ_¼Î ã ýË₁ΑΔ
 Αó^{3/4}ÄËÏ Ì ð. ±ÉΣ_Α n −ΑΔ ΑόΔ þ^{3/4}ΣΑ₁Δ^{3/4} ÿ Ì ðÀý u ±ý Û ð
 Σ_Α ðΔ¼₁ÉÄÍ Ì ð.

4.5.20.13 m, 2m, 4m, 8m --- ±ý Û ð ζ^{3/4} È₁ ÿ ÿ ÿ ÿ ¼₁ ÄÄ ΑόΔ ÿ ÿ Σ_Α
 Σ_ζ÷Σ_ι ðËø ÿ ÄÏ ðÄÏ ðÇÉ. Ο^{3/4}ΑόΔ þÃñ ¼₁ΑΔ ΑΔ u ±ý Û ð
 Σ_Α ðΔ¼₁ý ΣΑ₁Δ₁ËΔ. þÃñ ¼₁ΑΔ ã ýË₁Α¾₁ý ΑΔ ΣΑ₁Δ₁ËΔ. þ^{3/4}ΣΑ₁ø
 ÄÛË ΑόΔ Û ð ΣΑ₁¾₁ ÿ ÿ ÿ ÿ ËË. ±ó^{3/4} þ^{3/4}ΑόΔ Û Ì ð þ^{3/4}ΣΑ₁ÏÛÇ
 ζ^{3/4} ÄÄ^{3/4} ÿ ÿ ð^{3/4} ÄÉÏ ÿ ÿ ÿ ÿ Ì n −ΑΔ Αó¾₁ý Σ_Α ð^{3/4} ÿ ÿ ÿ ÿ ÿ.

Ο^{3/4}Α₁ΑΔ ΑόΔ, þÃñ ¼₁ΑΔ Αó^{3/4} ΣΑ₁Δ ð ΣΑ₁Δ ðÇ ζ^{3/4} Ä^{3/4} ÄÏ ÿ ÄÉ ÿ × ð."I"
 ±ý ΑΔ Ä^{3/4} Ì ½₁ ð^{3/4} Ì È₁ ðÏ ð.

ΑόΔ	ζ ^{3/4} È	ΣΑ ₁ Δ ^{3/4} ÿ Ì Óý Σ _Α ð	ΣΑ ₁ Δ ^{3/4} ÿ Ì ðÀý Σ _Α ð
1	m	u →	u ₁ →
2	2m	0 →	v ₂ →

$$v_2 - u_1 = -W(o - u) = Wu; mu_1 + 2mv_2 = mu$$

$$u_1 + 2V_2 = u; \therefore 3V_2 = u(1 + e); V_2 = \frac{1 + e}{3}u$$

$$u_1 = u - \frac{2}{3}(1 + e)u = \frac{u}{3}[3 - 2 - 2e] = \frac{1 - 2e}{3}u$$

±ÉΣ_Α þÃñ ¼₁ΑΔ ΑόΔ u₁ = $\frac{1 + e}{3}u$ ±ý Û ð Σ_Α ðΔ¼₁ý 3ΑΔ Αó^{3/4}
 ΣΑ₁Δ₁ËΔ. þ^{3/4}ÄÄË Ëý ΣΑ₁Δ^{3/4} ÿ Ì ðÛË « ÿ Αó ð Àý ÄÏÄ₁Û.

ΑόΔ	ζ ^{3/4} È	ΣΑ ₁ Δ ^{3/4} ÿ Ì Óý Σ _Α ð	ΣΑ ₁ Δ ^{3/4} ÿ Ì ðÀý Σ _Α ð
2	2m	u ₁ = $\frac{1 + e}{3}u$	<u>u₂</u>
3	4m	0	<u>v₃</u>

$$v_3 - u_2 = -e \left[0 - \left(\frac{1 + e}{3} \right) u \right] = \frac{1 + e}{3}u$$

$$2mU_2 + 4mV_3 = 2m \left(\frac{1 + e}{3} \right) u$$

$$\therefore U_2 + 2V_3 + \frac{1+e}{3}u$$

$$3V_3 = \left(\frac{1+e}{3}u\right)(1+e)$$

$$V_3 = \left(\frac{1+e}{2}\right)^2 u.$$

« ùÁîŞÈ n – ÁĐ ÁóĐ ŞÁîĐ´´ , ì Ì òÀŸ

$$V_n = \left[\frac{1+e}{3}\right]^{n-1} u \pm y \hat{U} \tilde{o} \text{ ŞÁ}_s \tilde{o} \text{Đ} \frac{1}{4} \text{É} \hat{A} \hat{I} \tilde{o}.$$

±ÉŞĀ « Ĩ ò¼Ā òĐ ŞÁîĐ´´ , ì Ì òÀŸ 2– ÁĐ, 3– ÁĐ, n– ÁĐ ÁóĐ , ÇŸ ŞĀ , í , ù Ó´´ ÈŞĀ

$$\left(\frac{1+e}{3}\right)u \cdot \left(\frac{1+e}{3}\right)^2 \dots \dots \dots \left(\frac{1+e}{3}\right)^{n-1} - \tilde{o}.$$

ÁóĐ , ù ç´´ È ÁĐ °Ÿ ù ÇÉ | ÁÉ e = 1.

∴ ŞÁîĐ´´ , ì Ì òÀŸ « òÁóĐ , ÇŸ ŞĀ , í , ù Ó´´ ÈŞĀ

$$\left(\frac{2}{3}\right)u \cdot \left(\frac{2}{3}\right)^2 u \dots \dots \dots \left(\frac{2}{3}\right)^{n-1} - \tilde{o}$$

$\left(\frac{2}{3}\right) \pm y \hat{A} \frac{1}{4} | \hat{A}_i \text{Đ} \hat{A}_s \frac{1}{4} \hat{A}_i$ (common ratio) | , ì Ì òÀŸ ÷ p´´ Á , ù ´ Ō | ÁŌ ì , ò | ¼ , ¼ | Ç « ´´ Á , Ÿ ÈÉ.

4.5.20.14 °ÁĀĪÉ ç´´ È ù´´ ¼Ā B,C ±y Ūō pŌÁóĐ , ù ´ Ō Şç÷Şçĵ òĒø µöĀø ÷ ùÇÉ. « Ş¼ ç´´ ÈŌ´´ ¼Ā A ±y Ūō ÁóĐ ÁÉĵĒĪ Ī 10ÁĒŞĀ , ò¼ø B,CĀŸ ¼Ÿ °Āø B´´ Ā ŞĀîĐ´´ ÈĐ. « ò¼´´ Ā ŞĀîĐ´´ , Āĵø Āĵ´´ °Āĵ , ŞĀĵø , ù ÁóĐ , ŪĪ ç´´ ¼ŞĀ çç , ŸŸÈÉ. ç´´ Ā ÁĐ °Ÿ | Ÿ e = 0.4 ±ÉŸ ±øĀĵĀ¼ ŞĀîĐ´´ , ŪĪ ì Ì òÀŸ « òÁóĐ , ÇŸ ŞĀ , í , ù ÇĪ , ì Ì òÀŸ . Ó¼ĀĀĪ Ī ÁóĐ , ÇŸ ŞĀîĐ´´ , ĀŸ « ´´ Áò Ì ŸĀŌĀĵ

ÁóĐ	ç´´ È	ŞĀîĐ´´ , ì Ì ÓŸ ŞĀ , ō	ŞĀîĐ´´ , ì Ì òÀŸ ŞĀ , ō
A	m	10 ÁĒĀç→	$\underline{v_1}$
B	m	0	$\underline{v_2}$

$$\underline{v_2} - \underline{v_1} = -w(0 - 10) = 10 \times 0.4 = 4.$$

$$m v_1' + m v_2' = 10m; v_1' + v_2' = 10; \therefore 2v_2' = 14$$

$$v_2' = 7 \text{ \AA} \quad v_1' = 3 \text{ \AA}$$

B, C ±ý Ûõ ÀóÐ, Çý ŠÁĎ'' , Ā'' Áôð, ĩĭ Āĵ Ú « '' ÁĀōĪ õ.

ÀóÐ	ĵ'' È	ŠÁĎ'' , ĩĭ Óý ŠĀ, õ	ŠÁĎ'' , ĩĭ ôÀý ŠĀ, õ
B	m	$\underline{7 \text{ \AA}}$	$\underline{0}$
C	m	$\underline{v_2'}$	$\underline{v_3'}$

$$\therefore v_3' - v_2' = -e(0 - 7) = 0.4 \times 7 = 2.8$$

$$m v_2' + m v_3' = 7m; v_2' + v_3' = 7; 2v_3' = 9.8$$

$$v_3' = 4.9 \text{ \AA} \quad v_2' = 2.1 \text{ \AA}$$

A, B ±ý Ûõ ÀóÐ, Çý pĀñ ĩĵĀĒĒĒ È ŠÁĎ'' , Āý « '' Áôð Àý ĀōĀĵ Ú

ÀóÐ	ĵ'' È	ŠÁĎ'' , ĩĭ Óý ŠĀ, õ	ŠÁĎ'' , ĩĭ ôÀý ŠĀ, õ
A	m	$\underline{v_1' = 3 \text{ \AA}}$	$\underline{v_1'}$
B	m	$\underline{v_2' = 2.1 \text{ \AA}}$	$\underline{v_2'}$

$$v_2' - v_1' = -e(2.1 - 3) = 0.36$$

$$m v_1' + m v_2' = m \times 3 + m \times 2.1; \quad 2v_2' = 5.46$$

$$v_2' = 2.73 \text{ \AA} \quad v_1' = 2.73 \text{ \AA}$$

B, C ±ý Ûõ ÀóÐ, Çý pĀñ ĩĀÐ ŠÁĎ'' , Āý « '' Áôð Àý ĀōĀĵ Ú

ÀóÐ	ĵ'' È	ŠÁĎ'' , ĩĭ Óý ŠĀ, õ	ŠÁĎ'' , ĩĭ ôÀý ŠĀ, õ
B	m	$\underline{v_2' = 2.73 \text{ \AA}}$	$\underline{v_2'}$
C	m	$\underline{v_3' = 4.9 \text{ \AA}}$	$\underline{v_3'}$

À¼õ 4-5-30

ŞÁj¼ñ | ſj ũ ŸËË. ŞÁjĐ'' ſì òÀŸ « ÅüËŸ ¼ñ °ŞÅ ſ Ÿ ÇÕõ
 ŞÁjĐ'' ſ Åjø ²üÄð¼ þÂî ſ - üËÄø þÆòÀŸ Å¼ð'' ¼Õõ ſj ñ ſ.

(Åñ ¼ $v_1' = -0.875\underline{i}; v_2' = 1.375\underline{i} + 1.732\underline{j}$ - üËø þÆòÀŸ Å¼õ 9.35%)

4.6. $\vec{r}_B = \vec{r}_A + \vec{r}_{B/A}$ (Rigid body)

4.6.1 $\vec{r}_B = \vec{r}_A + \vec{r}_{B/A}$

$\vec{r}_B = \vec{r}_A + \vec{r}_{B/A}$ (Rigid body)

$\vec{r}_B = \vec{r}_A + \vec{r}_{B/A}$ (Rigid body)

$\vec{r}_B = \vec{r}_A + \vec{r}_{B/A}$ (displacement)

$\vec{r}_B = \vec{r}_A + \vec{r}_{B/A}$ (displacement)

$\vec{r}_B = \vec{r}_A + \vec{r}_{B/A}$ (Positions)

$\vec{r}_B = \vec{r}_A + \vec{r}_{B/A}$ (Positions)

$$\vec{r}_B = \vec{r}_A + \vec{r}_{B/A}$$

$\vec{v}_B = \vec{v}_A + \vec{v}_{B/A}$ (Velocity)

$\vec{v}_B = \vec{v}_A + \vec{v}_{B/A}$ (Velocity)

$$\vec{v}_B = \vec{v}_A + \vec{v}_{B/A}$$

$\vec{v}_B = \vec{v}_A + \vec{v}_{B/A}$

$\vec{a}_B = \vec{a}_A$ (Acceleration)

$\vec{a}_B = \vec{a}_A$

$$\begin{aligned} \underline{r}_B &= \underline{r}_A + \underline{r}_{B/A} \\ \therefore \underline{v}_B &= \underline{v}_A + \underline{v}_{B/A} \\ \underline{v}_{B/A} &= \check{S} \wedge \underline{r}_{B/A} = \check{S} \underline{k} \wedge \underline{r}_{B/A} \\ \underline{v}_{B/A} &= r \check{S} \\ \underline{v}_B &= \underline{v}_A + \check{S} \underline{k} \wedge \underline{r}_{B/A} \end{aligned}$$

4.6.3.1 \check{O} $\frac{3}{4}$ \check{C} $\rho \hat{A} \hat{i}$ \check{O} $\frac{3}{4}$ \check{U} \check{C} \hat{A} \check{C} $\hat{E} \hat{I} \hat{I} \hat{A} \hat{O}$ \check{O} $\hat{A} \hat{A} \hat{O}$ (instantaneous centre of rotation in plane motion)

$\hat{A} \hat{i} \hat{D} \hat{A} \hat{i} \hat{E}$ \check{O} $\frac{3}{4}$ \check{C} \check{O} $\frac{3}{4}$ \check{U} \check{C} \hat{A} \check{C} $\hat{A} \hat{O}$

$$\underline{v}_A = \underline{v}_c + \underline{v}_{A/c}$$

$$\underline{v}_c = 0$$

($\rho \pm \check{y} \hat{A} \hat{D} \hat{a} \hat{i} \hat{O} \hat{A}$ $\frac{3}{4}$ \check{C} \hat{O} $\check{S} \hat{A}$ \check{O} $\frac{3}{4}$ \hat{i} \check{C} $\hat{E} \hat{I} \hat{I} \hat{A} \hat{O}$ \check{O} $\hat{A} \hat{A} \hat{O}$)

$\check{S} \hat{A} \hat{O} \hat{O}$

$$\underline{v}_{A/c} = r \check{S} = -r \underline{A} \check{S}$$

$$\therefore \underline{v}_A = r \underline{A} \check{S}$$

($\rho \check{D} \check{S} \hat{A}$ $\rho \hat{A} \hat{i}$ $\hat{A} \hat{A} \hat{O} \hat{i}$ \check{C} \hat{A} $\hat{I} \hat{A} \hat{E} \hat{A} \hat{y}$ $\hat{O} \hat{A} \hat{y} \hat{A} \hat{i} \frac{1}{4} \hat{i}$ \hat{O})

4.6.3.2 \check{O} $\frac{3}{4}$ \check{C} $\rho \hat{A} \hat{i}$ \check{O} $\frac{3}{4}$ \check{U} \check{C} \hat{A} \hat{O} $\hat{i} \hat{D} \hat{O} \hat{I}$ \hat{i} \check{O} (Relative acceleration in plane motion)

$\underline{v}_B = \underline{v}_A + \underline{v}_{B/A}$ $\hat{O} \hat{A} \hat{y} \hat{A} \hat{i} \hat{O} \hat{O} \frac{1}{4} \check{S} \hat{C} \hat{A} \hat{O}$ \hat{t} \hat{i} $\hat{E} \hat{O} \hat{D}$ \hat{A} \hat{O} $\hat{A} \hat{f}$ \hat{i} $\hat{O} \hat{O} \hat{O} \hat{S} \hat{A} \hat{i} \hat{D}$
 $\underline{a}_B = \underline{a}_A + \underline{a}_{B/A} \pm \check{y} \hat{E} \hat{i} \hat{O}$. $\rho \hat{i} \hat{i}$ $a_A, a_B \pm \check{y} \hat{A} \hat{E}$ $\frac{3}{4} \hat{E} \hat{C} \hat{O} \hat{I}$ \hat{i} \hat{i} \check{C} $\hat{i} \hat{O}$. $\hat{E} \hat{i} \hat{O} \underline{a}_{B/A}$
 \hat{i} $\hat{E} \hat{O} \hat{D}$ $\hat{B} \hat{y}$ $\hat{O} \hat{i} \hat{D} \hat{O} \hat{I}$ \hat{i} $\hat{A} \hat{i} \hat{O}$

$\hat{O} \hat{I}$ \hat{i} \check{O} $\underline{a}_{B/A}$ \hat{i} \check{C} \hat{A} \hat{i} $\frac{3}{4} \hat{i} \hat{S} \hat{i} \hat{O} \hat{I}$ \hat{i} $\hat{U} \hat{U}$ $\underline{a}_{B/A} \hat{t}^{-B/A}$ \hat{i} \hat{O} . $\rho \hat{D}$ $\hat{A} \hat{B}$
 $\hat{S} \hat{i} \hat{O} \hat{E} \hat{U}$ \hat{i} $\hat{O} \hat{i}$ $\hat{O} \frac{3}{4} \hat{i}$ \check{C} $\hat{A} \hat{O} \hat{O}$ \check{C} $\hat{A} \hat{O} \hat{O}$ $\hat{U} \hat{A} \hat{O} \hat{S} \hat{A}$ \hat{i} $\hat{O} \hat{i}$ $\hat{O} \hat{D} \hat{i}$ \check{C} \hat{A} $\hat{U} \hat{U}$ $(\underline{a}_{B/A})_n$
 \hat{i} \hat{O} . $\rho \hat{D}$ \hat{A} $\hat{O} \hat{U} \hat{C} \hat{C}$ \hat{A} $\hat{S} \hat{C} \hat{i}$ \check{C} \hat{A} $\frac{3}{4} \hat{C}$ $\hat{O} \hat{A} \hat{O}$ \hat{i} $\hat{A} \hat{O} \hat{A} \hat{i}$ \hat{O} .
 $\pm \hat{E} \hat{S} \hat{A}$

$$\begin{aligned} \underline{a}_{B/A} &= \left(\underline{a}_{B/A} \right)_t + \left(\underline{a}_{B/A} \right)_n \\ \left(\underline{a}_{B/A} \right)_t &= r \underline{k} \wedge \underline{r}_{B/A} \left(\underline{a}_{B/A} \right)_t = r \underline{r} \end{aligned}$$

$\check{S} \hat{A} \hat{O} \hat{O}$

$$\begin{aligned} (\underline{a}_{B/A})_n &= -\check{S}^2 \underline{r}_{B/A}; (\underline{a}_{B/A})_n = r \check{S}^2 \\ \therefore \underline{a}_{B/A} &= r \underline{k} \wedge \underline{r}_{B/A} - \check{S}^2 \underline{r}_{B/A} \\ \therefore \underline{a}_B &= \underline{a}_A + 2 \underline{k} \wedge \underline{r}_{B/A} - \check{S}^2 \underline{r}_{B/A} \end{aligned}$$

4.6.4 $\dot{\mathbf{r}}$ in a rotating frame (Rate of change of vector with respect to a rotating frame)

Let \mathcal{O}_{XYZ} and \mathcal{O}_{xyz} be two frames with origins O and O' respectively. \mathcal{O}_{xyz} rotates with angular velocity $\boldsymbol{\omega}$ relative to \mathcal{O}_{XYZ} . Let \mathbf{r} be a vector in \mathcal{O}_{xyz} . Then $\dot{\mathbf{r}}$ in \mathcal{O}_{XYZ} is given by:

$$\dot{\mathbf{r}}_{\mathcal{O}_{XYZ}} = \dot{\mathbf{r}}_{\mathcal{O}_{xyz}} + \boldsymbol{\omega} \times \mathbf{r}$$

$$\therefore \underline{\dot{Q}} = Q_x \dot{i} + Q_y \dot{j} + Q_z \dot{k}$$

$$\therefore (\dot{Q})_{\mathcal{O}_{XYZ}} = \frac{dQ}{dt} = Q_x \dot{i} + Q_y \dot{j} + Q_z \dot{k} + Q_x \frac{di}{dt} + Q_y \frac{dj}{dt} + Q_z \frac{dk}{dt}$$

$$(\dot{Q})_{\mathcal{O}_{XYZ}} = (\dot{Q})_{\mathcal{O}_{xyz}} + Q_x \frac{di}{dt} + Q_y \frac{dj}{dt} + Q_z \frac{dk}{dt}$$

$$\text{Since } \dot{\mathbf{r}}_{\mathcal{O}_{XYZ}} = \dot{\mathbf{r}}_{\mathcal{O}_{xyz}} + \boldsymbol{\omega} \times \mathbf{r} \text{ and } \dot{\mathbf{r}}_{\mathcal{O}_{XYZ}} = 0 \text{ (if } \mathbf{r} \text{ is constant in } \mathcal{O}_{XYZ}\text{)}$$

$$0 = \dot{\mathbf{r}}_{\mathcal{O}_{xyz}} + \boldsymbol{\omega} \times \mathbf{r} \implies \dot{\mathbf{r}}_{\mathcal{O}_{xyz}} = -\boldsymbol{\omega} \times \mathbf{r}$$

$$(\dot{Q})_{\mathcal{O}_{xyz}} = Q_x \frac{di}{dt} + Q_y \frac{dj}{dt} + Q_z \frac{dk}{dt}$$

Therefore, $(\dot{Q})_{\mathcal{O}_{XYZ}} = (\dot{Q})_{\mathcal{O}_{xyz}} + \boldsymbol{\omega} \times \mathbf{r}$. This is the general result for the rate of change of a vector in a rotating frame.

$$Q_x \frac{di}{dt} + Q_y \frac{dj}{dt} + Q_z \frac{dk}{dt} = \underline{\dot{S}}_r \wedge \underline{Q}$$

Let \mathcal{O}_{XYZ} and \mathcal{O}_{xyz} be two frames with origins O and O' respectively. \mathcal{O}_{xyz} rotates with angular velocity $\boldsymbol{\omega}$ relative to \mathcal{O}_{XYZ} . Let \mathbf{r} be a vector in \mathcal{O}_{xyz} . Then $\dot{\mathbf{r}}$ in \mathcal{O}_{XYZ} is given by:

$$Q_x \frac{di}{dt} + Q_y \frac{dj}{dt} + Q_z \frac{dk}{dt} = \underline{\dot{S}}_r \wedge \underline{Q}$$

$$\therefore (\dot{Q})_{\mathcal{O}_{XYZ}} = (\dot{Q})_{\mathcal{O}_{xyz}} + \underline{\dot{S}}_r \wedge \underline{Q}$$

4.6.5 Equation of motion for a rigid body

Let \mathcal{O} be a fixed frame and \mathcal{O}' be a rotating frame with origin O' . Let \mathbf{r} be a vector in \mathcal{O}' . Then the equation of motion for a rigid body is given by:

$$\sum \mathbf{M}_G = \dot{\mathbf{H}}_G$$

Let \mathcal{O} be a fixed frame and \mathcal{O}' be a rotating frame with origin O' . Let \mathbf{r} be a vector in \mathcal{O}' . Then the equation of motion for a rigid body is given by:

4.6.8 Angular Impulse and Angular Momentum

Consider a rigid body rotating with angular velocity ω about a fixed axis through the origin O . The angular momentum H_O is defined as the sum of the angular momenta of all particles i about O .

$$H_O = \sum r_i \wedge m_i v_i$$

where r_i is the position vector of particle i relative to O , and v_i is its velocity. For a rigid body rotating with angular velocity ω , the velocity of particle i is $v_i = \omega \wedge r_i$.

$$\left(m_i \frac{d}{dt} (v_i) = m_i a_i = F_i \right)$$

$$\therefore \frac{dH_O}{dt} = \dot{H}_O = \sum n_i \wedge F_i = \sum M_O$$

$$\int_1^2 dH_O = \int_1^2 \sum M_O dt;$$

$$(H_O)_2 = (H_O)_1 + \int_1^2 \sum M_O dt;$$

$$\begin{aligned} H_O &= \sum n_i \wedge m_i v_i \\ &= \sum n_i \wedge m_i (\omega \wedge r_i); \end{aligned}$$

Consider a rigid body rotating with angular velocity ω about a fixed axis through the origin O .

$$\omega \wedge r_i = \omega r \wedge l_r$$

where n_i is the normal to the area element dA_i at position r_i from the axis of rotation.

$$\therefore H_O = \sum \omega n_i (m_i r_i \wedge l_r)$$

$$= \sum \omega m_i r_i (r_i \wedge l_r)$$

$$r_i \wedge l_r = r_i l_r \wedge l_r = r_i k$$

$$\therefore H_O = \omega \left(\sum m_i r_i^2 \right) k$$

$$= I_O \omega k$$

$$(H_O)_2 = I_O \omega_2 k$$

$$(H_O)_1 = I_O \omega_1 k$$

$$\pm \int_1^2 \sum M_O dt = I_O (\omega_2 - \omega_1) k$$

$$\ll \text{øÄÐ } (I_0 W_2) = (I_0 w_1) + \int_{t_1}^{t_2} M_0 dt$$

4.6.9. ÍÆø - ó¼j ðð(Conservation of Angular Momenturn)

ðÉÚì ò|Áj Õù ´ýÈø ðÈÁ´´ °, ù |°ÁøÃÎ ò§ÁjÐ ðÈòùÇç Ì ÈòÐ ðjì ðòÃÎ ðÈÐ Á´´ °, ù ¼jì ðÇ´´ Á, ù ãî°ÃÁjÌ ò. t₁ §¿Äð¼ø |¼jÌ ¼çÌ |jÃ - ó¼í ð ù t₂ §¿Äð¼ø |¼jÌ ¼çÌ |jÃ - ó¼í ð ù Ì °i°ÁÁj, - ùÇÉ. |¼jÌ ¼çÁý «´´ ÈòÐ §¿Sj ðÏ ð ¼ç½ç×§Á, ò ±ó¼ ¼ç´´ °ÃÖö §°Áç ðòÃÎ ðÈÐ. «´´ ÈòÐ ÍÆø - ó¼í ð ù ò ²§¼Ûò ´Ö ðùÇç Ì ÈòÐ ¼jì ðòÃÎ ðÈÐ.

4.6.10. Áj¼çç ½ì ð ù

Áj¼çç 4.6.10.1

´Ö çç´´ ÄÄjÉ ðùÇç´´ Äì Ì ÈòÐ ¼jÌ ´ýÚ ÍÆýÚ þÁí Ì Á´´ ¼ " = 6(1+e^{-4t}) ±ýÈ °ÁýÄjÌ « ÈçÁç ðÈÐ. " -´´ ÄÄÉçÖö t ÄÉjÉÄÖö « ÇÁ¼òÃÎ ýÉÉ. ¼ ð¼ý §j½ « í ð |¼j´´ Ä× ù ¼ç´´ °§Á, ò ÁúÚò ÓÍ ð ò -´´ ÄÄü´´ È t=0, t=3 ÄÉjÉÄj, - ùÇ§ÁjÐ ¼ÉÄjÉç ð × ò.

¼É×:

$$n = 6(1 + e^{-4t})$$

$$w = \frac{d_n}{dt} = 6(-4)e^{-4t} = -24e^{-4t}$$

$$r = \frac{d^2 n}{dt^2} = -24(-4)e^{-4t} = 96e^{-4t}$$

$$n = 12 \quad \text{-´´ ÄÄý}$$

(i) t=0, w=-24 -´´ ÄÄý/(ÄÉjÉ)

r = 96 -´´ ÄÄý/(ÄÉjÉ)

(ii) t=3, 6(1+e⁻¹²)

$$w = -24e^{-12}$$

$$\boxed{r = 96e^{-12}}$$

Áj¼çç 4.6.10.2

ðùÇç´´ Ä´´ ÄÄÁjì |¼jÌ ¼ òi, Äö ´ýÈø ´Ö ÄÚ ÍüÈòÄðÍ ùÇÐ. |¼j¼ì ð¼ø òi, Äö çç´´ ÄÄj, - ùÇÐ. ÄÚ |¼jÍ Í Ú¼ç ðùÇçÄø Á´´ ° ´ýÚ ÄÄýÄì ðòÃÎ ðÈÐ. « ùÁ´´ ° ÓÍ ð ò a = (5t) Ä/(ÄÉjÉ)² ´ý´´ È

$$w = w_0 + \Gamma t$$

$$20 = 15 + 5t \quad 5t = 5, t = 1 \text{ s}$$

4.6.10.4

4.6.10.4. $\vec{v} = v_0 + \Gamma t$ $\vec{v} = 15 + 5t$ $v = 20$ $t = 1$ s. $\vec{a} = \frac{dv}{dt} = 5$ m/s². $\vec{a}_n = r\omega^2 = 2(3)^2 = 18$ m/s². $\vec{a}_t = r\Gamma = 2 \cdot 5 = 10$ m/s². $a = \sqrt{18^2 + 10^2} = \sqrt{324 + 100} = \sqrt{424} = 20.6$ m/s². $G = \frac{25 \cdot 10}{(20.6)^2} = 0.59$ g.

3.4. x

$$a = \sqrt{a_n^2 + a_t^2}$$

$$G = 25 \cdot 10 / (20.6)^2$$

$$a_n = r\omega^2 = 2(3)^2 = 18 \text{ m/s}^2$$

$$a_t = r\Gamma = 2 \cdot 5 = 10 \text{ m/s}^2$$

$$25 = \sqrt{18^2 + (2)r^2}$$

$$625 = 324 + 4r^2$$

$$4r^2 = 301 \quad r^2 = 75.25$$

$$r = 8.378 \text{ m}$$

4.6.10.5

4.6.10.5. $M = 2a$ $\vec{v} = v_0 + \Gamma t$ $\vec{v} = 15 + 5t$ $v = 20$ $t = 1$ s. $\vec{a} = \frac{dv}{dt} = 5$ m/s². $\vec{a}_n = r\omega^2 = 2(3)^2 = 18$ m/s². $\vec{a}_t = r\Gamma = 2 \cdot 5 = 10$ m/s². $a = \sqrt{18^2 + 10^2} = 20.6$ m/s². $G = \frac{25 \cdot 10}{(20.6)^2} = 0.59$ g.

3.4. x

$$(pU - pA) - (pU - pA) = \rho \cdot \frac{1}{2} \cdot v^2 - \rho \cdot \frac{1}{2} \cdot v_0^2 = \rho \cdot \frac{1}{2} \cdot (v^2 - v_0^2)$$

$$\frac{1}{2} \left(\frac{4}{3} M a^2 \right) w^2 - \frac{1}{2} \left(\frac{4}{3} M a^2 \right) (0) = M g (2a)$$

$$\frac{2}{3} a w^2 = 2g$$

$$w^2 = \frac{3g}{a} \therefore w = \sqrt{3g/a}$$

4.6.10.6

4.6.10.6. $a = \frac{dv}{dt} = 5$ m/s². $\vec{a}_n = r\omega^2 = 2(3)^2 = 18$ m/s². $\vec{a}_t = r\Gamma = 2 \cdot 5 = 10$ m/s². $a = \sqrt{18^2 + 10^2} = 20.6$ m/s². $G = \frac{25 \cdot 10}{(20.6)^2} = 0.59$ g.

$\dot{\theta} = \frac{1}{2} \dot{\phi}$

$\frac{3}{4} E \times$

$\frac{1}{2} Ma^2 + Ma^2 = \frac{3}{2} Ma^2$

$$\frac{1}{2} Ma^2 + Ma^2 = \frac{3}{2} Ma^2$$

$\frac{1}{2} \left(\frac{3}{2} Ma^2 \right) \omega^2 - \frac{1}{2} \left(\frac{3}{2} Ma^2 \right) (0)^2 = Mga$

$$\frac{1}{2} \left(\frac{3}{2} Ma^2 \right) \omega^2 - \frac{1}{2} \left(\frac{3}{2} Ma^2 \right) (0)^2 = Mga$$

$\omega = \sqrt{\frac{4ga}{3a}}$

$$\frac{3}{4} Ma^2 \omega^2 = mga$$

$$\omega = \sqrt{4g/3a}$$

4.6.10.7

A rod of length 0.2 m is pivoted at A and makes an angle of 45 degrees with the horizontal. A force of 0.1 N is applied at C, perpendicular to the rod. A force of 0.2 N is applied at B, perpendicular to the rod. The velocity of A is 2 m/s downwards.

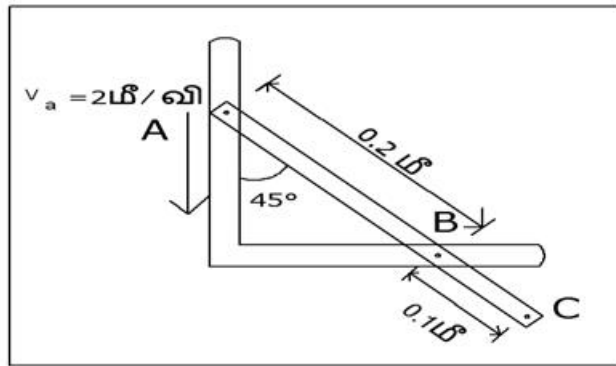


Fig. 4-6-2

$\frac{3}{4} E \times$

The velocity of B is given by $\underline{V}_B = \underline{V}_A + \underline{\omega} \wedge \underline{r}_{B/A}$

$$\underline{V}_B = \underline{V}_A + \underline{\omega} \wedge \underline{r}_{B/A}$$

$$V_B \underline{i} = 2 \underline{j} + [\underline{\omega} \wedge 0.2 \sin 45^\circ \underline{i} - 0.2 \cos 45^\circ \underline{j}]$$

$$\underline{V}_B i = -2\underline{j} + 0.2w \sin 45^\circ \underline{j} - 0.2w \cos 45^\circ \underline{i} \quad V_B = 0.2w \cos 45^\circ$$

$$0 = -2 + 0.2w \sin w$$

$$\cdot W = 14.1 \rightarrow \dots \hat{A} \hat{A} \hat{y} / (\hat{A} \hat{c} \hat{E} \hat{j} \hat{E})$$

$$V_B = 2 \hat{A} \hat{A} \hat{c} \hat{E} \hat{j} \hat{E}$$

Unit 5
 - $\tilde{A}_j \ddot{o} \times$
 (Friction)

$\dot{y} \ddot{E} | \tilde{A}_j \dot{y} \dot{U} | \frac{3}{4} \hat{I} \ddot{o} | \tilde{A}_j \ddot{O} \ddot{u} \ddot{U} \dot{I} \dot{c} \dot{1} \frac{1}{4} \dot{S} \dot{A} \dot{O} | \tilde{A}_j \ddot{O} \dot{C} \dot{y} \dot{A} \dot{D} \dot{A} \dot{u} | \dot{E}_j \ddot{O}$
 $| \tilde{A}_j \ddot{O} \dot{u} \dot{A} \dot{O} \dot{I} \dot{I} \frac{3}{4} \dot{A} \dot{o} \frac{3}{4} \hat{I} \dot{I} \dot{o} \dot{A} \dot{c} \dot{o} \dot{S} \dot{A} - \tilde{A}_j \ddot{o} \times \dot{A} \dot{c} \dot{o} \pm \dot{E} \dot{o} \dot{A} \dot{I} \dot{o}.$

5.1 - $\tilde{A}_j \ddot{o} \times \dot{A} \ddot{A} \ddot{E}$

$\dot{p} \dot{O} | \tilde{A}_j \ddot{O} \dot{u} \dot{u} \dot{y} \ddot{E} | \tilde{A}_j \dot{y} \dot{U} | \frac{3}{4} \dot{O} \dot{I} \dot{I} | \dot{I} \dot{I} \dot{n} \dot{E} \dot{O} \dot{o} \frac{3}{4} \dot{I} \dot{o}, \dot{O}$
 $| \tilde{A}_j \ddot{O} \dot{C}_j \dot{E} \dot{D} \dot{A} \dot{u} \dot{E} | \tilde{A}_j \ddot{O} \dot{C} \dot{y} \dot{A} \dot{D} \dot{A} \dot{O} \dot{I} \dot{I} \frac{3}{4} \dot{A} \dot{o} \frac{3}{4} \hat{I} \dot{o} \dot{A} \frac{3}{4} \dot{u} \dot{I} \ll \dot{A} \dot{u} \dot{E} \dot{y}$
 $| \frac{3}{4} \hat{I} \dot{O} \dot{u} \dot{C} \dot{A} \dot{o} \dot{c} \dot{O} \dot{o} \dot{A} \dot{c} \dot{o} \dot{I} \dot{I} \dot{I} \dot{I} \dot{A} \frac{1}{2} \dot{A}_j \dot{O} \dot{u} \dot{C} \ll \dot{u} \dot{A} \dot{O} | \tilde{A}_j \ddot{O} \dot{u} \dot{C} \dot{U} \dot{I} \frac{1}{4} \dot{A}$
 $\dot{A} \dot{n} \dot{O} - \tilde{A}_j \ddot{o} \times \pm \dot{E} \dot{o} \dot{A} \dot{I} \dot{o}.$

- $\tilde{A}_j \ddot{o} \times \pm \dot{y} \dot{A} \dot{D} \frac{3}{4} \dot{E}_j \dot{S} \dot{A} \dot{o} \dot{I} \dot{I} \dot{O} \dot{A} \dot{c} \dot{o} \dot{p} \dot{A} \dot{I} \dot{O} \dot{I} \dot{I} \dot{O} \frac{3}{4} \hat{I} \dot{o} \dot{A} \frac{3}{4} \dot{u} \dot{I} \dot{S} \dot{A} \dot{o}$
 $\ll \frac{3}{4} \dot{c} \dot{A}_j \dot{I} - \tilde{A}_j \ddot{o} \times \dot{c} \dot{c} \dot{u} \dot{A} \frac{3}{4} \dot{O} \dot{A} \dot{A} \dot{I} \dot{O} \dot{A} \dot{n} \dot{O} \dot{U} \dot{I} \dot{I} | \dot{c} \dot{A} - \tilde{A}_j \ddot{o} \times$ (Kinetic
 functional) $\dot{O} \dot{U} \dot{I} \dot{c} \dot{A} \dot{O} \dot{A} \frac{3}{4} \dot{y} \dot{c} \dot{c} \dot{A} \dot{I} \dot{I} \dot{o} \dot{A} \dot{E} \dot{I} \dot{I} \dot{c} \dot{c} \dot{u} \dot{A} \frac{3}{4} \dot{u} \dot{I} \dot{z} \dot{u} \dot{E} \dot{c} \dot{A} \dot{o} \frac{3}{4} \dot{I} \dot{E} \dot{A}$
 $| \dot{A} \dot{C} \dot{O} \dot{A} \dot{I} \dot{o} \dot{D} \dot{E} \dot{D} \dot{p} \dot{A} \dot{I} \dot{o} \dot{A} \dot{n} \dot{O} \dot{U} \dot{I} \dot{I} | \dot{c} \dot{A} - \tilde{A}_j \ddot{o} \times \dot{A} \dot{c} \dot{o} \pm \dot{o} \dot{S} \dot{A}_j \dot{D} \dot{o}$
 $\dot{p} \dot{A} \dot{I} \dot{I} \dot{c} \dot{A} - \tilde{A}_j \ddot{o} \times \dot{A} \dot{c} \dot{o} \dot{A} \dot{y} | \dot{A} \dot{O} \dot{o} \dot{A} \frac{3}{4} \dot{O} \dot{A} \dot{u} \dot{I} \dot{O} \dot{U} \dot{I} \dot{I} \dot{E} \dot{A}_j \dot{I} - \dot{u} \dot{C} \dot{D}.$

$\dot{I} \dot{E} \dot{u} \dot{O} \dot{A} \dot{o} \frac{1}{4} \dot{A} \dot{O} \dot{S} \dot{A} \dot{u} \dot{U} \frac{3}{4} \dot{O} \dot{I} \dot{I} - \dot{o} \dot{A} \dot{o} \dot{I} \dot{u} \dot{C} \dot{c} \dot{A} \dot{A} \dot{A} \dot{O} - \dot{u} \dot{C} \dot{D} \dot{I} - \tilde{A}_j \ddot{o} \times$
 $\dot{z} \dot{u} \dot{A} \dot{I} \dot{E} \dot{D} \dot{A} \dot{c} \times \dot{o} \dot{A} \dot{u} \dot{p} \dot{A} \dot{o} \dot{I} \dot{I} \dot{A} \dot{a} \dot{A} \dot{o} | \tilde{A}_j \ddot{O} \dot{o} \dot{U} \dot{I} \dot{I} \dot{p} \dot{o} \frac{3}{4} \dot{I} \dot{A} - \dot{u} \dot{C} \dot{D} \dot{I}$
 $- \tilde{A}_j \ddot{o} \times \dot{O} \dot{E} \dot{I} \frac{1}{2} \dot{O} \dot{I} \dot{O} \frac{3}{4} \hat{I} \dot{I} - \dot{u} \dot{C} \dot{D} \dot{I} \ll \dot{S} \frac{3}{4} \dot{S}_j \dot{A} \dot{o} \frac{3}{4} \dot{O} \dot{O} \dot{E} \dot{C} \dot{A} \frac{3}{4} \dot{I} \dot{E} \dot{A} \dot{I} \dot{p} \dot{A} \dot{o} \dot{I} \dot{I} \dot{A}$
 $\dot{a} \dot{A} \dot{o} | \tilde{A}_j \ddot{O} \dot{o} \dot{U} \dot{I} \dot{I} - \dot{u} \dot{C} \dot{D} \dot{I} - \tilde{A}_j \ddot{o} \times \dot{A} \dot{c} \dot{o} \dot{I} \dot{E} \dot{O} \dot{A} \dot{O} \frac{1}{4} \dot{O} \frac{3}{4} \hat{I} \dot{I} \ll \dot{C} \dot{A} \dot{O} \ll \dot{A} \dot{E} \dot{D}.$

$\dot{p} \dot{O} | \tilde{A}_j \ddot{O} \dot{u} \dot{u} \dot{y} \ddot{E} | \tilde{A}_j \dot{y} \dot{U} | \frac{3}{4} \dot{O} \dot{I} \dot{I} | \dot{I} \dot{I} \dot{u} \dot{U} \dot{o} \dot{c} \dot{c} \dot{A} \dot{A} \dot{O},$
 $\ll \dot{o} | \tilde{A}_j \ddot{O} \dot{o} \dot{U} \dot{I} \dot{I} \dot{p} \dot{I} \dot{A} \dot{O} \dot{A} \dot{I} \dot{o} - \tilde{A}_j \ddot{o} \times \dot{A} \dot{c} \dot{o} \frac{3}{4} \dot{I} \dot{I} \dot{A} \dot{u} \dot{E} | \tilde{A}_j \ddot{O} \dot{C} \dot{y}$
 $\dot{A} \dot{A} \frac{1}{4} \dot{O} \frac{3}{4} \dot{y} \dot{A}_j \dot{A} \dot{c} \dot{A}_j \dot{I} \dot{I} \dot{I} \dot{O} \dot{A} \dot{I} \dot{E} \dot{D}.$

- $\frac{1}{4} \dot{E} \dot{E} \dot{A}_j \dot{p} \dot{A} \dot{I} \dot{O} \dot{c} \dot{c} \dot{E} \dot{A} \dot{O} \dot{I} \dot{E} \ll \dot{o} \dot{A} \dot{D} \dot{O} \dot{U} \dot{I} \dot{c} \dot{A} \dot{O} \dot{E} \dot{O} \dot{u} \dot{C} \dot{A} \dot{I} \dot{o} \dot{A} \dot{o} \frac{1}{4}$
 $\dot{A} \dot{o} \frac{1}{4} \dot{A} \dot{o} \dot{A} \dot{I} \frac{3}{4} \dot{c} \dot{A} \dot{p} \dot{A} \dot{o} \dot{c} \dot{c} \dot{A} - \tilde{A}_j \ddot{o} \times \dot{I} \dot{I} | \dot{c} \dot{A} \dot{A} \dot{A} \dot{O} \dot{O} \pm \dot{o} \dot{A} \dot{A}_j \dot{I} \dot{I}$ (Range of Static
 Friction) $\dot{O} \frac{3}{4} \dot{O} \dot{A} \dot{I} \dot{E} \dot{D} \dot{p} \dot{o} \dot{c} \dot{c} \dot{A} \dot{A} \dot{O} - \tilde{A}_j \ddot{o} \times \dot{A} \dot{c} \dot{o} \dot{A} \dot{y} \dot{A} \frac{3}{4} \dot{O} \dot{O} \dot{O} \dot{A} \dot{c} \dot{c} \dot{A} \dot{I} \dot{I}$
 $- | \dot{c} \dot{A} \frac{3}{4} \dot{I} \dot{E} \dot{O} \dot{A} \dot{y} \dot{A}_j \dot{I} \dot{I} \dot{C}_j \dot{I} \dot{o} \frac{3}{4} \dot{E} \dot{A}_j \dot{E} \dot{O} \dot{A} \dot{I} \dot{o}.$

5.2 $\dot{c} \dot{c} \dot{A} \dot{A} \dot{A} \dot{O} - \tilde{A}_j \ddot{o} \times \dot{A} \dot{O} \dot{c} \dot{c} \dot{u} \dot{A} \dot{y} \dot{A} \dot{O} \dot{A}_j \dot{U}$

$\dot{A} \dot{O} \dot{c} \dot{c} \dot{1}$

$\dot{p} \dot{O} | \tilde{A}_j \ddot{O} \dot{u} \dot{u} \dot{y} \ddot{E} | \tilde{A}_j \dot{y} \dot{U} | \frac{3}{4} \dot{O} \dot{I} \dot{I} | \dot{I} \dot{I} \dot{n} \dot{E} \dot{O} \dot{o} \frac{3}{4} \dot{I} \dot{o}, \ll \dot{A} \dot{u} \dot{U} \dot{u}$
 $\dot{y} \dot{E} \dot{y} \dot{A} \dot{D} | \dot{O} \dot{A} \dot{o} \dot{A} \dot{I} \dot{o} - \tilde{A}_j \ddot{o} \times \dot{A} \dot{c} \dot{o} \dot{E} \dot{D} \frac{3}{4} \dot{c} \dot{c} \dot{O}, \ll \dot{A} \dot{u} \dot{E} \dot{y} | \frac{3}{4} \hat{I} \dot{O} \dot{u} \dot{C} \dot{c} \dot{p} \dot{A} \dot{I} \dot{O}$
 $| \frac{3}{4} \hat{I} \dot{I} \dot{I} \dot{O} \dot{A} \dot{O} \dot{o} \frac{3}{4} \dot{c} \dot{c} \dot{O} \dot{I} \dot{I} \pm \frac{3}{4} \dot{O} \dot{A}_j \dot{I} \dot{o}.$

$\dot{A} \dot{O} \dot{c} \dot{c} \dot{2}$

$| \tilde{A}_j \ddot{O} \dot{u} \dot{O} \dot{A} \dot{c} \dot{c} \dot{A} \dot{A} \dot{O} \dot{u} \dot{C} | \tilde{A}_j \ddot{O} \dot{D}, - \tilde{A}_j \ddot{o} \times \dot{A} \dot{y} \ll \dot{C} \times | \tilde{A}_j \ddot{O} \dot{C} \dot{y}$
 $\dot{p} \dot{A} \dot{I} \dot{O} \dot{I} \dot{I} \dot{O} \frac{3}{4} \hat{I} \dot{o} \dot{A} \frac{3}{4} \dot{u} \dot{I} \dot{I} \dot{O} \dot{I} \dot{c} \dot{A}_j \dot{O} \dot{S} \dot{A}_j \frac{3}{4} \dot{c} \dot{A} \frac{3}{4} \dot{I} \dot{o}.$

$\pm \dot{o} \dot{A} - \tilde{A}_j \ddot{o} \times$ (Limiting friction)

$\dot{A} \ddot{A} \ddot{E}$

$\dot{O} | \tilde{A}_j \ddot{O} \dot{u} \dot{S} \dot{A} | \dot{E}_j \dot{O} | \tilde{A}_j \ddot{O} \dot{C} \dot{y} \dot{A} \dot{D} \dot{O} | \dot{c} \dot{A}_j \dot{A} \dot{O} \dot{I} \dot{I} \dot{U} \dot{c} \dot{c} \dot{A} \dot{A} \dot{A} \dot{O} \dot{o} \frac{3}{4} \dot{I} \dot{o}$
 $\ll \dot{I} \dot{O} \dot{A} \dot{c} \dot{c} \dot{A} \pm \dot{o} \dot{A} \dot{A} \dot{I} \dot{I} \dot{I} \dot{y} \dot{E} \dot{D} \pm \dot{E} \dot{o} \dot{A} \dot{I} \dot{o} \ll \dot{o} \dot{S} \dot{A}_j \dot{D} \dot{c} \dot{c} \dot{O} \dot{o} - \tilde{A}_j \ddot{o} \times \pm \dot{o} \dot{A}$
 $- \tilde{A}_j \ddot{o} \times \pm \dot{E} \dot{o} \dot{A} \dot{I} \dot{o}.$

$\dot{A} \dot{O} \dot{c} \dot{c} \dot{3}$

$| \tilde{A}_j \ddot{O} \dot{u} \dot{u} - \tilde{A}_j \ddot{O} \dot{o} | \tilde{A}_j \ddot{O} \dot{D} \dot{c} \dot{c} \frac{1}{4} \dot{I} \dot{I} \dot{o} \pm \dot{o} \dot{A} - \tilde{A}_j \ddot{o} \times \dot{A} \dot{c} \dot{o}, | \frac{3}{4} \hat{I} \dot{I} \dot{I} \dot{O}$
 $\frac{3}{4} \dot{C} \dot{o} \frac{3}{4} \dot{y} | \dot{O} \dot{I} \dot{I} \dot{O} \dot{D} \dot{A} \dot{c} \dot{c} \dot{O} \dot{I} \dot{I} \dot{S}_j \dot{A} \dot{c} \dot{c} \frac{3}{4} \dot{O} \dot{O} \ll \dot{A} \dot{O} \dot{o}.$

Á¼ 4

« ùÁjÚ 2üÁî õ ±ø¨ Ä - Ájö×Á¨ º, |ÁjÖû ú |¾jî õ
 ŞÄüÄÄöÜ Ü¨ ¼Ä « Ç¨ ÄÖö (size) ÄÊÄö¨ ¾Öö (shape) ºjÁj¾Öî ì õ.

Á¼ 5

Ö |ÁjÖû ŞÄjËjÖ |ÁjÖÇyÁÐ ÄØì ç pÁî õ - ñ ¼jì ì õŞÄjÐ
 - ÁjöÄy ¾¨ º pÁî õ¾¨ ºì ì ±¾Öjì õ. - ÁjöÄy « Ç× |ÁjÖÇy ºj÷Ø
 ŞÄjð¨ ¾jì ºj÷Ø¾¾ÖÄ. - Éjø - ÁjöÄjÉÐ |ºì ì ò¾jì î ì ºÄÖÁî õ ±¾Ö÷Ø
 ¾jì ì òŞ¾jì | jüÜö ÄÇ ¾Ö |ÁjÖû müÄÄÖóÐ pÁî õ |¾j¼í ì õ
 ¾Ö½ö¾Ö - úÇ ÄÇ ¾Ö¾Öüî î ºüÜî ì º Äjì õ.

5.3 - Ájö×ì | Ø (Coefficient of friction)

±ø¨ Ä - ÁjöÄjÉÐ |ºì ì òÐ ±¾Ö÷Ø¾jì | Ä¨ ºÖ¼y | jüÜö ÁjËj
 ÄÇ ¾Ö - Ájö×ì | Ø ±ÉöÄî õ - ±yÜö ±Ø÷¾jø « Ð ì Èü öÄî õ.
 ºÄÇ¨ Ä « Äü öÄî õ ç¨ ÄÄÄÖî ì õŞÄjÐ F ±yÁÐ - Ájö¨ ÄÖö R ±yÁÐ
 |ºì ì òÐ ±¾Ö÷Ø¾jì | Ä¨ º¨ ÄÖö ì Èö¾jø,

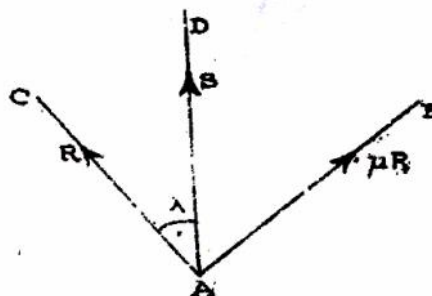
$$\frac{F}{R} = \mu$$

« ¾jÄÐ F = µR - ì õ.

|ÁjÖû ±ø¨ Ä ºÄÇ¨ Ä¨ Ä « ì | jÄÄÖî ì õ ç¨ Ä¨ Ä Çø, « Ş¾ Ä¾Öö¨ ¼Ä
 Rì ì F ±yÜö - Ájö×Á¨ º - R³ Ä¾jì ì º Äjì õ. ŞÄÖö ºy¨ ÈjÁjyÜ
 |¾jî õ |ÄüŞÄÜ |ÁjÖûŞºjËjÜ ì ì - ÄÜ¨ ¼Ä Ä¾Öö ÄjËjÜî Üî õ.

5.4 - Ájö×ì Şj½ö (Angle of friction)

ºÄÇ¨ Ä, ±ø¨ Ä ºÄÇ¨ Ä¨ Ä « ì ì õŞÄjÐ - Ájö×ö, |ºì ì òÐ ±¾Ö÷Ø
 ¾jì | Öö ºŞÄ¾ÉÄ¨ ºÄjî î Şº÷ì ì öÄËy |ºì ì òŞ¾jì | püÄ¨ º - ñ ¼jì ì õ
 Şj½ö - Ájö×ì Şj½ö ±ÉöÄî õ. « ò¾ÉÄ¨ º Ä¨ ÇjÁ¾Ö÷Ø¾jì | õ
 ±ÉöÄî õ.



Ä¾Ö 5-1

±î ò¾ pÖ|ÁjÖû Üö A ±yÜöÄ¾ö¾Ö |¾jî Ä¾jì | jüÜö. Ä¾Ö 5-
 1ø AC, AB ±yÜö Şj½ö | ü |ºì ì òÐ ±¾Ö÷Ø¾jì | Ä¨ º R, - Ájö×Á¨ º - R
 ±yÄÄüËy |ºÄÖÁî õ ¾¨ º º Çì ì Èü öî õ. püÄñ ì Ä¨ º Çy
 |¾jî ÄÄy Ä¨ º Ä S ±yÁÐ ì Èü öî õ. « Ð |ºÄÖÁî õ ¾¨ º Ä AD
 ±yÜö Şj½ö ì ÈöÄ¾jì | jüÜö.

« ö|ÁjÖÐ cÄD ±yÁÐ - Ájö×ì Şj½öÄjì õ. « º¾ } ±Éì | jüÜö.

$$R, -R = \pm \mu R$$

$$-R = S \sin \theta$$

$$R = S \cos \theta$$

$$\mu = \tan \theta$$

$$\therefore F \leq \mu R$$

$$F \leq \mu R$$

5.5 Cone of friction

The cone of friction is a cone of semi-angle λ where $\lambda = \tan^{-1} \mu$. The cone is shown in the diagram below.

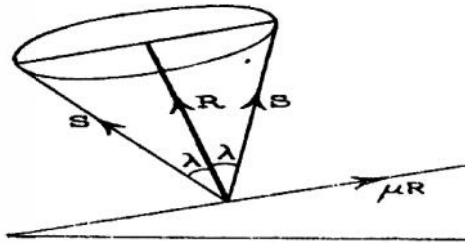


Fig 5-2

The angle λ is given by $\lambda = \tan^{-1}(\mu)$. The cone of friction is a cone of semi-angle λ where $\lambda = \tan^{-1} \mu$. The cone is shown in the diagram below. The cone is a cone of semi-angle λ where $\lambda = \tan^{-1} \mu$. The cone is shown in the diagram below.

(i) The cone of friction is a cone of semi-angle λ where $\lambda = \tan^{-1} \mu$. The cone is shown in the diagram below.

(ii) The cone of friction is a cone of semi-angle λ where $\lambda = \tan^{-1} \mu$. The cone is shown in the diagram below.

(iii) The cone of friction is a cone of semi-angle λ where $\lambda = \tan^{-1} \mu$. The cone is shown in the diagram below.

5.6 Band - brake and Belt friction

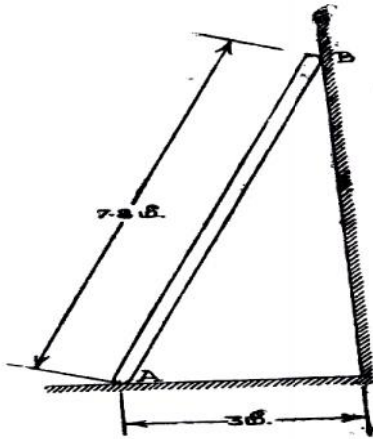
The band brake and belt friction are shown in the diagram below. The band brake is a band of material that is wrapped around a drum and is used to stop the drum from rotating. The belt friction is a belt that is wrapped around two pulleys and is used to transmit power from one pulley to the other.

5.7 - $\vec{F}_f \times \vec{v} = -\mu \vec{v}$ (Dry Friction)
 - $\mu = 0$ (Unlubricated) $\mu = 0.3$ (Lubricated)
 - $\vec{F}_f = \mu \vec{N}$ (Coulomb Friction) $\pm \vec{v}$

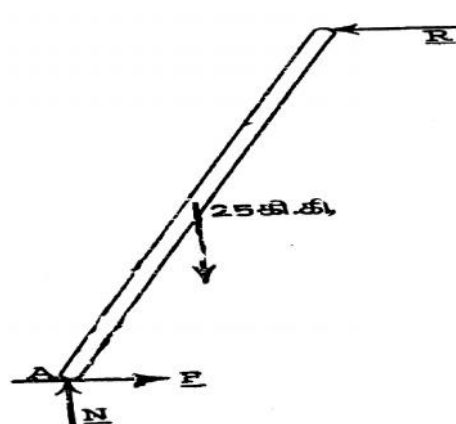
5.7.1 $\vec{F}_f \propto \vec{v}$ (Fluid Friction)
 $\vec{F}_f = -k \vec{v}$ (layers) $\vec{F}_f = -k \vec{v}$

5.7.2 $\vec{F}_f \propto \vec{v}^2$ (Internal Friction)
 $\vec{F}_f = -k \vec{v}^2$ (Kinetic Friction) $\vec{F}_f = -k \vec{v}^2$

$\vec{F}_f \propto \vec{v}^2$
 5.1 $\vec{F}_f \propto \vec{v}^2$ $\vec{F}_f = 7.8 \vec{v}^2$
 $\vec{F}_f \propto \vec{v}^2$ $\vec{F}_f = 5.5 \vec{v}^2$
 $\vec{F}_f \propto \vec{v}^2$ $\vec{F}_f = 0.30 \vec{v}^2$



Á¼õ 5-5



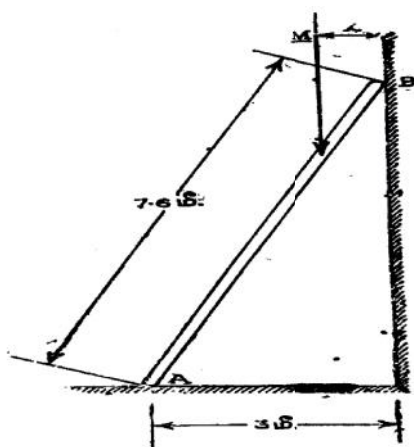
Á¼õ 5-6

$\sum F_y = 0 \rightarrow N - 25 = 0 \therefore N = 25$
 $\sum M_B = 0 \rightarrow 7.2F + 1.5(25) - 3(25) = 0$
 $F = 5.21$

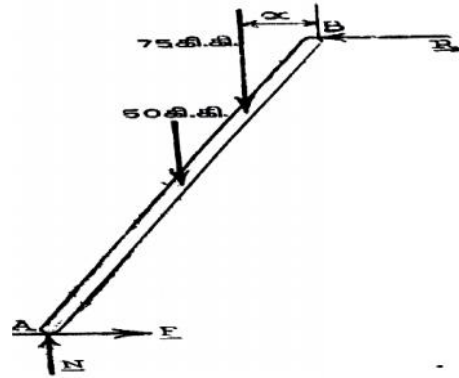
$$F' \pm 0 \cdot \ddot{A} - \ddot{A}_i \ddot{o} \times \ddot{A} \ddot{c} \cdot \ddot{o} = -N$$

$$= 0.3 \times 25 = 7.5 \text{ t}$$

$F = 5.21 < 7.5$ $\pm \ddot{y} \ddot{E} \ddot{i} \ddot{A} \ddot{3} \ddot{4} \ddot{i} \ddot{o} \ddot{2} \ddot{1} \ddot{2} \ddot{o} \ddot{A} \ddot{c} \ddot{c} \ddot{A} \ddot{A} \ddot{A} \ddot{O} \ddot{i} \ddot{l} \ddot{o} \ddot{\pm} \ddot{E} \ddot{U} \ddot{3} \ddot{4} \ddot{A} \ddot{i} \ddot{U} \ddot{E} \ddot{A} \ddot{i} \ddot{o}$
 $\ddot{A} \ddot{i} \ddot{3} \ddot{4} \ddot{i} \ddot{o} \ddot{5} \ddot{-} \ddot{2} \ddot{.} \ddot{S} \ddot{A} \ddot{U} \ddot{U} \ddot{E} \ddot{A} \ddot{U} \ddot{2} \ddot{i} \ddot{2} \ddot{o} \ddot{7} \ddot{5} \ddot{t} \ddot{.} \ddot{t} \ddot{\pm} \ddot{1} \ddot{4} \ddot{O} \ddot{U} \ddot{C} \ddot{O} \ddot{A} \ddot{E} \ddot{3} \ddot{4} \ddot{y} \ddot{2} \ddot{1} \ddot{2} \ddot{A} \ddot{O} \ddot{2} \ddot{U} \ddot{A} \ddot{3} \ddot{4} \ddot{i} \ddot{U} \ddot{i} \ddot{U} \ddot{.}$



$\ddot{A} \ddot{1} \ddot{o}$
 $\ddot{5} \ddot{-} \ddot{7}$



$\ddot{A} \ddot{1} \ddot{o}$
 $\ddot{5} \ddot{-} \ddot{8}$
 $\ddot{2} \ddot{1} \ddot{2}$

$\ddot{z} \ddot{.} \ddot{A} \ddot{-} \ddot{A} \ddot{o} \ddot{A} \ddot{c} \ddot{i} \ddot{l} \ddot{o} \ddot{3} \ddot{4} \ddot{O} \ddot{1} \ddot{2} \ddot{o} \ddot{3} \ddot{4} \ddot{O} \ddot{A} \ddot{E} \ddot{3} \ddot{4} \ddot{U} \ddot{i} \ddot{l} \ddot{o} \ddot{I} \ddot{A} \ddot{U} \ddot{E} \ddot{U} \ddot{i} \ddot{l} \ddot{o} \ddot{p} \ddot{.} \ddot{1} \ddot{4} \ddot{S} \ddot{A} \ddot{O} \ddot{U} \ddot{C} \ddot{x} \ddot{\pm} \ddot{y} \ddot{U} \ddot{o}$
 $\ddot{1} \ddot{3} \ddot{4} \ddot{.} \ddot{A} \ddot{.} \ddot{A} \ddot{i} \ddot{.} \ddot{i} \ddot{n} \ddot{.} (\ddot{A} \ddot{1} \ddot{o} \ddot{5} \ddot{-} \ddot{7} \ddot{o} \ddot{A} \ddot{i} \ddot{.} \ddot{i} \ddot{x} \ddot{o})$
 $\ddot{p} \ddot{o} \ddot{I} \ddot{A} \ddot{i} \ddot{O} \ddot{D} \ddot{2} \ddot{1} \ddot{2} \ddot{A} \ddot{O} \ddot{I} \ddot{o} \ddot{A} \ddot{O} \ddot{A} \ddot{I} \ddot{o} \ddot{A} \ddot{c} \ddot{.} \ddot{o} \ddot{.} \ddot{u} \ddot{A} \ddot{1} \ddot{o} \ddot{5} \ddot{-} \ddot{8} \ddot{o} \ddot{.} \ddot{i} \ddot{O} \ddot{A} \ddot{O} \ddot{I} \ddot{u} \ddot{C} \ddot{E} \ddot{.}$

$\ddot{p} \ddot{o} \ddot{3} \ddot{4} \ddot{i} \ddot{.} \ddot{1} \ddot{2} \ddot{i} \ddot{l} \ddot{p} \ddot{A} \ddot{n} \ddot{1} \ddot{4} \ddot{i} \ddot{A} \ddot{D} \ddot{A} \ddot{.} \ddot{i} \ddot{l} \ddot{\pm} \ddot{I} \ddot{o} \ddot{D} \ddot{i} \ddot{.} \ddot{i} \ddot{O} \ddot{1} \ddot{4} \ddot{i} \ddot{l} \ddot{o} \ddot{.} \ddot{p} \ddot{i} \ddot{l} \ddot{4} \ddot{1} \ddot{3} \ddot{4} \ddot{i} \ddot{A} \ddot{i}$
 $\ddot{1} \ddot{2} \ddot{A} \ddot{i} \ddot{u} \ddot{-} \ddot{C} (3 \ddot{A} \ddot{c} \ddot{.} \ddot{o} \ddot{u} \ddot{:} \ddot{N}, \ddot{F}, \ddot{R}; \ddot{1} \ddot{3} \ddot{4} \ddot{i} \ddot{.} \ddot{A} \ddot{x} \ddot{:} \ddot{X}) \ddot{A} \ddot{c} \ddot{.} \ddot{o} \ddot{C} \ddot{.} \ddot{E} \ddot{o} \ddot{D} \ddot{O} \ddot{O} \ddot{3} \ddot{4} \ddot{C}$
 $\ddot{A} \ddot{c} \ddot{.} \ddot{o} \ddot{C} \ddot{i} \ddot{E} \ddot{3} \ddot{4} \ddot{i} \ddot{o} \ddot{a} \ddot{y} \ddot{U} \ddot{o} \ddot{A} \ddot{c} \ddot{.} \ddot{A} \ddot{i} \ddot{o} \ddot{A} \ddot{y} \ddot{A} \ddot{i} \ddot{l} \ddot{.} \ddot{C} \ddot{A} \ddot{.} \ddot{A} \ddot{A} \ddot{U} \ddot{i} \ddot{.} \ddot{O} \ddot{E} \ddot{O} \ddot{o} \ddot{.} \ddot{S} \ddot{A} \ddot{O} \ddot{o}$
 $\ddot{A} \ddot{O} \ddot{i} \ddot{1} \ddot{3} \ddot{4} \ddot{O} \ddot{i} \ddot{l} \ddot{2} \ddot{U} \ddot{E} \ddot{3} \ddot{4} \ddot{i} \ddot{E} \ddot{n} \ddot{F}' = -N \pm \ddot{y} \ddot{E} \ddot{o} \ddot{A} \ddot{y} \ddot{A} \ddot{i} \ddot{l} \ddot{o} \ddot{A} \ddot{A} \ddot{y} \ddot{A} \ddot{i} \ddot{o} \ddot{3} \ddot{4} \ddot{S} \ddot{A} \ddot{n} \ddot{E}$
 $\ddot{A} \ddot{O} \ddot{.} \ddot{E} \ddot{D} \ddot{.} \ddot{\pm} \ddot{E} \ddot{S} \ddot{A}$

$$\sum F_y = 0 \rightarrow N - 25 - 75 = 0 \therefore N = 100 \text{ t} \uparrow$$

$$F' = -N \rightarrow F' = 0.3 \times (100) = 30 \text{ t}$$

$$\therefore F = -N = 30 \text{ t} \rightarrow$$

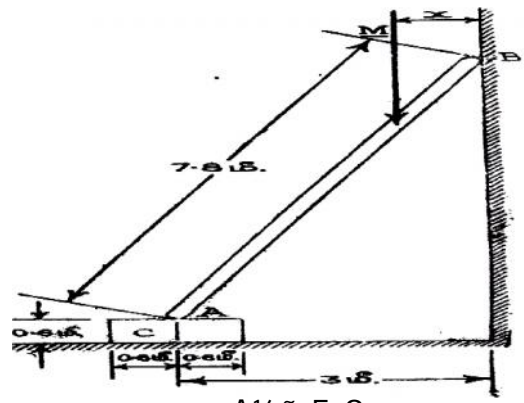
$$\sum M_B = 0 \rightarrow x(75) + 1.5(25) - 3(100) + 7.2(30) = 0$$

$$\therefore x = 1.035 \text{ Af}$$

$\ddot{A} \ddot{i} \ddot{3} \ddot{4} \ddot{i} \ddot{o} \ddot{5} \ddot{-} \ddot{3} \ddot{O} \ddot{y} \ddot{\pm} \ddot{I} \ddot{o} \ddot{3} \ddot{4} \ddot{.} \ddot{1} \ddot{2} \ddot{i} \ddot{l} \ddot{o} \ddot{2} \ddot{1} \ddot{2} \ddot{A} \ddot{y} \ddot{a} \ddot{A} \ddot{o} \ddot{p} \ddot{y} \ddot{U} \ddot{o} \ddot{o} \ddot{E} \ddot{D} \ddot{1} \ddot{3} \ddot{4} \ddot{i} \ddot{.} \ddot{A} \ddot{x}$
 $\ddot{S} \ddot{A} \ddot{S} \ddot{A} \ddot{1} \ddot{o} \ddot{O} \ddot{A} \ddot{3} \ddot{4} \ddot{i} \ddot{.} \ddot{5} \ddot{0} \ddot{t} \ddot{.} \ddot{t} \ddot{\pm} \ddot{1} \ddot{4} \ddot{O} \ddot{U} \ddot{C} \ddot{D} \ddot{o} \ddot{3} \ddot{4} \ddot{.} \ddot{A} \ddot{A} \ddot{A} \ddot{O} \ddot{O} \ddot{D} \ddot{0} \ddot{.} \ddot{6} \ddot{A} \ddot{D} \ddot{1} \ddot{4} \ddot{.} \ddot{-} \ddot{A} \ddot{A} \ddot{O} \ddot{o}$
 $\ddot{-} \ddot{u} \ddot{C} \ddot{I} \ddot{A} \ddot{D} \ddot{E} \ddot{.} \ddot{A} \ddot{o} \ddot{3} \ddot{4} \ddot{.} \ddot{A} \ddot{A} \ddot{O} \ddot{A} \ddot{1} \ddot{o} \ddot{5} \ddot{-} \ddot{9} \ddot{o} \ddot{.} \ddot{i} \ddot{O} \ddot{E} \ddot{A} \ddot{A} \ddot{i} \ddot{U} \ddot{.} \ddot{A} \ddot{o} \ddot{D} \ddot{\ll} \ddot{3} \ddot{4} \ddot{y} \ddot{S} \ddot{A} \ddot{O} \ddot{2} \ddot{1} \ddot{2} \ddot{A} \ddot{y}$
 $\ddot{U} \ddot{O} \ddot{.} \ddot{E} \ddot{\ll} \ddot{.} \ddot{A} \ddot{A} \ddot{3} \ddot{4} \ddot{i} \ddot{U} \ddot{i} \ddot{U} \ddot{.} \ddot{B} \ddot{A} \ddot{O} \ddot{I} \ddot{A} \ddot{U} \ddot{E} \ddot{U} \ddot{i} \ddot{l} \ddot{o} \ddot{2} \ddot{1} \ddot{2} \ddot{i} \ddot{l} \ddot{o} \ddot{-} \ddot{u} \ddot{C} \ddot{-} \ddot{A} \ddot{i} \ddot{o} \ddot{x} \ddot{i} \ddot{1} \ddot{.} \ddot{O}$
 $\ddot{0} \ddot{.} \ddot{2} \ddot{0} \ddot{\pm} \ddot{y} \ddot{U} \ddot{o} \ddot{A} \ddot{A} \ddot{O} \ddot{2} \ddot{1} \ddot{2} \ddot{i} \ddot{l} \ddot{o} \ddot{I} \ddot{A} \ddot{D} \ddot{E} \ddot{i} \ddot{l} \ddot{o} \ddot{-} \ddot{u} \ddot{C} \ddot{-} \ddot{A} \ddot{i} \ddot{o} \ddot{x} \ddot{i} \ddot{1} \ddot{.} \ddot{O} \ddot{0} \ddot{.} \ddot{3} \ddot{5} \ddot{\pm} \ddot{y} \ddot{U} \ddot{o}$
 $\ddot{3} \ddot{4} \ddot{.} \ddot{A} \ddot{i} \ddot{l} \ddot{o} \ddot{I} \ddot{A} \ddot{D} \ddot{E} \ddot{i} \ddot{l} \ddot{o} \ddot{-} \ddot{u} \ddot{C} \ddot{-} \ddot{A} \ddot{i} \ddot{o} \ddot{x} \ddot{i} \ddot{1} \ddot{.} \ddot{O} \ddot{0} \ddot{.} \ddot{2} \ddot{5} \ddot{\pm} \ddot{y} \ddot{U} \ddot{o} \ddot{1} \ddot{.} \ddot{U} \ddot{.} \ddot{A} \ddot{E} \ddot{3} \ddot{4} \ddot{U} \ddot{.} \ddot{1} \ddot{4} \ddot{A}$
 $\ddot{\pm} \ddot{1} \ddot{4} \ddot{O} \ddot{o} \ddot{.} \ddot{2} \ddot{1} \ddot{2} \ddot{A} \ddot{C} \ddot{U} \ddot{.} \ddot{1} \ddot{4} \ddot{A} \ddot{\pm} \ddot{1} \ddot{4} \ddot{O} \ddot{o} \ddot{O} \ddot{o} \ddot{3} \ddot{4} \ddot{A} \ddot{A} \ddot{i} \ddot{3} \ddot{4} \ddot{i} \ddot{.} \ddot{1} \ddot{2} \ddot{i} \ddot{l} \ddot{o} \ddot{1} \ddot{.} \ddot{i} \ddot{l} \ddot{o} \ddot{D} \ddot{U} \ddot{C}$
 $\ddot{A} \ddot{3} \ddot{4} \ddot{O} \ddot{D} \ddot{C} \ddot{i} \ddot{x} \ddot{o} \ddot{1} \ddot{.} \ddot{U} \ddot{.} \ddot{2} \ddot{1} \ddot{2} \ddot{A} \ddot{y} \ddot{p} \ddot{A} \ddot{i} \ddot{o} \ddot{A} \ddot{O} \ddot{.} \ddot{A} \ddot{.} \ddot{A} \ddot{\ll} \ddot{.} \ddot{1} \ddot{4} \ddot{O} \ddot{3} \ddot{4} \ddot{i} \ddot{o} \ddot{x} \ddot{\pm} \ddot{y} \ddot{U} \ddot{o}$
 $\ddot{1} \ddot{3} \ddot{4} \ddot{i} \ddot{.} \ddot{A} \ddot{.} \ddot{A} \ddot{i} \ddot{.} \ddot{i} \ddot{n} \ddot{.} \ddot{p} \ddot{D} \ddot{a} \ddot{y} \ddot{E} \ddot{i} \ddot{A} \ddot{3} \ddot{4} \ddot{i} \ddot{E} \ddot{z} \ddot{.} \ddot{A} \ddot{i} \ddot{l} \ddot{\pm} \ddot{I} \ddot{o} \ddot{D} \ddot{i} \ddot{.} \ddot{i} \ddot{O} \ddot{1} \ddot{4} \ddot{i} \ddot{l} \ddot{o} \ddot{.} \ddot{2} \ddot{1} \ddot{2}$
 $\ddot{I} \ddot{A} \ddot{D} \ddot{E} \ddot{-} \ddot{.} \ddot{A} \ddot{.} \ddot{A} \ddot{3} \ddot{4} \ddot{E} \ddot{O} \ddot{A} \ddot{I} \ddot{o} \ddot{3} \ddot{4} \ddot{O} \ddot{A} \ddot{O} \ddot{I} \ddot{\ll} \ddot{A} \ddot{U} \ddot{E} \ddot{O} \ddot{I} \ddot{o} \ddot{A} \ddot{O} \ddot{A} \ddot{I} \ddot{o} \ddot{A} \ddot{c} \ddot{.} \ddot{o} \ddot{.} \ddot{u} \ddot{5} \ddot{-} \ddot{9} \ddot{,} \ddot{5} \ddot{-} \ddot{1} \ddot{0}$

±ýÛõ Ä¼í Çø ð¼ðÀðí ùÇÉ. þíì 8 ð¼Äí ½Äí ù Ç (6Äí ð ù, 2 ð¼Äí Ä× ù) ¾ÉðÄí ð¼ðÀðí ÄíÛ ù ÄíýÛíì ð 3 ðÄí Äí ðÄýÄíÄí Ç Ä ÄÄÛí ÖÉðõ.

BÄø ÄØí ð ç¼úÄ¾íø F'₂=0.20N₂ -ì ð. 8Äð ðÄýÄíÄí Ç ±ýÛõ ÄðÉÄý Äø¾Çð¾ø « øÄð ù¾Çð¾ø ÄØí ð ðüÄí ð ±Éì ð ðñ Ä ÄÄÛí ðÄí ð. ÄÄø ÄØí ð ç¼ø ð ±Éì ð ðñ Äí ð ðÄð¼ ½ììì ð¾× ð ½Äíð. þóç Ä ±Ç¾É¾ø ÄÄø ÄØí ð ðüÄí ðÉð ±Éì ð ðñ Äí ð ù Ä ÄÄÛí ðÄðí ùÇÉ.



Ä¼õ 5-9

$$\therefore F_1 = F_1' = \sim_1 N_1 = 0.35 N_1$$

$$F_2 = F_2' = \sim_2 N_2 = 0.20 N_2$$

$$\sum F_x = 0 \rightarrow F_1 - N_2 = 0 \rightarrow F_1 = N_2$$

$$\therefore N_2 = F_1 = F_1' = 0.35 N_1$$

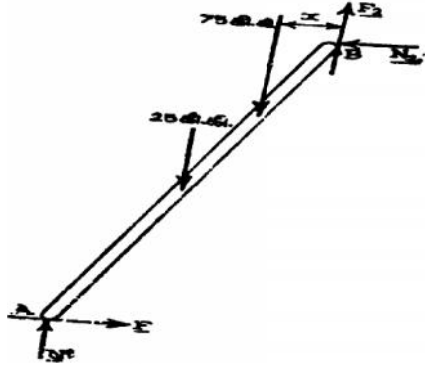
$$\sum F_y = 0 \rightarrow N_1 + F_2 - 25 - 75 = 0$$

$$\ll \text{¾Äð } N_1 + 0.20 N_2 = 100$$

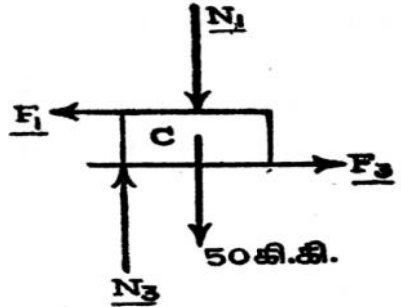
$$\ll \text{¾Äð, } N_1 + 0.20(0.35) N_2 = 100$$

$$N_1 = \frac{100}{1.07} = 93.45 \text{ ç. ç.}$$

$$F_1 = F_1' = 0.35(93.45) = 32.7 \text{ ç. ç.}$$



Ä¼õ 5-10



Ä¼õ 5-11

$\sum F_y = 0 \rightarrow N_3 - 93.45 - 50 = 0 \ll \text{øÄÐ}$

$N_2 = 143.45 \uparrow \text{ } \ll \text{øÄÐ}$

$\sum F_x = 0 \rightarrow F_3 - 32.7 = 0 \ll \text{øÄÐ} \quad F_3 = 32.7 \text{ } \ll \text{øÄÐ}$

$F_3' = \sim_3 N_3 = 0.25(143.45) = 35.85 \text{ } \ll \text{øÄÐ}$

$F_3' = \sim_3 N_3 = 0.25(143.45) = 35.85 \text{ } \ll \text{øÄÐ}$

$F_3 < F_3' \pm \text{ýÚ} \text{ } \ll \text{øÄÐ}$

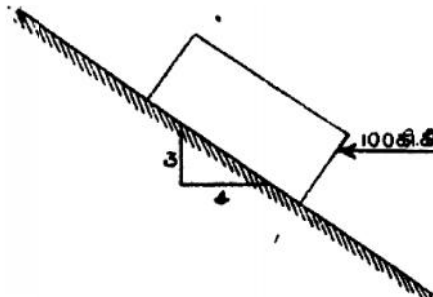
$\sum M_B = 0 \pm \text{ýÚ} \text{ } \ll \text{øÄÐ}$

$x(75) + 1.5(25) + 7.2(32.7) - 3(93.45) = 0 \text{ } \ll \text{øÄÐ}$

$\therefore x = .0987 \text{ } \ll \text{øÄÐ}$

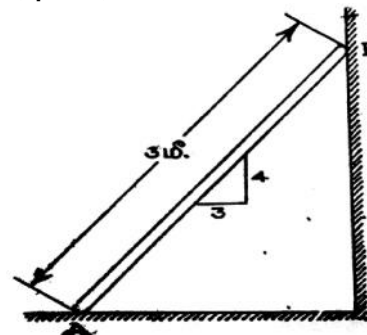
$\text{ } \ll \text{øÄÐ}$

$5.1 \quad 125 \text{ } \ll \text{øÄÐ}$



$\text{ } \ll \text{øÄÐ}$

$5.2 \quad 10 \text{ } \ll \text{øÄÐ}$



$\text{ } \ll \text{øÄÐ}$

$5.3 \quad 50 \text{ } \ll \text{øÄÐ}$

5.4. A wheel of radius $R = 0.3$ m is in contact with a horizontal surface at point A and a vertical wall at point B. The center of mass is at the center of the wheel. The weight of the wheel is $P = 120$ N. The wheel is in equilibrium. Find the reaction forces at points A and B.

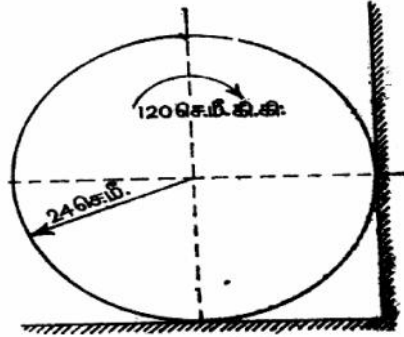


Figure 5-14

5.5. A wheel of radius $R = 0.45$ m is in contact with a horizontal surface at point A and a vertical wall at point B. The center of mass is at the center of the wheel. The weight of the wheel is $P = 120$ N. The wheel is in equilibrium. Find the reaction forces at points A and B.

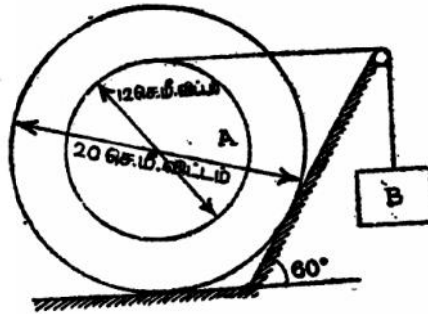


Figure 5-15

5.6. A wheel of radius $R = 0.20$ m is in contact with a horizontal surface at point A and a vertical wall at point B. The center of mass is at the center of the wheel. The weight of the wheel is $P = 120$ N. The wheel is in equilibrium. Find the reaction forces at points A and B.

